STAT

June 22, 1965

	LINEAR PHASOLVER MEASURING ENGINE
	Measuring the measuring engine is a difficult proposition and linear measuring is tougher than rotary measuring because of scale factor variations.
\$	So far, the test data seems to indicate that the Linear Phasolver electronics and patterns can measure to a fraction of 1/10 micron is trying to prove it by measuring gage block lengths. The variables they must contend with are:
	a) Manual dexterity of the physical arrangement. The principal precaution is to not tilt the gage block and thus not measure a false length.
	b) Variations in null position of microinch meter. Over short periods, this appears to be accurate to a few micro inches.
(c) Thermal variations in gage block lengths. They have obtained additional gage blocks to make a complete set for measuring 1/8 mm increments within the 1 mm pole pair length in addition to the five lengths of 23 mm, 30 mm, 60 mm, 125 mm, and 250 mm. Thus handling and thermal problems are decreased.
	d) Temperature and humidity effects on other components. Room temperature is continuously recorded and is within 1°F. Humidity is continuously recorded and is within about 3%.
	In a meeting at

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Linear Phasolver Measuring Engine -2

June 22, 1965

resolution peatabil:	the day highly skeptical of the practicability of olver approach, particularly the electronics. was able to demonstrate better than 1/10 micron on and better than 1/2 micron peak to peak reity. By the end of the day, wing reservations:	STAT STAT
a)	A laser interferometer by its geometry appeared to be easier to incorporate into a measuring machine than the phasolver.	
ъ)	The phasolver cost of 2-axis system was high.	STAT
c)	In principle, a laser interferometer is much simpler and should be ; more accurate than the phasolver.	
d)	The scale error in the present phasolver feasi- bility model would not meet his requirements.	
On the or	ther hand and the others seemed to be dithat:	STAT
a)	The linear phasolver did produce a unique, un- ambiguous measurement of position.	
b)	There was no limitation on slewing rate from one measuring point to another.	
c)	The velocity error was probably satisfactory for servo drive of a slaved platen to retain stereo registration while moving.	
d)	Repeatability accuracy was 1/2 micron peak to peak or better.	
do with a	tional point that came out of the meeting had to skew and tilt of the phasolver plates. Part of the test program calls for measurement of the ity of phasolver accuracy to relative skew of the	STAT
the plate guiding v skew to e gap to 10 variation	nd coupler plates and variations of the gap between es, including tiltindicated that the ways and air bearings on his machine would hold only a few seconds of arc and variations in the 00 microinches (2½ microns), peak to peak. These has are so small that measuring their effect on olver is of second order of importance.	STAT
wave cyc	has now turned their attention to scale factor. ctor error has two parts: a) error within a sine le pole pair (a pole pair is one millimeter long) he incremental error from pole pair to pole pair	STAT

Approved For Pologge 2006/06/28 · CIA-RDP78R04770A002900020007-3

Linear Phasolver Measuring Engine -3

June 22, 1965

over the 20 inch length. It should be noted that both these errors are systematic and can be corrected by computer computation.

Non-Linear scale error within a pole pair can be corrected by balancing the amplitude and quadrature of the driver pattern exciting voltages. The uncorrected non-linear error was 60 microns p-p. By balancing, this has been brought down to about 1.8 micron p-p including repeatability error. (Note this is later data than the previously reported 0.8 micron p-p scale error.) Further reduction is probably possible.

The scale error over 250 mm is about 18 microns with about a 3 micron curvature (i.e. non linearity). In discussion with their consultant from UCLA, they decided that the resistance of the coupler pattern (which is about 2,000 ohms) was probably introducing a phase shift as it varied from near zero when measuring at one end to its maximum value when measuring at the other end. Tests this week and last tend to confirm that the coupler pattern resistance is causing the 3 micron non-linearity in the overall scale factor.	STAT STAT
The cause of the linear error in the scale factor has not been determined measurement of the patterns indicates the scale factor error should only be about 3 microns whereas the test data indicate it is about 18 microns. Thermal expansion or contraction of the glass bar on which the coupler pattern is placed may be a factor. If the temperature of the glass bar at the time of making the pattern at and measuring the pattern at is different by about 6.7 C from the tempera-	STAT STAT STAT
ture of the glass bar during the present test program, a scale factor error of the right magnitude could occur. Temperature difference is, however, probably only one contributor.	
The accounting procedure has adjusted their man hour rates upward for the year due to increased overhead. This adjustment makes the contract over expended and they have officially stopped work. There is no estimate as to when they might resume work, if at all.	STAT
The next phase of the phasolver program should, it seems to me, be a check of the effect of temperature and humidity and probably should be run under the direction ofto permit their thorough evaluation of the device. With concurrance I discussed the possibility of running such a test in the clean room with	STAT STAT STAT

Linear Phasolver Measuring Engine -4 June 22, 1965

General Manager of	STAT
Both were in favor of such a test and will discuss it with John on his next trip.	STAT
Unfortunately, the clean room is not too well adapted to such a test. The rooms are not separately controlled. The present instrumentation will only produce 45% ±Sfelative humidity. It would probably be more suitable, but more expensive, to run the test in a commercial environmenta chamber. Is planning to investigate the possibility of running a simultaneous test of a laser interferometer measuring device. He has nothing immediately at hand for such a test.	STAT
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