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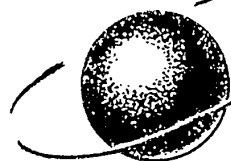
No. 59

PROJECT PRAIRIE GRASS, A FIELD PROGRAM  
IN DIFFUSION  
VOLUME I

EDITED BY  
MORTON L. BARAD

JULY 1958

GRD



GEOPHYSICS RESEARCH DIRECTORATE  
AIR FORCE CAMBRIDGE RESEARCH CENTER  
AIR RESEARCH AND DEVELOPMENT COMMAND  
UNITED STATES AIR FORCE  
BEDFORD, MASSACHUSETTS

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Project 7657

Atmospheric Analysis Laboratory  
GEOPHYSICS RESEARCH DIRECTORATE  
AIR FORCE CAMBRIDGE RESEARCH CENTER  
AIR RESEARCH AND DEVELOPMENT COMMAND  
UNITED STATES AIR FORCE  
Bedford, Mass.

## PREFACE

During the Summer of 1956, sixty scientists, technicians, and test support personnel participated in an experimental program in micrometeorology. This program, nicknamed Project Prairie Grass, was conducted in north-central Nebraska near the town of O'Neill. Four universities and two government agencies participated in the field program, which was conceived and directed by personnel of the Atmospheric Analysis Laboratory of the Geophysics Research Directorate, Air Force Cambridge Research Center. The participants represented Massachusetts Institute of Technology, Texas A&M Research Foundation, University of Washington, University of Wisconsin, Air Weather Service, and units of the Air Force Cambridge Research Center.

The primary objective in Project Prairie Grass was to determine the rate of diffusion of a tracer gas as a function of meteorological conditions. The purposes of this paper are (1) to describe the equipment and procedures used in dispensing and sampling of the gas, analysing gas samples, measuring meteorological parameters, and reducing and processing data; and (2) to present tabulations of the data collected. It is not the intention here to present analyses of the data, evaluate existing diffusion models, or develop new models. Such analyses have been initiated by the research teams that participated in Project Prairie Grass and by other research groups under contract with the Geophysics Research Directorate. It is expected that their findings will be published in professional journals and in contract reports. It is hoped that other scientists, using the material contained in this report, will also undertake studies of the diffusion problem.

This report is being presented in three volumes to facilitate reading of text and use of data. Volume I contains an introductory

chapter which provides a background of the field program. Chapter 2 contains a description, by Texas A&M personnel, of the field site at O'Neill. The surface weather observations made by the Texas A&M group are presented in Chapter 3. Chapter 4 contains the surface synoptic charts prepared by GRD personnel. A description of the diffusion technique as well as tabulations of the diffusion data are presented in Chapter 5 by MIT personnel. Chapter 6 includes a description of the instrumentation used by MIT to measure wind speed and direction parameters, as well as tabulations of the wind data.

Volume II opens in Chapter 7 with a description of the instrumentation used by the Texas A&M group to determine mean profiles of air temperature, soil temperature, and wind speed as well as other terms necessary in calculating the heat budget at the air-earth interface. Chapter 8 includes the profile data collected during the test periods as well as during other periods during the summer. In Chapter 9, Texas A&M scientists describe a method of computing heat budget terms and present a tabulation of such terms for the test periods. Another technique for determining the heat budget terms was employed by a University of Wisconsin team. Their technique and computed heat budget terms appear in Chapter 10. A technique of determining temperature profiles by optical methods is being developed by research workers at the University of Washington. A description of the optical method technique and the data collected at O'Neill are presented in Chapter 11. The rawinsonde data collected by Air Weather Service personnel and edited by GRD personnel are presented in Chapter 12. This volume concludes with a description by GRD personnel of the instrumentation and techniques used in airplane observations of temperature and humidity; and the data collected during the gas releases are tabulated.

Volume III is not expected to be ready for publication before

the end of 1958. Present plans for this volume call for presenting (1) descriptions of the bi-vane anemometry employed by MIT in the measurement of eddy components for determining turbulence spectra and scales of turbulence; descriptions of the procedures employed by Iowa State College in reducing bi-vane data, and by GRD in computing spectra and scales of turbulence; and (2) descriptions of the sonic anemometry employed by the University of Wisconsin in determining turbulence spectra. The spectra and scale data will also be presented in Volume III.

The people who participated in Project Prairie Grass are to be congratulated for the diligence and efficiency they exhibited during the planning for and the performance of the field experiments and during the preparation of this report. They are to be commended for a spirit of cooperation, so necessary in making the program a successful one. A list of the participants follows:

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Our thanks go to the residents of O'Neill, Nebraska for their valuable assistance in the solution of a variety of problems which arose in the course of the field program.

Morton L. Barad  
Geophysics Research Directorate

#### ABSTRACT

Project Prairie Grass was a field program designed to provide experimental data on the diffusion of a tracer gas over a range of 800 meters. In each of 70 experiments the gas was released continuously for 10 minutes at a source located near ground level. The gas releases were made over a flat prairie in Nebraska under a variety of meteorological conditions during July and August of 1956.

This paper includes a brief history of the project and detailed descriptions of the tracer technique and the meteorological equipment used in the field program. Tabulations of the diffusion data and the meteorological data collected during the gas releases are also presented. In addition, this paper contains data on the heat budget at the air-earth interface during other selected periods during the Summer of 1956.

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PROJECT PRAIRIE GRASS, A FIELD PROGRAM IN DIFFUSION

CHAPTER 1  
INTRODUCTION

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Project Prairie Grass is the name given to a field program conducted near O'Neill, Nebraska during the Summer of 1956. The main objective in this program was to learn how the diffusion of a tracer gas emitted continuously at a point source near ground level varies with meteorological conditions. This report contains descriptions of the techniques and procedures employed in the program and summaries of the data collected. The purpose in this introductory chapter is to present an account of the historical background of Project Prairie Grass in order that the reader may understand why the research was undertaken and why certain techniques were employed in the field program.

There is little doubt that advances made in diffusion theory and experimentation directly aid in solving a number of practical problems in the atmospheric boundary layer. In the field of air pollution abatement, for example, advances made in diffusion research lead to more intelligent choices of plant location, design of plant buildings and stacks, periods of stack emission, etc. In the field of crop spraying, as another example, progress made through diffusion studies leads to better selection of spray altitudes, spray periods, etc.

There are, however, a number of other boundary layer problems which can also be brought nearer to solution by the insight gained through diffusion research. To solve such problems as the forecasting

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of fog, frost, or low-level wind shear, for example, an increased understanding of the basic mixing processes at work in the lower atmosphere is necessary. In attempts to understand these processes, investigators have studied the diurnal and height variations of turbulent fluxes of momentum, heat, and water vapor. Although these fluxes can be measured at a number of points in space, research workers generally find it difficult to interpret such measurements. Though one may have some success in describing the region through which the property is transported, he is usually at a loss to quantitatively define the source of the property. However, if a distinctive tracer is introduced into the atmosphere at a source which can be precisely defined as to location and strength and if concentrations of this tracer are measured downwind from this source, a means is provided of gaining greater insight into the basic mixing mechanism present in the atmosphere. It is not surprising then that micrometeorologists and hydrodynamicists interested in turbulence phenomena should apply general hypotheses to the development of diffusion theory and should seek to employ data from diffusion experiments to test their diffusion hypotheses. Diffusion theory and experimentation, then, provide more than solutions to specific air pollution problems; they provide a means of improving our understanding of turbulence phenomena.

In this analysis of the situation, the chain of activity goes from general turbulence hypotheses to a specific diffusion hypothesis to experimental verification. A study of the literature reveals that much work has been done, particularly in the past 25 years, in the development of general turbulence and diffusion hypotheses. However, very little has been done in the collection of accurate diffusion data with which to test the diffusion hypotheses.

In January of 1953, a number of university and government scientists engaged in micrometeorological research assembled in Boston to participate in the planning of the Great Plains Turbulence Field Program, a program held later that year near O'Neill, Nebraska. <sup>1</sup>

Although the participants at this planning session were prepared to make a variety of meteorological measurements, no one was prepared to make quantitative measurements of diffusion. It seemed that none of the participants had both a satisfactory tracer technique and the equipment necessary to collect tracer samples in a dense network of stations.

At this point the Geophysics Research Directorate decided to support the development of a tracer technique which would be suitable for studying diffusion rates over a range of about 1 km when the tracer was emitted continuously at a fixed point near ground level. Actually, the development of two tracer techniques was supported. The first involved the use of tritiated ethane, a radioactive tracer. <sup>2</sup> Because of the relatively high costs in manpower and material which would have been imposed if this technique had been used, it was shelved in favor of the second technique, developed by MIT at its Round Hill Field Station. \* This technique called for the use of sulfur dioxide as the tracer.

It will be noted that the tracer technique was developed for continuous emission. Historically, theoretical work usually starts with diffusion from an instantaneous point source, with the growth of a small puff of smoke, for example, and then proceeds by integration to other sources such as the continuous source, line sources, etc. Yet, historically, most of the experimental work has begun with the continuous point source. There appear to be at least three reasons for preferring the continuous source over the instantaneous one. First, the engineering of the continuous source with reproducible characteristics, experiment after experiment, is generally simpler. Second, the statistical interpretation of the concentration measurements at downwind stations is simpler, particularly where time-mean concentrations are found, as they were in Project Prairie Grass. Third, the determination of what constitutes pertinent meteorological data and the provision of such data

\*See Chapter 5 for a description of the technique developed by MIT.

are generally simpler. For these reasons, principally, a continuous source was chosen for Project Prairie Grass.

In the diffusion experiments an emission time of 10 minutes was chosen. This time was a compromise, arrived at after considering such factors as the cost of tracer gas, practical rates of emission, distance between the samplers closest to the source and the most distant ones, and desirability of having fairly stable time-mean diffusion patterns in the area downwind from the source.

In experiments of this sort, it is desirable that the cost of tracer material be low and that the tracer can be emitted at a fairly constant rate. It is desirable that tracer losses on ground, vegetation, and other surfaces in the area sampled be negligibly low. It is desirable that the sampling rate for each sampler be constant throughout an experiment and that this rate be uniform from sampler to sampler. If the measurements are to be used to evaluate existing hypotheses or to construct new models, it is important that there be an adequately dense network of samplers. Therefore, if hundreds of samplers are to be exposed at one time and if spares are to be available, the samplers must be relatively inexpensive. It is necessary that the analysis of samples be accurate, cover a wide range of concentrations, and be accomplished in relatively short time. It is believed that the diffusion technique developed by MIT meets these requirements very well.

By the Spring of 1955, a decision was made to shift the experimental program from the Round Hill Field Station of MIT to a site which would permit the collection of sulfur dioxide samples over greater downwind distances and over more uniform terrain and vegetation. A section of land near O'Neill, Nebraska was chosen as the site of the field program.\*

\*The land leased was Section 14, Township 29 North, Range 11 West, Holt County, Nebraska.

The square mile chosen had the following characteristics:

1. It was a fairly flat area, as Figure 1.1 indicates. The contour lines shown in Figure 1.1 are for 1-foot intervals. The gas source was located at the center of five concentric semicircles having radii of 50, 100, 200, 400, and 800 meters. North of the E-W line passing through the source, the topography is very flat, being within  $\pm 3$  feet of the mean elevation in that part of the section. The topography rises gently to the southwest with an average grade of about 10 feet per half-mile, and to the southeast with an average grade of about 20 feet per half-mile.
2. Logistical and technical considerations had led to the decision to sample the gas on semicircular arcs rather than on full circular arcs. In a study of the wind climatology of the O'Neill area, it was found that wind directions between  $120^\circ$  and  $240^\circ$  occur more than 50 percent of the time in July and August. On this basis, primarily, the sampling grid was laid out as shown in Figure 1.1.
3. The vegetative cover was fairly uniform as to grass type. The "hayfield" was mowed prior to the experiments, and since there was little precipitation during the months of July and August, the grass height was fairly uniform during the program.
4. The site was relatively free of obstructions to air flow. Most of the equipment used in dispensing the gas was placed in a dugout 50 m upwind of the actual source. A laboratory building and three Jamesway huts were erected over 300 m east-southeast of the source. With the exception of cup anemometers and wind vanes mounted on wooden posts near the source and 450 m north of the source, the meteorological equipment, trailers, and Jamesway huts were all located on the observation line, downwind of the 800 m sampling arc.
5. The nearest farmhouse was over 1300 m northwest of the source. As a result, there were no complaints from nonparticipants about the gas which, on a few occasions, was pungent on the observation line, about 900 m from the source.
6. Stable a-c power was brought to various points in the field. The overhead power line starting at Opportunity Road is shown in Figure 1.1.

The O'Neill area had other advantages: friendly and cooperative townspeople, an airport, and adequate housing.

In diffusion experiments of the type conducted at O'Neill, it is

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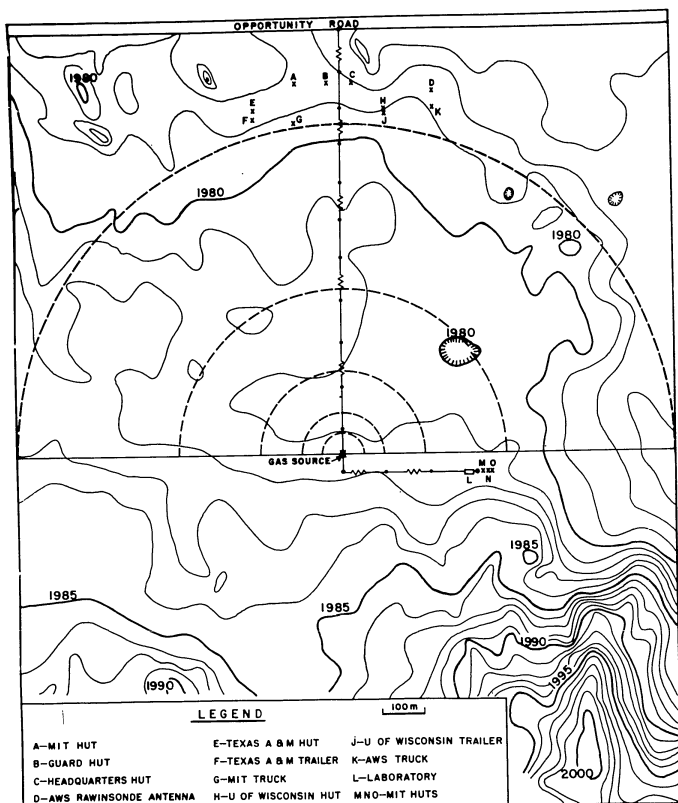


Figure 1.1 Topography of field site and layout of equipment

considered essential that a number of meteorological measurements be made to characterize the experiments and to provide measurements of parameters required for evaluating diffusion models calling for the use of these parameters. Thus, in the Prairie Grass experiments, many of the measurements were suggested by existing diffusion hypotheses. For example, the Sutton hypothesis calls for determining wind profile and gustiness parameters. The Calder-Deacon hypotheses suggest the determination of wind profile parameters and, in implying that the Richardson Number or stability ratio is useful, suggest the measurement of temperature profile. The works of Inoue and Ogura suggest the determination of turbulence spectra and scales of turbulence. Other meteorological measurements were made because there was some evidence that they might be called for in new diffusion models or in the forecasting of diffusion patterns from limited meteorological data.

For the meteorological measurements to be useful, past history in experimental micrometeorology has shown that they must be representative and very accurate. It was the overall impression of the biased participating scientists, as well as those who visited the field program, that the meteorological measurements which accompanied the diffusion experiments were of very high caliber.

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1. Lettau, H. H. and Davidson, B., "Exploring the Atmosphere's First Mile," Pergamon Press Inc., N. Y. (1957)
2. "Development of a Tracer Technique," Final Report, Contract No. AF19(604)-1045, Tracerlab, Inc. (1955)

CHAPTER 2  
A DESCRIPTION OF THE FIELD SITE  
IN PROJECT PRAIRIE GRASS

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Texas A&M Research Foundation

The observation site was an extensive, virtually level field previously used to pasture cattle. The field was uncultivated and covered with native prairie grasses. Prior to the first observation period, the grass was mowed and little growth occurred thereafter due to arid climatic conditions.

2.1 Location

The experimental site was located about five miles northeast of the center of O'Neill, Nebraska. Geographical coordinates are Latitude, 42° 29.6' North; Longitude, 98° 34.3' West; altitude at gas source, 1980 feet above mean sea level.

2.2 Landscape

The field is part of a nearly-level upland. The land rises moderately to the southeast to a hill about 0.6 miles from the gas source. There is no surface drainage pattern at all. Rain water soaks into the soil immediately, or accumulates in small depressions until it all infiltrates or evaporates. The drainage pattern of Redbird Creek (a tributary of the Niobrara River) has advanced southward to within about a mile of the site. To the west, south, and east, there are not even intermittent streams for several miles.

From the site, then, except for carefully placed project equipment, one has an unobstructed view for miles (Figure 2.1). Since there are no hills or mountains in the distance, there is no distinct horizon. Toward the southeast the hill forms a visibility mask at 1.5 miles. The unobstructed view is felt only when distant thunderstorms, etc., are observed. Otherwise, there is nothing to see in the distance.

\*Present affiliation: U. S. Navy Electronics Laboratory

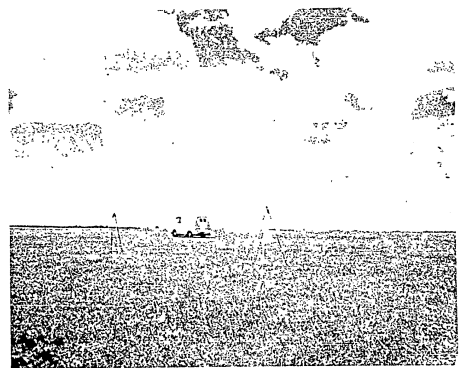


Figure 2.1 View looking southwest from center of observation line at north side of site. Photograph taken in mid-August

Land is laid out in mile-square fields, with a farmstead on many of these "country blocks." There was one farmstead, with its cluster of buildings and trees, about 1300 meters northwest of the gas source.

2.3 Soil

The site was in a hayfield on O'Neill loam, upland phase.<sup>1</sup> This soil has a black, top soil about 25 cm thick. It is loose and friable, and with profuse grass roots forms a tough sod. Organic matter content was determined to be 4 percent. The top soil is underlain by a brown subsoil, about 20 cm thick. Both these layers have good water-holding capacity. From a 45-cm depth to 60 cm, there is a light brown layer of compacted soil. Soil particles are plate-like and horizontal, and this layer is very difficult to cut into from above. However, a small clod of this material may easily be crumbled by lateral compression. Through this compacted layer, few grass roots penetrate.

There are decayed roots, up to 1 cm diameter, of shrubs which once grew here and which did penetrate this layer to the sand below.

Below the compacted layer, from a 60-cm depth to at least a 120-cm depth, the soil is a loose, coarse sand with much gravel. Water held here is only very slowly available to the grass, because few roots penetrate to the sand and water movement upward through the sand and the compacted layer is extremely slow.

Bulk densities of the soil were determined on 10 July, 16 July, 6 August, and 29 August near the Texas A&M instrumentation location. The best values, in grams of dry soil material per cubic centimeter of the natural soil, are given in Table 2.1.

Table 2.1. Values of bulk density

DEPTH (cm)	BULK DENSITY (gm/cm <sup>3</sup> )
0 - 10	1.05
10-20	1.15
20-30	1.25
30-40	1.34
40-50	1.35
50-60	1.36
60-70	1.41
70-80	1.47
80-90	1.54
90-100	1.60

#### 2.4 Vegetation

The wild hay was cut on 28 June. Through July and August, the field was dominated by the brown stubble 5 to 6 cm high, with some sparse stubble up to 20 cm high. After a rain, the field had a greenish brown appearance for a day or two. This was due to a short, fine, green grass coming up, and to the greening of some species of brownish grass that was still alive. Growth of the vegetation, as a whole, was slight, and the amount of dead and living plants standing up remained fairly constant. In late August, scattered, small, green

shrubs became more conspicuous. These shrubs attained a height of approximately 18 centimeters.

There were a few small prickly pears in the field. There was scarcely any litter of plant material lying loose on top of the soil. Dried and weathered cakes of cow dung were spread about rather evenly, about one per three square meters.

#### 2.5 Albedo

Measurements of albedo on 10-11 July; 24-25-26 July; and 8-9 August show that the albedo is lowest at solar noon, and greater near sunrise and sunset. Average values for those days are given in Table 2.2.

Table 2.2. Values of albedo

TIME (CST)	ALBEDO
0605	0.331
0705 & 1805	.254
0805 & 1705	.212
0905 & 1605	.203
1005 & 1505	.190
1105 & 1405	.187
1205 & 1305	0.184

The albedo varies somewhat with solar angle, cloudiness, moisture on the grass, and changes in the vegetation with time.

#### 2.6 General Weather

Precipitation was measured daily from 29 June through 28 August. Maximum and minimum instrument shelter temperatures were measured from 10 July onward. These data are given in Table 2.3. On most of the days that precipitation occurred, one or more huge thunderstorms were visible from the site. These were accompanied by many cloud-to-ground lightning flashes. No lightning strikes near the site were observed, although electrical interference sometimes halted the use of the thermoelectric temperature measuring system. The only hail storm of the summer, with hailstones about 2 cm in diameter, occurred on 29 June.



Table 2.3. General weather

	Maximum Temperature (°F)	Minimum Temperature (°F)	Precipitation (in.)	Notes
29 June	-	-	0.58	Hail 2 cm in diameter
30	-	-	.00	
1 July	-	-	.23	
2	-	-	.00	
3	-	-	.00	
4	-	-	.21	
5	-	-	.00	
6	-	-	.00	
7	-	-	.00	
8	-	-	.00	
9	-	-	.00	
10	90.0	51.0	.00	Moisture determination
11	96.1	69.2	.00	
12	89.7	60.4	.01	
13	88.0	59.6	.00	
14	98.8	64.9	.08	
15	85.0	64.4	.00	
16	87.1	60.3	.00	Moisture determination
17	90.9	57.2	.00	
18	87.0	60.3	.21	
19	77.7	55.6	.04	
20	81.6	50.9	.00	
21	*	52.0	.00	
22	*	*	.00	
23	92.0	*	.00	
24	89.0	65.0	.00	
25	96.0	55.0	.00	
26	103.9	69.8	.00	
27	88.8	69.6	.00	
28	78.3	60.4	.00	
29	85.8	57.2	.00	
30	95.8	69.0	.03	
31	69.2	64.2	.04	
1 August	81.5	63.9	.32	
2	92.8	67.8	.08	
3	96.8	69.0	.19	
4	90.0	69.2	.11	
5	93.1	58.3	0.00	

\*Thermometers were not reset.

Table 2.3. (cont.)

	Maximum Temperature (°F)	Minimum Temperature (°F)	Precipitation (in.)	Notes
6 August	88.2	63.0	0.06	Moisture determination
7	89.8	61.0	.00	
8	89.0	59.4	.04	
9	89.9	58.5	.01	
10	84.9	56.0	.04	
11	84.5	57.7	.00	
12	90.0	63.5	.01	
13	93.0	60.0	.00	
14	96.2	66.0	.00	
15	100.0	54.1	.25	
16	86.9	65.5	.00	
17	83.2	66.0	.00	
18	68.0	56.0	.20	
19	72.0	43.7	.00	
20	73.8	49.7	.00	
21	88.3	46.2	.00	
22	95.9	51.6	.00	
23	90.4	56.3	.00	
24	92.8	48.9	.00	
25	95.5	58.0	.00	
26	99.8	67.0	.00	
27	95.5	58.4	.01	
28	94.1	58.7	0.00	
29	-	50.3	-	Moisture determination

### 2.7 Soil Moisture

Soil moisture was generally deficient, and no crop of hay was produced after the mowing in late June. Moisture determinations were made on 10 July, 16 July, 6 August, and 29 August along with the bulk density determinations. The values are sufficiently accurate for estimating the heat capacity of the soil. They are not, in themselves, sufficient for specifying availability of soil moisture for evaporation and transpiration. No independent determinations of soil wilting point were made. Due to lateral variability and inadequacy of sampling, these moisture determinations do not permit the computing of changes in soil moisture content for the field.

Values of soil moisture, as percent dry weight, are given in Table 2.4.

Table 2.4. Values of soil moisture as percent dry weight

DEPTH (cm)	10 JULY	16 JULY	6 AUG	29 AUG	AVE OF 4
0-10	7.2	6.8	9.2	6.6	7.5
10-20	7.0	6.3	6.6	6.5	6.6
20-30	3.8	6.3	3.0	6.0	4.8
30-40	4.2	4.9	2.8	4.4	4.1
40-50	5.1	3.9	2.9	5.6	4.4
50-60	3.1	3.7	3.5	6.7	4.2
60-70	1.9	3.4	6.2	3.8	3.8
70-80	1.8	3.2	3.8	2.9	2.9
80-90	2.9	4.8	2.6	2.4	3.2
90-100	5.7	4.8	1.8	2.4	3.7

Most likely all of these values, except those above a 20-cm depth on 6 August, and those of the compacted layer and the sand below, represent the wilting point of the individual samples, or are very slightly higher. These soil samples at the wilting point were dusty and dirty. The loose sand below was cool (about 25°C) and moist to the touch throughout the summer. However, its actual content of water was slight. The high moisture percentages down to 20 cm on 6 August reflect an increase in available moisture from recent rains. The soil in the field, as a whole, appeared to be driest on 29 August although the sample moisture determinations do not bear this out.

Since the soil was near the wilting point all summer, average values of the heat capacity per unit volume are sufficiently accurate for all soil heat computations. These values are given in Table 2.5.

Table 2.5. Values of heat capacity per unit volume

DEPTH (cm)	$\rho C_p$ (cal/cm <sup>3</sup> deg)
0-10	0.26
10-20	.28
20-30	.28
30-40	.30
40-50	.30
50-60	.30
60-70	.31
70-80	.31
80-90	.33
90-100	0.35

#### REFERENCES

1. Moran, W. J., et al., "Soil Survey of Holt County, Nebraska," United States Department of Agriculture (1938)



Table 2.1 (Continued)

These entries on this form are \_\_\_\_\_ with verification data.

To convert to C.C.T. (Miles) \_\_\_\_\_ hours.

STATION	MONTH	YEAR	DAY	TIME	WIND	DIR	VELOCITY	TEMP	REL. HUM.	SEA	REMARKS
41	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
42	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
43	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
44	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
45	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
46	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
47	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL

Table 2.1 (Continued)

These entries on this form are \_\_\_\_\_ with verification data.

To convert to C.C.T. (Miles) \_\_\_\_\_ hours.

STATION	MONTH	YEAR	DAY	TIME	WIND	DIR	VELOCITY	TEMP	REL. HUM.	SEA	REMARKS
48	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
49	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
50	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
51	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
52	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
53	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
54	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
55	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
56	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
57	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
58	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
59	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
60	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL

Table 2.1 (Continued)

These entries on this form are \_\_\_\_\_ with verification data.

To convert to C.C.T. (Miles) \_\_\_\_\_ hours.

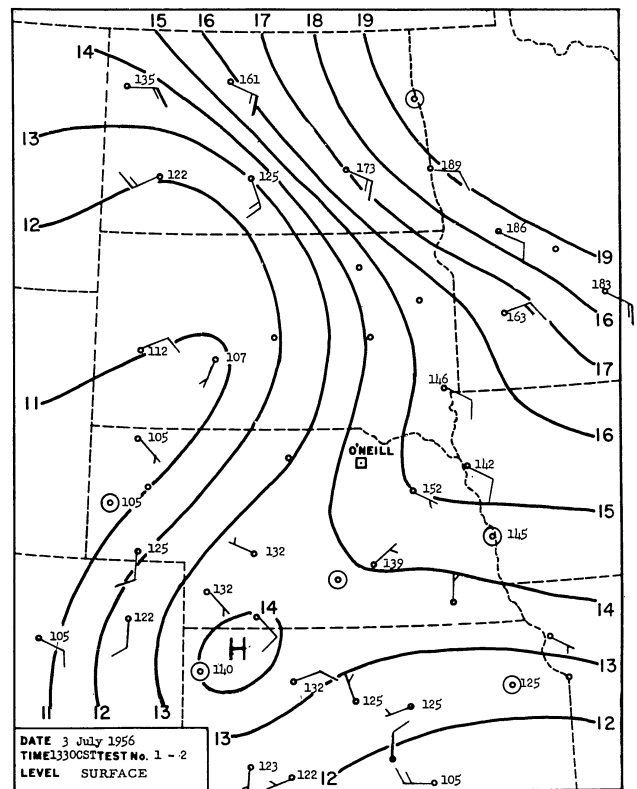
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62	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
63	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
64	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
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66	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
67	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
68	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
69	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL	UNL
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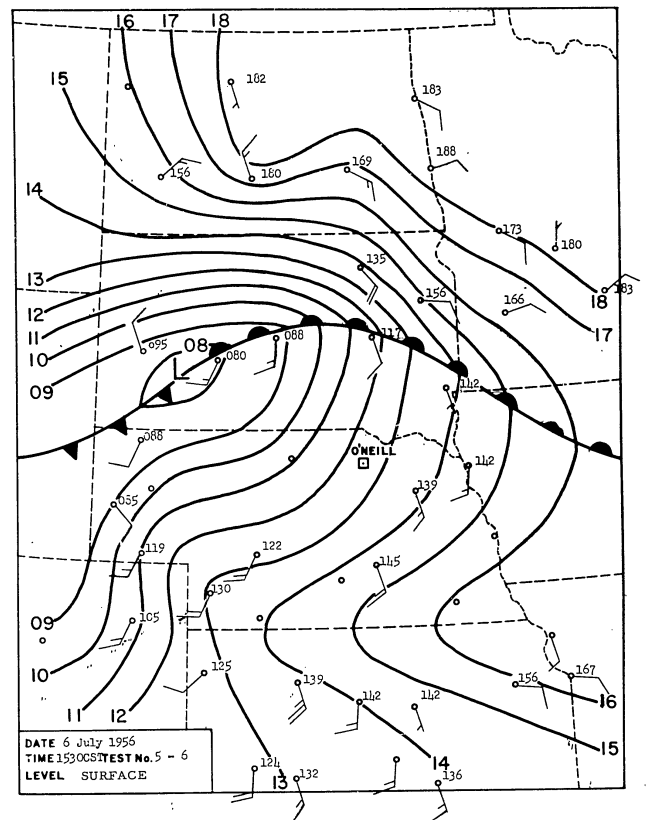
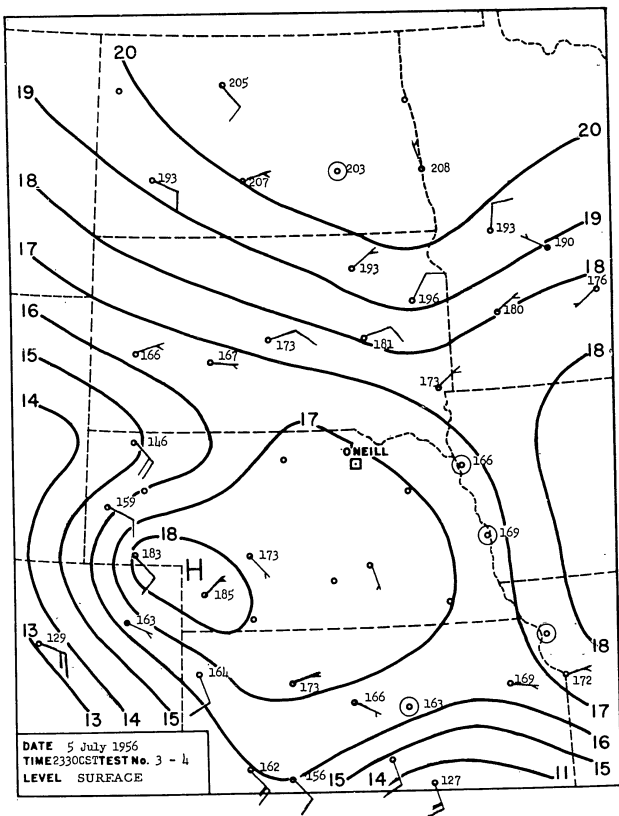
CHAPTER 4  
SYNOPTIC INFORMATION

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Air Force Cambridge Research Center

At an early stage of the field program, it became very apparent that use of only National Weather Analysis Center facsimile maps and prognoses would not suffice for the purposes of forecasting wind direction for gas releases. Consequently, sectional, sea-level, pressure maps were plotted and analyzed, using hourly airways sequences from the network of stations lying in the area extending from approximately 93°W to 104°W Longitude and from the United States-Canadian border southward to 37°N Latitude. Occasionally, coverage was extended westward as far as approximately 120°W, and southward to about 35°N. Isobars were drawn at 1 mb intervals. These maps revealed many small-scale features of the circulation which seldom appeared on the large-scale facsimile maps, and which often exercised primary control over the airflow at O'Neill. This type of analysis greatly facilitated the wind direction forecasting problem, and enabled more effective scheduling of gas releases.

The accompanying maps were prepared from hourly airways sequences. Times were selected so that, in most cases, the map represents the sea-level pressure pattern existing midway between two gas releases. The only values plotted are the surface wind speed and direction and the sea-level pressure report from the station. Temperatures were used in some of the analyses, but omitted from the figures in the interest of clarity of reproduction. Standard analysis procedure was used, except that the isobar interval is 1 millibar. All analyses were checked for consistency with the U. S. Weather Bureau analyses for the same period. The isobar labels are the last two digits of the sea-level pressure: 13 = 1013 millibars.

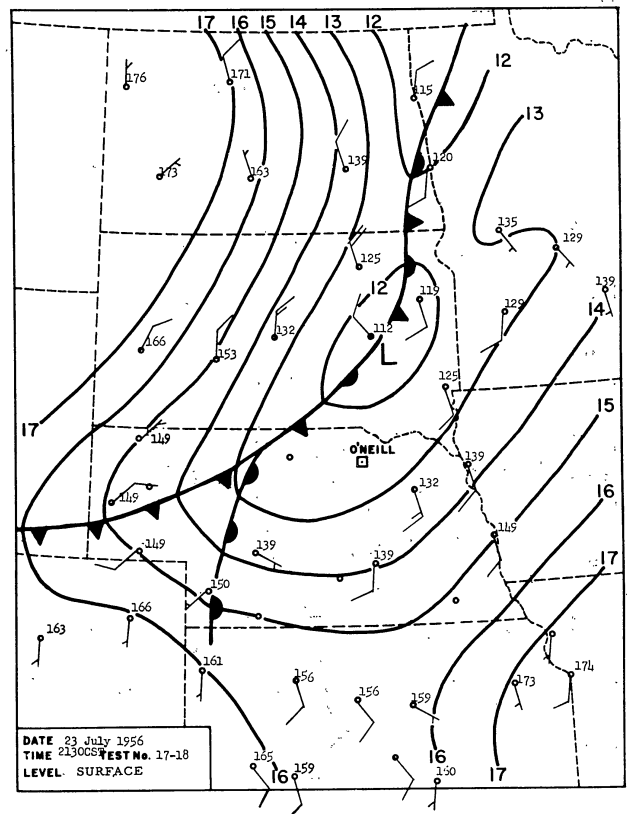
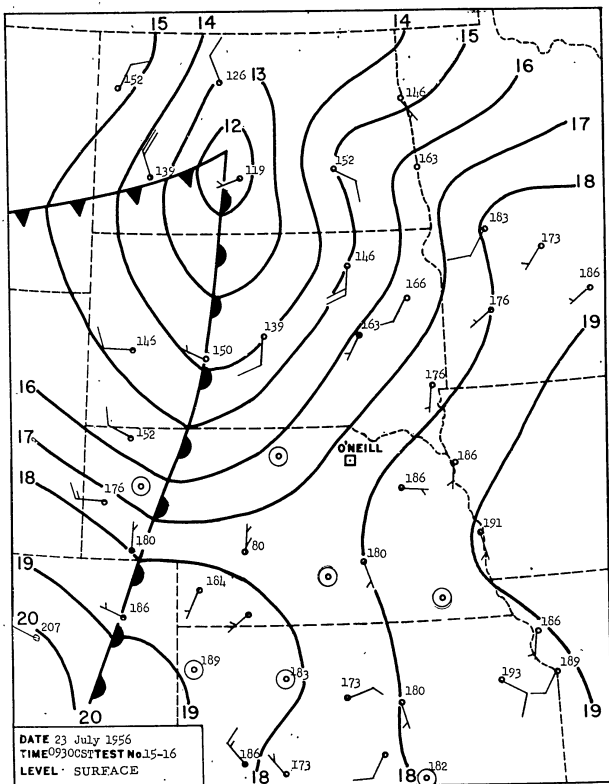


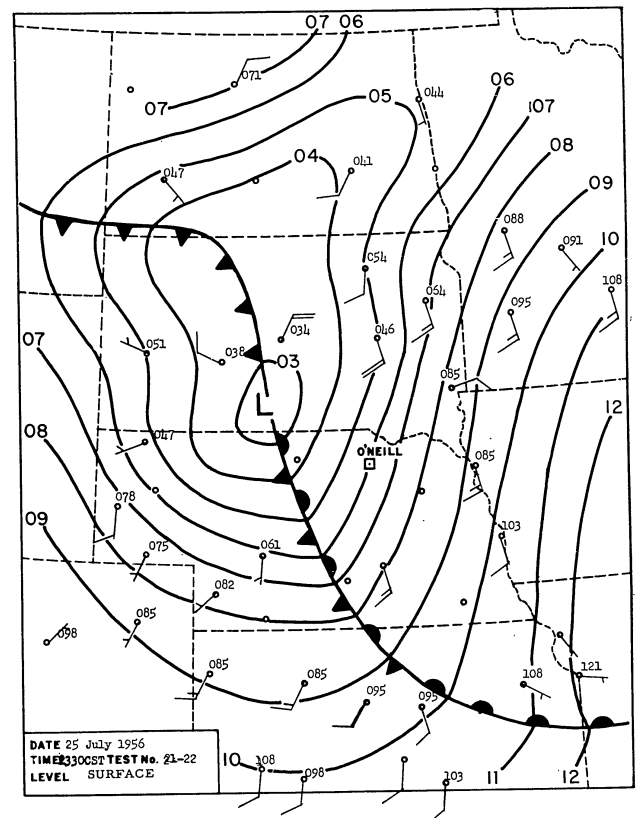
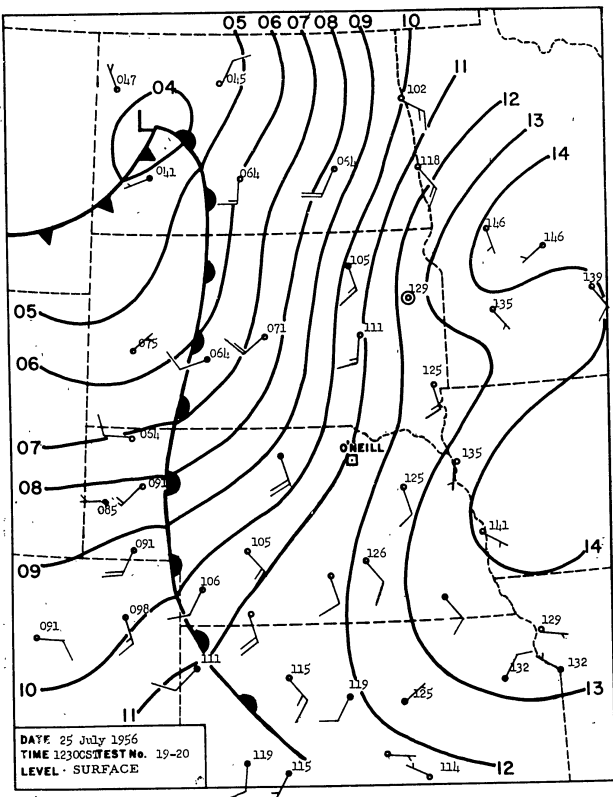


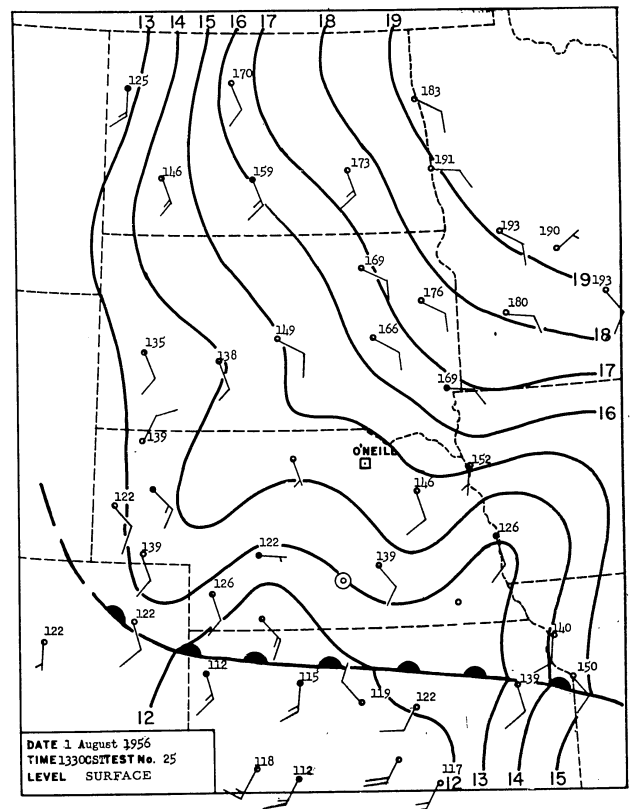
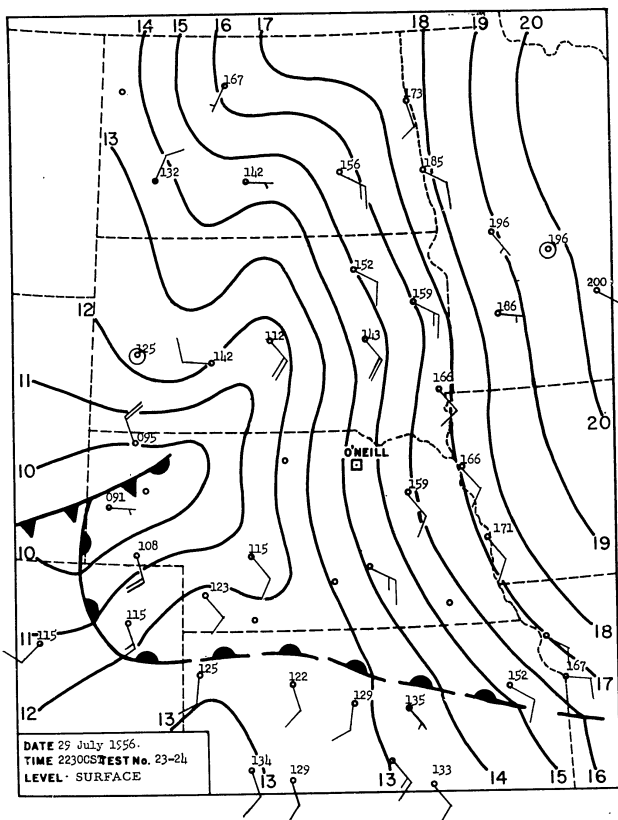


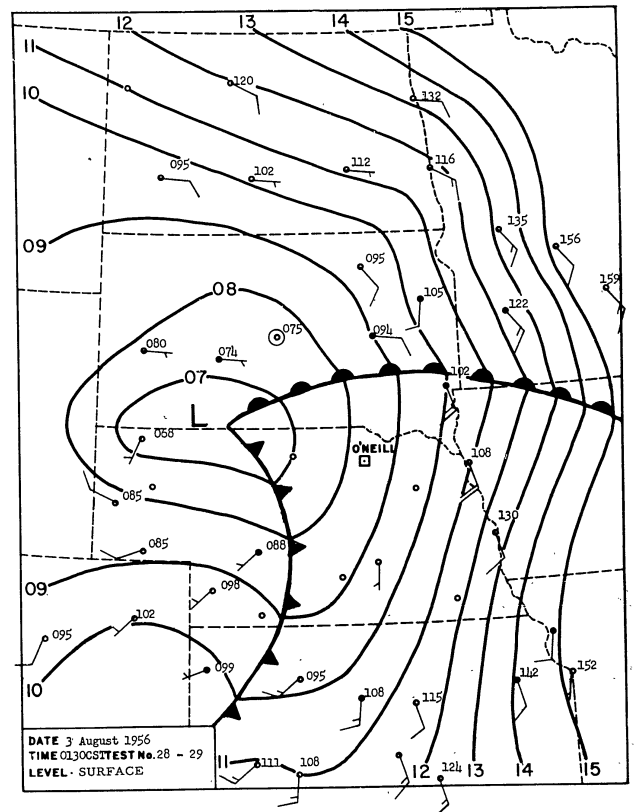
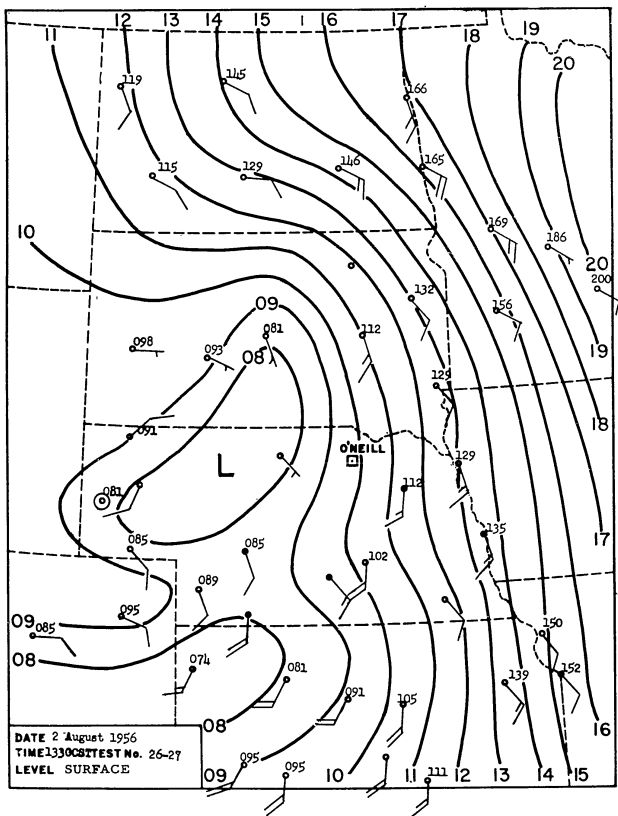


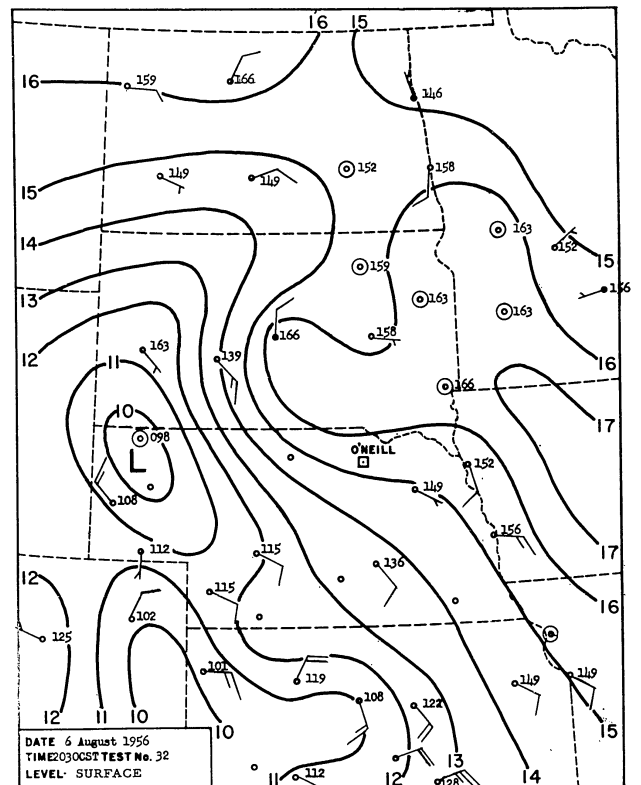
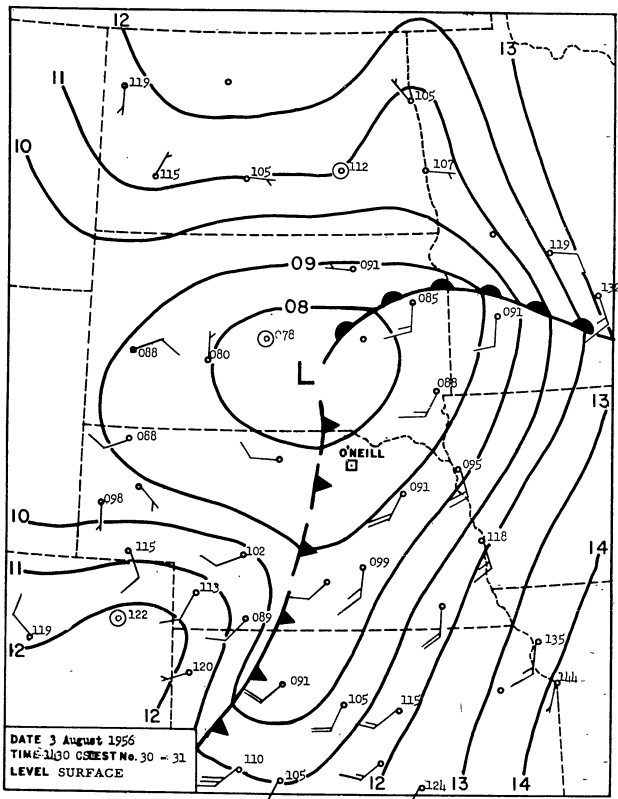


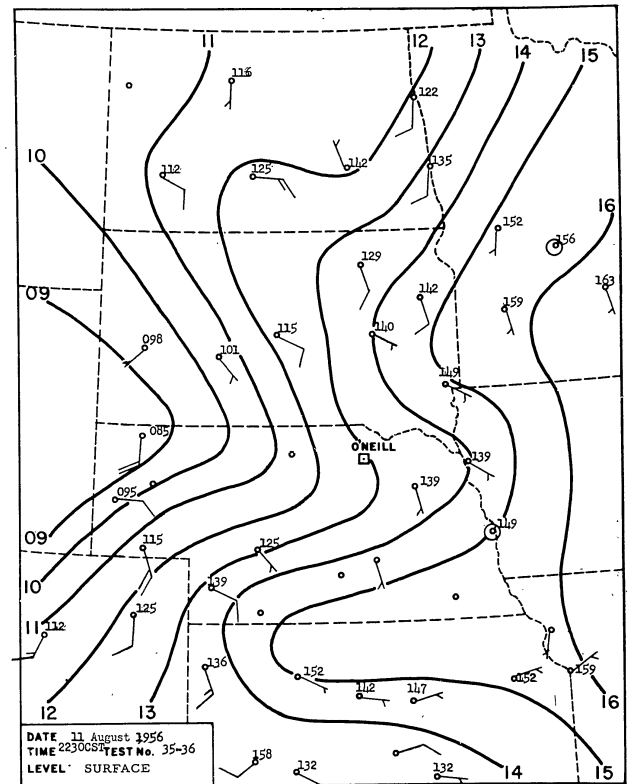
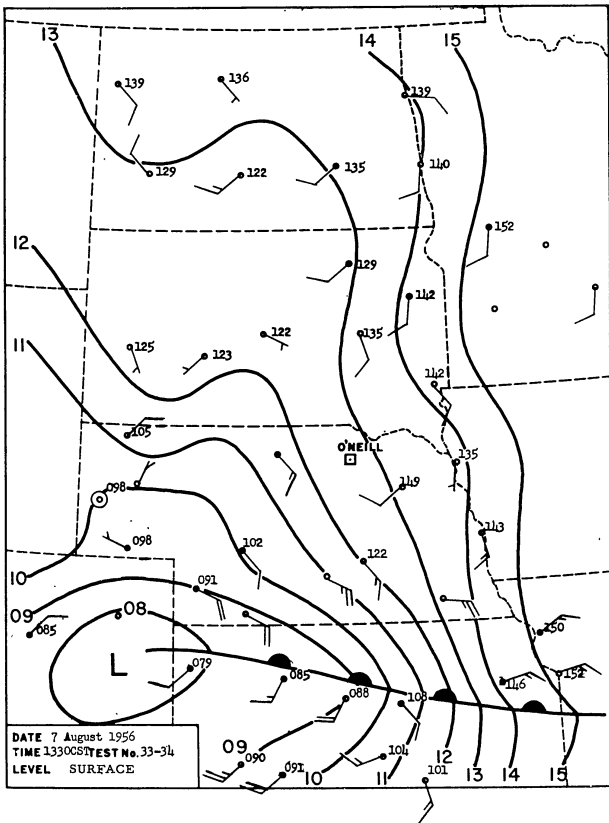


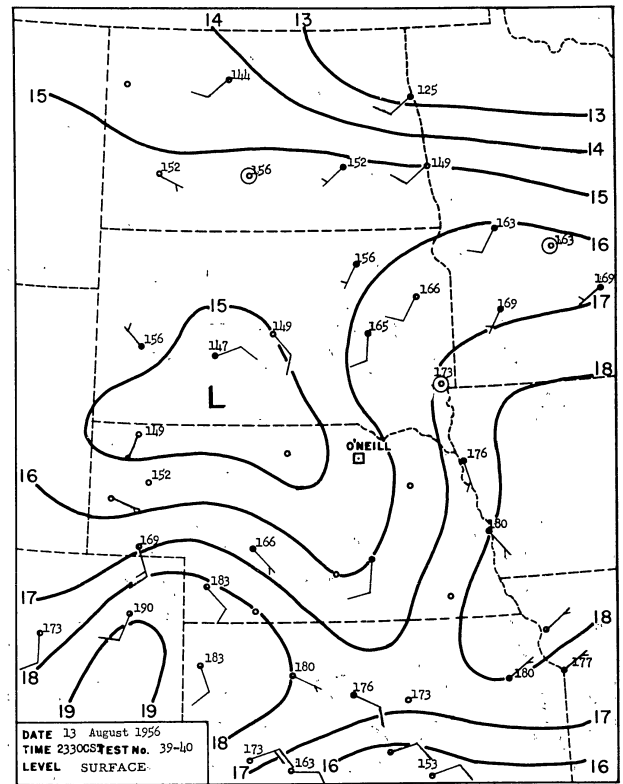
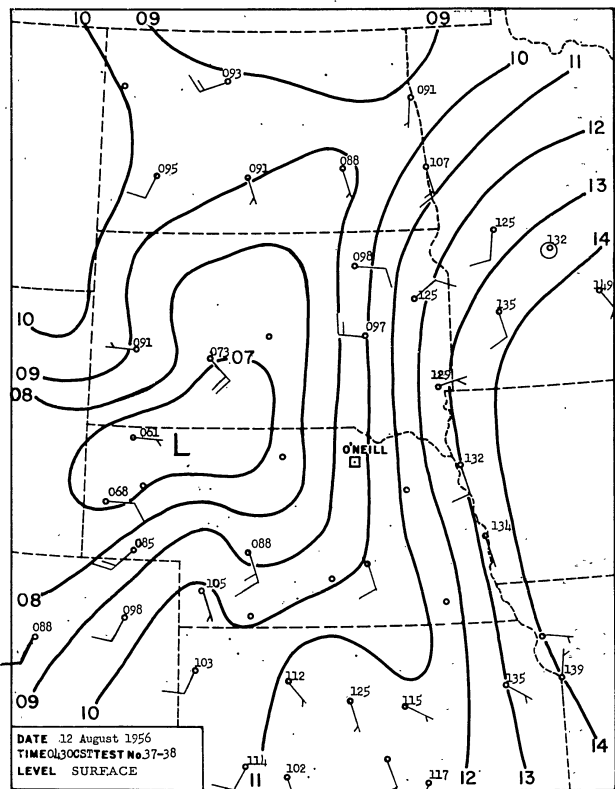






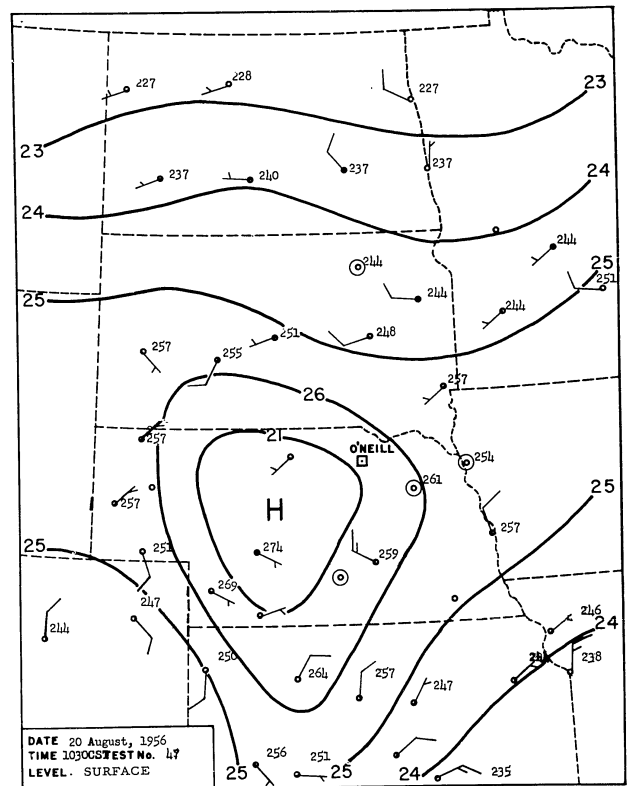
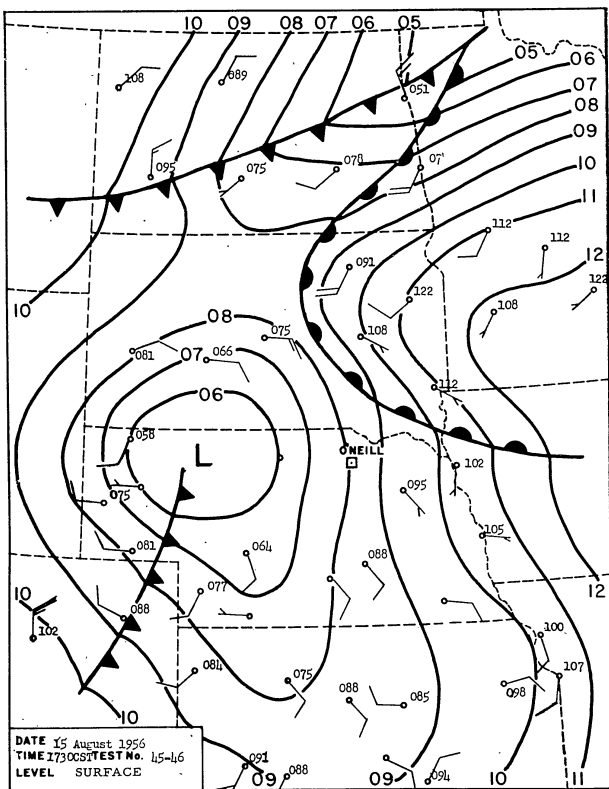


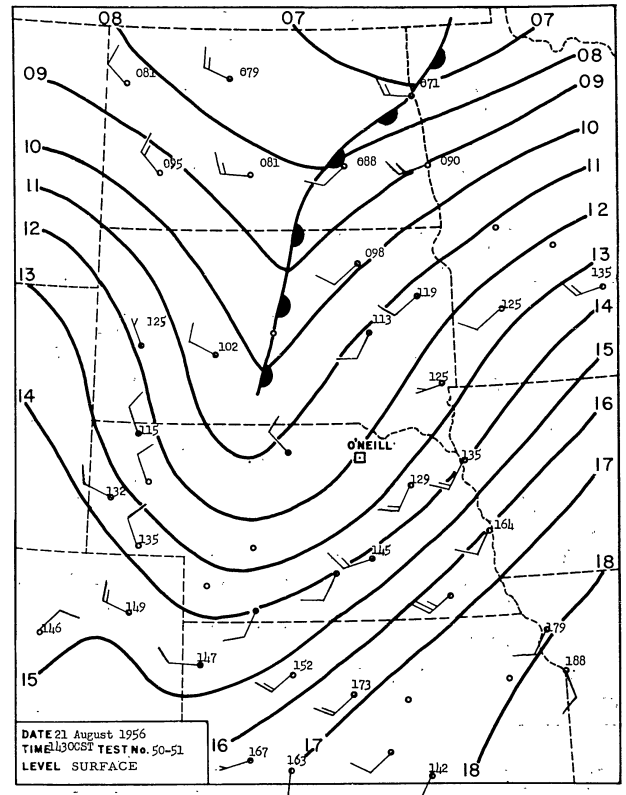
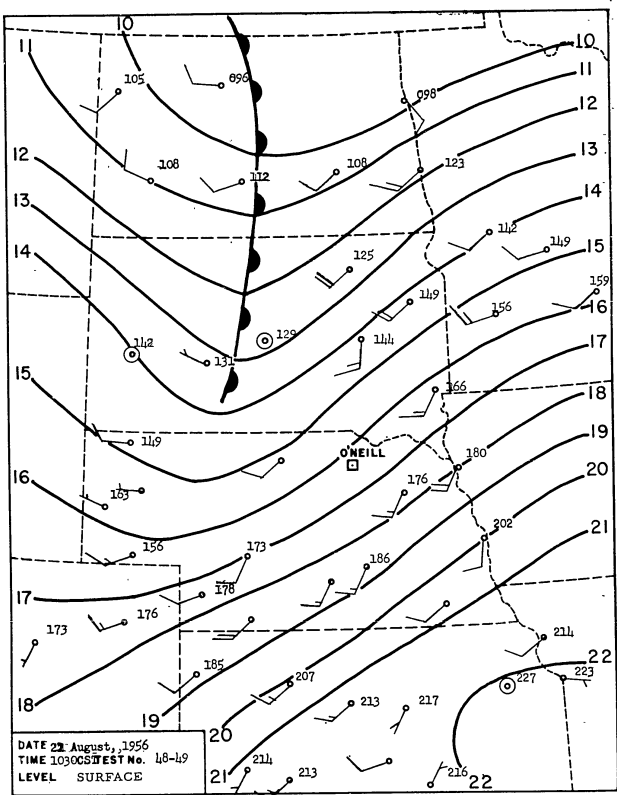


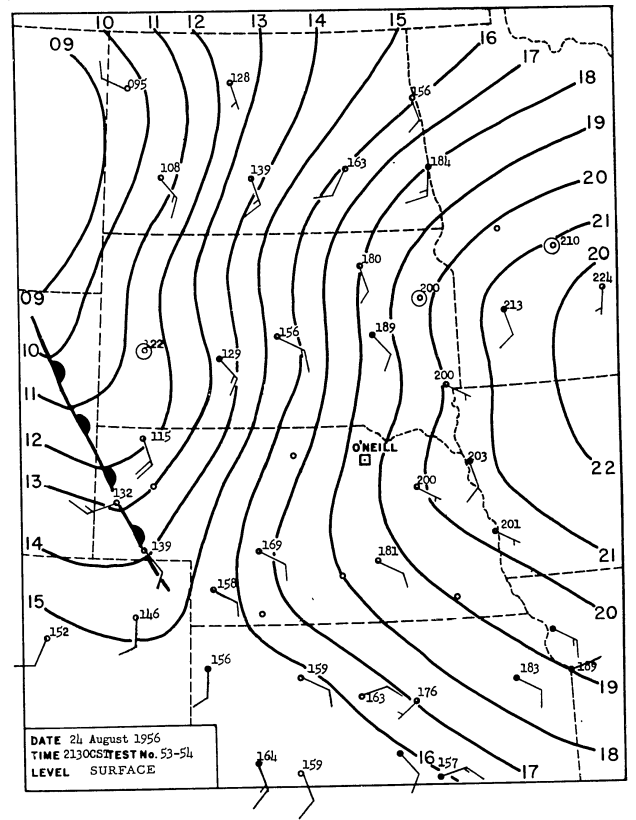
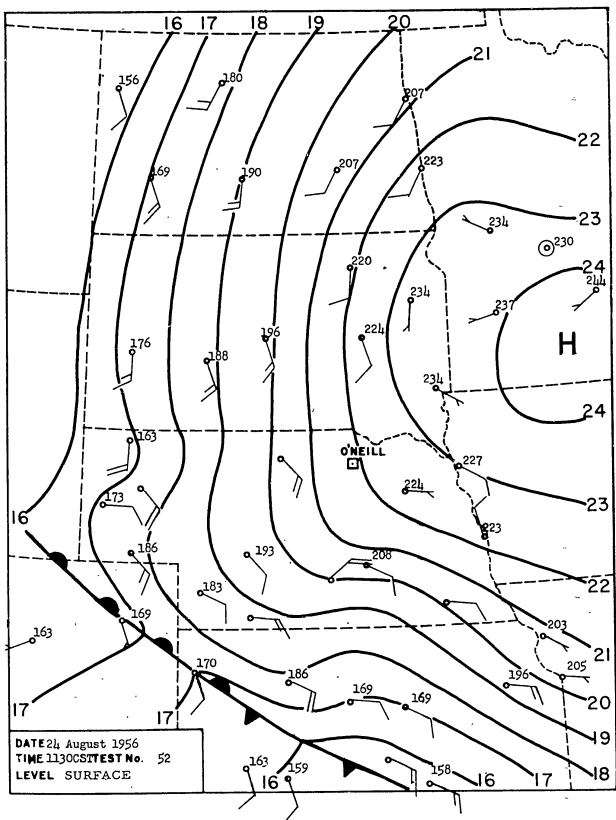


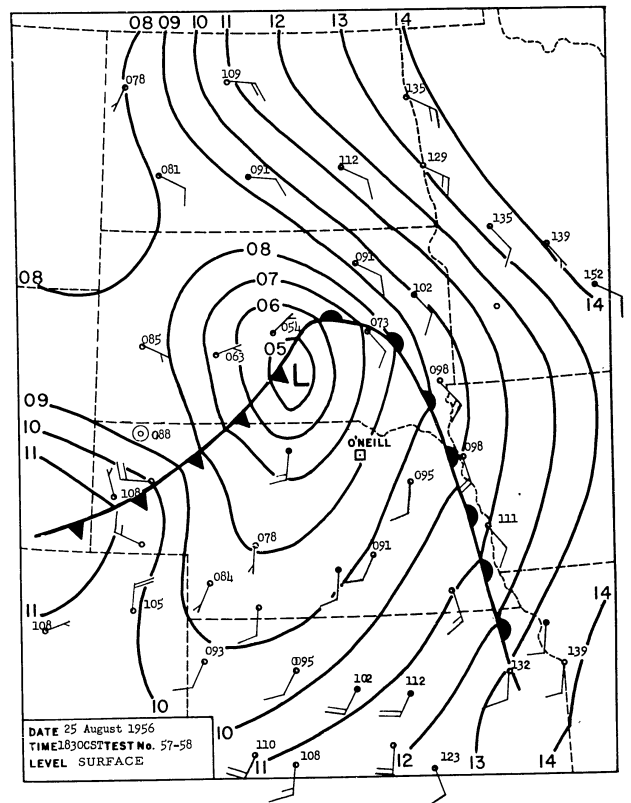
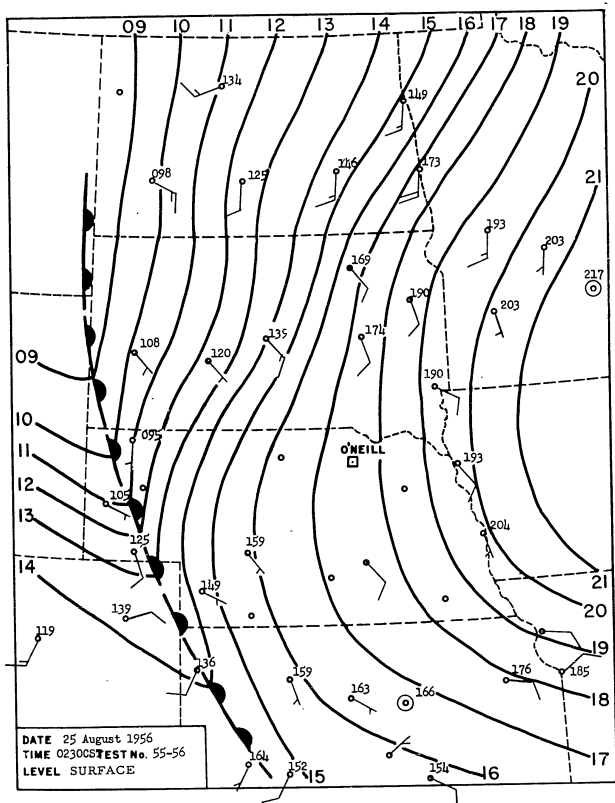


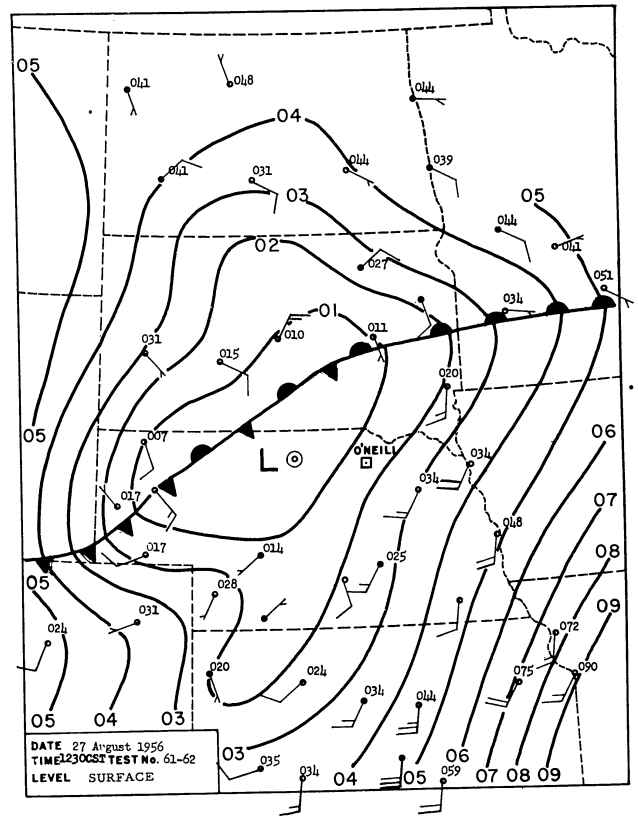
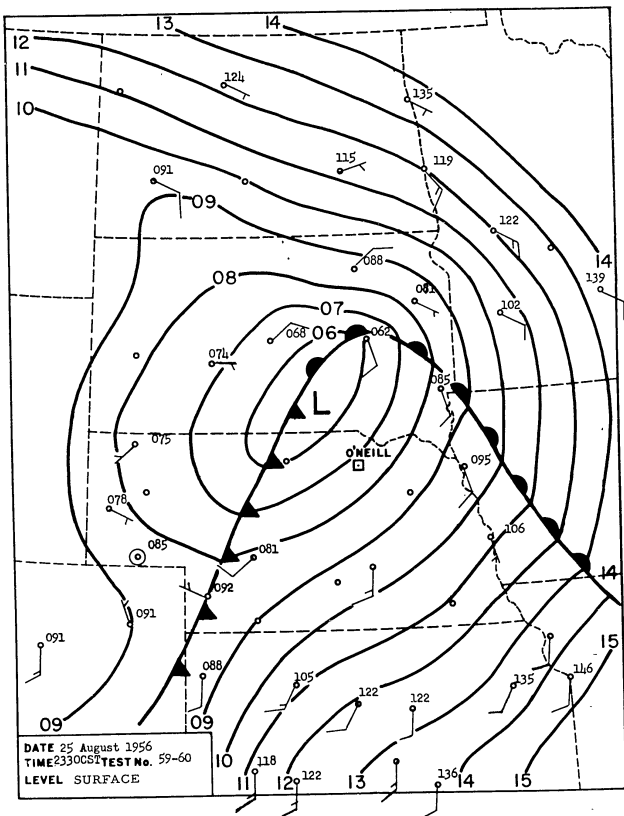


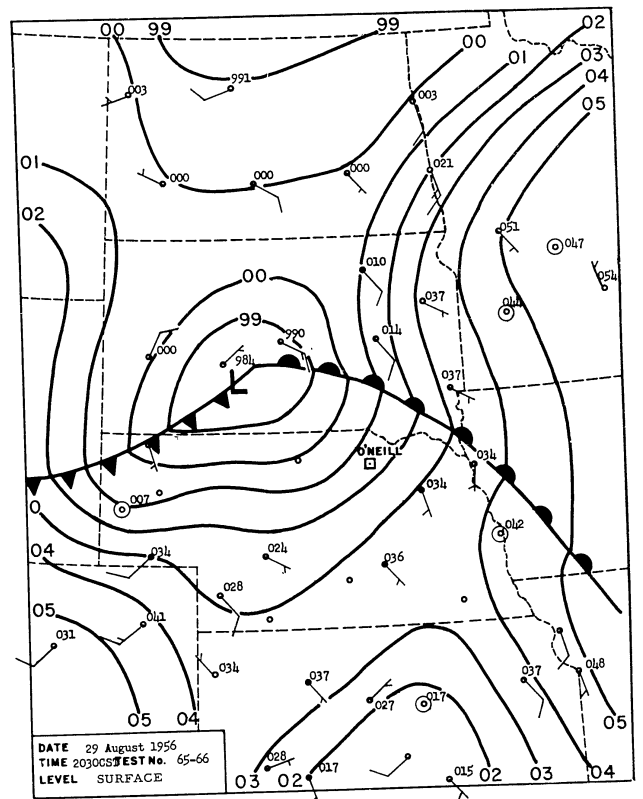
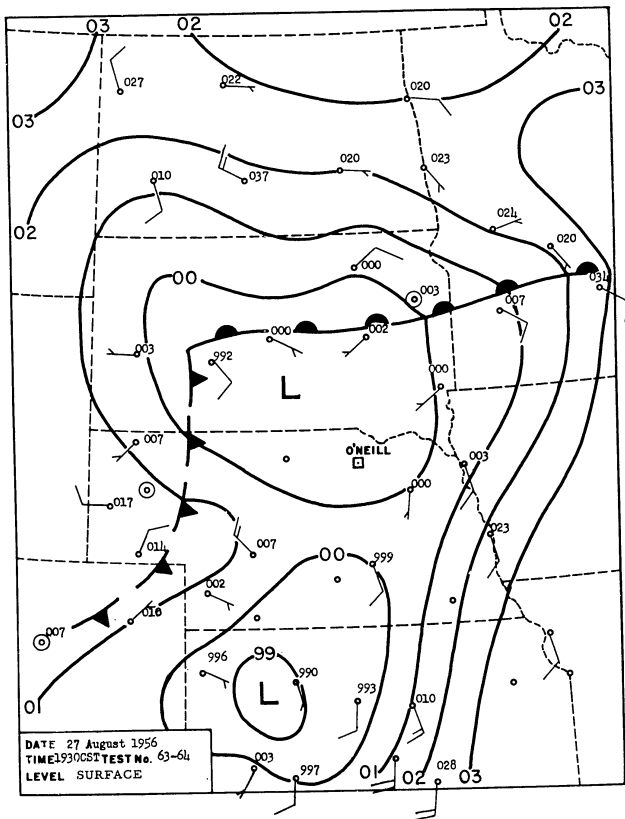


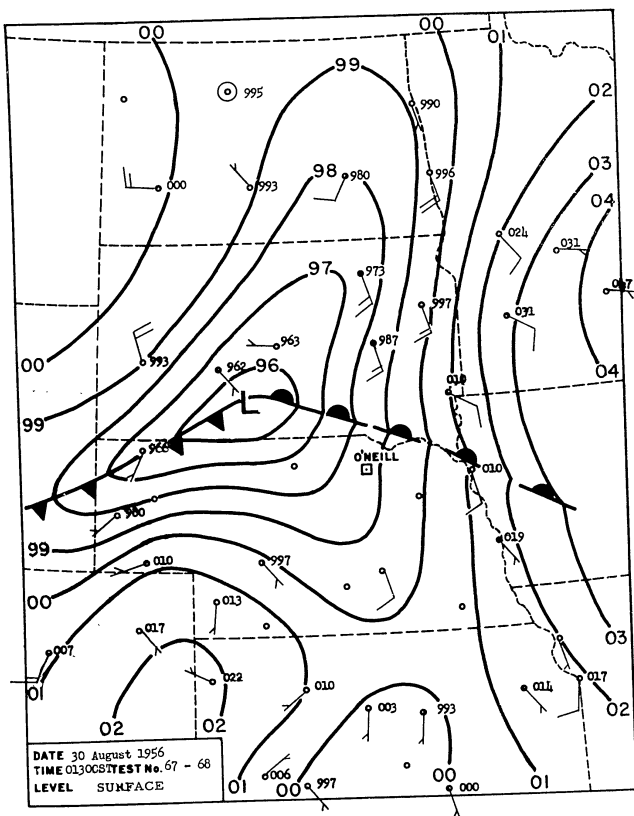












CHAPTER 5  
DIFFUSION MEASUREMENTS DURING PROJECT PRAIRIE GRASS

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Massachusetts Institute of Technology

5.1 Introduction

The diffusion measurements obtained during Project Prairie Grass comprise average or time-mean concentrations determined at selected points downwind from a continuous point source of sulfur-dioxide gas located near ground level. Sulfur dioxide is relatively inexpensive and readily available; the sampling technique is based on firmly established and extremely simple physical principles, and is capable of resolving minute concentrations of the order of 0.01 parts per million. The sampling network utilized midget impingers mounted at a height of 1.5 m along five semicircular, concentric arcs located within 800 m of the release-point. Limited vertical sampling was carried out along the 100-m arc by means of impingers mounted at 9 levels on 6 lightweight towers. Electrically-operated vacuum units suitably positioned within the sampling network provided aspiration for the impingers. During the diffusion experiments, air was drawn into the impingers through short sections of capillary tubing and bubbled through a dilute hydrogen-peroxide solution. Sulfur dioxide present in the air samples combined with the hydrogen peroxide to form sulfuric acid. Average gas concentrations were determined from laboratory measurements of the electrical conductivity of the aspirated solutions.

Data are available for approximately 70 diffusion experiments carried out in a wide variety of weather conditions. Approximately half the data refer to unstable (daytime) thermal stratification and the remainder were obtained at night in the presence of temperature inversions. In the experiments, the sampling networks were put in operation just before the start of the gas release which lasted for 10 minutes; operation of the networks continued for several additional minutes after

the end of the gas release to permit the wind to transport the tracer beyond the 800-m arc. A detailed description of the apparatus and techniques used during the diffusion experiments is given below.

5.2 Generation of the Tracer

The basic features of the sulfur-dioxide generator are shown schematically in Figure 5.1 and a photograph of the field installation of the generating equipment is presented in Figure 5.2. Operation of the generator may be described as follows: Liquid sulfur dioxide from an inverted 150-lb cylinder was vaporized in a specially-constructed chamber immersed in 150 gallons of hot water contained in a large circular tank. Approximately  $3 \times 10^6$  calories were required to vaporize the sulfur dioxide released during each experiment. This amount of heat must be supplied from an external source to maintain a constant rate of emission consistent with efficient source operation. Otherwise, the attendant rapid cooling of the gas-liquid interface produces excessive pressure decreases throughout the system and a consequent steady decrease in the rate of emission. The requisite heat transfer was facilitated by continuous circulation of the heated water in the large tank through a 100-ft coil of copper tubing placed inside the vaporization chamber; thermostatically-controlled immersion heaters rated at 10 kw maintained the water temperature at approximately 50°C. It was frequently necessary, during the latter part of the daytime gas releases, to add liquid sulfur dioxide to the vaporization chamber to maintain the required emission rate; electric strip heaters attached to the exterior of the inverted steel cylinder aided in effecting this transfer. From the vaporizer, the gas flowed through a pressure regulator and an adjustable valve controlling the flow rate into a large iron case meter (American Meter Company Type 500B). Total output registered on a special indicating dial at the top of the meter case. The gas meter was adjusted at the factory to read about 1 percent low with an accuracy of  $\pm 0.5$  percent. Pressure and temperature of the gas were measured both at the inlet and outlet

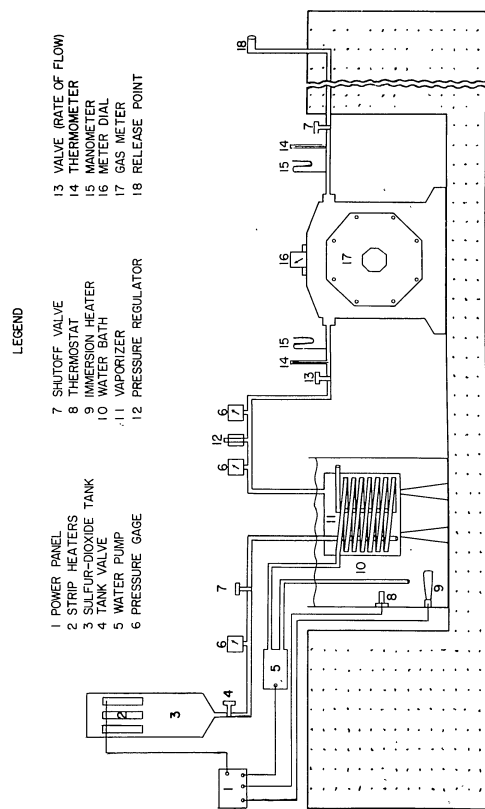


Figure 5.1 Schematic diagram of sulfur-dioxide generator.



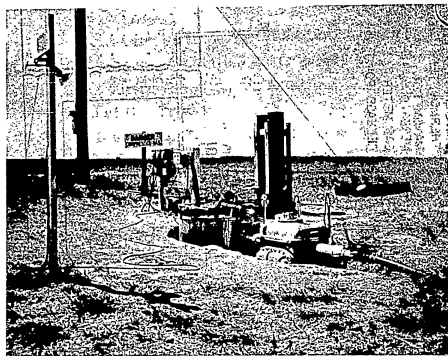


Figure 5.2 Field installation of sulfur-dioxide generating apparatus.

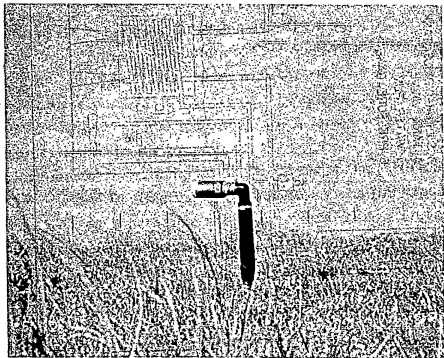


Figure 5.3 Release-point for the tracer.

of the meter to permit accurate reduction of the total amount of gas released to a source strength expressed in  $\text{g sec}^{-1}$ . As shown in Figure 5.2, the gas meter and the large water tank were set in a shallow trench to minimize the disturbance to the natural air flow immediately upwind from the release point for the sulfur-dioxide gas. The tracer was conducted from the meter outlet through a 50-m length of 2-inch plastic pipe buried just beneath the surface of the ground, and was released horizontally at a height of 46 centimeters. A photograph of the orifice is presented in Figure 5.3; the picture was taken prior to the start of the field experiments before the grass at the field site was mowed. In six experiments (Nos. 63-68), the height of the release point was adjusted to 1.5 m, the height of the samplers in the horizontal sampling network.

The rate of tracer emission was adjustable over a wide range; the maximum source strength of about  $100 \text{ g sec}^{-1}$  was utilized during the daytime releases. Uniformity of the emission rate was checked during the releases by marking the passage of each 10 cu ft of gas through the meter on an Esterline-Angus recorder; a manually-operated switch activated a sidemarker pen that put a pip at the side of the moving chart roll. During all nighttime experiments and during most daytime experiments, observed variations in the emission rate were less than 5 percent. In a few daytime gas releases, the emission rate during the last minute of source operation was from 5 to 10 percent below the initial rate.

### 5.3 Description of the Sampling Network

Average gas concentrations were determined at approximately six hundred individual sampling stations located within a semicircle of radius 800 m centered on the release point for the tracer. As shown in Figure 1.1, the base line of the horizontal sampling network was oriented along a true East-West line to take advantage of prevailing southerly winds. Midget impingers (Mine Safety Appliance Company) were mounted at a height of 1.5 m on steel fence posts located along five

semicircular arcs. The posts were spaced at intervals of 2 degrees along the 50-, 100-, 200-, and 400-m arcs; at 800 m, a separation interval of 1 degree was used. The posts for each arc were numbered consecutively, Post Number 1 being located at the intersection of the arc with the western limb of the base line (that is at a true angular bearing of 270 degrees from the release point). Details of the impinger installation are shown in Figures 5.4 and 5.5, and a view of part of the fence post array along the 100-m arc appears in Figure 5.7.

Each impinger contained 10 ml of dilute (slightly acidified) hydrogen peroxide solution. Use of capillaries (see Figure 5.5) reduced the variations in flow rate between impingers to within 1 or 2 percent; otherwise, variations of the order of 10 percent were frequently present. Each section of precision bore capillary tubing (inside diameter -  $0.0252 \pm 0.0003$  in.; length - 1.330 to 1.335 in.) was tested individually in the laboratory with a standard impinger; only those sections that were within 1.5 percent of standard were selected for field use. Air thus drawn into the impingers passed down the central glass tubes and was broken into tiny bubbles as it impinged upon the bottom of the glass flasks. Sulfur dioxide present in the air reacted with the hydrogen peroxide to form sulfuric acid. The collection efficiency of the impingers, as indicated by laboratory tests described below, was greater than 97 percent for all the Prairie Grass experiments.

Aspiration of the impingers was provided by 11 vacuum units (electric motor, pump, tank, vacuum regulator) apportioned as follows along the various arcs: one unit at 50 m; two units at 100 m (one for the vertical network described below), 200 m, and 400 m; and four units at 800 meters. One of the units used in field experiments is shown in Figure 5.6. The 1/3-hp motor, pump, and tank are sold commercially for use with farm milking machines (Sears Roebuck and Company); the diaphragm-type regulator (Fisher Governor Company Type 734A), seen at the extreme left of the photograph, maintained the line vacuum within 1 to 2 percent of the desired value during the 10-minute sampling period.

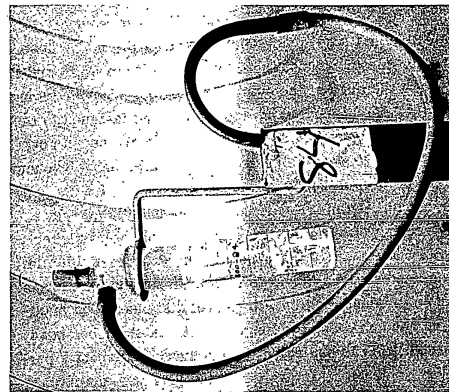


Figure 5.5 Close-up of midget impinger in operation.

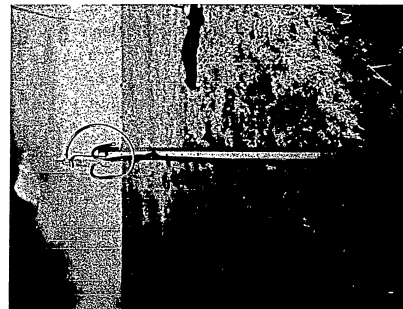


Figure 5.4 Midget impinger mounted at height of 1.5 m on steel fence post.

A visual check on the line vacuum was provided by a mercury manometer mounted on a steel fence post. Heavy-wall rubber hose was attached to the inlets of the vacuum tanks (see Figure 5.6) and laid on the ground along the arcs of the sampling network. Copper tubing was inserted in the hose at each sampling station and fastened to the steel fence posts (see Figure 5.4). The impingers were set in ring holders attached to the tops of the posts and connected to the vacuum line by short lengths of gum rubber tubing (see Figure 5.5). An aspiration rate of  $1.0 \text{ liter min}^{-1}$  was used at 50 and 100 m; this required a line vacuum of 51 mm of mercury. A somewhat higher aspiration rate ( $1.5 \text{ liter min}^{-1}$ , requiring a line vacuum of 100 mm of mercury) was used at the other arcs to compensate in part for the expected decrease in concentration with travel distance. The maximum drop in line vacuum along the longest sections of rubber hose was about 4 percent; this is equivalent to a reduction of about 2 percent in the rate of aspiration. Operation of the vacuum-pump motors was controlled from a central switchboard located along the center-line of the sampling network at a travel distance of about 450 m from the release point. Line vacuums were checked and necessary adjustments made just before the start of each diffusion experiment.

Average gas concentrations were also determined along the vertical from midjet impingers mounted at nine levels on each of six towers located along the 100-m arc. The lightweight television-type towers (Alproco, Inc.) were spaced at intervals of 14 degrees and were positioned symmetrically with respect to the center line of the horizontal sampling network. A photograph of the tower array appears in Figure 5.7. The towers were constructed of aluminum alloy with triangular cross sections measuring 8-1/2 inches on a side; each tower rested on a small cement base and was supported at three levels by 3/16-inch stranded-steel guy wires. The technique for installing the impingers on the towers is illustrated in Figure 5.8. Heavy rubber hose similar to that used in the horizontal network was

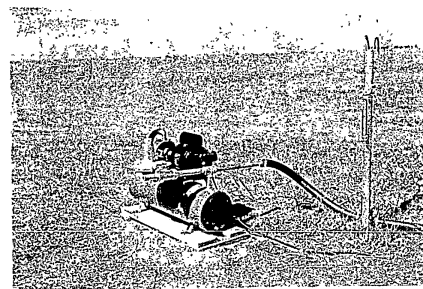


Figure 5.6 Vacuum unit used to aspirate midjet impingers; mercury manometer indicating line vacuum is mounted on steel post.

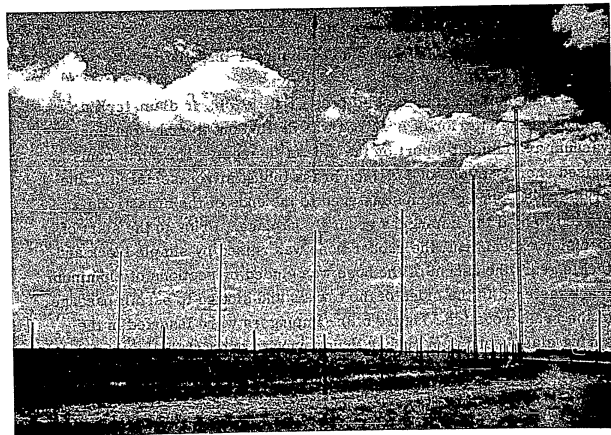


Figure 5.7 Tower array at 100-m arc.



Figure 5.8 Close-up of impinger installation on tower

fitted with short lengths of solid brass rod (5/8 in. in diameter); a portion of the interior of each rod was drilled out to make the line vacuum available at a port on the side of the rods. The ports comprised short sections of 1/4-inch brass tubing silver-soldered to the brass rods. Spring clamps fastened to the ends of the brass rods served to hold the impingers securely in place. Prior to the start of a diffusion experiment, the rubber hose was raised by simple block and tackle gear; the ascent of the hose was guided by sections of aluminum track fastened to the sides of the towers and slotted to permit passage of the brass rods (see Figure 5.8). Impingers were inserted in the spring clamps and gum rubber tubing used to connect the impinger outlets to the line-vacuum ports. At the conclusion of the experiment, the rubber hose was lowered and the impingers removed for transport

to the laboratory and subsequent analysis. The rope used to raise and lower the vertical sampling apparatus appears at the extreme right of Figure 5.8. This simple technique worked very satisfactorily. A single vacuum unit located at the center of the 100-m arc provided aspiration for the impingers on the 6 towers. Concentrations were determined at 9 levels on each tower: 0.5, 1.0, 1.5, 2.5, 4.5, 7.5, 10.5, 13.5, and 17.5 meters.

#### 5.4 Laboratory Procedure

The successful execution of the diffusion experiments depended in large measure upon careful analytic procedure and high standards of cleanliness. Any contamination of the impinger solutions seriously impaired the high degree of resolution otherwise obtainable in the measurements. A special laboratory building was erected at the field site to provide storage space for the impingers and auxiliary apparatus, as well as working space for analysis of the aspirated solutions. The building was of double-wall plywood construction, fully insulated, and painted white on the exterior to minimize the absorption of solar radiation. Incursions of dust were largely eliminated through the use of sealed windows and a single entrance on the north side of the building, sheltered from the prevailing southerly winds. An exterior view of the laboratory building appears in Figure 5.9. Suitable temperatures were maintained within the laboratory building by two air conditioners.

Diffusion experiments were scheduled in pairs, each experiment requiring the use of 599 impingers. The impingers were filled by means of pipettes that automatically metered 10 ml of solution. The filling operation is shown in Figure 5.10; the wire basket appearing in the figure contains approximately 50 impingers. After the impingers were filled with hydrogen-peroxide solution, the baskets were stored on shelves in the laboratory (see Figure 5.11) until the field crew took them to the sampling network. Much of the work of installing the impingers within the network and returning the samplers to the laboratory was performed by 12 high-school age boys from O'Neill, Nebraska.



Figure 5.11 Shelves for storage of impinger baskets.



Figure 5.9 Exterior of laboratory.

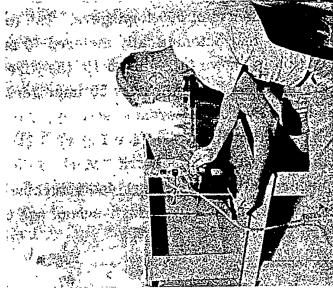


Figure 5.10 Filling impingers with solution.

The following precautions were taken to avoid any mixup in the impingers: All baskets were clearly labeled with respect to the appropriate arc and the spaces for individual impingers were numbered according to the posts of the horizontal sampling network; the impingers in each



Figure 5.12 Analysis team determining conductance of aspirated solutions

basket were similarly labeled. There were two complete sets of impingers; the baskets of one set were painted blue and those of the second set were painted red. Only one set was ever permitted to leave the laboratory during preparations for a gas release. The impingers for the vertical sampling network were placed in separate baskets and clearly labeled. The field crew left the sampling network area after the impingers had been installed and waited for the conclusion of the experiment. Then, after the tracer had cleared the networks and the meteorological measurements were ended, the field crew collected the impingers and returned the baskets to the laboratory for analysis.

The analysis consisted of measuring the electrical conductance of the aspirated solutions using conductivity cells and Wheatstone bridges. The impinger baskets were placed one at a time in a constant-temperature water bath. When the bath temperature reached the prescribed value, the conductance of the solution in each impinger was measured. An analysis team is shown in Figure 5.12; the man standing has removed the top of the impinger assembly and inserted the dip-type conductivity cell into the solution; the man seated is reading the resistance on a Wheatstone bridge. This equipment was duplicated at

the other end of the laboratory. When all the conductances had been determined and checked for accuracy, the impingers were emptied, rinsed, and refilled with solution in preparation for the next experiment. After the laboratory and field crews had become proficient, it was possible to conduct four diffusion experiments within an 8-hour period.

Reduction of the electrical conductivities to gas concentrations is based on well-known laboratory procedures.\* Calibration curves may be obtained directly by determining the conductance of sulfuric acid solutions of known normality. Equivalent conductance for these solutions is tabulated in standard reference books for a wide range of normality and temperature. The relationship between the specific conductance of a solution at a temperature of 27°C and the normality of the solution is shown in Figure 5.13. The scale at the right of the figure expresses normality in terms of milligrams of sulfur dioxide per cubic meter of air for 10 ml of absorbing solution and a sample volume of air of 15 liters. The reference level for zero concentration was obtained from the average conductance of aspirated solutions contained in impingers that were clearly in sectors of the sampling network outside the limits of the gas plume. The uncertainty in the laboratory technique for determining conductance is less than 2 percent within the normal range of concentrations.

##### 5.5 Collection Efficiency of the Midget Impingers

The apparatus shown in Figure 5.14 was used to determine collection efficiencies of the midget impingers in the laboratory. Sulfur dioxide gas and air were metered into the vertical pipe at the left and entered the large mixing tank; the mixture was removed from the tank and drawn through the pipe and rubber hose shown at the right of the photograph by an exhaustor located outside the laboratory building. Both the amount of air and sulfur dioxide were adjustable over a

\*For a previous application of this method see: Dean, R. S., and others, 1944: Report submitted to the Trail Arbitral Tribunal. Bull. U. S. Bureau of Mines, No. 453.

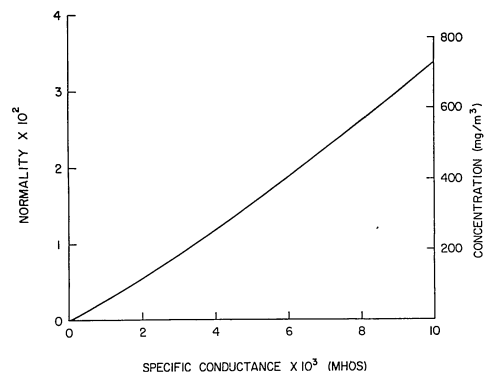


Figure 5.13 Calibration curve showing specific conductance as function of normality and concentration.

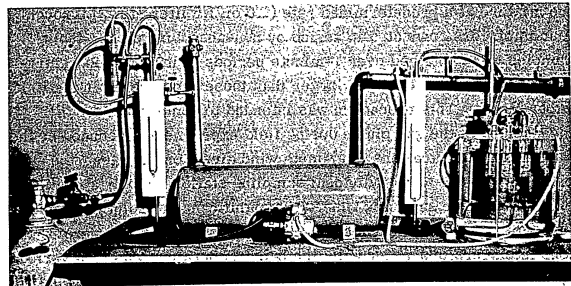


Figure 5.14 Apparatus for determining collection efficiency of midget impingers.

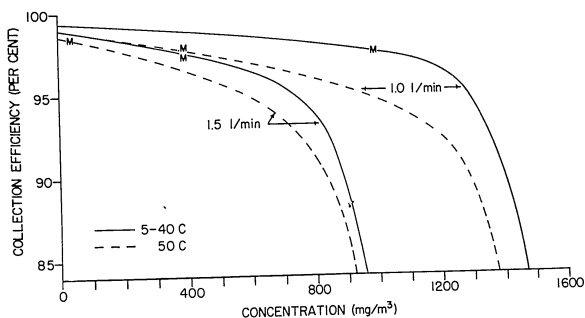


Figure 5.15 Collection efficiencies of midjet impingers used in Prairie Grass diffusion experiments

wide range. The mixture was sampled through ports in the exit pipe in the following manner: The small vacuum pump in the foreground drew the mixture at a predetermined rate ( $1.0$  or  $1.5 \text{ liter min}^{-1}$ ) through four impingers connected in series by non-absorbing plastic tubing. Samples were obtained over 1-minute periods at levels of concentration approximately 10 times larger than those encountered in the field experiments. This procedure was intended to compensate for the meandering of the gas plume during field experiments produced by the larger-scale fluctuations in azimuth wind direction; in effect, the gas plume is present at an individual sampling station for only a fraction of the 10-minute sampling time. The significance of solution temperature on the measurement technique was investigated by immersing the four impingers in a water bath; the bath temperature was then varied over the range from  $5^\circ$  to  $50^\circ\text{C}$ . Conductivity measurements of the solutions in the four impingers provided concentration data used in calculating the collection efficiencies presented in Figure 5.15.

The results are directly applicable to the Project Prairie Grass diffusion experiments; the concentrations plotted in Figure 5.15 are adjusted for the 10-minute sampling periods of the field experiments (that is they are  $1/10$  the values determined from the laboratory tests described above). Maximum 10-minute concentrations measured during the Prairie Grass experiments are indicated in the figure by the symbol **M**. The data indicate that the collection efficiencies during Prairie Grass were greater than 97 percent in all cases. The sharp decrease in collection efficiency with increasing concentration exhibited by the curves is associated with the removal of hydrogen peroxide from the solution; the concentration at which this occurs can be altered by changing the amount of hydrogen peroxide in the solution. The solution used during Prairie Grass, and in the laboratory experiments for determining the collection efficiency, was prepared by adding 50 ml of 30 percent hydrogen peroxide and 10 ml of  $1/10$  normal sulfuric acid to 18 liters of distilled water. The solution's temperature appears to have no significant effect on collection efficiency for temperatures within the  $5^\circ$  to  $40^\circ\text{C}$  range; for temperatures of  $50^\circ\text{C}$ , the collection efficiency is somewhat reduced as indicated by the dashed lines in Figure 5.15.

#### 5.6 Discussion of the Reliability of the Concentration Measurements

As pointed out, above, determining time-mean gas concentrations involves a relatively large number of individual measurement techniques and pieces of equipment. With few exceptions, the uncertainties associated with these individual procedures are all within the range of from 1 to 2 percent. It is also evident that many, if not most, of these uncertainties are probably random and tend largely to compensate one another. The accuracy of the determination of average source strength for individual gas releases depends principally upon the reliability of the gas meter and on the representativeness of the temperature measurements obtained, during the releases, at the inlet and outlet of the meter.

In calculating the weight of gas released, arithmetic means of the

inlet and outlet measurements were used. For the nighttime gas releases, there is no significant difference between the two sets of data. During the daytime releases, the inlet temperature is frequently 10° to 12°C lower than the outlet temperature. In these cases, use of the average temperature might lead to uncertainties of the order of 1 to 2 percent in the calculated source strength. Changes in ambient air temperature have only a slight effect on the mechanical parts of the gas meter; the manufacturer states that the temperature coefficient for the displacement mechanism is approximately 0.05 percent per degree Fahrenheit. Over the range of temperatures encountered during the experiments, this would result in an uncertainty of about 1 percent. Duration of the gas release was controlled within limits of 1 to 2 percent. Residual sulfur dioxide remaining in the plastic pipe used to conduct the tracer from the meter to the release-point constitutes approximately 1 percent of the total volume released during nighttime experiments and about 0.5 percent of the total volume released during the daytime experiments. This appears to be a negligible source of error. The adjustment in the gas meter at the factory, resulting in dial readings approximately 1 percent too low, is offset very nicely by the collection efficiency of the impingers which averages approximately 99 percent.

Possible sources of error in the collection of gas samples exist principally in variations in the rate of aspiration and loss of solution due to evaporation. As mentioned above, laboratory tests of individual impingers and capillaries limited the variation in flow rate under standard vacuum to a range of 1 to 2 percent. In field use, line vacuum depended upon the initial adjustment based on mercury manometer readings, the sensitivity of the vacuum regulators, and the line drop along the arcs. Each of these factors contains an uncertainty of about 1 to 2 percent with respect to the aspiration rate. All concentrations were calculated on the assumption that the volume of absorbing solution in the impingers remained unchanged during the experiments. There is

actually a small reduction in volume due to loss of water vapor during aspiration. Similar loss of sulfuric acid is considered insignificant in view of its very low vapor pressure.

The water vapor loss may be estimated in two ways. The amount of water vapor required to saturate the entrained air may be calculated from a knowledge of the aspiration rate, air temperature, relative humidity, and the duration of the sampling period. The latter comprises both the actual operation time of the sampling networks during each gas release and the time required to check the line vacuum prior to the start of each release. No records were kept of the total aeration time which varied from experiment to experiment and from one arc to another. However, a period of about 18 to 30 minutes was usually required. Calculations based on the maximum aeration time of 30 minutes and an aspiration rate of 1.0 liter  $\text{min}^{-1}$  indicate, for the nighttime experiments, a median error of 2 percent and an extreme range from 0.6 to 5.0 percent. Similar calculations for the daytime experiments indicate a median error of 5.5 percent with an extreme range from 2 to 10 percent. Loss of solution by evaporation may also be estimated from differences in the conductance of aspirated solutions in impingers located outside the limits of the time-mean gas plume and the conductance of unaspirated solutions in spare impingers. These data are available for practically all the experiments and permit calculation of correction factors at each travel distance.

The principal source of uncertainty in this method is the presence of background contaminants that may affect the conductance of the aspirated solutions; it appears that this factor is generally quite small and probably does not account for more than a 1 or 2 percent variation in conductance. Approximate correction factors based on conductances are presented in Table 5.4; the results indicate a median error of 3 to 5 percent for the nighttime experiments and of 6 to 9 percent for the daytime experiments. The lower estimates refer to the concentration measurements at 50 and 100 m, and the higher estimates refer to the



remaining travel distances and reflect principally the difference in rates of aspiration discussed above.

The laboratory analysis of the aspirated solutions was performed in the following manner: Baskets containing about fifty impingers were placed one at a time in the water baths. When the proper bath temperature had been attained, a dip-type conductivity cell was inserted in one impinger and the conductance determined. Then the cell was removed, excess solution was shaken off, and the cell was inserted in the next impinger, and the process repeated. This procedure entailed a slight carry-over of solution from one impinger to the next. The usual practice involved determination of conductances from one edge of the plume to a point slightly beyond the peak concentration; the analysis then continued from the other edge of the plume towards the peak. The reduction in concentration produced by the carry-over and subsequent dilution of solutions is estimated to be from 0 to 1 percent. The Wheatstone bridge had an uncertainty of about 1 percent. Errors due to the original adjustment of the conductivity cells and to changes in cell constants are believed to be about 1 or 2 percent. A change of about 7 percent was noted in the constant of one conductivity cell during the period of the experiments; conductances determined with this cell were subsequently adjusted. Electrolytic solutions have temperature coefficients of resistance of about 2 percent per degree Centigrade; since the water bath temperature was maintained constant within 0.1°C, variations in solution temperature may be neglected as a possible source of error.

Reduction of the electrical conductivities of the aspirated solutions to concentrations was based on results of laboratory determinations of the specific conductance of sulfuric acid solutions of known normality. The values thus obtained are in substantial agreement with those derived from published data. The calibration curves used in reducing the measured conductances are believed accurate to about  $\pm 3$  percent. The reference level for zero concentration was obtained from the arithmetic mean of the conductances of aspirated solutions contained in

impingers located outside the limits of the time-mean gas plume. In general, this concentration level is almost entirely due to the small amount of sulfuric acid added in preparing the dilute hydrogen-peroxide solution. It does not, therefore, indicate the presence of any significant amount of sulfur-dioxide in the atmosphere at the Prairie Grass field site. As the limit of resolution of the sampling technique is approached, the uncertainty of determination increases rapidly; for concentrations less than  $0.10 \text{ mg m}^{-3}$ , this uncertainty is approximately 25 percent.

Approximate checks on the reliability of the concentration measurements were obtained by comparing the calculated source strengths with the mass transport of sulfur-dioxide gas through a vertical cross section at a travel distance of 100 meters. This is the only distance at which vertical concentration data are available. The results indicate that the estimates for the mass transport are about 10 percent higher, on the average, than the calculated source strengths for the nighttime experiments; a similar average discrepancy of about 15 percent is noted in the case of the daytime experiments. Roughly one-third of these differences can be explained by the loss of solution due to evaporation; the remainder may be due in part to undetected systematic errors in the sampling technique, to overestimates of the mean wind speed, and to errors inherent in the method of computing the mass transport. At any rate, there is no evidence of any significant loss of sulfur dioxide due to absorption by vegetation or any other factor. It appears likely that the absolute magnitudes of the Prairie Grass diffusion measurements are accurate to within 10 percent and that the relative concentrations are accurate to within 5 percent.

Summaries of the results of the Prairie Grass diffusion measurements are presented in Tables 5.1 to 5.3. Table 5.1 summarizes the source strengths for the individual experiments calculated on the basis of the total volumes of gas released and the temperature and pressure of the gas as it passed through the meter. Ten-minute average gas concentrations measured at a height of 1.5 m at five travel

distances are summarized in Table 5.2. The average concentrations determined from the vertical sampling array at 100 m are presented in Table 5.3. Slow-response meteorological data, useful in converting the concentrations to standard values, are found in Tables 5.4 and 5.5.

Table 5.1. Source strengths Q expressed in  $\text{g sec}^{-1}$  for individual Prairie Grass diffusion experiments

Run No.	Q ( $\text{g sec}^{-1}$ )	Run No.	Q ( $\text{g sec}^{-1}$ )	Run No.	Q ( $\text{g sec}^{-1}$ )
1	81.5	24	41.2	46	99.7
2	83.9	25	101.4	47	103.1
3	56.3	26	97.6	48S	104.0
4	50.5	27	96.8	48	104.1
5	77.8	28	41.7	49	102.0
6	89.5	29	41.5	50	102.8
7	89.9	30	98.4	51	102.4
8	91.1	31	96.0	52	104.0
9	92.0	32	41.4	53	45.2
10	92.1	33	94.7	54	43.4
11	95.9	34	97.4	55	45.3
12	99.1	35S	41.8	56	45.9
13	61.1	35	38.8	57	101.5
14	49.1	36	40.0	58	40.5
15	95.5	37	40.3	59	40.2
16	93.0	38	45.4	60	38.5
17	56.5	39	40.7	61	102.1
18	57.6	40	40.5	62	102.1
19	101.8	41	39.9	65	44.1
20	101.2	42	56.4	66	43.1
21	50.9	43	98.9	67	45.0
22	48.4	44	100.7	68	42.8
23	40.9	45	100.8		

Table 5.2

Ten-minute average gas concentrations measured during Project Prairie Grass at a height of 1.5 m at five travel distances: 50, 100, 200, 400, and 800 m. Entries are in units of  $\text{mg m}^{-3}$ . Individual sampling stations at each travel distance are identified in terms of post numbers which are consecutive; Post No. 1 is located due west of the release-point (that is, at a true angular bearing of 270 degrees from the source). A 2-degree angular separation between adjacent stations was used at the four shorter travel distances and a 1-degree angular separation was used at 800 m.

#### Remarks

No data are presented for Runs No. 63 and 64 due to the presence of extremely light and variable winds. Data for all other experiments have been included. The measurements obtained under stable nighttime conditions should be interpreted with care. In particular, when the wind speed at a height of 2 m is  $< 2 \text{ m sec}^{-1}$ , significant vertical stratification may occur in the plume; in some cases, the plume axis is found below the height of the sampling stations at the shorter travel distances. If this phenomenon is not taken into account, the measurements indicate an increase in axial concentration with increasing travel distance. The vertical concentration measurements presented in Table 5.3 are useful in resolving these problems. With regard to the tabular entries, the letter "M" indicates missing data and the blank spaces denote no measurable concentration.

Run No. 4 - Gas released for 9.5 minutes only. Concentrations have been adjusted to a 10-minute release period.

Run No. 25 - Several gnats were caught in the capillary tubes used as entrances to the samplers. All concentrations known to have been influenced have been indicated as missing.

Runs No. 30 and 31 - Background resistances unusually low and variable. Data believed not significantly affected, except for concentrations below  $5 \text{ mg m}^{-3}$ .

- Run No. 45 - Concentration at Post 38 of the 50-m arc is an adjusted value.
- Run No. 47 - Rate of gas release during the first 90 seconds of the run varied by perhaps + 50 percent of the average rate for the 10-minute period.
- Run No. 50 - Vacuum line to Sampler 62 of the 200-m arc became disconnected during the run. All values measured at this arc are too low.
- Run No. 51 - Vacuum line to Sampler 56 of the 400-m arc is believed to have been disconnected throughout the run. All values for this arc have been adjusted to make allowance for the reduced vacuum.
- Run No. 57 - Vacuum line to Sampler 47 of the 100-m arc is believed to have become disconnected. All values measured at this arc are probably too low.

DATE 3 July 1956  
 TIME 1100-1110 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 1

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						0.145
2	2						24	47	123	14.8	1.18	0.310	0.215
3	3						48						0.205
4	4						25	49	109	14.7	1.23	0.295	0.215
5	5						50						0.250
6	6						26	51	89.4	14.5	0.970	0.090	0.160
7	7	0.110	0.160				52						0.105
8	8						27	53	92.9	14.2	0.995	0.090	0.100
9	9	1.49	0.700				54						0.090
10	10						28	55	115	13.5	1.70	0.420	0.100
11	11	6.13	0.870				56						0.165
12	12						29	57	122	17.0	1.99	0.520	0.190
13	13	25.3	0.765				58						0.185
14	14						30	59	118	13.8	2.20	0.510	0.170
15	15	37.0	2.20				60						0.145
16	16						31	61	106	14.9	2.51	0.495	0.085
17	17	50.9	2.17	0.155			62						0.100
18	18						32	63	114	19.1	2.05	0.725	0.070
19	19	63.8	6.22	0.755	0.030		64						0.060
20	20						33	65	108	18.4	1.57	1.12	0.075
21	21	66.9	11.6	0.675	0.015		66						0.090
22	22						34	67	88.1	17.1	2.35	0.895	0.045
23	23	77.7	9.64	0.525	0.045		68						0.050
24	24						35	69	70.5	17.3	2.79	1.02	0.020
25	25	89.1	9.07	0.455	0.070		70						0.030
26	26					0.055	36	71	80.6	18.2	3.56	0.410	0.045
27	27	139	14.3	0.920	0.255	0.020	72						
28	28					0.015	37	73	99.5	20.2	3.71	0.665	
29	29	119	11.6	1.28	0.140	0.065	74						
30	30					0.010	38	75	112	25.4	3.97	0.610	
31	31	134	18.7	.995	0.270	0.000	76						
32	32					0.045	39	77	123	19.8	4.08	0.650	
33	33	103	19.5	1.87	0.295	0.020	78						
34	34					0.025	40	79	140	24.0	4.07	0.460	
35	35	84.0	22.0	1.77	0.160	0.025	80						
36	36					0.025	41	81	120	21.7	3.34	0.340	
37	37	107	25.6	3.82	0.090	0.055	82						
38	38					0.070	42	83	124	24.4	3.62	0.255	
39	39	106	23.8	4.38	0.130	0.150	84						
40	40					0.155	43	85	121	19.3	2.12	0.060	
41	41	103	22.5	4.25	0.225	0.170	86						
42	42					0.195	44	87	125	17.5	1.73		
43	43	95.7	11.2	2.06	0.385	0.155	88						
44	44					0.150	45	89	95.0	11.6	1.56		
45	45	88.1	10.9	1.94	0.410	0.160	90						

Table 5.2 (Continued)  
 DATE 3 July 1956  
 TIME 1100-1110 CST  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 1

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
46	91	60.6	8.01	0.945		69	136							
47	92					69	137							
47	93	60.6	7.39	0.825		70	138							
48	94					70	139							
48	95	41.1	8.42	0.215		71	140							
49	96					71	141							
49	97	34.7	5.21	0.070		72	142							
50	98					72	143							
50	99	20.0	1.46			73	144							
51	100					73	145							
51	101	12.8	0.230			74	147							
52	102					74	148							
52	103	7.32	0.345			75	149							
53	104					75	150							
53	105	4.47	0.100			76	151							
54	106					76	152							
54	107	3.11				77	153							
55	108					77	154							
55	109	0.185				78	155							
56	110					78	156							
56	111					79	157							
57	112					79	158							
57	113					80	159							
58	114					80	160							
58	115					81	161							
59	116					81	162							
59	117					82	163							
60	118					82	164							
60	119					83	165							
61	120					83	166							
61	121					84	167							
62	122					84	168							
62	123					85	169							
63	124					85	170							
63	125					86	171							
64	126					86	172							
64	127					87	173							
65	128					87	174							
65	129					88	175							
66	130					88	176							
66	131					89	177							
67	132					89	178							
67	133					90	179							
68	134					90	180							
68	135					91	181							

Table 5.2 (Continued)  
 DATE 3 July 1956  
 TIME 1500-1510 CST  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 2

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
1	1	37.4	0.030			46								0.210
2	2					24	47	146	23.9	3.80	0.355			0.165
2	3	38.5				25	48	124	25.5	4.61	0.350	0.160		0.200
3	4					26	49	124	25.4	4.71	0.400	0.100		0.165
3	5	23.8	2.10			26	51	124	25.4	4.71	0.400	0.100		0.165
4	6					27	52	135	29.7	4.77	0.450	0.055		0.105
4	7	30.4	3.20			27	53	135	29.7	4.77	0.450	0.055		0.105
5	8					28	54	148	31.2	3.43	1.13			0.120
5	9	38.6	2.00			28	55	148	31.2	3.43	1.13			0.120
6	10					29	56	163	36.9	3.90	1.14			0.130
6	11	58.4	1.77			29	57	163	36.9	3.90	1.14			0.130
7	12					30	58	144	45.9	4.56	1.06			0.060
7	13	73.3	1.88	0.220		30	59	144	45.9	4.56	1.06			0.060
8	14					31	60	147	36.3	9.87	0.710			0.085
8	15	67.6	2.87	1.04	0.085	31	61	147	36.3	9.87	0.710			0.085
9	16					32	62	174	42.3	6.29	0.400			0.120
9	17	56.4	8.93	1.24	0.205	32	63	174	42.3	6.29	0.400			0.120
10	18					33	64	153	47.9	4.28	0.870			0.115
10	19	83.9	13.8	1.63	0.160	33	65	153	47.9	4.28	0.870			0.115
11	20					34	66	163	44.7	2.85	0.050			0.050
11	21	81.5	17.1	2.18	0.320	34	67	163	44.7	2.85	0.050			0.050
12	22					35	68	135	44.3	2.52	0.040			0.040
12	23	66.8	12.6	2.32	0.285	35	69	135	44.3	2.52	0.040			0.040
13	24					36	70	128	14.9	1.42	0.095			0.095
13	25	66.9	13.5	4.21	0.125	36	71	128	14.9	1.42	0.095			0.095
14	26					37	72	100	7.38	0.400				0.130
14	27	95.0	10.6	3.28	0.100	37	73	100	7.38	0.400				0.130
15	28					38	74	74.0	0.265	0.050				0.115
15	29	118	11.3	1.67	0.105	38	75	74.0	0.265	0.050				0.115
16	30					39	76	34.4	0.450	0.085				0.085
16	31	132	12.6	1.12	0.075	39	77	34.4	0.450	0.085				0.085
17	32					40	78		6.61	0.180				0.180
17	33	129	21.8	2.19	0.065	40	79		6.61	0.180				0.180
18	34					41	80		2.59	0.075				0.075
18	35	141	28.5	3.73	0.140	41	81		2.59	0.075				0.075
19	36					42	82		0.805	0.050				0.050
19	37	190	38.3	3.70	0.210	42	83		0.805	0.050				0.050
20	38					43	84							0.050
20	39	175	35.6	4.05	0.250	43	85							0.050
21	40					44	86							0.195
21	41	154	35.9	4.17	0.195	44	87							0.195
22	42					45	88							0.275
22	43	192	26.9	4.33	0.270	45	89							0.275
23	44					46	90							0.200
23	45	175	27.3	3.67	0.430	46	91							0.200

DATE 5 July 1956  
TIME 2200-2210 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 3

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
1	1					46								
2	2					24	47							
3	3					48								
4	4					25	49							
5	5					50								
6	6					26	51							
7	7					52								
8	8					27	53							
9	9					28	55							
10	10					56								
11	11					29	57							
12	12					58								
13	13					30	59							
14	14					60								
15	15					61								
16	16					31	61							
17	17					62								
18	18					32	63							
19	19					64								
20	20					33	65							0.060
21	21					66								0.260
22	22					34	67							0.275
23	23					68								0.245
24	24					35	69							0.235
25	25					70								0.215
26	26					36	71							0.205
27	27					72								0.250
28	28					37	73							0.200
29	29					74								0.190
30	30					38	75	0.175						0.195
31	31					76								0.205
32	32					39	77	0.435	0.035	0.025				0.215
33	33					78								0.200
34	34					40	79	0.640	0.030	0.025				0.215
35	35					80								0.215
36	36					41	81	1.43	0.035	0.025	0.030			0.210
37	37					82								0.235
38	38					42	83	2.16	0.035	0.025	0.030			0.220
39	39					84								0.195
40	40					43	85	3.68	0.065	0.015	0.035			0.195
41	41					86								0.205
42	42					44	87	5.84	0.375	0.005	0.025			0.190
43	43					88								0.200
44	44					45	89	7.61	1.28	0.005	0.025			0.200
45	45					90								0.215

DATE 5 July 1956  
TIME 2200-2210 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 3

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
46	91	9.69	2.79	0.015		0.235	136							0.630
47	93	11.6	4.25	0.110	0.010	0.220	69	137	30.9	43.5	19.8	5.84		0.560
48	94					0.205	138							0.580
49	95	12.1	6.48	0.320	0.020	0.245	70	139	29.1	44.3	25.0	6.78		0.470
50	96					0.260	71	141	33.2	47.6	28.6	8.77		0.255
51	97	15.2	5.85	1.03	0.010	0.235	72	142						0.140
52	98					0.245	72	143	32.3	50.9	30.0	12.1		0.025
53	99	19.5	11.7	2.25	0.020	0.200	73	144						
54	100					0.220	73	145	27.8	57.3	37.6	14.1		
55	101	22.1	13.5	3.87	0.020	0.185	74	146						
56	102					0.155	74	147	21.9	45.6	41.0	16.3		
57	103	22.1	14.6	4.97	0.020	0.125	75	148						
58	104					0.120	75	149	24.6	56.6	53.1	16.6		
59	105	22.7	16.7	6.55	0.035	0.125	76	150						
60	106					0.140	76	151	19.1	50.0	61.5	14.7		
61	107	25.1	17.6	8.49	0.055	0.120	77	152	18.8	54.6	67.2	15.4		
62	108					0.125	77	153						
63	109	24.6	19.2	10.6	0.120	0.105	78	154						
64	110					0.075	78	155	19.1	58.7	65.7	16.7		
65	111	27.0	21.5	11.0	0.170	0.115	79	156						
66	112					0.075	79	157	14.3	58.7	71.7	15.1		
67	113	27.9	23.9	10.4	0.275	0.110	80	158						
68	114					0.115	80	159	17.1	42.5	56.4	14.0		
69	115	28.4	23.7	11.6	0.385	0.105	81	160						
70	116					0.100	81	161	17.4	43.1	51.2	14.4		
71	117	34.1	24.8	11.1	0.690	0.085	82	162						
72	118					0.105	82	163	15.3	54.5	63.4	16.9		
73	119	41.6	23.4	12.3	0.860	0.085	83	164						
74	120					0.040	83	166	9.98	70.8	63.4	17.6		
75	121	38.4	24.3	12.2	1.15	0.065	84	167						
76	122					0.090	84	167	8.34	99.0	60.9	18.4		
77	123	42.5	23.9	13.6	1.57	0.105	85	168						
78	124					0.145	85	169	14.4	103	55.1	0.250		
79	125	41.1	24.6	13.9	1.24	0.155	86	170						
80	126					0.200	86	171	24.2	140	65.5	10.1		
81	127	44.6	26.3	14.3	2.62	0.185	87	172						
82	128					0.290	87	173	32.6	207	68.7	0.830		
83	129	39.3	28.8	16.4	2.93	0.375	88	174						
84	130					0.330	88	175	32.4	246	80.0	0.010		
85	131	33.9	34.5	15.8	3.77	0.445	89	176						
86	132					0.485	89	177	28.1	226	76.9	0.010		
87	133	33.2	36.3	16.9	4.60	0.545	90	178						
88	134					0.645	90	179	29.7	201	58.7	0.010		
89	135	29.7	39.8	19.4	4.99	0.625	91	180						
90	136						91	181	13.7	181	18.1	0.005		

DATE 6 July 1956  
TIME 0100-0110 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 4

POST NO.	ARC					POST NO.	ARC						
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m	800m
1	1	1.37	0.535	0.345	0.030	0.005	46					0.025	
2	3						24	47	1.93	1.27	1.27	3.57	0.020
3	4	1.53	0.470	0.335	0.075		48					0.035	
4	6						25	49	2.23	1.48	1.36	4.25	0.025
5	8	1.42	0.500	0.315	0.130	0.015	50					0.020	
6	10					0.020	26	51	2.48	1.63	1.45	4.56	0.010
7	12	1.23	0.525	0.310	0.190	0.005	52					0.025	
8	14					0.020	27	53	2.78	1.94	1.55	4.56	0.030
9	16	1.31	0.530	0.350	0.235	0.015	54					0.045	
10	18					0.020	28	55	3.09	1.88	1.65	5.09	0.050
11	20	1.42	0.575	0.350	0.375	0.005	56					0.050	
12	22						29	57	3.71	2.04	1.80	5.24	0.035
13	24	1.51	0.545	0.420	0.450	0.010	58					0.030	
14	26						30	59	4.53	2.42	2.03	5.41	0.030
15	28	1.66	0.580	0.440	0.585		60					0.020	
16	30						31	61	5.13	2.49	2.13	5.83	0.035
17	32	1.59	0.625	0.490	0.665		62					0.040	
18	34						32	63	5.78	3.03	2.24	6.08	0.045
19	36	1.43	0.645	0.510	0.795		64					0.060	
20	38						33	65	6.88	3.17	2.32	6.21	0.020
21	40	1.66	0.705	0.550	0.960	0.005	66					0.050	
22	42					0.020	34	67	7.89	3.62	2.49	6.54	0.040
23	44	1.54	0.785	0.615	1.06		68					0.050	
24	46						35	69	9.09	3.63	2.57	6.48	0.035
25	48	1.64	0.815	0.655	1.28	0.035	70					0.050	
26	50					0.010	36	71	10.3	4.17	2.55	6.87	0.060
27	52	1.47	0.860	0.700	1.33	0.065	72					0.065	
28	54					0.090	37	73	12.6	5.26	2.57	7.36	0.075
29	56	1.83	0.910	0.700	1.53	0.010	74					0.075	
30	58					0.030	38	75	14.1	6.75	2.55	7.38	0.090
31	60	1.89	0.910	0.750	1.75	0.110	76					0.085	
32	62					0.010	39	77	14.6	6.38	2.49	8.01	0.055
33	64	1.69	1.26	0.815	1.98	0.140	78					0.080	
34	66					0.085	40	79	12.9	6.41	2.58	8.94	0.060
35	68	1.78	1.19	0.855	2.18	0.010	80					0.060	
36	70						41	81	12.2	6.09	2.69	9.43	0.080
37	72	1.77	1.19	0.950	2.23		82					0.040	
38	74						42	83	10.8	5.29	2.91	9.96	0.025
39	76	1.82	1.15	1.04	2.33	0.005	84					0.055	
40	78						43	85	9.54	5.01	2.96	11.2	0.095
41	80	1.93	1.27	1.12	2.60	0.010	86					0.055	
42	82						44	87	9.09	4.42	3.17	12.7	0.050
43	84	1.93	1.38	1.11	2.83	0.005	88					0.105	
44	86						45	89	9.09	3.38	3.15	15.1	0.090
45	88	2.10	1.32	1.26	3.07	0.060	90					0.100	

DATE 6 July 1956  
TIME 0100-0110 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 4

POST NO.	ARC					POST NO.	ARC						
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m	800m
46	91	8.81	3.81	3.39	17.3	0.120	136					10.7	
47	92					0.115	69	137	84.8	194	115	47.8	8.37
48	93	10.5	3.66	3.47	20.5	0.140	138					5.11	
49	94					0.135	70	139	78.0	218	152	66.7	1.53
50	95	14.3	3.71	3.61	24.1	0.135	140					0.220	
51	96					0.080	71	141	69.6	174	151	8.48	
52	97	27.0	4.80	3.95	24.5	0.085	142						
53	98					0.065	72	143	62.8	140	65.5	0.135	
54	99	54.5	7.93	4.84	23.3	0.110	144						
55	100					0.110	73	145	58.1	87.8	2.02		
56	101	98.8	10.7	7.34	23.3	0.140	146						
57	102					0.120	74	147	53.1	42.6	0.050		
58	103	135	14.8	13.7	24.2	0.095	148						
59	104					0.085	75	149	32.2	4.58			
60	105	153	36.5	25.8	27.4	0.105	150						
61	106					0.135	76	151	9.90	0.170			
62	107	169	91.1	35.4	30.9	0.125	152						
63	108					0.160	77	153	0.535	0.045			
64	109	186	161	70.6	29.8	0.245	154						
65	110					0.285	78	155	0.275				
66	111	177	199	104	26.6	0.285	156						
67	112					0.300	79	157	0.065				
68	113	196	221	133	26.7	0.355	158						
69	114					0.465	80	159	0.040				
70	115	208	216	105	24.8	0.460	160						
71	116					0.585	81	161					
72	117	238	213	80.2	22.3	0.670	162						
73	118					0.715	82	163					
74	119	267	202	66.7	17.7	0.935	164						
75	120					1.22	83	165					
76	121	261	212	55.1	15.6	1.66	166						
77	122					2.22	84	167					
78	123	268	210	48.3	14.8	2.91	168						
79	124					3.61	85	169					
80	125	235	186	50.2	14.9	4.33	170						
81	126					5.61	86	171					
82	127	221	177	49.2	13.8	6.61	172						
83	128					6.37	87	173					
84	129	196	182	59.6	15.9	6.84	174						
85	130					8.18	88	175					
86	131	159	159	68.2	17.1	9.01	176						
87	132					10.1	89	177					
88	133	135	161	73.6	20.1	10.6	90	178					
89	134					11.2	91	179					
90	135	107	163	77.3	27.7	11.4	180						
91	181						181						

DATE 6 July 1956  
 TIME 1400-1410' CST

Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 5

POST NO.	ARC					POST NO.	ARC					
	Inner Arce 800m arc	50m	100m	200m	400m		800m	Inner Arce 800m arc	50m	100m	200m	400m
1	1					46						
2	2					24	47					
3	3					48						
4	4					25	49	0.315				
5	5					50						
6	6					26	51	2.69				
7	7					52						
8	8					27	53	8.84				
9	9					54						
10	10					28	55	13.1	0.360			
11	11					56						
12	12					29	57	10.9	2.82			
13	13					30	58					
14	14					30	59	10.8	4.71			
15	15					60						
16	16					31	61	13.7	3.17	0.085		
17	17					62						
18	18					32	63	17.9	2.28	0.675		
19	19					64						
20	20					33	65	18.6	2.87	1.42	0.040	
21	21					66						
22	22					34	67	17.3	5.00	1.17	0.080	
23	23					68						
24	24					35	69	15.3	5.97	1.28	0.395	
25	25					70						
26	26					36	71	18.3	6.45	1.66	0.520	
27	27					72						
28	28					37	73	32.7	9.42	2.35	0.710	0.045
29	29					74						
30	30					38	75	55.7	13.4	4.39	0.650	0.110
31	31					76						
32	32					39	77	71.9	21.9	5.97	1.18	0.155
33	33					78						
34	34					40	79	91.5	27.2	9.19	1.75	0.200
35	35					80						
36	36					41	81	115	36.3	10.0	1.81	0.320
37	37					82						
38	38					42	83	150	45.3	10.0	1.60	0.205
39	39					84						
40	40					43	85	197	48.2	9.69	1.75	0.295
41	41					86						
42	42					44	87	203	53.3	11.1	1.97	0.420
43	43					88						
44	44					45	89	174	55.7	14.8	2.82	0.480
45	45					90						0.390

DATE 6 July 1956  
 TIME 1400-1410' CST

Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 5

POST NO.	ARC					POST NO.	ARC						
	Inner Arce 800m arc	50m	100m	200m	400m		800m	Inner Arce 800m arc	50m	100m	200m	400m	800m
46	91	159	47.0	11.8	2.28	0.370						136	
	92					0.440						69	137
47	93	156	44.4	10.4	1.75	0.320						138	
	94					0.285						70	139
48	95	159	40.1	8.87	1.26	0.260						140	
	96					0.280						71	141
49	97	137	28.5	5.30	1.18	0.240						142	
	98					0.155						72	143
50	99	103	19.1	5.04	1.00	0.105						144	
	100					0.075						73	145
51	101	67.4	11.8	2.50	0.365	0.035						146	
	102											74	147
52	103	39.9	5.09	0.950	0.040							148	
	104											75	149
53	105	16.4	1.56	0.335								150	
	106											76	151
54	107	8.01	0.415	0.040								152	
	108											77	153
55	109	2.87	0.050									154	
	110											78	155
56	111	1.23	0.040									156	
	112											79	157
57	113	0.570	0.055									158	
	114											80	159
58	115	0.075										160	
	116											81	161
59	117											162	
	118											82	163
60	119											164	
	120											83	165
61	121											166	
	122											84	167
62	123											168	
	124											85	169
63	125											170	
	126											86	171
64	127											172	
	128											87	173
65	129											174	
	130											88	175
66	131											176	
	132											89	177
67	133											178	
	134											90	179
68	135											180	
												91	181

DATE 6 July 1956  
TIME 1700-1710 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 6

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
2	2					24	47					
3	3					48						
4	4					25	49					
5	5					50						
6	6					51						
7	7					52						
8	8					27	53					
9	9					54						
10	10					28	55					
11	11					56						
12	12					29	57					
13	13					58						
14	14					30	59					
15	15					60						
16	16					31	61					
17	17					62						
18	18					32	63					
19	19					64						
20	20					33	65	0.040				
21	21					66						
22	22					34	67	0.455				
23	23					68						
24	24					35	69	1.85	0.060			
25	25					70						
26	26					36	71	5.37	0.605			
27	27					72						
28	28					37	73	18.9	2.45	0.200		
29	29					74						
30	30					38	75	46.1	9.84	1.52	0.035	
31	31					76						
32	32					39	77	81.5	23.0	2.72	0.235	0.035
33	33					78						
34	34					40	79	118	34.4	6.42	0.690	0.095
35	35					80						
36	36					41	81	188	47.3	11.5	1.85	0.135
37	37					82						
38	38					42	83	240	82.9	14.6	3.25	0.440
39	39					84						
40	40					43	85	261	80.6	17.5	3.50	0.835
41	41					86						
42	42					44	87	251	80.3	24.2	4.00	0.765
43	43					88						
44	44					45	89	263	70.2	19.0	4.24	0.885
45	45					90						0.795

DATE 6 July 1956  
TIME 1700-1710 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 6

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	218	59.3	14.3	3.27	0.960	136					
47	92					1.03	69	137				
48	93	182	65.3	13.7	3.23	1.12	138					
49	94					0.820	70	139				
50	95	146	45.2	11.9	3.23	0.720	140					
51	96					0.520	71	141				
52	97	133	35.1	10.5	2.05	0.570	142					
53	98					0.460	72	143				
54	99	106	31.4	6.12	1.43	0.320	144					
55	100					0.255	73	145				
56	101	72.5	16.5	3.95	0.615	0.075	146					
57	102					0.020	74	147				
58	103	46.7	8.66	2.63	0.175	0.020	148					
59	104					0.155	75	149				
60	105	19.5	3.66	0.835	0.020		150					
61	106						76	151				
62	107	8.64	1.65	0.095			152					
63	108						77	153				
64	109	3.02	0.445				154					
65	110						78	155				
66	111	0.610	0.060				156					
67	112						79	157				
68	113	0.065					158					
69	114						80	159				
70	115						160					
71	116						81	161				
72	117						162					
73	118						82	163				
74	119						164					
75	120						83	165				
76	121						166					
77	122						84	167				
78	123						168					
79	124						85	169				
80	125						170					
81	126						86	171				
82	127						172					
83	128						87	173				
84	129						174					
85	130						88	175				
86	131						176					
87	132						89	177				
88	133						178					
89	134						90	179				
90	135						180					
							91	181				



DATE 10 July 1956  
TIME 1400-1410 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 7

POST NO.	ARC					POST NO.	ARC					
	Inner Axis 800m arc	50m	100m	200m	400m		800m	Inner Axis 800m arc	50m	100m	200m	400m
1	1					46						
2	2					24	47	35.4	5.18			
3	3					48						
4	4					25	49	35.1	8.25	0.005		
5	5					50						
6	6					26	51	48.6	7.88	0.020		
7	7					52						
8	8					27	53	55.1	9.88	0.395		
9	9					54						
10	10					28	55	62.1	11.6	1.28		
11	11					56						
12	12					29	57	73.1	13.8	3.60		
13	13					58						
14	14					30	59	70.1	11.1	2.35		
15	15					60						
16	16					31	61	55.1	10.1	1.74		
17	17					62						
18	18					32	63	54.3	8.42	2.11		
19	19					64						
20	20					33	65	46.1	6.83	3.18		
21	21					66						
22	22					34	67	54.0	7.26	2.14		
23	23					68						
24	24					35	69	43.1	5.60	1.21	0.035	
25	25					70						
26	26					36	71	38.4	5.12	0.975	0.035	
27	27					72						
28	28					37	73	29.0	5.69	0.645	0.140	
29	29					74						
30	30					38	75	29.3	8.46	0.435	0.100	
31	31	0.015				76						
32	32					39	77	39.6	7.88	0.465	0.165	
33	33	0.015				78						
34	34					40	79	49.1	11.3	0.905	0.400	
35	35	0.130				80						
36	36					41	81	85.7	18.6	2.86	0.210	
37	37	0.830	0.035			82						
38	38					42	83	63.5	18.8	4.21	0.270	0.035
39	39	1.76	0.035			84						
40	40					43	85	82.4	22.4	4.49	0.380	0.050
41	41	6.98	0.260			86						0.035
42	42					44	87	97.8	23.3	4.57	0.550	0.060
43	43	15.2	0.930			88						0.045
44	44					45	89	87.9	M	4.64	0.700	0.045
45	45	26.3	1.79	0.030		90						0.080

DATE 10 July 1956  
TIME 1400-1410 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 7

POST NO.	ARC					POST NO.	ARC					
	Inner Axis 800m arc	50m	100m	200m	400m		800m	Inner Axis 800m arc	50m	100m	200m	400m
46	91	79.4	19.4	3.23	0.760	0.065	69	136				
47	92				0.040	0.040	93	137	68.0	11.2	1.25	
48	93	67.4	17.4	4.41	0.680	0.035	94	138				
49	94				0.020	0.020	70	139	39.0	6.90	0.840	
50	95	54.3	15.5	3.47	0.390	0.025	95	140				
51	96				0.035	0.035	71	141	32.7	3.29	0.380	
52	97	46.4	11.7	2.28	0.305	0.045	96	142				
53	98				0.025	0.025	72	143	28.4	3.45		
54	99	40.7	10.2	1.89	0.360	0.035	97	144				
55	100				0.040	0.040	73	145	21.6	5.96	0.110	
56	101	53.9	11.3	1.78	0.430	0.040	98	146				
57	102				0.040	0.040	74	147	24.6	3.24		
58	103	56.7	11.8	1.81	0.480	0.010	99	148				
59	104				0.025	0.025	75	149	18.5	0.755		
60	105	58.2	11.7	1.65	0.380	0.035	100	150				
61	106				0.035	0.035	76	151	12.0	0.175		
62	107	41.6	8.82	1.92	0.265	0.030	101	152				
63	108				0.060	0.060	77	153	17.3			
64	109	30.5	6.77	1.67	0.385	0.050	102	154				
65	110				0.045	0.045	78	155	14.9			
66	111	33.5	5.69	1.85	0.450	0.065	103	156				
67	112				0.040	0.040	79	157	7.98			
68	113	32.9	5.91	1.53	0.285	0.070	104	158				
69	114				0.025	0.025	80	159	1.20			
70	115	39.6	5.73	1.55	0.220	0.045	105	160				
71	116				0.065	0.065	81	161	0.115			
72	117	51.2	7.79	1.23	0.170	0.040	106	162				
73	118				0.045	0.045	82	163	0.085			
74	119	61.1	9.71	1.39	0.175	0.045	107	164				
75	120				0.020	0.020	83	165	0.040			
76	121	57.0	13.5	2.51	0.140	0.010	108	166				
77	122				0.010	0.010	84	167	0.015			
78	123	47.9	14.4	5.14	0.125	0.030	109	168				
79	124				0.050	0.050	85	169	0.030			
80	125	54.3	16.1	3.69	0.070	0.025	110	170				
81	126				0.035	0.035	86	171	0.020			
82	127	53.4	17.0	3.42	0.375		111	172				
83	128						87	173	0.035			
84	129	65.1	19.5	4.18	0.490		88	174				
85	130						89	175	0.045			
86	131	70.4	19.4	2.89	0.135		90	176				
87	132						89	177	0.025			
88	133	65.6	21.2	2.44	0.060		90	178				
89	134						90	179				
90	135	73.8	14.4	1.66			91	180	0.020			
								181				

DATE 10 July 1956  
TIME 1700-1710 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.8

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
2	2					47						
3	3					48						
4	4					49						
5	5					50						
6	6					51						
7	7					52						
8	8					53						
9	9					54						
10	10					55						
11	11					56						
12	12					57						
13	13					58						
14	14					59						
15	15					60						
16	16					61						
17	17					62						
18	18					63	0.025					
19	19					64						
20	20					65	0.030					
21	21					66						
22	22					67	0.030					
23	23					68						
24	24					69	0.010					
25	25					70						
26	26					71	0.025					
27	27					72						
28	28					73	0.170					
29	29					74						
30	30					75	5.34	0.025				
31	31					76						
32	32					77	14.6	0.130	0.035			
33	33					78						
34	34					79	18.2	1.79	0.100			
35	35					80						
36	36					81	20.7	4.71	0.580			
37	37					82						
38	38					83	27.0	6.23	1.46	0.205		
39	39					84						0.045
40	40					85	54.9	11.5	2.75	0.440	0.060	
41	41					86						0.060
42	42					87	101	23.6	3.03	0.610	0.130	
43	43					88						0.130
44	44					89	186	51.2	6.49	1.10	0.205	
45	45					90						0.290

DATE 10 July 1956  
TIME 1700-1710 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.8

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	260	73.1	11.8	2.34	0.355	136					
47	92					0.445	69	137	0.035			
48	93	341	89.9	23.6	3.74	0.585	138					
49	94					0.525	70	139				
50	95	422	115	25.7	3.79	0.535	140					
51	96					0.675	71	141				
52	97	381	111	26.4	3.97	0.695	142					
53	98					0.695	72	143				
54	99	326	92.1	23.9	4.25	0.495	144					
55	100					0.545	73	145				
56	101	267	68.3	17.7	3.35	0.635	146					
57	102					0.725	74	147				
58	103	204	50.6	13.1	2.71	0.605	148					
59	104					0.495	75	149				
60	105	140	41.1	10.5	1.80	0.545	150					
61	106					0.425	76	151				
62	107	91.1	24.0	5.04	1.15	0.300	152					
63	108					0.300	77	153				
64	109	62.7	9.33	2.97	1.15	0.220	154					
65	110					0.165	78	155				
66	111	61.2	8.55	2.46	0.530	0.160	156					
67	112					0.055	79	157				
68	113	36.3	6.87	2.49	0.200	0.045	158					
69	114					0.030	80	159				
70	115	23.0	7.26	1.31	0.070	0.020	160					
71	116						81	161				
72	117	14.0	3.45	0.330			162					
73	118						82	163				
74	119	10.9	1.86	0.180			164					
75	120						83	165				
76	121	10.4	0.735				166					
77	122						84	167				
78	123	10.1	1.08				168					
79	124						85	169				
80	125	6.46	0.975				170					
81	126						86	171				
82	127	5.42	0.975				172					
83	128						87	173				
84	129	2.06	1.01				174					
85	130						88	175				
86	131	1.29	0.135				176					
87	132						89	177				
88	133	0.440	0.070				90	178				
89	134						179					
90	135	0.235					180					
							91	181				

DATE 11 July 1956  
TIME 1000-1010 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.9

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						
2	2						24	47					
3	3						48						
4	4						25	49					
5	5						50						
6	6						26	51					
7	7						52						
8	8						27	53					
9	9						54						
10	10						28	55					
11	11						56						
12	12						29	57					
13	13						58						
14	14						30	59					
15	15						60						
16	16						31	61					
17	17						62						
18	18						32	63					
19	19						64						
20	20						33	65					
21	21						66						
22	22						34	67					
23	23						68						
24	24						35	69					
25	25						70						
26	26						36	71					
27	27						72						
28	28						37	73					
29	29						74						
30	30						38	75					
31	31						76						
32	32						39	77					
33	33						78						
34	34						40	79					
35	35						80						
36	36						41	81					
37	37						82						
38	38						42	83	0.025				
39	39						84						
40	40						43	85	0.250				
41	41						86						
42	42						44	87	1.50				
43	43						88						
44	44						45	89	5.66	0.290			
45	45						90						

DATE 11 July 1956  
TIME 1000-1010 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.9

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91	20.4	2.30				136						0.035
47	92						69	137	19.8	6.78	1.16	0.258	0.045
48	93	39.8	5.79				138						0.020
49	94						70	139	12.8	4.28	0.515	0.125	0.015
50	95	44.9	9.18	0.120			140						
51	96						71	141	11.3	1.48	0.200	0.115	
52	97	56.1	17.3	1.68			142						
53	98						72	143	5.39	0.590	0.165	0.015	
54	99	67.2	26.9	4.67	0.175		144						
55	100					0.035	73	145	2.21	0.090	0.040	0.010	
56	101	33.5	28.2	8.93	1.00	0.055	146						
57	102					0.135	74	147	1.00	0.020			
58	103	115	32.9	9.83	2.48	0.255	148						
59	104					0.415	75	149	0.150				
60	105	148	42.6	12.5	2.90	0.520	150						
61	106					0.480	76	151					
62	107	183	56.1	14.2	2.14	0.440	152						
63	108					0.470	77	153					
64	109	200	55.7	11.3	2.26	0.470	154						
65	110					0.450	78	155					
66	111	198	45.9	10.9	2.29	0.405	156						
67	112					0.375	79	157					
68	113	171	44.4	12.2	2.53	0.450	158						
69	114					0.470	80	159					
70	115	159	48.5	12.6	2.68	0.510	160						
71	116					0.340	81	161					
72	117	130	41.3	10.6	2.63	0.245	162						
73	118					0.315	82	163					
74	119	123	38.7	9.73	1.85	0.380	164						
75	120					0.385	83	165					
76	121	114	34.5	8.46	2.12	0.395	166						
77	122					0.450	84	167					
78	123	102	26.0	6.50	1.57	0.405	168						
79	124					0.295	85	169					
80	125	72.9	17.6	4.78	0.925	0.200	170						
81	126					0.150	86	171					
82	127	48.6	11.5	3.31	0.825	0.115	172						
83	128					0.090	87	173					
84	129	41.0	8.63	2.97	0.595	0.095	174						
85	130					0.130	88	175					
86	131	32.9	7.04	2.29	0.655	0.155	176						
87	132					0.145	89	177					
88	133	26.9	8.31	2.48	0.875	0.095	178						
89	134					0.060	90	179					
90	135	25.2	8.90	2.75	0.535	0.050	180						
91	181						91	181					

DATE 11 JULY 1956  
TIME 1200-1210 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 10

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
46	91					69	136							0.055
47	92					70	137	170	41.1	6.21	1.22			0.065
48	93					71	138							0.095
49	94					72	139	158	29.7	6.88	0.860			0.125
50	95	0.175				73	140							0.115
51	96					74	141	137	24.3	7.76	0.690			0.090
52	97	0.590				75	142							0.100
53	98					76	143	117	24.3	7.74	0.700			0.070
54	99	3.69				77	144							0.130
55	100					78	145	117	24.2	5.34	0.780			0.135
56	101	8.78				79	146							
57	102					80	147	102	24.3	2.96	0.630			
58	103	15.5				81	148							
59	104					82	149	97.5	27.6	3.32	0.600			
60	105	25.5				83	150							
61	106					84	151	110	28.2	4.05	0.120			
62	107	36.3	0.070			85	152							
63	108					86	153	88.2	21.2	2.06	0.120			
64	109	39.0	0.890			87	154							
65	110					88	155	80.7	11.4	1.19	0.190			
66	111	47.6	1.86			89	156							
67	112					90	157	57.8	10.6	0.785	0.325			
68	113	38.1	4.20	0.195		91	158							
69	114					92	159	45.2	8.61	1.02	0.150			
70	115	38.7	8.73	0.485	0.110	93	160							
71	116					94	161	31.2	6.84	1.82	0.035			
72	117	32.3	9.17	0.605	0.150	95	162							
73	118					96	163	25.8	3.80	1.74				
74	119	38.7	10.3	0.825	0.095	97	164							
75	120				0.040	98	165	20.3	1.88	0.775				
76	121	52.5	8.72	1.51	0.250	99	166							
77	122				0.050	100	167	17.7	1.36	0.030				
78	123	61.7	12.2	2.25	0.540	101	168							
79	124				0.070	102	169	12.8	1.16					
80	125	90.0	17.7	4.28	0.590	103	170							
81	126				0.055	104	171	6.30	0.935					
82	127	124	30.0	8.95	0.560	105	172							
83	128				0.050	106	173	3.68	0.490					
84	129	161	37.4	11.4	0.820	107	174							
85	130				0.090	108	175	1.50	0.055					
86	131	179	39.2	8.18	2.70	109	176							
87	132				0.175	110	177	89	177	0.335				
88	133	165	39.9	10.4	1.98	111	178							
89	134				0.155	112	179							
90	135	164	43.1	10.1	1.28	113	180							
91	136				0.125	114	181							

DATE 14 July 1956  
TIME 0800-0810 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 11

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
1	1					24	46							
2	2					25	47							
3	3					26	48							
4	4					27	49							
5	5					28	50							
6	6					29	51							
7	7					30	52							
8	8					31	53							
9	9					32	54							
10	10					33	55							
11	11					34	56							
12	12					35	57							
13	13					36	58							
14	14					37	59							
15	15					38	60							
16	16					39	61							
17	17					40	62							
18	18					41	63							
19	19					42	64							
20	20					43	65							
21	21					44	66							
22	22					45	67							
23	23					46	68							
24	24					47	69							
25	25					48	70							
26	26					49	71							
27	27					50	72							
28	28					51	73							
29	29					52	74							
30	30					53	75							
31	31					54	76							
32	32					55	77							
33	33					56	78							
34	34					57	79							
35	35					58	80							
36	36					59	81							
37	37					60	82							
38	38					61	83							
39	39					62	84							
40	40					63	85							
41	41					64	86							
42	42					65	87							
43	43					66	88							
44	44					67	89							
45	45					68	90							
46	46					69	91							
47	47					70	92							
48	48					71	93							
49	49					72	94							
50	50					73	95							
51	51					74	96							
52	52					75	97							
53	53					76	98							
54	54					77	99							
55	55					78	100							
56	56					79	101							
57	57					80	102							
58	58					81	103							
59	59					82	104							
60	60					83	105							
61	61					84	106							
62	62					85	107							
63	63					86	108							
64	64					87	109							
65	65					88	110							
66	66					89	111							
67	67					90	112							
68	68					91	113							
69	69					92	114							
70	70					93	115							
71	71					94	116							
72	72					95	117							
73	73					96	118							
74	74					97	119							
75	75					98	120							
76	76					99	121							
77	77					100	122							
78	78					101	123							
79	79					102	124							
80	80					103	125							
81	81					104	126							
82	82					105	127							
83	83					106	128							
84	84					107	129							
85	85					108	130							
86	86					109	131							
87	87					110	132							
88	88					111	133							
89	89					112	134							
90	90					113	135							
91	91					114</								

DATE 14 July 1956  
TIME 0800-0810 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.11

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46 91	209	72.3	20.5	3.64	0.480	136						
92					0.950	69	137					
47 93	263	87.0	28.9	6.67	1.27	138						
94					1.67	70	139					
48 95	273	89.3	29.5	7.61	1.68	140						
96					1.72	71	141					
49 97	269	83.0	27.7	7.10	1.42	142						
98					1.02	72	143					
50 99	251	75.3	23.0	4.57	0.920	144						
100					0.590	73	145					
51 101	204	56.6	11.6	2.46	0.383	146						
102					0.225	74	147					
52 103	124	32.0	5.86	0.775	0.170	148						
104					0.085	75	149					
53 105	68.3	13.8	1.54	0.245	0.015	150						
106					0.020	76	151					
54 107	35.4	4.59	0.475	0.030		152						
108						77	153					
55 109	19.4	0.600	0.030	0.020		154						
110						78	155					
56 111	5.87	0.070	0.020			156						
112						79	157					
57 113	0.990	0.025				158						
114						80	159					
58 115	0.080					160						
116						81	161					
59 117	0.045					162						
118						82	163					
60 119						164						
120						83	165					
61 121						166						
122						84	167					
62 123						168						
124						85	169					
63 125						170						
126						86	171					
64 127						172						
128						87	173					
65 129						174						
130						88	175					
66 131						176						
132						89	177					
67 133						178						
134						90	179					
68 135						180						
						91	181					

DATE 14 July 1956  
TIME 1000-1010 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.12

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1 1						46						
2 2						24	47					
3 3						48						
4 4						25	49					
5 5						50						
6 6						26	51					
7 7						52						
8 8						27	53					
9 9						54						
10 10						28	55					
11 11						56						
12 12						29	57					
13 13						58						
14 14						30	59					
15 15						60						
16 16						31	61					
17 17						62						
18 18						32	63					
19 19						64						
20 20						33	65					
21 21						66						
22 22						34	67					
23 23						68						
24 24						35	69					
25 25						70						
26 26						36	71					
27 27						72						
28 28						37	73					
29 29						74						
30 30						38	75					
31 31						76						
32 32						39	77	0.115				
33 33						78						
34 34						40	79	1.39				
35 35						80						
36 36						41	81	4.95	0.105			
37 37						82						
38 38						42	83	5.28	1.50			
39 39						84						
40 40						43	85	10.3	3.23			
41 41						86						
42 42						44	87	20.1	5.00	0.095		
43 43						88						
44 44						45	89	39.8	8.40	1.75	0.030	
45 45						90						

DATE 14 July 1956  
TIME 1000-1010 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.12

POST NO.	ARC					POST NO.	ARC								
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91		67.7	18.9	3.76	0.320									136
	92					0.040	69								137
47	93		84.0	25.7	6.96	1.49	0.115								138
	94					0.380	70								139
48	95		92.7	24.5	7.67	1.78	0.470								140
	96					0.480	71								141
49	97		86.7	26.3	7.02	1.67	0.450								142
	98					0.440	72								143
50	99		109	36.0	9.17	2.13	0.510								144
	100					0.630	73								145
51	101		130	47.0	16.0	3.55	0.770								146
	102					0.970	74								147
52	103		173	57.2	18.2	5.03	1.22								148
	104					1.46	75								149
53	105		216	61.5	20.6	5.46	1.49								150
	106					1.58	76								151
54	107		218	58.7	19.1	4.97	1.54								152
	108					1.34	77								153
55	109		186	60.0	19.6	4.18	1.04								154
	110					0.580	78								155
56	111		168	53.9	17.2	3.44	0.310								156
	112					0.130	79								157
57	113		129	44.6	10.7	2.08	0.075								158
	114					0.060	80								159
58	115		107	31.4	5.25	0.340									160
	116						81								161
59	117		78.2	13.6	2.83										162
	118						82								163
60	119		48.8	5.03	0.735										164
	120						83								165
61	121		27.2	2.70	0.040										166
	122						84								167
62	123		12.1	0.590											168
	124						85								169
63	125		12.7	0.085											170
	126						86								171
64	127		0.235												172
	128						87								173
65	129		0.330												174
	130						88								175
66	131														176
	132						89								177
67	133														178
	134						90								179
68	135														180
							91								181

DATE 22 July 1956  
TIME 2000-2010 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.13

POST NO.	ARC					POST NO.	ARC								
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1														46
	2					24									47
2	3														48
	4					25									49
3	5														50
	6					26									51
4	7														52
	8					27									53
5	9														54
	10					28									55
6	11														56
	12					29									57
7	13														58
	14					30									59
8	15														60
	16					31									61
9	17														62
	18					32									63
10	19														64
	20					33									65
11	21														66
	22					34									67
12	23														68
	24					35									69
13	25														70
	26					36									71
14	27														72
	28					37									73
15	29														74
	30					38									75
16	31														76
	32					39									77
17	33														78
	34					40									79
18	35														80
	36					41									81
19	37														82
	38					42									83
20	39														84
	40					43									85
21	41														86
	42					44									87
22	43														88
	44					45									89
23	45														90

DATE 22 July 1956  
TIME 2000 - 2010 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 13

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
46	91		103	246	30.2									
47	93		87.3	281	87.1									
48	95		114	419	287	7.25								
49	97		174	330	490	53.0	0.035							
50	99		174	227	253	113	7.93							
51	101		161	146	141	58.8	17.6							
52	103		141	104	118	51.5	17.7							
53	105		105	82.4	127	60.3	18.4							
54	107		83.3	76.4	130	77.0	32.7							
55	109		60.0	65.4	138	98.3	74.6							
56	111		40.4	49.1	122	131	104							
57	113		25.5	36.5	78.3	115	44.5							
58	115		16.5	24.9	35.0	30.3	0.030							
59	117		13.1	14.0	8.83	0.275								
60	119		10.8	5.39	1.33	0.020								
61	121		5.70	1.41	0.050									
62	123		2.87	0.175										
63	125		1.09											
64	127		0.295											
65	129		0.075											
66	131													
67	133													
68	135													

DATE 22 July 1956  
TIME 2200-2210 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 14

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
1	1													
2	2													
3	3													
4	4													
5	5													
6	6													
7	7													
8	8													
9	9													
10	10													
11	11													
12	12													
13	13													
14	14													
15	15													
16	16													
17	17													
18	18													
19	19													
20	20													
21	21													
22	22													
23	23													

DATE 22 July 1956  
TIME 2200-2210 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.14

POST NO.	ARC					POST NO.	ARC						
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m	800m
46	91	9.69	2.54	1.20	0.335	2.83	69	136					
	92					2.28	69	137					
47	93	4.28	2.07	1.13	3.47	2.64	70	138					
	94					2.90	70	139					
48	95	3.68	1.80	0.930	1.79	3.17	71	140					
	96					3.33	71	141					
49	97	3.51	2.00	0.830	1.18	3.43	72	142					
	98					3.49	72	143					
50	99	3.44	1.95	0.850	0.860	2.86	73	144					
	100					1.88	73	145					
51	101	3.41	1.86	0.900	0.620	1.76	74	146					
	102					1.38	74	147					
52	103	4.05	1.94	1.02	0.450	1.26	75	148					
	104					1.22	75	149					
53	105	3.90	2.07	1.23	0.460	0.775	76	150					
	106					0.480	76	151					
54	107	3.81	2.19	1.29	0.465	0.460	77	152					
	108					0.305	77	153					
55	109	3.51	2.03	1.10	0.385	0.185	78	154					
	110					0.150	78	155					
56	111	2.81	1.79	0.940	0.300	0.090	79	156					
	112					0.050	79	157					
57	113	2.12	1.62	0.760	0.240	0.025	80	158					
	114						80	159					
58	115	1.50	1.34	0.570	0.155		81	160					
	116						81	161					
59	117	1.06	0.985	0.415	0.090		82	162					
	118						82	163					
60	119	0.725	0.730	0.180			83	164					
	120						83	165					
61	121	0.450	0.330	0.030			84	166					
	122						84	167					
62	123	0.180	0.055				85	168					
	124						85	169					
63	125	0.070					86	170					
	126						86	171					
64	127						87	172					
	128						87	173					
65	129						88	174					
	130						88	175					
66	131						89	176					
	132						89	177					
67	133						90	178					
	134						90	179					
68	135						91	180					
							91	181					

DATE 23 July 1956  
TIME 0800-0810 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.15

POST NO.	ARC					POST NO.	ARC						
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m	800m
1	1					46							
	2					24							
2	3					48							
	4					25							
3	5					26							
	6					51							
4	7					52							
	8					27							
5	9					54							
	10					28							
6	11					56							
	12					29							
7	13					58							
	14					30							
8	15					60							
	16					31							
9	17					62							
	18					32							
10	19					64							
	20					33							
11	21					66							
	22					34							
12	23					68							
	24					35							
13	25					70							
	26					36							
14	27					72							
	28					37							
15	29					74				0.025			
	30					74							
16	31					38				1.25			
	32					76							
17	33					39				7.40			
	34					78							
18	35					40				9.69			
	36					80							
19	37					41				16.2		0.025	
	38					82							
20	39					42				28.2		0.190	
	40					84							
21	41					43				29.7		1.21	
	42					86							
22	43					44				31.1		4.38	
	44					88							
23	45					45				20.6		5.06	
						90							



DATE 23 July 1956  
TIME 0800-0810 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.15

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	19.7	13.5				136					
47	92						69	4.31	2.76	0.135		
48	93	29.1	6.12	0.165			137					
49	94						138					
50	95	41.1	4.11	0.435			70	0.860	0.200			
51	96						139					
52	97	70.1	7.17	0.740	0.035		140					
53	98						71	0.040				
54	99	99.6	15.6	0.950	0.030		141					
55	100						142					
56	101	146	21.6	2.26	0.110		72					
57	102						143					
58	103	197	38.6	3.89	0.335		73					
59	104						144					
60	105	245	53.3	5.74	0.500	0.065	74					
61	106					0.150	145					
62	107	291	75.9	8.52	0.930	0.205	75					
63	108					0.365	146					
64	109	336	75.9	14.5	1.23	0.410	76					
65	110					0.470	147					
66	111	414	80.4	21.1	2.44	0.460	77					
67	112					0.390	148					
68	113	414	107	21.7	3.91	0.360	78					
69	114					0.158	149					
70	115	408	100	20.6	4.78	0.535	79					
71	116					0.495	150					
72	117	353	88.2	21.6	3.76	0.450	80					
73	118					0.445	151					
74	119	249	76.5	19.6	2.25	0.415	81					
75	120					0.410	152					
76	121	222	61.5	15.0	2.32	0.310	82					
77	122					0.245	153					
78	123	201	48.0	12.3	2.09	0.175	83					
79	124					0.270	154					
80	125	125	38.4	9.61	0.530	0.245	84					
81	126					0.220	155					
82	127	111	30.6	7.59	0.520	0.270	85					
83	128					0.220	156					
84	129	86.1	19.7	6.90	0.780	0.255	86					
85	130					0.140	157					
86	131	46.2	17.1	4.94	1.11	0.045	87					
87	132						158					
88	133	34.4	11.9	4.11	0.415		88					
89	134						159					
90	135	16.5	4.95	0.870	0.070		160					
							161					

DATE 23 July 1956  
TIME 1000-1010 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.16

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1						46					
2	2						47					
3	3					24	48					
4	4					25	49					
5	5					26	50					
6	6					27	51					
7	7					28	52					
8	8					29	53					
9	9					30	54					
10	10					31	55					
11	11					32	56					
12	12					33	57					
13	13					34	58					
14	14					35	59					
15	15					36	60					
16	16					37	61					
17	17					38	62					
18	18					39	63					
19	19					40	64					
20	20					41	65	1.10				
21	21					42	66					
22	22					43	67	10.3				
23	23					44	68					
24	24					45	69	20.0	0.035			
25	25					46	70					
26	26					47	71	29.9	0.110			
27	27					48	72					
28	28					49	73	39.9	0.550			
29	29					50	74					
30	30					51	75	48.0	2.25			
31	31					52	76					
32	32					53	77	64.1	7.17	0.025		
33	33					54	78					
34	34					55	79	84.8	12.3	0.030		
35	35					56	80					
36	36					57	81	125	20.7	0.375		
37	37					58	82					
38	38					59	83	136	21.6	1.71		
39	39					60	84					
40	40					61	85	143	30.3	1.74		
41	41					62	86					
42	42					63	87	179	32.7	2.69		
43	43					64	88					
44	44					65	89	182	34.4	3.82	0.085	
45	45					66	90					

DATE 23 July 1956  
TIME 1000-1010 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.16

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	165	29.7	5.14	0.075	0.015	136					
92						0.030	69	137	3.08	0.140	0.015	
47	93	143	26.9	6.36	0.625	0.030		138				
94						0.040	70	139	1.33	0.035		
48	95	155	24.0	6.39	0.345	0.045		140				
96						0.045	71	141	0.055	0.025		
49	97	121	21.6	5.16	0.340	0.045		142				
98						0.035	72	143	0.025			
50	99	118	22.8	3.62	0.190	0.030		144				
100						0.015	73	145				
51	101	116	21.9	2.54	0.150	0.025		146				
102						0.015	74	147				
52	103	103	15.6	1.86	0.245	0.045		148				
104						0.050	75	149				
53	105	93.9	15.5	1.27	0.190	0.045		150				
106						0.030	76	151				
54	107	82.1	13.8	0.635	0.215	0.040		152				
108						0.040	77	153				
55	109	80.9	12.8	1.04	0.235	0.045		154				
110						0.080	78	155				
56	111	81.3	11.8	1.89	0.190	0.070		156				
112						0.075	79	157				
57	113	71.7	10.8	1.32	0.585	0.040		158				
114						0.055	80	159				
58	115	61.2	9.28	2.41	0.715	0.050		160				
116						0.065	81	161				
59	117	84.3	15.3	2.89	0.905	0.035		162				
118						0.075	82	163				
60	119	99.0	24.9	4.03	0.955	0.045		164				
120						0.030	83	165				
61	121	87.0	22.5	4.40	0.625			166				
122							84	167				
62	123	74.7	23.1	4.42	0.695			168				
124							85	169				
63	125	58.8	15.9	3.50	0.380			170				
126							86	171				
64	127	48.6	10.8	2.49	0.135			172				
128							87	173				
65	129	35.7	8.49	0.865				174				
130							88	175				
66	131	27.8	3.08	0.475				176				
132							89	177				
67	133	22.8	1.38	0.240				178				
134							90	179				
68	135	14.8	0.930	0.025				180				
							91	181				

DATE 23 July 1956  
TIME 2000-2010 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.17

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1											
2	2					24	46					
3	3					47						
4	4					48						
5	5					25	49					
6	6					50						
7	7					26	51					
8	8					52						
9	9					27	53					
10	10					54						
11	11					28	55					
12	12					56						
13	13					29	57					
14	14					58						
15	15					30	59					
16	16					60						
17	17					31	61					
18	18					62						
19	19					32	63					
20	20					64						
21	21					33	65					
22	22					66						
23	23					34	67					
24	24					68						
25	25					35	69					
26	26					70						
27	27					36	71					
28	28					72						
29	29					37	73	0.160				
30	30					74						
31	31					38	75	1.40	0.030			
32	32					76						
33	33					39	77	20.1	0.345			
34	34					78						
35	35					40	79	54.3	2.96	0.110	0.025	
36	36					80						
37	37					41	81	159	20.1	1.84	0.150	
38	38					82						0.085
39	39					42	83	302	76.2	13.4	2.03	0.435
40	40					84						1.86
41	41					43	85	518	177	46.8	13.1	4.34
42	42					86						8.09
43	43					44	87	633	269	83.2	26.9	9.74
44	44					88						9.04
45	45					45	89	645	254	86.2	25.7	6.28
						90						2.98

Table 5.2 (Continued)

DATE 23 July 1956  
TIME 2000 - 2010 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.17

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	561	164	46.0	8.63	0.755	69	136				
92						0.285	69	137				
47	93	330	90.6	14.4	1.11	0.035	70	138				
94							70	139				
48	95	195	33.2	2.70			71	141				
96							71	142				
49	97	106	8.93	0.245			72	143				
98							72	144				
50	99	29.4	1.00				73	145				
100							73	146				
51	101	8.72	0.090				74	147				
102							74	148				
52	103	1.19					75	149				
104							75	150				
53	105	0.235					76	151				
106							76	152				
54	107						77	153				
108							77	154				
55	109						78	155				
110							78	156				
56	111						79	157				
112							79	158				
57	113						80	159				
114							80	160				
58	115						81	161				
116							81	162				
59	117						82	163				
118							82	164				
60	119						83	165				
120							83	166				
61	121						84	167				
122							84	168				
62	123						85	169				
124							85	170				
63	125						86	171				
126							86	172				
64	127						87	173				
128							87	174				
65	129						88	175				
130							88	176				
66	131						89	177				
132							89	178				
67	133						90	179				
134							90	180				
68	135						91	181				

Table 5.2 (Continued)

DATE 23 July 1956  
TIME 2200-2210 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 18

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1						24	46				
2	2						24	47				
3	3						25	48				
4	4						25	49				
5	5						26	50				
6	6						26	51				
7	7						27	52				
8	8						27	53				
9	9						28	54				
10	10						28	55				
11	11						29	56				
12	12						29	57				
13	13						30	58				
14	14						30	59				
15	15						31	60				
16	16						31	61				
17	17						32	62				
18	18						32	63				
19	19						33	64				
20	20						33	65				
21	21						34	66				
22	22						34	67				
23	23						35	68				
24	24						35	69				
25	25						36	70				
26	26						36	71				
27	27						37	72				
28	28						37	73				
29	29						38	74				
30	30						38	75				
31	31						39	76				
32	32						39	77	0.095			
33	33						40	78				
34	34						40	79	0.645			
35	35						41	80				
36	36						41	81	5.57	0.095		
37	37						42	82				
38	38						42	83	29.6	1.59	0.025	
39	39						43	84				
40	40						43	85	106	17.1	0.730	
41	41						44	86				
42	42						44	87	218	69.6	14.3	0.640
43	43						45	88				
44	44						45	89	368	158	50.9	11.7
45	45						90	90				0.040
												0.665

DATE 23 July 1956  
TIME 2200 -2210 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.18

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
46	91	584	257	95.0	32.3	5.04	136							
92						11.6	69	137						
47	93	620	242	82.4	29.5	14.0	138							
94						11.3	139							
48	95	615	177	51.4	17.9	8.49	140							
96						8.34	71	141						
49	97	467	152	52.0	16.8	9.35	142							
98						6.86	72	143						
50	99	321	118	31.6	8.56	2.38	144							
100						0.435	73	145						
51	101	206	42.2	6.64	0.695	0.080	146							
102						0.075	74	147						
52	103	72.6	6.66	0.545	0.055	0.035	148							
104							75	149						
53	105	17.4	0.783	0.065			150							
106							76	151						
54	107	3.15	0.085				152							
108							77	153						
55	109	1.49					154							
110							78	155						
56	111	0.025					156							
112							79	157						
57	113						158							
114							80	159						
58	115						160							
116							81	161						
59	117						162							
118							82	163						
60	119						164							
120							83	165						
61	121						166							
122							84	167						
62	123						168							
124							85	169						
63	125						170							
126							86	171						
64	127						172							
128							87	173						
65	129						174							
130							88	175						
66	131						176							
132							89	177						
67	133						178							
134							90	179						
68	135						180							
							91	181						

DATE 25 July 1956  
TIME 1100-1110 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.19

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
1	1					46								
2	2					24	47	2.52						
3	3					48								
4	4					25	49	4.13						
5	5					50								
6	6					26	51	11.3	0.225					
7	7					52								
8	8					27	53	21.0	1.91	0.025				
9	9					54								
10	10					28	55	33.5	4.38	0.330				
11	11					56								
12	12					29	57	48.6	8.57	0.745				
13	13					58								
14	14					30	59	57.2	14.2	1.86	0.180			
15	15					60								
16	16					31	61	76.2	20.4	3.36	0.620			
17	17					62								
18	18					32	63	108	27.9	5.65	0.520			
19	19					64								0.045
20	20					33	65	144	39.2	8.21	0.735	0.080		
21	21					66								0.105
22	22					34	67	141	41.3	12.1	1.73	0.090		
23	23					68								0.125
24	24					35	69	164	41.3	10.5	2.30	0.135		
25	25					70								0.185
26	26					36	71	182	33.8	6.79	2.09	0.230		
27	27					72								0.365
28	28					37	73	213	47.0	4.72	0.980	0.210		
29	29					74								0.220
30	30					38	75	218	54.3	6.41	0.655	0.225		
31	31					76								0.190
32	32					39	77	210	51.0	6.60	1.08	0.185		
33	33					78								0.175
34	34					40	79	192	51.0	8.21	1.89	0.160		
35	35					80								0.245
36	36					41	81	198	47.9	11.3	1.81	0.260		
37	37					82								0.370
38	38					42	83	180	47.1	13.4	1.88	0.285		
39	39					84								0.215
40	40					43	85	152	49.7	11.4	2.13	0.135		
41	41					86								0.135
42	42					44	87	142	36.9	10.8	1.87	0.090		
43	43					88								0.075
44	44					45	89	107	27.3	7.28	0.445	0.035		
45	45					90								0.015

DATE 25 July 1956  
 TIME 1100 - 1110 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.19

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
46	91	62.3	21.8	3.50	0.090									
	92					69	136							
47	93	44.3	13.2	1.16			137							
	94						138							
48	95	30.3	4.53	0.390		70	139							
	96						140							
49	97	23.0	1.59	0.110		71	141							
	98						142							
50	99	16.8	0.970			72	143							
	100						144							
51	101	10.2	0.140			73	145							
	102						146							
52	103	2.85	0.025			74	147							
	104						148							
53	105	0.930				75	149							
	106						150							
54	107	0.115				76	151							
	108						152							
55	109	0.045				77	153							
	110						154							
56	111					78	155							
	112						156							
57	113					79	157							
	114						158							
58	115					80	159							
	116						160							
59	117					81	161							
	118						162							
60	119					82	163							
	120						164							
61	121					83	165							
	122						166							
62	123					84	167							
	124						168							
63	125					85	169							
	126						170							
64	127					86	171							
	128						172							
65	129					87	173							
	130						174							
66	131					88	175							
	132						176							
67	133					89	177							
	134						178							
68	135					90	179							
							180							
						91	181							

DATE 25 July 1956  
 TIME 1300-1310 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.20

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
1	1													
	2					46								
2	3					24	47							
	4						48							
3	5					25	49							
	6						50							
4	7					26	51							
	8						52							
5	9					27	53							
	10						54							
6	11					28	55							
	12						56							
7	13					29	57	0.180						
	14						58							
8	15					30	59	1.23						
	16						60							
9	17					31	61	2.79	0.060					
	18						62							
10	19					32	63	5.60	0.615					
	20						64							
11	21					33	65	9.97	2.36	0.015				
	22						66							
12	23					34	67	20.4	2.75	0.350				
	24						68							0.025
13	25					35	69	45.6	8.22	1.94	0.105			0.050
	26						70							0.125
14	27					36	71	89.0	18.6	4.47	1.09	0.235		0.350
	28						72							0.650
15	29					37	73	130	38.0	8.95	1.90	0.470		0.795
	30						74							0.735
16	31					38	75	149	51.0	12.9	2.76	0.795		0.735
	32						76							0.565
17	33					39	77	162	52.2	14.7	3.42	0.735		0.495
	34						78							0.460
18	35					40	79	170	47.1	15.9	3.06	0.495		0.305
	36						80							0.325
19	37					41	81	170	46.5	11.4	2.88	0.305		0.445
	38						82							0.400
20	39					42	83	171	46.5	10.7	2.08	0.400		0.335
	40						84							0.315
21	41					43	85	170	39.6	9.22	2.33	0.335		0.430
	42						86							0.380
22	43					44	87	146	36.6	8.74	1.97	0.355		0.230
	44						88							
23	45					45	89	134	30.2	8.95	1.42	0.380		
							90							

DATE 25 July 1956  
 TIME 1300 - 1310 CST  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 20

Table 5.2 (Continued)

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	120	33.9	8.16	1.47	0.205	69	136				
	92					0.210	69	137				
47	93	114	32.7	6.56	1.25	0.110	70	138				
	94					0.075	70	139				
48	95	99.9	27.9	5.62	1.01	0.060		140				
	96					0.065	71	141				
49	97	83.4	20.4	4.28	0.675	0.095	71	142				
	98					0.050	72	143				
50	99	57.9	9.77	2.47	0.270		72	144				
	100						73	145				
51	101	35.6	6.24	1.49	0.030			146				
	102						74	147				
52	103	26.1	3.68	0.325			74	148				
	104						75	149				
53	105	21.2	0.925	0.045				150				
	106						76	151				
54	107	11.2	0.095					152				
	108						77	153				
55	109	1.88						154				
	110						78	155				
56	111	0.225						156				
	112						79	157				
57	113							158				
	114						80	159				
58	115							160				
	116						81	161				
59	117							162				
	118						82	163				
60	119							164				
	120						83	165				
61	121							166				
	122						84	167				
62	123							168				
	124						85	169				
63	125							170				
	126						86	171				
64	127							172				
	128						87	173				
65	129							174				
	130						88	175				
66	131							176				
	132						89	177				
67	133							178				
	134						90	179				
68	135							180				
							91	181				

DATE 25 July 1956  
 TIME 2200-2210 CST  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 21

Table 5.2 (Continued)

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					24	46					
	2					24	47					
	3					25	48					
	4					25	49					
3	5					26	50					
	6					26	51					
4	7					27	52					
	8					27	53					
5	9					28	54					
	10					28	55					
6	11					29	56					
	12					29	57					
7	13					30	58					
	14					30	59					
8	15					31	60					
	16					31	61					
9	17					32	62					
	18					32	63					
10	19					33	64					
	20					33	65					
11	21					34	66					
	22					34	67	0.230				
12	23					35	68					
	24					35	69	0.925				
13	25					36	70					
	26					36	71	2.55	0.025			
14	27					37	72					
	28					37	73	6.63	0.380			
15	29					38	74					
	30					38	75	15.6	2.39	0.040		
16	31					39	76					
	32					39	77	39.3	8.70	0.975	0.095	
17	33					40	78					0.020
	34					40	79	66.5	22.5	5.29	1.11	0.215
18	35					41	80					0.595
	36					41	81	131	41.0	11.6	3.22	0.915
19	37					42	82					1.26
	38					42	83	210	65.9	19.1	4.72	1.11
20	39					43	84					1.46
	40					43	85	287	91.7	27.1	8.37	2.31
21	41					44	86					3.03
	42					44	87	275	96.6	29.6	9.03	3.26
22	43					45	88					2.95
	44					45	89	265	91.5	27.8	8.43	1.99
23	45					90	90					0.955

Table 5.2 (Continued)  
 DATE 25 July 1956  
 TIME 2200 -2210 CST  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.21

POST NO.	ARC					POST NO.	ARC						
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m	800m
46	91	201	66.3	17.1	2.18	0.280	69	136					
	92					0.075		137					
47	93	129	34.7	4.38	0.485		70	139					
	94							140					
48	95	76.2	12.0	1.51	0.035		71	141					
	96							142					
49	97	35.6	1.83	0.140			72	143					
	98							144					
50	99	10.6	0.415				73	145					
	100							146					
51	101	1.36	0.085				74	147					
	102							148					
52	103	0.110					75	149					
	104							150					
53	105	0.025					76	151					
	106							152					
54	107	0.045					77	153					
	108							154					
55	109						78	155					
	110							156					
56	111						79	157					
	112							158					
57	113						80	159					
	114							160					
58	115						81	161					
	116							162					
59	117						82	163					
	118							164					
60	119						83	165					
	120							166					
61	121						84	167					
	122							168					
62	123						85	169					
	124							170					
63	125						86	171					
	126							172					
64	127						87	173					
	128							174					
65	129						88	175					
	130							176					
66	131						89	177					
	132							178					
67	133						90	179					
	134							180					
68	135						91	181					

Table 5.2 (Continued)  
 DATE 26 July 1956  
 TIME 0000-0010 CST  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.22

POST NO.	ARC					POST NO.	ARC						
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m	800m
1	1						24	46					
	2							47					
2	3						25	48					
	4							49					
3	5						26	51					
	6							52					
4	7						27	53					
	8							54					
5	9						28	55					
	10							56					
6	11						29	57					
	12							58					
7	13						30	59					
	14							60					
8	15						31	61					
	16							62					
9	17						32	63					
	18							64					
10	19						33	65	0.235				
	20							66					
11	21						34	67	1.56				
	22							68					
12	23						35	69	4.65	0.035			
	24							70					
13	25						36	71	11.7	0.865			
	26							72					
14	27						37	73	27.0	4.22	0.060		
	28							74					
15	29						38	75	59.0	11.4	1.04		
	30							76					
16	31						39	77	117	30.8	5.92	0.230	
	32							78					0.015
17	33						40	79	170	55.8	14.4	2.37	0.040
	34							80					0.305
18	35						41	81	213	78.5	25.5	7.11	0.685
	36							82					2.13
19	37						42	83	224	81.8	27.7	8.64	2.51
	38							84					2.31
20	39						43	85	200	60.3	16.3	4.75	1.74
	40							86					0.865
21	41						44	87	143	33.8	7.45	1.71	0.450
	42							88					0.205
22	43						45	89	84.6	16.7	3.75	0.695	0.075
	44							90					0.020
23	45												

DATE 26 July 1956  
TIME 0000 - 0010 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.22

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m	50m	100m	200m		400m	800m	Inner Arcs	800m	50m	100m	200m	400m
46	91		37.4	6.78	0.895	0.065		69	136					
47	92							70	137					
47	93		18.5	2.24	0.265			70	138					
48	94							70	139					
48	95		7.08	0.480	0.070			71	140					
49	96							71	141					
49	97		2.60	0.080	0.020			71	142					
49	98							72	143					
50	99		0.750					72	144					
50	100							73	145					
51	101		0.185					73	146					
51	102							74	147					
52	103		0.030					74	148					
53	104							75	149					
53	105							75	150					
54	106							76	151					
54	107							76	152					
54	108							77	153					
55	109							77	154					
56	110							78	155					
56	111							78	156					
56	112							79	157					
57	113							80	158					
58	114							80	159					
58	115							81	160					
58	116							81	161					
59	117							82	162					
59	118							82	163					
60	119							83	164					
60	120							83	165					
61	121							83	166					
61	122							84	167					
62	123							84	168					
62	124							85	169					
63	125							85	170					
63	126							86	171					
64	127							86	172					
64	128							87	173					
65	129							87	174					
65	130							88	175					
66	131							88	176					
66	132							89	177					
67	133							89	178					
67	134							90	179					
68	135							90	180					
								91	181					

DATE 29 July 1956  
TIME 2100-2110 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.23

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m	50m	100m	200m		400m	800m	Inner Arcs	800m	50m	100m	200m	400m
1	1							46						
2	2							24	47	24.5	8.39	2.20	0.245	
2	3							48						
3	4							25	49	16.4	3.84	0.555	0.045	
3	5							50						
4	6							26	51	7.53	1.42	0.080		
4	7							52						
5	8							27	53	3.60	0.360	0.025		
5	9							54						
6	10							28	55	1.48	0.080	0.025		
6	11							56						
7	12							29	57	0.300				
7	13							58						
8	14							30	59	0.185				
8	15							60						
9	16							31	61	0.045				
9	17							62						
10	18							32	63					
10	19	0.060						64						
11	20							33	65					
11	21	0.670						66						
12	22							34	67					
12	23	3.42	0.045					68						
13	24							35	69					
13	25	9.87	1.18					70						
14	26							36	71					
14	27	33.6	5.04	0.120				72						
15	28							37	73					
15	29	69.6	15.6	1.66	0.050			74						
16	30							38	75					
16	31	95.0	32.9	7.95	0.740	0.035		76						
17	32					0.165		39	77					
17	33	124	43.7	13.7	1.51	0.260		78						
18	34					0.595		40	79					
18	35	145	52.8	18.1	4.81	1.24		80						
19	36					1.87		41	81					
19	37	170	61.7	19.5	6.36	2.09		82						
20	38					1.66		42	83					
20	39	176	55.2	16.8	3.94	1.34		84						
21	40					1.15		43	85					
21	41	136	40.4	10.6	2.71	0.875		86						
22	42					0.485		44	87					
22	43	94.7	23.7	5.82	1.77	0.345		88						
23	44					0.125		45	89					
23	45	54.9	14.3	4.49	0.810			90						



DATE 29 July 1956  
TIME 2300-2310 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.24

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						0.110
2	2					24	47	101	34.8	10.9	2.60	0.345
3	3					48						0.795
4	4					25	49	124	45.3	14.9	5.00	1.23
5	5					50						1.60
6	6					26	51	158	50.4	17.0	5.58	1.81
7	7					52						1.92
8	8					27	53	152	50.7	16.0	5.43	1.68
9	9					54						1.19
10	10					28	55	144	46.5	14.9	4.24	0.645
11	11					56						0.435
12	12					29	57	125	39.2	9.56	1.68	0.185
13	13					58						0.110
14	14					30	59	86.4	22.4	4.05	0.420	0.035
15	15					60						
16	16					31	61	51.5	10.0	1.73	0.055	
17	17					62						
18	18					32	63	29.6	4.32	0.215		
19	19					64						
20	20					33	65	13.3	0.990			
21	21					66						
22	22					34	67	4.37	0.155			
23	23					68						
24	24					35	69	1.44				
25	25					70						
26	26					36	71	0.250				
27	27					72						
28	28					37	73	0.025				
29	29	0.040				74						
30	30					38	75					
31	31	0.130				76						
32	32					39	77					
33	33	0.510	0.020			78						
34	34					40	79					
35	35	0.830	0.120			80						
36	36					41	81					
37	37	3.62	0.310			82						
38	38					42	83					
39	39	10.0	0.800	0.050		84						
40	40					43	85					
41	41	31.1	2.25	0.245		86						
42	42					44	87					
43	43	53.4	9.21	1.07	0.050	88						
44	44					45	89					
45	45	79.7	21.9	4.30	0.755	90						

DATE 1 August 1956  
TIME 1300-1310 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 25

POST NO.	ARC					POST NO.	ARC						
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m	800m
1	1					46							
2	2					24	47						
3	3					48							
4	4					25	49						
5	5					50							
6	6					26	51	0.830					
7	7					52							
8	8					27	53	7.61					
9	9					54							
10	10					28	55	19.2	0.100				
11	11					56							
12	12					29	57	27.3	1.67			0.020	
13	13					58							
14	14					30	59	28.8	3.33	0.015	0.030	0.045	
15	15					60							0.060
16	16					31	61	20.6	8.73	0.730	0.050	0.050	
17	17					62							0.105
18	18					32	63	26.4	8.45	1.64	0.100	0.075	
19	19					64							M
20	20					33	65	47.6	9.05	2.64	0.125	0.045	
21	21					66							0.050
22	22					34	67	74.7	12.7	2.03	0.370	0.060	
23	23					68							0.110
24	24					35	69	96.0	17.3	2.13	0.330	0.090	
25	25					70							0.075
26	26					36	71	129	21.9	1.25	0.440	0.055	
27	27					72							0.035
28	28					37	73	212	23.6	1.89	1.46	0.030	
29	29					74							0.035
30	30					38	75	264	41.0	3.19	0.900	M	
31	31					76							0.020
32	32					39	77	299	38.9	3.11	1.30	M	
33	33					78							0.025
34	34					40	79	305	40.1	2.81	1.10	0.025	
35	35					80							0.060
36	36					41	81	296	37.5	5.08	0.800	0.105	
37	37					82							0.065
38	38					42	83	255	33.5	3.19	0.450	0.170	
39	39					84							0.175
40	40					43	85	206	31.8	4.32	0.600	0.185	
41	41					86							0.125
42	42					44	87	186	27.2	2.86	0.540	0.060	
43	43					88							0.055
44	44					45	89	156	20.1	0.960	0.470	0.065	
45	45					90							0.065

DATE 1 August 1956  
TIME 1300 - 1310 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 25

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	170	14.8	1.15	0.425	M	136					
	92				0.045	69	137	9.95	1.62	0.040		
47	93	156	15.6	1.56	M	0.055	138					
	94				0.065	70	139	0.660				
48	95	161	17.3	2.29	0.275	0.065	140					
	96				0.075	71	141	0.135				
49	97	102	20.3	0.645	0.395	0.115	142					
	98				0.080	72	143	0.025				
50	99	116	27.3	3.55	0.485	0.105	144					
	100				0.165	73	145					
51	101	112	29.9	5.16	0.755	0.200	146					
	102				0.145	74	147					
52	103	91.7	24.8	8.14	0.685	0.220	148					
	104				0.040	75	149					
53	105	91.5	22.5	7.34	0.595	0.225	150					
	106				0.235	76	151					
54	107	85.5	18.0	3.11	0.685	0.230	152					
	108				0.040	77	153					
55	109	92.1	13.7	3.74	M	0.165	154					
	110				0.095	78	155					
56	111	85.2	13.7	0.855	0.815	0.085	156					
	112					79	157					
57	113	74.7	11.9	0.735	0.715	0.045	158					
	114				0.050	80	159					
58	115	53.4	14.9	0.715	1.11		160					
	116					81	161					
59	117	73.5	12.3	2.42	1.16		162					
	118					82	163					
60	119	80.4	13.3	3.02	1.19		164					
	120					83	165					
61	121	80.7	17.3	3.92	0.805		166					
	122					84	167					
62	123	119	26.4	3.69	0.875		168					
	124					85	169					
63	125	148	26.4	5.41	0.370		170					
	126					86	171					
64	127	105	28.8	4.87	0.300		172					
	128					87	173					
65	129	66.9	16.7	6.42	0.340		174					
	130					88	175					
66	131	34.1	19.2	5.99	0.465		176					
	132					89	177					
67	133	8.19	18.5	0.515	0.155		178					
	134					90	179					
68	135	23.9	5.80	0.320			180					
						91	181					

DATE 2 August 1956  
TIME 1200-1210 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 26

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1						46					
	2						24	47				
2	3						48					
	4						25	49				
3	5						50					
	6						26	51				
4	7						52					
	8						27	53				
5	9						54					
	10						28	55				
6	11						56					
	12						29	57				
7	13						58					
	14						30	59				
8	15						60					
	16						31	61				
9	17						62					
	18						32	63	0.030			
10	19						64					
	20						33	65	1.62			
11	21						66					
	22						34	67	2.69			
12	23						68					
	24						35	69	8.09			
13	25						70					
	26						36	71	17.0	0.510		
14	27						72					
	28						37	73	34.7	5.84	0.080	
15	29						74					
	30						38	75	46.5	13.8	0.560	
16	31						76					
	32						39	77	59.1	17.1	1.22	0.025
17	33						78					
	34						40	79	73.8	21.8	1.53	0.055
18	35						80					
	36						41	81	79.4	22.8	3.23	0.305
19	37						82					
	38						42	83	93.2	23.7	6.62	0.490
20	39						84					
	40						43	85	127	28.5	6.92	1.26
21	41						86					
	42						44	87	133	35.9	7.52	2.16
22	43						88					
	44						45	89	121	33.5	9.60	2.18
23	45						90					

Table 5.2 (Continued)  
 DATE 2 August 1956  
 TIME 1200-1210 CST  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.26

POST NO.	ARC					POST NO.	ARC					
	Inner Arms 800m arc	50m	100m	200m	400m		800m	Inner Arms 800m arc	50m	100m	200m	400m
46	91	123	37.4	10.1	2.18	0.365	136					
	92					0.385	69	137				
47	93	121	38.4	10.3	2.07	0.340		138				
	94					0.325	70	139				
48	95	114	36.3	11.6	2.48	0.280		140				
	96					0.280	71	141				
49	97	126	41.6	12.2	2.54	0.285		142				
	98					0.310	72	143				
50	99	132	48.5	12.9	2.75	0.335		144				
	100					0.445	73	145				
51	101	144	47.1	11.8	1.92	0.465		146				
	102					0.360	74	147				
52	103	158	42.6	10.6	1.59	0.280		148				
	104					0.265	75	149				
53	105	148	39.5	9.80	0.925	0.300		150				
	106					0.360	76	151				
54	107	121	33.6	6.92	1.23	0.310		152				
	108					0.370	77	153				
55	109	96.8	25.8	5.68	1.47	0.355		154				
	110					0.355	78	155				
56	111	70.1	18.6	4.28	1.60	0.415		156				
	112					0.320	79	157				
57	113	50.4	13.1	4.13	1.13	0.185		158				
	114					0.150	80	159				
58	115	34.7	7.13	2.57	0.745	0.085		160				
	116					0.055	81	161				
59	117	24.6	6.12	0.990	0.255			162				
	118						82	163				
60	119	21.5	6.21	1.22	0.240			164				
	120						83	165				
61	121	16.4	6.03	1.56	0.155			166				
	122						84	167				
62	123	11.8	5.15	1.56	0.235			168				
	124						85	169				
63	125	7.17	3.39	1.29	0.190			170				
	126						86	171				
64	127	5.57	3.18	1.34	0.130			172				
	128						87	173				
65	129	3.90	1.97	0.980	0.050			174				
	130						88	175				
66	131	1.49	0.910	0.580				176				
	132						89	177				
67	133	0.190	0.245	0.125				178				
	134						90	179				
68	135			0.030				180				
							91	181				

Table 5.2 (Continued)  
 DATE 2 August 1956  
 TIME 1400-1410 CST  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.27

POST NO.	ARC					POST NO.	ARC					
	Inner Arms 800m arc	50m	100m	200m	400m		800m	Inner Arms 800m arc	50m	100m	200m	400m
1	1					46						
	2					24	47					
2	3						48					
	4					25	49					
3	5						50					
	6					26	51					
4	7						52					
	8					27	53					
5	9						54					
	10					28	55					
6	11						56					
	12					29	57					
7	13						58					
	14					30	59					
8	15						60					
	16					31	61	0.030				
9	17						62					
	18					32	63	0.540				
10	19						64					
	20					33	65	1.79	0.240			
11	21						66					
	22					34	67	7.08	1.64	0.205		
12	23						68					
	24					35	69	12.2	4.01	0.690		
13	25						70					
	26					36	71	18.8	6.57	2.57	0.080	
14	27						72					0.050
	28					37	73	24.5	10.1	4.29	0.890	0.050
15	29						74					0.130
	30					38	75	40.2	14.4	3.78	0.990	0.165
16	31						76					0.170
	32					39	77	59.1	17.4	4.56	1.07	0.185
17	33						78					0.255
	34					40	79	93.9	19.8	6.23	1.23	0.390
18	35						80					0.580
	36					41	81	133	32.1	7.81	2.48	0.710
19	37						82					0.800
	38					42	83	159	49.1	12.4	3.73	0.840
20	39						84					0.870
	40					43	85	200	60.0	17.7	4.73	0.980
21	41						86					0.930
	42					44	87	221	73.1	19.7	4.17	0.940
22	43						88					0.750
	44					45	89	221	57.3	17.8	3.66	0.670
23	45						90					0.520

DATE 2 August 1956  
 TIME 1400-1410 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.27

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	188	45.3	13.7	2.33	0.405	136					
	92					0.505	69	137				
47	93	164	41.4	9.77	2.36	0.355		138				
	94					0.350	70	139				
48	95	164	49.8	11.7	2.40	0.355		140				
	96					0.355	71	141				
49	97	150	50.1	14.2	2.39	0.330		142				
	98					0.225	72	143				
50	99	132	44.6	13.1	1.56	0.185		144				
	100					0.165	73	145				
51	101	132	36.2	9.37	1.00	0.145		146				
	102					0.120	74	147				
52	103	141	36.3	5.06	0.355	0.100		148				
	104					0.060	75	149				
53	105	123	23.0	3.86	0.050	0.050		150				
	106					0.025	76	151				
54	107	101	19.2	1.69				152				
	108						77	153				
55	109	63.3	10.8	0.535				154				
	110						78	155				
56	111	34.4	5.49	0.025				156				
	112						79	157				
57	113	22.1	1.55					158				
	114						80	159				
58	115	7.86	0.415					160				
	116						81	161				
59	117	3.27						162				
	118						82	163				
60	119	0.940						164				
	120						83	165				
61	121	0.210						166				
	122						84	167				
62	123							168				
	124						85	169				
63	125							170				
	126						86	171				
64	127							172				
	128						87	173				
65	129							174				
	130						88	175				
66	131							176				
	132						89	177				
67	133							178				
	134						90	179				
68	135							180				
							91	181				

DATE 3 August 1956  
 TIME 0000-0010 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.28

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1						46					
	2						24	47				
2	3							48				
	4						25	49				
3	5							50				
	6						26	51				
4	7							52				
	8						27	53				
5	9							54				
	10						28	55				
6	11							56				
	12						29	57				
7	13							58				
	14						30	59				
8	15							60				
	16						31	61				
9	17							62				
	18						32	63				
10	19							64				
	20						33	65	0.070			
11	21							66				
	22						34	67	0.180			
12	23							68				
	24						35	69	12.0	0.370		
13	25							70				
	26						36	71	42.5	5.81	0.065	
14	27							72				
	28						37	73	100	20.4	1.03	0.045
15	29							74				
	30						38	75	152	45.6	8.24	0.120
16	31							76				
	32						39	77	218	79.8	22.4	2.28
17	33							78				
	34						40	79	299	115	33.9	10.4
18	35							80				0.055
	36						41	81	378	156	42.8	18.2
19	37							82				2.35
	38						42	83	488	192	57.9	21.1
20	39							84				8.65
	40						43	85	450	179	59.5	19.0
21	41							86				2.57
	42						44	87	408	144	46.9	13.5
22	43							88				0.250
	44						45	89	326	98.3	24.3	4.93
23	45							90				0.030

DATE 3 August 1956  
TIME 0000-0010 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 28

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	209	52.2	13.9	0.755							
47	92					69	136					
47	93	107	17.4	4.82	0.020		137					
48	94						138					
48	95	50.7	5.75	0.490	0.020	70	139					
49	96						140					
49	97	21.3	1.10	0.030		71	141					
50	98						142					
50	99	5.91	0.115			72	143					
51	100						144					
51	101	0.610				73	145					
52	102						146					
52	103					74	147					
53	104						148					
53	105					75	149					
54	106						150					
54	107					76	151					
55	108						152					
55	109					77	153					
56	110						154					
56	111					78	155					
57	112						156					
57	113					79	157					
58	114						158					
58	115					80	159					
59	116						160					
59	117					81	161					
60	118						162					
60	119					82	163					
61	120						164					
61	121					83	165					
62	122						166					
62	123					84	167					
63	124						168					
63	125					85	169					
64	126						170					
64	127					86	171					
65	128						172					
65	129					87	173					
66	130						174					
66	131					88	175					
67	132						176					
67	133					89	177					
68	134						178					
68	135					90	179					
							180					
						91	181					

DATE 3 AUGUST 1956  
TIME 0200 - 0210 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 29

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91											
47	92					69	136					1.06
47	93						137	115	43.5	15.4	4.18	0.870
48	94						138					1.41
48	95	0.025				70	139	101	46.8	16.7	5.97	1.80
49	96						140					1.44
49	97	0.020				71	141	81.0	30.8	8.31	3.09	1.23
50	98						142					0.880
50	99	0.070				72	143	38.1	11.1	2.93	0.715	0.455
51	100						144					0.150
51	101	0.170				73	145	15.6	3.47	0.735	0.125	0.035
52	102						146					0.010
52	103	0.790				74	147	4.13	0.845	0.180	0.055	
53	104						148					
53	105	2.43	0.025			75	149	0.920	0.305	0.115	0.025	
54	106						150					
54	107	6.93	0.205			76	151	0.380	0.135	0.055		
55	108						152					
55	109	16.7	1.23	0.015		77	153	0.185	0.055	0.015		
56	110						154					
56	111	44.6	6.32	0.370		78	155	0.100				
57	112						156					
57	113	91.5	16.5	1.94	0.180	79	157	0.040				
58	114				0.025		158					
58	115	127	35.7	8.63	1.27	80	159					
59	116				0.085		160					
59	117	167	63.0	19.9	5.45	81	161					
60	118				0.230		162					
60	119	234	79.5	27.6	9.18	82	163					
61	120				1.40		164					
61	121	234	87.8	24.2	7.37	83	165					
62	122				2.60		166					
62	123	248	74.9	21.8	5.66	84	167					
63	124				1.78		168					
63	125	191	71.1	21.9	7.62	85	169					
64	126				1.24		170					
64	127	186	51.5	13.3	4.48	86	171					
65	128				1.82		172					
65	129	152	41.7	12.6	2.90	87	173					
66	130				1.60		174					
66	131	146	45.6	12.6	3.24	88	175					
67	132				0.905		176					
67	133	128	40.5	11.2	3.55	89	177					
68	134				0.625		178					
68	135	112	35.6	10.6	2.65	90	179					
					0.795		180					
					0.835		181					

DATE 3 August 1956  
TIME 1300-1310 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.30

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
2	2					24	47					
3	3					48						
4	4					25	49					
5	5					50						
6	6					26	51					
7	7					52						
8	8					27	53					
9	9					28	54					
10	10					28	55					
11	11					29	56					
12	12					29	57					
13	13					30	58					
14	14					30	59					
15	15					31	60					
16	16					31	61					
17	17					32	62					
18	18					32	63					
19	19					33	64					
20	20					33	65					
21	21					34	66					
22	22					34	67	0.250				
23	23					35	68					
24	24					35	69	1.79				
25	25					36	70					
26	26					36	71	3.68				
27	27					37	72					
28	28					37	73	6.29				
29	29					38	74					
30	30					38	75	9.72				
31	31					39	76					
32	32					39	77	12.6	1.92			
33	33					40	78					
34	34					40	79	17.6	0.675			
35	35					41	80					
36	36					41	81	26.0	1.68			
37	37					42	82					
38	38					42	83	38.3	5.52	0.870		
39	39					43	84					
40	40					43	85	50.9	17.1	2.83		
41	41					44	86					
42	42					44	87	70.8	20.7	3.77	0.740	
43	43					45	88					
44	44					45	89	88.4	26.9	5.19	1.19	
45	45					90						0.430

DATE 3 August 1956  
TIME 1300-1310 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.30

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	91.7	25.8	5.12	1.27	0.500	136					
47	92					0.210	69	137				
48	93	98.0	28.2	7.60	1.01	0.180	138					
49	94					0.190	70	139				
50	95	100	29.3	6.61	0.880	0.190	140					
51	96	115	27.8	8.59	1.29	0.160	71	141				
52	97					0.020	142					
53	98					0	72	143				
54	99	141	32.9	9.49	2.21	0.020	144					
55	100					0.260	73	145				
56	101	141	41.0	9.49	2.23	0.260	146					
57	102					0.360	74	147				
58	103	146	52.2	12.5	2.99	0.440	148					
59	104					0.320	75	149				
60	105	203	66.2	17.5	2.57	0.380	150					
61	106					0.680	76	151				
62	107	221	67.8	17.0	3.02	0.620	152					
63	108					0.600	77	153				
64	109	203	54.3	15.0	2.36	0.630	154					
65	110					0.660	78	155				
66	111	177	51.2	12.0	2.68	0.440	156					
67	112					0.150	79	157				
68	113	150	41.1	10.1	1.91	0.250	158					
69	114					0.200	80	159				
70	115	125	34.8	8.89	1.36	0.200	160					
71	116						81	161				
72	117	94.2	25.1	5.61	0.680		82	162				
73	118						83	163				
74	119	71.6	17.1	2.12	0.610		84	164				
75	120						85	165				
76	121	39.3	9.48	1.36	0.470		86	166				
77	122						87	167				
78	123	35.7	6.32	2.42	0.640		88	168				
79	124						89	169				
80	125	21.3	5.46	2.08	0.460		90	170				
81	126						91	171				
82	127	18.8	5.12	1.73			92	172				
83	128						93	173				
84	129	11.8	2.31				94	174				
85	130						95	175				
86	131	4.56	0.735				96	176				
87	132						97	177				
88	133	1.64					98	178				
89	134						99	179				
90	135	0.660					100	180				
91	136						101	181				

DATE 3 AUGUST 1956  
TIME 1500 - 1510 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 31

Table 5.2 (Continued)

Inner Arcs	800m arc	ARC					Inner Arcs	800m arc	ARC				
		50m	100m	200m	400m	800m			50m	100m	200m	400m	800m
46	91						136						0.590
47	92						69	137	158	51.3	14.5	3.02	0.710
47	93							138					0.780
48	94						70	139	170	56.3	17.5	3.81	1.03
48	95							140					1.62
48	96						71	141	177	59.0	14.8	4.04	1.67
49	97							142					1.46
49	98						72	143	135	44.3	15.4	4.41	1.30
50	99							144					1.23
50	100						73	145	85.7	33.5	14.0	3.62	1.23
51	101							146					0.760
51	102						74	147	54.9	22.4	7.15	1.60	0.190
52	103							148					0.230
52	104						75	149	37.8	11.8	2.97	0.910	0.310
53	105	0.405	0.375					150					
53	106						76	151	22.1	5.37	1.63	0.290	
54	107	1.58	0.765					152					
54	108						77	153	11.4	3.80	0.900		
55	109	2.15	1.82	0.560				154					
55	110						78	155	4.37	2.46			
56	111	11.7	3.59	1.75	0.610	0.550		156					
56	112						79	157	4.02	0.960			
57	113	24.2	7.26	3.44	0.880	0.310		158					
57	114						80	159	1.89	0.225			
58	115	39.2	12.6	4.17	1.42	0.630		160					
58	116						81	161	0.735				
59	117	55.8	17.3	5.42	1.48	1.40		162					
59	118						82	163					
60	119	85.1	22.7	6.87	2.05	0.400		164					
60	120						83	165					
61	121	124	31.2	9.81	2.69	0.620		166					
61	122						84	167					
62	123	155	41.1	11.0	3.35	0.320		168					
62	124						85	169					
63	125	137	37.2	9.11	2.15	0.940		170					
63	126						86	171					
64	127	129	34.4	8.31	1.18	0.950		172					
64	128						87	173					
65	129	116	37.2	8.31	0.890	0.660		174					
65	130						88	175					
66	131	135	36.6	7.61	1.00	0.660		176					
66	132						89	177					
67	133	152	33.6	7.33	1.36	0.720		178					
67	134						90	179					
68	135	165	40.1	10.3	2.79	0.850		180					
							91	181					

DATE 6 August 1956  
TIME 2000-2010 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 32

Table 5.2 (Continued)

Inner Arcs	800m arc	ARC					Inner Arcs	800m arc	ARC				
		50m	100m	200m	400m	800m			50m	100m	200m	400m	800m
1	1							46					
	2						24	47					
2	3							48					
	4						25	49					
3	5							50					
	6						26	51					
4	7							52					
	8						27	53					
5	9							54					
	10						28	55					
6	11							56					
	12						29	57					
7	13							58					
	14						30	59					
8	15							60					
	16						31	61					
9	17							62					
	18						32	63	0.085				
10	19							64					
	20						33	65	0.090				
11	21							66					
	22						34	67	0.565				
12	23							68					
	24						35	69	3.12	0.075			
13	25							70					
	26						36	71	7.22	0.660			
14	27							72					
	28						37	73	32.1	6.39			
15	29							74					
	30						38	75	78.5	31.5	0.750		
16	31							76					
	32						39	77	207	57.3	14.5	0.395	
17	33							78					0.015
	34						40	79	356	162	53.1	7.17	0.115
18	35							80					1.66
	36						41	81	615	434	129	46.8	6.18
19	37							82					19.7
	38						42	83	729	624	285	121	41.1
20	39							84					56.6
	40						43	85	707	518	205	50.3	31.3
21	41							86					6.20
	42						44	87	608	240	45.2	3.98	0.270
22	43							88					0.030
	44						45	89	369	58.8	1.83	0.045	0.010
23	45							90					0.015

DATE 6 August 1956  
TIME 2000 - 2010 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.32

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	132	6.35	0.015			136					
	92						137					
47	93	44.9	0.435	0.010			138					
	94						139					
48	95	8.55	0.050	0.010			140					
	96						141					
49	97	0.850					142					
	98						143					
50	99	0.080					144					
	100						145					
51	101						146					
	102						147					
52	103						148					
	104						149					
53	105						150					
	106						151					
54	107						152					
	108						153					
55	109						154					
	110						155					
56	111						156					
	112						157					
57	113						158					
	114						159					
58	115						160					
	116						161					
59	117						162					
	118						163					
60	119						164					
	120						165					
61	121						166					
	122						167					
62	123						168					
	124						169					
63	125						170					
	126						171					
64	127						172					
	128						173					
65	129						174					
	130						175					
66	131						176					
	132						177					
67	133						178					
	134						179					
68	135						180					
							181					

DATE 7 August 1956  
TIME 1300-1310 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.33

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
							46					
1	1						47					
	2					24	48					
2	3						49					
	4					25	50					
3	5						51					
	6					26	52					
4	7						53					
	8					27	54					
5	9						55					
	10					28	56					
6	11						57					
	12					29	58					
7	13						59					
	14					30	60					
8	15						61					
	16					31	62					
9	17						63					
	18					32	64					
10	19						65	0.790				
	20					33	66					
11	21						67	2.33	0.070			
	22					34	68					
12	23						69	4.78	0.820	0.090		
	24					35	70					
13	25						71	12.0	2.88	0.240		
	26					36	72					
14	27						73	27.8	5.90	0.935		
	28					37	74					
15	29						75	40.4	11.1	1.86	0.175	
	30					38	76					
16	31						77	51.3	18.9	4.20	0.465	
	32					39	78					
17	33						79	55.7	21.6	5.04	0.925	0.030
	34					40	80					0.080
18	35						81	60.8	17.7	4.23	1.13	0.085
	36					41	82					0.100
19	37						83	59.9	15.6	3.76	0.675	0.145
	38					42	84					0.125
20	39						85	57.2	17.6	4.01	0.725	0.140
	40					43	86					0.160
21	41						87	71.3	21.5	4.62	1.02	0.195
	42					44	88					0.335
22	43						89	106	24.6	6.44	1.42	0.425
	44					45	90					0.465
23	45											



DATE 7 August 1956  
TIME 1300 - 1310 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.33

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91	138	48.3	7.67	2.28	0.590	69	136					
	92					0.640	69	137					
47	93	158	50.9	10.9	3.01	0.520	70	138					
	94					0.440	70	139					
48	95	191	59.1	16.6	2.62	0.420	71	140					
	96					0.710	71	141					
49	97	207	63.6	17.5	3.95	0.740	72	142					
	98					0.680	72	143					
50	99	180	62.7	19.1	3.59	0.660	73	144					
	100					0.560	73	145					
51	101	158	52.4	13.8	3.03	0.500	74	146					
	102					0.230	74	147					
52	103	128	40.2	7.93	1.23	0.070	75	148					
	104						75	149					
53	105	85.5	20.1	4.26	0.590		76	150					
	106						76	151					
54	107	49.2	9.77	1.38	0.080		77	152					
	108						77	153					
55	109	23.9	2.88	0.415			78	154					
	110						78	155					
56	111	7.95	0.880	0.045			79	156					
	112						79	157					
57	113	2.43	0.135				80	158					
	114						80	159					
58	115	0.485	0.025				81	160					
	116						81	161					
59	117	0.200					82	162					
	118						82	163					
60	119						83	164					
	120						83	165					
61	121						84	166					
	122						84	167					
62	123						85	168					
	124						85	169					
63	125						86	170					
	126						86	171					
64	127						87	172					
	128						87	173					
65	129						88	174					
	130						88	175					
66	131						89	176					
	132						89	177					
67	133						90	178					
	134						90	179					
68	135						91	180					
	136						91	181					

DATE 7 August 1956  
TIME 1500-1510 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.34

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						
	2						24	47	60.8	15.9	2.22	0.135	
2	3						48						
	4						25	49	99.6	24.9	6.95	0.525	0.045
3	5						50						0.080
	6						26	51	130	34.7	11.4	1.44	0.130
4	7						52						0.320
	8						27	53	152	45.5	14.4	3.28	0.570
5	9						54						0.700
	10						28	55	180	60.2	16.1	3.83	0.870
6	11						56						1.17
	12						29	57	201	68.7	18.3	4.48	1.06
7	13						58						1.18
	14						30	59	192	64.1	20.0	4.65	1.12
8	15						60						1.27
	16						31	61	162	59.7	18.6	5.10	1.30
9	17						62						1.04
	18						32	63	162	51.0	15.7	4.23	0.970
10	19						64						0.720
	20						33	65	130	40.5	11.9	2.61	0.390
11	21						66						0.100
	22						34	67	102	26.1	5.12	0.805	0.045
12	23						68						0.030
	24						35	69	70.2	13.3	1.42	0.155	0.015
13	25						70						
	26						36	71	46.1	5.99	0.250	0.040	
14	27						72						
	28						37	73	25.5	3.02	0.025	0.015	
15	29						74						
	30						38	75	11.5	0.595	0.020		
16	31						76						
	32						39	77	6.68	0.040	0.025		
17	33						78						
	34						40	79	3.69				
18	35	0.065					80						
	36						41	81	0.525				
19	37	0.380					82						
	38						42	83	0.070				
20	39	3.96					84						
	40						43	85	0.040				
21	41	12.7	0.495				86						
	42						44	87					
22	43	19.2	3.12	0.040			88						
	44						45	89					
23	45	33.3	6.54	0.700	0.015		90						

DATE 7 August 1956  
TIME 2303-2313 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 35-S<sup>+</sup>

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						1.19
2	2						24	47	339	133	45.0	12.5	2.94
3	3						48						4.35
4	4						25	49	387	136	43.1	14.7	5.27
5	5						50						5.29
6	6						26	51	366	130	35.2	11.7	4.17
7	7						52						2.76
8	8						27	53	296	91.5	24.1	8.41	1.54
9	9						54						0.985
10	10						28	55	185	62.1	13.6	3.18	0.520
11	11						56						
12	12						29	57	99.6	24.8	3.53	0.610	
13	13						58						
14	14						30	59	49.4	6.87	0.510	0.055	
15	15						60						
16	16						31	61	20.9	0.580	0.055		
17	17						62						
18	18						32	63	5.87	0.095	0.025		
19	19						64						
20	20						33	65	0.705				
21	21						66						
22	22						34	67	0.135				
23	23						68						
24	24						35	69					
25	25						70						
26	26						36	71					
27	27						72						
28	28						37	73					
29	29						74						
30	30						38	75					
31	31	0.055					76						
32	32						39	77					
33	33	0.415					78						
34	34						40	79					
35	35	0.385					80						
36	36						41	81					
37	37	3.53	0.190				82						
38	38						42	83					
39	39	15.5	1.35	0.035			84						
40	40						43	85					
41	41	58.7	8.64	0.600			86						
42	42						44	87					
43	43	136	34.1	5.29	0.335		88						
44	44						45	89					
45	45	231	81.6	24.1	4.41	0.265	90						

DATE 11 August 1956  
TIME 2130-2140 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 35

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						
2	2						24	47	182	6.81			
3	3						48						
4	4						25	49	87.0	0.490			
5	5						50						
6	6						26	51	24.2				
7	7						52						
8	8						27	53	3.78				
9	9						54						
10	10						28	55	0.440				
11	11						56						
12	12						29	57					
13	13						14						
14	14						30	59					
15	15						60						
16	16						31	61					
17	17						62						
18	18						32	63					
19	19						64						
20	20						33	65					
21	21						66						
22	22						34	67					
23	23	0.225					68						
24	24						35	69					
25	25	2.15	0.105			0.065	70						
26	26					3.23	36	71					
27	27	14.3	2.07	1.59	0.435	13.8	72						
28	28					10.2	37	73					
29	29	59.3	16.4	14.7	13.0	10.2	74						
30	30					6.74	38	75					
31	31	168	61.4	45.8	32.8	5.77	76						
32	32					7.41	39	77					
33	33	359	180	75.6	37.4	5.91	78						
34	34					4.75	40	79					
35	35	312	228	145	41.9	3.52	80						
36	36					3.21	41	81					
37	37	591	575	253	76.2	2.47	82						
38	38					1.03	42	83					
39	39	641	575	200	50.5	0.225	84						
40	40					0.130	43	85					
41	41	650	405	81.1	8.45	0.080	86						
42	42						44	87					
43	43	552	198	14.8	0.420		88						
44	44						45	89					
45	45	366	54.6	0.755			90						

DATE 11 August 1956  
TIME 2330-2340 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.36

POST NO.			ARC					POST NO.			ARC				
Inner	Arcs	800m	50m	100m	200m	400m	800m	Inner	Arcs	800m	50m	100m	200m	400m	800m
1	1							46							
2	2							47		0.090					
3	3							48							
4	4							49		0.095					
5	5							50							
6	6							51		0.105	0.035				
7	7							52							
8	8							53		0.140	0.045				
9	9							54							
10	10							55		0.135	0.085				
11	11							56							
12	12							57		0.185	0.075				
13	13							58							
14	14							59		2.95	0.130	0.040			
15	15							60							
16	16							61		12.0	0.140	0.040			
17	17							62							
18	18							63							
19	19							64		83.5	2.19	0.025			
20	20							65		251	24.3	0.220			
21	21							66							
22	22							67		492	161	6.51	0.055		
23	23							68							
24	24							69		747	405	71.4	0.445		
25	25							70							0.045
26	26							71		830	540	203	17.9	0.160	
27	27							72							0.760
28	28							73		794	431	152	64.6	2.63	
29	29							74							5.85
30	30							75		660	266	79.2	38.9	15.5	
31	31							76							29.8
32	32							77		423	130	59.2	31.3	38.6	
33	33							78							21.9
34	34							79		210	53.3	26.0	20.7	2.34	
35	35							80							
36	36							81		76.2	10.3	3.25	1.08		
37	37							82							
38	38							83		21.9	0.580	0.054			
39	39							84							
40	40							85		5.45					
41	41							86							
42	42							87		1.74					
43	43							88							
44	44							89							
45	45	0.075						90							

DATE 12 August 1956  
TIME 0300-0310 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO.37

POST NO.			ARC					POST NO.			ARC				
Inner	Arcs	800m	50m	100m	200m	400m	800m	Inner	Arcs	800m	50m	100m	200m	400m	800m
1	1							46							
2	2							47							
3	3							48							
4	4							49							
5	5							50							
6	6							51							
7	7							52							
8	8							53							
9	9							54							
10	10							55							
11	11							56							
12	12							57							
13	13							58							
14	14							59							
15	15							60							
16	16							61							
17	17							62							
18	18							63							
19	19							64							
20	20							65							
21	21							66							
22	22							67							
23	23							68							
24	24							69							
25	25							70							
26	26							71							
27	27							72							
28	28							73							
29	29							74							
30	30							75							
31	31							76							
32	32							77		0.055					
33	33							78							
34	34							79		0.795	0.025				
35	35							80							
36	36							81		3.09	0.325				
37	37							82							
38	38							83		11.8	1.53	0.040			
39	39							84							
40	40							85		27.8	6.53	0.780	0.045		
41	41							86							
42	42							87		53.0	17.6	4.53	0.860	0.050	
43	43							88							0.230
44	44							89		99.3	37.1	10.3	3.06	0.795	
45	45							90							1.41

DATE 12 August 1956  
TIME 0300-0310 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.37

POST NO.	ARC					POST NO.	ARC						
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m	800m
46	91	173	55.8	16.4	5.54	1.94	69	136					
47	93	176	60.9	18.5	4.29	1.55	70	137					
48	94					1.44	71	138					
48	95	224	78.0	18.9	5.40	1.34	71	139					
49	96					1.46	71	140					
49	97	224	74.1	22.9	7.39	2.08	72	141					
49	98					2.02	72	142					
50	99	170	57.6	18.5	4.61	1.62	72	143					
50	100					0.975	73	144					
51	101	128	36.6	8.01	2.03	0.480	73	145					
51	102					0.150	74	146					
52	103	68.9	15.5	3.31	0.520	0.025	74	147					
52	104						75	148					
53	105	28.4	6.42	0.905	0.100		75	149					
53	106						75	150					
54	107	15.5	1.56	0.085			76	151					
54	108						76	152					
55	109	7.86	0.490	0.080			77	153					
55	110						77	154					
56	111	3.53	0.130				78	155					
56	112						78	156					
57	113	1.39	0.055				79	157					
57	114						80	158					
58	115	0.055					80	159					
58	116						81	160					
59	117	0.020					81	161					
59	118						82	162					
60	119						82	163					
60	120						83	164					
61	121						83	165					
61	122						84	166					
62	123						84	167					
62	124						85	168					
63	125						85	169					
63	126						86	170					
64	127						86	171					
64	128						87	172					
65	129						87	173					
65	130						88	174					
66	131						88	175					
66	132						89	176					
67	133						89	177					
67	134						90	178					
68	135						90	179					
							91	180					
							91	181					

DATE 12 August 1956  
TIME 0500-0510 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.38

POST NO.	ARC					POST NO.	ARC						
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m	800m
1	1					24	46						
2	2					24	47						
2	3					25	48						
3	4					25	49						
3	5					26	50						
4	6					26	51						
4	7					27	52						
5	8					27	53						
5	9					28	54						
6	10					28	55						
6	11					29	56						
7	12					29	57						
7	13					30	58						
8	14					30	59						
8	15					31	60						
9	16					31	61	0.020					
9	17					32	62						
10	18					32	63	0.350					
10	19					33	64						
11	20					33	65	1.74					
11	21					34	66						
12	22					34	67	5.48	0.210				
12	23					35	68						
13	24					35	69	19.4	1.08	0.020			
13	25					36	70						
14	26					36	71	54.6	5.00	0.270			
14	27					37	72						
15	28					37	73	126	19.8	1.85	0.055		
15	29					38	74						
16	30					38	75	219	57.6	11.5	1.36	0.075	
16	31					39	76						0.520
17	32					39	77	333	118	33.0	7.90	1.66	
17	33					40	78						3.85
18	34					40	79	330	153	51.4	18.7	6.01	
18	35					41	80						6.44
19	36					41	81	360	134	46.9	13.7	4.63	
19	37					42	82						1.91
20	38					42	83	273	87.3	17.4	3.44	0.580	
20	39					43	84						0.085
21	40					43	85	170	31.5	4.61	0.430		
21	41					44	86						
22	42					44	87	84.3	7.55	0.980	0.050		
22	43					45	88						
23	44					45	89	30.3	1.97	0.140	0.025		
23	45					90	90						

DATE 12 August 1956  
TIME 0500-0510 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 38

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	2.64	0.300				136					
	92						137					
47	93	1.38	0.050				138					
	94						139					
48	95	0.210					140					
	96						141					
49	97	0.030					142					
	98						143					
50	99						144					
	100						145					
51	101						146					
	102						147					
52	103						148					
	104						149					
53	105						150					
	106						151					
54	107						152					
	108						153					
55	109						154					
	110						155					
56	111						156					
	112						157					
57	113						158					
	114						159					
58	115						160					
	116						161					
59	117						162					
	118						163					
60	119						164					
	120						165					
61	121						166					
	122						167					
62	123						168					
	124						169					
63	125						170					
	126						171					
64	127						172					
	128						173					
65	129						174					
	130						175					
66	131						176					
	132						177					
67	133						178					
	134						179					
68	135						180					
							181					

DATE 13 August 1956  
TIME 2230-2240 CST

Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

RUN NO. 39

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
	1						46					M
	2					24	47	362	117	36.8	8.24	M
2	3						48					M
	4					25	49	470	140	42.7	17.0	M
3	5						50					M
	6					26	51	425	161	54.2	20.1	2.16
4	7						52					1.56
	8					27	53	378	130	49.6	10.7	1.83
5	9						54					1.36
	10					28	55	249	79.7	20.6	3.43	0.835
6	11						56					M
	12					29	57	155	37.5	4.42	0.540	M
7	13						58					M
	14					30	59	92.2	13.1	1.95	0.080	
8	15						60					
	16					31	61	38.6	2.13	0.180		
9	17						62					
	18					32	63	11.6	0.310			
10	19						64					
	20					33	65	2.62	0.015			
11	21						66					
	22					34	67	0.445				
12	23						68					
	24					35	69	0.005				
13	25						70					
	26					36	71					
14	27						72					
	28					37	73					
15	29						74					
	30					38	75					
16	31						76					
	32					39	77					
17	33	0.225	0.040				78					
	34					40	79					
18	35	1.22	0.110				80					
	36					41	81					
19	37	7.83	0.340	0.050			82					
	38					42	83					
20	39	30.3	1.86	0.210	0.060		84					
	40						85					
21	41	91.8	11.1	0.350	0.075	M	86					
	42						87					
22	43	182	39.6	4.62	0.045	M	88					
	44						89					
23	45	276	98.4	23.8	1.38	M	90					

DATE 14 August 1956, TIME 0030-0040 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.40

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
2	2					24	47					
3	3					48						
4	4					25	49					
5	5					50						
6	6					26	51					
7	7					52						
8	8					27	53					
9	9					54						
10	10					28	55					
11	11					56						
12	12					29	57					
13	13					58						
14	14					30	59					
15	15					60						
16	16					31	61					
17	17					62						
18	18					32	63					
19	19					64						
20	20					33	65					
21	21					66						
22	22					34	67					
23	23					68						
24	24					35	69	0.295				
25	25					70						
26	26					36	71	0.640				
27	27					72						
28	28					37	73	2.85	0.080			
29	29					74						
30	30					38	75	11.6	0.455	0.025		
31	31					76						
32	32					39	77	24.9	2.97	0.180	M	
33	33					78						
34	34					40	79	64.8	14.2	2.33	M	
35	35					80						0.035
36	36					41	81	156	42.2	11.5	M	0.260
37	37					82						0.735
38	38					42	83	227	76.4	25.8	M	1.38
39	39					84						1.64
40	40					43	85	318	105	27.9	M	1.72
41	41					86						1.57
42	42					44	87	312	99.9	26.8	M	1.55
43	43					88						1.49
44	44					45	89	281	77.1	24.3	M	1.56
45	45					90						1.38

DATE 14 August 1956, TIME 0030-0040 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO.40

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	215	75.6	18.5	4.95	1.34						136
47	92					1.28	69	137				138
48	93	201	53.7	17.7	3.73	1.36						139
49	94					1.15	70	139				140
50	95	204	52.7	16.6	5.05	0.900						141
51	96					1.22	71	141				142
52	97	168	55.8	14.5	4.60	1.36						143
53	98					1.62	72	143				144
54	99	180	74.1	23.7	5.85	1.79						145
55	100					2.21	73	145				146
56	101	185	76.4	32.7	14.6	3.33						147
57	102					3.99	74	147				148
58	103	125	49.1	14.5	5.85	6.48						149
59	104					2.80	75	149				150
60	105	68.3	16.1	2.15	0.375	0.465						151
61	106					0.045	76	151				152
62	107	33.0	2.19	0.085			77	152				153
63	108						78	153				154
64	109	10.7	0.195				79	154				155
65	110						80	155				156
66	111	1.35					81	156				157
67	112						82	157				158
68	113	0.150					83	158				159
69	114						84	159				160
70	115	0.025					85	160				161
71	116						86	161				162
72	117						87	162				163
73	118						88	163				164
74	119						89	164				165
75	120						90	165				166
76	121						91	166				167
77	122						92	167				168
78	123						93	168				169
79	124						94	169				170
80	125						95	170				171
81	126						96	171				172
82	127						97	172				173
83	128						98	173				174
84	129						99	174				175
85	130						100	175				176
86	131						101	176				177
87	132						102	177				178
88	133						103	178				179
89	134						104	179				180
90	135						105	180				181

DATE 14 AUGUST 1956  
 TIME 0300-0310 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 41

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91					69	136					
47	92					70	137					
48	93					71	138					
49	94	0.260				72	139					
50	95					73	140					
51	96	2.60	0.185			74	141					
52	97					75	142					
53	98	22.7	1.92	0.125		76	143					
54	99					77	144					
55	100	74.7	18.6	2.27	0.235	78	145					
56	101				0.010	79	146					
57	102	198	59.7	17.6	4.32	80	147					
58	103				0.240	81	148					
59	104	378	142	48.8	16.7	82	149					
60	105				4.34	83	150					
61	106	450	189	67.8	25.0	84	151					
62	107				8.57	85	152					
63	108				9.92	86	153					
64	109	362	144	39.0	9.00	87	154					
65	110				0.400	88	155					
66	111	236	64.7	9.81	0.675	89	156					
67	112				0.055	90	157					
68	113	106	15.0	0.765		91	158					
69	114						159					
70	115	33.6	2.10	0.035			160					
71	116						161					
72	117	4.97	0.295				162					
73	118						163					
74	119	0.270					164					
75	120						165					
76	121						166					
77	122						167					
78	123						168					
79	124						169					
80	125						170					
81	126						171					
82	127						172					
83	128						173					
84	129						174					
85	130						175					
86	131						176					
87	132						177					
88	133						178					
89	134						179					
90	135						180					
91	136						181					

DATE 14 AUGUST 1956  
 TIME 0500-0510 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 42

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91					69	136					
47	92					70	137	1.05	0.055			
48	93					71	138					
49	94					72	139	0.075				
50	95					73	140					
51	96					74	141					
52	97					75	142					
53	98					76	143					
54	99					77	144					
55	100					78	145					
56	101	0.580				79	146					
57	102					80	147					
58	103	0.945				81	148					
59	104					82	149					
60	105	2.61				83	150					
61	106					84	151					
62	107	9.68	0.440			85	152					
63	108					86	153					
64	109	21.0	2.88	0.075	0.005	87	154					
65	110					88	155					
66	111	50.3	5.87	1.07	0.045	89	156					
67	112					90	157					
68	113	106.	25.2	5.24	1.07	91	158					
69	114				0.070		159					
70	115	183	53.6	15.6	3.48	0.280	160					
71	116				0.725		161					
72	117	242	83.9	25.3	7.12	1.31	162					
73	118				1.70		163					
74	119	276	100	31.5	7.77	2.13	164					
75	120				1.95		165					
76	121	254	84.8	23.4	5.59	2.11	166					
77	122				2.11		167					
78	123	204	56.1	15.5	5.16	1.94	168					
79	124				1.76		169					
80	125	127	41.3	12.6	4.17	1.36	170					
81	126				0.815		171					
82	127	103	32.3	8.56	1.94	0.310	172					
83	128				0.070		173					
84	129	76.2	17.1	2.76	0.455	0.020	174					
85	130						175					
86	131	48.6	4.52	0.595	0.060		176					
87	132						177					
88	133	19.7	1.23	0.090			178					
89	134						179					
90	135	5.18	0.225				180					
91	136						181					

DATE 15 August 1956  
TIME 1200-1210 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 43

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						0.055
2	2						47	2.43	0.240	0.025	0.278		0.060
3	3						48						0.125
4	4						49	3.71	0.628	0.245	0.514	0.085	
5	5						50						0.075
6	6						51	10.4	1.91	0.965	0.615	0.085	
7	7						52						0.100
8	8						53	26.1	3.42	1.72	0.568	0.090	
9	9						54						0.095
10	10						55	38.7	5.30	1.80	0.578	0.105	
11	11						56						0.090
12	12						57	49.4	8.58	2.63	0.738	0.035	
13	13						58						0.060
14	14						59	64.5	21.3	3.79	0.825	0.085	
15	15						60						0.075
16	16						61	81.2	33.2	5.27	1.29	0.050	
17	17						62						0.095
18	18						63	111	36.6	7.65	1.02	0.165	
19	19						64						0.145
20	20						65	126	39.0	9.47	0.935	0.075	
21	21						66						0.060
22	22						67	114	26.4	6.31	0.735	0.080	
23	23						68						0.065
24	24						69	116	20.6	3.97	0.745	0.075	
25	25						70						0.075
26	26						71	123	23.3	5.13	0.825	0.070	
27	27						72						0.080
28	28						73	114	26.4	6.93	0.715	0.070	
29	29						74						0.100
30	30						75	137	40.4	7.09	1.47	0.120	
31	31						76						0.135
32	32						77	153	42.3	11.9	1.82	0.250	
33	33						78						0.255
34	34						79	189	46.5	14.7	2.40	0.305	
35	35						80						0.450
36	36						81	219	51.2	16.9	2.63	0.450	
37	37						82						0.490
38	38						83	249	58.2	14.0	2.45	0.540	
39	39						84						0.490
40	40						85	225	57.3	11.6	2.10	0.460	
41	41						86						0.410
42	42						87	200	48.8	10.5	2.07	0.330	
43	43	0.025					88						0.275
44	44						89	177	40.8	7.21	1.76	0.205	
45	45	0.465				0.080	90						0.205

DATE 15 August 1956  
TIME 1200-1210 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 43

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91	135	30.9	6.81	1.36	0.220	69	136					
	92					0.240	70	137					
47	93	121	30.5	7.09	0.910	0.235	71	138					
	94					0.155	72	139					
48	95	114	19.5	5.55	0.710	0.155	73	140					
	96					0.125	74	141					
49	97	81.6	23.6	4.99	0.490	0.100	75	142					
	98					0.070	76	143					
50	99	66.0	18.6	3.12	0.325	0.060	77	144					
	100					0.015	78	145					
51	101	49.8	11.1	1.24	0.135	0.030	79	146					
	102						80	147					
52	103	31.5	6.83	0.125			81	148					
	104						82	149					
53	105	8.55	2.22	0.045			83	150					
	106						84	151					
54	107	4.77	0.520				85	152					
	108						86	153					
55	109	4.40	0.035				87	154					
	110						88	155					
56	111	1.77					89	156					
	112						90	157					
57	113	1.49					91	158					
	114						92	159					
58	115	0.045					93	160					
	116						94	161					
59	117						95	162					
	118						96	163					
60	119						97	164					
	120						98	165					
61	121						99	166					
	122						100	167					
62	123						101	168					
	124						102	169					
63	125						103	170					
	126						104	171					
64	127						105	172					
	128						106	173					
65	129						107	174					
	130						108	175					
66	131						109	176					
	132						110	177					
67	133						111	178					
	134						112	179					
68	135						113	180					
							114	181					



DATE 15 August 1956  
TIME 1400-1410 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.44

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
2	2					24	47	41.4	9.18	1.33	0.320	
3	3					48						
4	4					25	49	36.0	7.85	1.03	0.408	
5	5					50						0.060
6	6					26	51	35.1	6.30	1.84	0.300	0.080
7	7					52						0.060
8	8					27	53	58.7	9.24	3.99	0.875	0.125
9	9					54						0.145
10	10					28	55	98.5	21.3	5.47	1.25	0.125
11	11					56						0.240
12	12					29	57	120	28.1	7.16	1.54	0.185
13	13					58						0.205
14	14					30	59	153	36.3	6.67	1.30	0.220
15	15					60						0.240
16	16					31	61	148	40.4	7.34	1.03	0.215
17	17					62						0.135
18	18					32	63	150	42.9	12.2	1.23	0.200
19	19					64						0.130
20	20					33	65	156	46.2	15.1	2.94	0.150
21	21					66						0.210
22	22					34	67	143	45.9	13.2	2.77	0.385
23	23					68						0.305
24	24					35	69	162	44.0	12.2	2.46	0.565
25	25					70						0.575
26	26	0.065				36	71	162	44.6	9.87	2.60	0.545
27	27	1.56				72						0.575
28	28					37	73	188	39.8	9.37	2.54	0.585
29	29	4.01	0.040			74						0.605
30	30					38	75	191	49.8	10.9	3.12	0.465
31	31	5.48	0.375			76						0.445
32	32					39	77	168	53.9	12.4	2.72	0.445
33	33	11.9	1.23	0.195		78						0.345
34	34					40	79	135	39.5	9.87	1.96	0.310
35	35	16.1	4.16	1.18		80						0.290
36	36					41	81	109	31.1	7.67	1.98	0.240
37	37	27.0	9.24	2.75	0.030	82						0.210
38	38					42	83	89.0	18.9	6.17	1.77	0.165
39	39	32.0	15.2	2.55	0.125	84						0.135
40	40					43	85	70.1	12.6	3.60	0.835	0.195
41	41	42.9	14.7	3.44	0.385	86						0.160
42	42					44	87	69.3	10.5	1.81	0.555	0.150
43	43	48.8	15.3	5.24	0.265	88						0.170
44	44					45	89	46.5	6.35	1.18	0.195	0.195
45	45	48.5	12.4	2.75	0.405	90						0.105

DATE 15 August 1956  
TIME 1400-1410 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.44

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	23.6	2.78	0.355	0.060							
47	92					69	136					
48	93	18.5	1.36	0.085	0.055							
49	94					70	138					
50	95	8.43	0.500	0.070	0.030							
51	96					71	140					
52	97	6.17	0.090									
53	98					72	142					
54	99	2.87										
55	100					73	143					
56	101	0.355										
57	102					74	144					
58	103											
59	104					75	145					
60	105											
61	106					76	146					
62	107											
63	108					77	147					
64	109											
65	110					78	148					
66	111											
67	112					79	149					
68	113											
69	114					80	150					
70	115											
71	116					81	151					
72	117											
73	118					82	152					
74	119											
75	120					83	153					
76	121											
77	122					84	154					
78	123											
79	124					85	155					
80	125											
81	126					86	156					
82	127											
83	128					87	157					
84	129											
85	130					88	158					
86	131											
87	132					89	159					
88	133											
89	134					90	160					
90	135											
91	136					91	161					

DATE 15 August 1956  
TIME 1700-1710 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 45

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						
2	2						24	47	0.065				
3	3						48						
4	4						25	49	0.520				
5	5						50						
6	6						26	51	3.08	0.040			
7	7						52						
8	8						27	53	11.5	0.140			
9	9						54						
10	10						28	55	27.8	0.790	0.085		
11	11						56						
12	12						29	57	45.8	3.24	0.660		
13	13						58						
14	14						30	59	71.7	11.3	1.04	0.075	
15	15						60						
16	16						31	61	114	25.5	5.40	0.740	0.060
17	17						62						0.115
18	18						32	63	168	48.9	11.6	3.98	0.225
19	19						64						0.685
20	20						33	65	204	73.2	21.5	4.95	1.06
21	21						66						1.80
22	22						34	67	246	86.9	28.6	7.12	2.50
23	23						68						2.94
24	24						35	69	266	99.0	31.4	8.93	2.20
25	25						70						1.84
26	26						36	71	291	98.6	29.8	7.24	1.43
27	27						72						1.82
28	28						37	73	285	86.3	24.2	6.85	2.27
29	29						74						2.81
30	30						38	75	297	89.3	28.6	8.37	2.29
31	31						76						1.90
32	32						39	77	362	114	41.4	6.56	1.50
33	33						78						0.735
34	34						40	79	288	105	28.1	3.39	0.330
35	35						80						0.125
36	36						41	81	215	58.4	10.9	1.17	0.060
37	37						82						0.025
38	38						42	83	150	32.7	3.97	0.420	0.010
39	39						84						
40	40						43	85	105	18.0	1.45	0.075	
41	41						86						
42	42						44	87	65.7	8.06	0.450		
43	43						88						
44	44						45	89	34.2	1.47	0.025		
45	45	0.040					90						

DATE 15 August 1956  
TIME 1700-1710 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 45

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91	10.9	0.170				136						
92							69	137					
47	93	1.88	0.035				138						
94							70	139					
48	95	0.545					140						
96							71	141					
49	97						142						
98							72	143					
50	99						144						
100							73	145					
51	101						146						
102							74	147					
52	103						148						
104							75	149					
53	105						150						
106							76	151					
54	107						152						
108							77	153					
55	109						154						
110							78	155					
56	111						156						
112							79	157					
57	113						158						
114							80	159					
58	115						160						
116							81	161					
59	117						162						
118							82	163					
60	119						164						
120							83	165					
61	121						166						
122							84	167					
62	123						168						
124							85	169					
63	125						170						
126							86	171					
64	127						172						
128							87	173					
65	129						174						
130							88	175					
66	131						176						
132							89	177					
67	133						178						
134							90	179					
68	135						180						
181							91	181					

DATE 15 August 1956  
TIME 1845-1855 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 46

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						1.01
2	2						24	47	434	114	27.8	4.84	1.12
3	3						48						1.31
4	4						25	49	363	111	32.8	8.48	2.62
5	5						50						3.08
6	6						26	51	267	92.1	32.0	11.0	2.83
7	7						52						1.74
8	8						27	53	206	72.5	22.1	6.63	0.895
9	9						54						0.445
10	10						28	55	147	41.0	11.8	1.44	0.110
11	11						56						0.060
12	12						29	57	99.0	28.4	4.29	0.235	0.015
13	13						58						
14	14						30	59	54.5	17.1	0.480		
15	15						60						
16	16						31	61	37.1	4.79			
17	17						62						
18	18						32	63	18.9	0.265			
19	19						64						
20	20						33	65	11.4	0.130			
21	21						66						
22	22						34	67	1.88	0.040			
23	23						68						
24	24						35	69	0.370	0.140			
25	25						70						
26	26						36	71	0.160	0.155			
27	27	0.065	0.110	0.055			72						
28	28						37	73					
29	29	0.535	0.125	0.055			74						
30	30						38	75					
31	31	4.59	0.325	0.085			76						
32	32						39	77					
33	33	16.4	2.09	0.420	0.050		78						
34	34						40	79					
35	35	59.3	13.5	3.53	0.715	0.095	80						
36	36					0.445	41	81					
37	37	177	58.8	17.6	3.95	1.10	82						
38	38					3.22	42	83					
39	39	384	131	53.1	15.0	6.08	84						
40	40					6.33	43	85					
41	41	512	198	60.8	20.9	3.63	86						
42	42					3.11	44	87					
43	43	564	188	47.8	12.6	4.01	88						
44	44					3.06	45	89					
45	45	546	142	33.3	9.79	1.86	90						

DATE 20 AUGUST 1956  
TIME 1000 - 1010 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 47

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91						136						
47	92						69	137	49.2	6.32	1.49	0.405	0.035
48	93						138						0.040
49	94						70	139	68.1	7.22	1.29	0.515	0.075
50	95						140						0.090
51	96						71	141	67.5	11.3	2.09	0.445	0.095
52	97						142						0.110
53	98						72	143	92.7	18.0	2.69	0.825	0.100
54	99						144						0.100
55	100						73	145	139	24.8	3.72	0.745	0.100
56	101						146						0.110
57	102						74	147	182	35.4	3.67	0.685	0.140
58	103						148						0.200
59	104						75	149	213	47.6	6.46	1.06	0.240
60	105						150						0.205
61	106						76	151	218	42.6	9.49	1.38	0.205
62	107						152						0.180
63	108						77	153	224	42.8	7.33	1.29	0.180
64	109						154						0.165
65	110						78	155	260	42.3	6.02	2.00	0.175
66	111						156						0.125
67	112						79	157	263	47.6	5.51	1.36	0.145
68	113						158						0.165
69	114						80	159	278	47.4	7.70	1.42	0.165
70	115						160						0.165
71	116						81	161	293	45.8	7.09	1.12	0.105
72	117						162						0.085
73	118						82	163	284	53.3	6.65	0.975	0.100
74	119						164						0.125
75	120						83	165	221	45.5	7.84	1.02	0.120
76	121	0.480					166						0.110
77	122						84	167	192	41.6	8.33	0.955	0.085
78	123	2.18					168						0.055
79	124						85	169	158	41.7	7.40	1.38	0.080
80	125						170						0.065
81	126	4.61	0.080				86	171	122	39.0	9.39	0.845	
82	127						172						
83	128	9.56	1.20	0.040			87	173	85.2	26.0	5.86	0.695	
84	129						174						
85	130	19.7	6.32	0.625			88	175	42.3	15.6	4.10	0.565	
86	131						176						
87	132	25.7	6.00	0.415	0.135		89	177	87.1	10.2	3.34	1.415	
88	133						178						
89	134	33.5	4.92	0.735	0.155		90	179	22.2	7.46	2.54	0.435	
90	135						180						
91	136	37.1	5.61	0.795	0.225		91	181	21.3	4.43	1.32	0.470	

DATE 20 August 1956  
 TIME 1233-1243 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 48-S

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
2	2					24	1.92					
3	3					48						
4	4					25	1.85					
5	5					50						
6	6					26	1.83					
7	7					52						
8	8					27	3.03					
9	9					54						
10	10					28	4.89					
11	11					56						
12	12					29	4.74					
13	13					58						
14	14					30	5.51					
15	15					60						
16	16					31	5.97					
17	17					62						
18	18					32	13.3	0.040				
19	19					64						
20	20					33	19.2	0.130				
21	21					66						
22	22					34	26.9	0.620				
23	23					68						
24	24					35	27.3	1.01				
25	25					70						
26	26					36	31.5	3.66				
27	27					72						
28	28					37	35.3	4.35				
29	29					74						
30	30					38	39.6	4.88				
31	31	0.045				76						
32	32					39	51.8	8.52				
33	33	0.070				78						
34	34					40	49.5	10.1	0.150			
35	35	0.155				80						
36	36					41	57.0	10.3	0.255			
37	37	0.245				82						
38	38					42	55.2	12.8	0.260			
39	39	0.355				84						
40	40					43	74.7	9.38	0.455			
41	41	0.595				86						
42	42					44	62.3	9.03	1.11			
43	43	1.15				88						
44	44					45	57.0	8.40	1.12			
45	45	1.25				90						

DATE 20 August 1956  
 TIME 1233-1243 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 48-S

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	71.0	5.60	0.695		136						0.070
47	92					69	137	143	40.4	5.51	1.18	0.185
48	93	76.2	7.35	0.875		138						0.095
49	94					70	139	125	45.2	11.6	2.12	0.140
50	95	58.8	4.98	0.645		140						0.145
51	96					71	141	115	36.0	8.93	1.31	0.180
52	97	50.6	3.45	0.745		142						0.140
53	98					72	143	85.4	29.3	9.83	1.27	0.120
54	99	47.3	4.40	0.945		144						0.060
55	100					73	145	78.6	22.5	5.11	1.16	0.045
56	101	46.4	6.66	1.22		146						0.090
57	102					74	147	57.0	14.4	2.52	0.745	0.040
58	103	39.2	7.91	0.845	0.020	148						0.035
59	104					75	149	39.6	15.0	3.23	0.525	
60	105	37.1	5.58	0.905	0.065	150						
61	106					76	151	45.2	16.2	2.64	0.340	
62	107	39.5	5.72	0.905		152						
63	108					77	153	42.8	9.56	1.80	0.130	
64	109	38.6	7.38	1.05	0.105	154						
65	110					78	155	33.5	6.45	2.42		
66	111	42.8	7.98	0.865	0.190	156						
67	112					79	157	16.8	7.13	0.695		
68	113	54.8	8.48	0.935	0.215	158						
69	114					80	159	17.6	3.27	0.185		
70	115	80.6	9.41	1.44	0.235	160						
71	116					81	161	19.5	1.39	0.030		
72	117	74.0	9.62	0.955	0.255	162						
73	118					82	163	10.2	0.355			
74	119	66.2	8.16	1.07	0.050	164						
75	120					83	165	1.21				
76	121	60.8	7.62	0.895	0.010	166						
77	122					84	167	0.150				
78	123	74.0	6.66	1.29	0.025	168						
79	124					85	169	0.065				
80	125	78.6	4.91	0.755	0.075	170						
81	126					86	171	0.055				
82	127	89.9	8.16	0.915	0.275	172						
83	128					87	173	0.040				
84	129	97.8	18.9	3.08	0.535	174						
85	130					88	175					
86	131	101	22.8	2.23	0.365	176						
87	132					89	177					
88	133	130	26.0	2.02	0.045	90	179					
89	134					91	180					
90	135	140	24.6	3.13	0.725	0.115						

DATE 21 AUGUST 1956  
 TIME 0900-0910 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 48

POST NO.		ARC					POST NO.		ARC				
Inner	800m	50m	100m	200m	400m	800m	Inner	800m	50m	100m	200m	400m	800m
Arcs	arc						Arcs	arc					
46	91						136						
47	92						137	41.4	8.79	1.11	0.020		
48	93						138						
49	94						139	26.2	3.06	0.055			
50	95	0.030					140						
51	96						141	17.6	0.730	0.025			
52	97	0.545					142						
53	98						143	7.58	0.065				
54	99	2.40					144						
55	100						145	1.52					
56	101	6.29	0.065				146						
57	102						147	0.215					
58	103	12.3	0.480				148						
59	104						149	0.010					
60	105	20.0	3.20				150						
61	106						151						
62	107	29.4	5.13	0.085			152						
63	108						153						
64	109	36.9	6.15	0.700	0.020		154						
65	110						155						
66	111	40.7	7.25	1.20	0.110	0.040	156						
67	112						157						
68	113	53.9	13.8	1.82	0.400	0.055	158						
69	114						159						
70	115	83.0	21.8	4.71	0.950	0.285	160						
71	116						161						
72	117	97.5	31.7	8.12	1.54	0.395	162						
73	118						163						
74	119	155	39.3	10.5	2.07	0.410	164						
75	120						165						
76	121	130	48.0	14.1	3.05	0.640	166						
77	122						167						
78	123	186	56.6	17.1	3.45	0.760	168						
79	124						169						
80	125	209	65.0	17.0	3.64	0.990	170						
81	126						171						
82	127	127	65.6	15.5	4.66	1.31	172						
83	128						173						
84	129	224	59.7	13.8	4.68	0.970	174						
85	130						175						
86	131	158	39.9	11.6	3.32	0.760	176						
87	132						177						
88	133	105	26.3	8.81	0.990	0.025	178						
89	134						179						
90	135	62.1	18.0	3.54	0.085		180						
							181						

DATE 21 August 1956  
 TIME 1100-1110 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>)  
 RUN NO. 49

POST NO.		ARC					POST NO.		ARC				
Inner	800m	50m	100m	200m	400m	800m	Inner	800m	50m	100m	200m	400m	800m
Arcs	arc						Arcs	arc					
1	1						46						
2	2						47						
3	3						48						
4	4						49						
5	5						50						
6	6						51						
7	7						52						
8	8						53						
9	9						54						
10	10						55						
11	11						56						
12	12						57						
13	13						58						
14	14						59						
15	15						60						
16	16						61						
17	17						62						
18	18						63						
19	19						64						
20	20						65						
21	21						66						
22	22						67						
23	23						68						
24	24						69						
25	25						70						
26	26						71	0.110					
27	27						72						
28	28						73	0.175					
29	29						74						
30	30						75	0.430					
31	31						76						
32	32						77	4.19	0.265				
33	33						78						
34	34						79						
35	35						80	7.10	1.14				
36	36						81	9.99	2.78	0.215			
37	37						82						
38	38						83	8.72	3.53	1.75	0.040		
39	39						84						
40	40						85	16.5	4.89	1.85	0.620		
41	41						86						
42	42						87	29.9	9.45	2.31	0.850	0.070	
43	43						88						
44	44						89	49.5	12.4	3.63	1.35	0.145	
45	45						90						

DATE 21 August 1956  
TIME 1100-1110 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 49

POST NO.	ARC					POST NO.	ARC								
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91		67.1	17.9	5.15	1.15	0.065		136						
	92						0.075		69	137	0.605				
47	93	54.0	18.8	4.48	0.755	0.110			136						
	94					0.115			70	139					
48	95	68.7	21.2	3.99	0.285	0.080			140						
	96					0.095			71	141					
49	97	101	21.5	3.92	0.505	0.115			142						
	98					0.085			72	143					
50	99	128	26.0	5.08	0.945	0.155			144						
	100					0.175			73	145					
51	101	140	35.1	3.35	1.83	0.270			146						
	102					0.275			74	147					
52	103	155	38.6	10.5	2.28	0.415			148						
	104					0.535			75	149					
53	105	164	44.3	10.8	2.55	0.515			150						
	106					0.545			76	151					
54	107	173	57.3	11.8	2.21	0.525			152						
	108					0.585			77	153					
55	109	189	60.0	15.4	2.62	0.625			154						
	110					0.535			78	155					
56	111	201	66.8	15.0	3.00	0.465			156						
	112					0.525			79	157					
57	113	209	65.1	18.7	3.32	0.575			158						
	114					0.555			80	159					
58	115	200	57.3	15.8	2.48	0.455			160						
	116					0.535			81	161					
59	117	161	38.9	10.9	2.25	0.445			162						
	118					0.320			82	163					
60	119	121	34.2	9.38	1.46	0.300			164						
	120					0.300			83	165					
61	121	105	26.7	6.58	1.50	0.225			166						
	122					0.215			84	167					
62	123	71.7	18.6	3.37	1.09	0.205			168						
	124					0.135			85	169					
63	125	56.6	13.8	2.74	0.645	0.065			170						
	126					0.035			86	171					
64	127	37.7	9.33	2.84	0.360	0.035			172						
	128					0.035			87	173					
65	129	20.0	4.59	1.46	0.175	0.030			174						
	130								88	175					
66	131	9.42	0.970	0.565	0.075				176						
	132								89	177					
67	133	6.33	0.285	0.095					178						
	134								90	179					
68	135	2.90	0.075						180						
									91	181					

DATE 21 August 1956  
TIME 1400-1410 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 50

POST NO.	ARC					POST NO.	ARC								
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91								136						0.440
	92								69	137	107	31.7	7.69	2.46	0.360
47	93	0.060							138						0.350
	94								70	139	73.1	20.0	3.45	1.04	0.300
48	95	0.580							140						0.190
	96								71	141	42.2	10.1	1.62	0.375	0.130
49	97	3.20							142						0.085
	98								72	143	27.0	5.31	0.680	0.045	0.045
50	99	14.2	0.075						144						
	100								73	145	24.8	1.20	0.055		
51	101	19.2	0.450	0.025					146						
	102								74	147	9.62	0.180			
52	103	17.1	2.00	0.140					148						
	104								75	149	4.32	0.150			
53	105	22.8	4.23	0.260	0.015				150						
	106								76	151	3.45	0.050			
54	107	25.4	7.52	0.370	0.050				152						
	108								77	153	2.43				
55	109	45.5	9.72	1.95	0.040				154						
	110					0.045			78	155	0.790				
56	111	66.0	15.9	3.45	0.190	0.075			156						
	112					0.080			79	157	0.345				
57	113	88.5	25.7	4.76	1.12	0.195			158						
	114					0.280			80	159	0.050				
58	115	112	30.9	7.12	1.94	0.280			160						
	116					0.285			81	161					
59	117	136	32.7	8.55	1.92	0.255			162						
	118					0.215			82	163					
60	119	156	42.8	7.98	1.62	0.190			164						
	120					0.160			83	165					
61	121	159	46.1	7.46	1.37	0.145			166						
	122					0.150			84	167					
62	123	165	42.8	M	1.65	0.150			168						
	124					0.160			85	169					
63	125	201	47.0	7.56	1.88	0.180			170						
	126					0.255			86	171					
64	127	231	51.2	9.76	2.30	0.370			172						
	128					0.340			87	173					
65	129	243	64.7	14.3	2.12	0.310			174						
	130					0.390			88	175					
66	131	237	77.0	18.3	2.74	0.450			176						
	132					0.490			89	177					
67	133	227	72.5	15.0	3.63	0.450			178						
	134					0.600			90	179					
68	135	162	55.2	14.3	3.83	0.470			180						
									91	181					

DATE 21 AUGUST 1956  
TIME 1530-1540 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 51

Table 5.2 (Continued)

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
46	91					69	136							0.045
92						137	80.6	25.5	1.98	0.520	0.135			
47	93					138					0.135			
94						70	139	84.9	30.8	4.70	0.760	0.230		
48	95	0.025				140					0.225			
96						71	141	80.3	22.2	5.45	1.13	0.185		
49	97	0.040				142					0.180			
98						72	143	60.6	14.8	4.60	1.03	0.145		
99						144					0.210			
50	100	0.060				73	145	71.6	14.2	3.97	0.860	0.210		
51	101	0.085				146					0.135			
102						74	147	99.3	17.1	4.68	1.21	0.155		
52	103	0.095				148					0.210			
104						75	149	150	27.3	5.61	1.80	0.300		
53	105	0.065				150					0.315			
106						76	151	201	47.3	9.33	2.47	0.410		
54	107	0.090				152					0.450			
108						77	153	227	68.7	12.7	3.12	0.430		
55	109	0.105				154					0.410			
110						78	155	246	71.0	18.4	2.72	0.285		
56	111	0.155				156					0.285			
112						79	157	267	68.1	18.6	2.97	0.240		
57	113	0.205				158					0.185			
114						80	159	219	70.2	15.3	2.10	0.230		
58	115	1.14				160					0.290			
116						81	161	191	55.7	10.6	1.43	0.320		
59	117	2.61				162					0.155			
118						82	163	155	39.5	6.33	1.66	0.120		
60	119	3.48				164					0.205			
120						83	165	119	34.7	9.33	2.81	0.035		
61	121	4.28				166								
122						84	167	97.2	34.1	8.40	1.53			
62	123	5.48	0.110			168								
124						85	169	75.3	23.3	5.35	0.730			
63	125	8.19	1.74			170								
126						86	171	62.7	14.6	3.29	0.045			
64	127	11.7	3.54			172								
128						87	173	38.0	9.39	2.16				
65	129	17.0	4.01	0.155		174								
130						88	175	27.6	6.09	0.650				
66	131	36.3	3.89	1.14	0.010	176								
132						89	177	14.4	4.98	0.080				
67	133	54.6	7.07	1.68	0.205	178								
134						90	179	9.39	3.02					
68	135	91.1	16.8	1.55	0.400	180								
						91	181	8.61	0.450					

DATE 24 August 1956  
TIME 1117-1127 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 52

Table 5.2 (Continued)

POST NO.	ARC					POST NO.	ARC									
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m	
1	1		21.2	5.24	0.135					46				0.015		
	2									24	46	104	18.3	2.45	0.570	0.040
2	3		27.3	12.7	0.480					48				0.050		
	4									25	49	112	21.2	2.39	0.350	0.040
3	5		32.0	12.2	1.25					50				0.035		
	6									26	51	94.1	24.5	3.27	0.200	0.040
4	7		41.1	12.0	1.59					52				0.040		
	8									27	53	104	20.1	5.13	0.100	0.050
5	9		35.3	9.68	1.90					54				0.040		
	10									28	55	145	20.1	4.35	0.085	0.060
6	11		43.4	9.59	1.28					56				0.050		
	12									29	57	176	30.3	3.92	0.380	
7	13		40.8	9.78	1.63					58						
	14									30	59	168	29.0	2.68	0.360	
8	15		42.6	10.5	1.72			0.060		60				0.010		
	16							0.035		31	61	153	27.9	1.57	0.155	
9	17		45.0	11.7	1.88			0.055	0.030	62				0.035		
	18							0.025		32	63	140	18.5	0.940	0.025	0.005
10	19		45.6	9.06	1.56			0.090		64						
	20							0.020		33	65	110	8.84	0.350	0.050	
11	21		73.8	7.10	1.68			0.150		66						
	22									34	67	76.8	7.05	0.070		
12	23		92.6	9.93	1.26			0.360	0.030	68						
	24									35	69	51.2	4.53			
13	25		99.5	22.2	0.790			0.330	0.035	70						
	26							0.055		36	71	44.6	3.84			
14	27		108	29.6	0.700			0.290	0.025	72						
	28							0.035		37	73	42.6	3.15			
15	29		129	26.9	2.28			0.295		74						
	30							0.005		38	75	50.9	2.91			
16	31		137	21.2	3.71			0.420		76						
	32							0.015		39	77	43.4	1.92			
17	33		137	19.8	4.89			0.800	0.010	78						
	34							0.015		40	79	24.9	0.215			
18	35		80.3	17.9	4.81			1.05		80						
	36									41	81	7.88	0.015			
19	37		88.4	19.5	4.71			0.970	0.015	82						
	38							0.030		42	83	5.45	0.015			
20	39		73.1	21.3	5.98			0.460	0.055	84						
	40							0.060		43	85	3.23	0.010			
21	41		78.5	21.9	4.05			0.440	0.080	86						
	42							0.015		44	87	2.34				
22	43		84.0	23.1	3.14			0.450	0.015	88						
	44							0.030		45	89	0.325				
23	45		80.8	15.5	3.54			0.740	0.100	90						

DATE 24 August 1956  
TIME 2000-2010 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 53

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
2	2					47	155	4.53				
3	3					48						
4	4					49	37.8	0.115				
5	5					50						
6	6					51	2.76					
7	7					52						
8	8					53	0.035					
9	9					54						
10	10					55						
11	11					56						
12	12					57						
13	13					58						
14	14					59						
15	15					60						
16	16					61						
17	17					62						
18	18					63						
19	19					64						
20	20					65						
21	21					66						
22	22					67						
23	23					68						
24	24					69						
25	25					70						
26	26					71						
27	27	0.110				72						
28	28					73						
29	29	2.60				74						
30	30					75						
31	31	23.1	0.710	0.050		76						
32	32					77						
33	33	109	16.7	0.775	0.035	78						
34	34					79						
35	35	218	102	21.0	0.925	80						
36	36				0.150	81						
37	37	608	305	115	31.7	82						
38	38				4.41	83						
39	39				24.7	84						
40	40	786	534	233	86.2	85						
41	41	923	488	162	50.3	86						
42	42				12.8	87						
43	43	755	258	28.4	3.48	88						
44	44				0.210	89						
45	45	410	47.1	0.955	0.025	90						

DATE 24 August 1956  
TIME 2200-2210 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 54

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						3.60
2	2					47						7.92
3	3					48						9.51
4	4					49						6.62
5	5					50						2.64
6	6					51						0.800
7	7					52						0.050
8	8					53						0.070
9	9					54						0.080
10	10					55						0.085
11	11					56						0.015
12	12					57						0.070
13	13					58						0.070
14	14					59						
15	15					60						
16	16					61						
17	17					62						
18	18					63						0.070
19	19					64						
20	20					65						
21	21					66						
22	22					67						
23	23					68						
24	24					69						
25	25					70						
26	26					71						
27	27					72						
28	28					73						
29	29					74						
30	30					75						
31	31					76						
32	32					77						
33	33	0.240				78						
34	34					79						
35	35	0.780				80						
36	36					81						
37	37	6.81	0.190	0.135		82						
38	38					83						
39	39	29.1	2.04	0.180		84						
40	40					85						
41	41	80.1	13.8	1.11	0.050	86						
42	42					87						
43	43	152	44.4	8.01	0.880	88						0.040
44	44					89						0.155
45	45	261	99.3	32.2	7.12	90						1.04



DATE 25 August 1956  
TIME 0100-0110 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.55

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						
2	2						24	47	0.485	0.010			
3	3						48						
4	4						25	49	0.635	0.020			
5	5						50						
6	6						26	51	2.45	0.030			
7	7						52						
8	8						27	53	8.16	0.190			
9	9						54						
10	10						28	55	20.6	1.01	0.035		
11	11						56						
12	12						29	57	44.7	5.49	0.430		
13	13						58						
14	14						30	59	86.9	18.5	2.53	0.345	0.025
15	15						60						0.115
16	16						31	61	145	44.7	13.4	2.10	0.365
17	17						62						0.885
18	18						32	63	182	66.8	22.4	5.54	1.85
19	19						64						2.49
20	20						33	65	219	84.2	27.2	7.83	2.83
21	21						66						2.39
22	22						34	67	218	82.7	26.3	7.35	1.81
23	23						68						1.19
24	24						35	69	192	65.6	18.7	3.45	0.615
25	25						70						0.275
26	26						36	71	156	38.0	6.09	0.860	0.085
27	27						72						0.020
28	28						37	73	97.2	14.9	1.36	0.046	
29	29						74						
30	30						38	75	50.1	4.04	0.335		
31	31						76						
32	32						39	77	14.3	0.805	0.090		
33	33						78						
34	34						40	79	1.61	0.300			
35	35						80						
36	36						41	81	0.580	0.080			
37	37						82						
38	38						42	83	0.160				
39	39						84						
40	40						43	85	0.050				
41	41						86						
42	42						44	87					
43	43						88						
44	44						45	89					
45	45	0.330					90						

DATE 25 August 1956  
TIME 0300-0310 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.56

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						
2	2						24	47	0.335	0.130			
3	3						48						
4	4						25	49	2.90	0.155	0.020		
5	5						50						
6	6						26	51	8.55	0.405	0.035		
7	7						52						
8	8						27	53	33.0	3.50	0.245		
9	9						54						
10	10						28	55	77.9	14.1	2.13	0.055	
11	11						56						
12	12						29	57	156	40.5	9.01	1.18	0.050
13	13						58						0.195
14	14						30	59	216	74.0	22.7	4.90	0.745
15	15						60						2.08
16	16						31	61	284	110	33.0	11.3	3.78
17	17						62						4.50
18	18						32	63	308	110	36.3	12.6	4.74
19	19						64						4.20
20	20						33	65	279	91.7	28.7	8.46	2.48
21	21						66						0.905
22	22						34	67	218	70.2	16.7	2.89	0.230
23	23						68						0.075
24	24						35	69	147	36.9	5.58	0.510	0.025
25	25						70						
26	26						36	71	92.7	13.0	0.915	0.030	
27	27						72						
28	28						37	73	41.3	2.81	0.095	0.010	
29	29						74						
30	30						38	75	10.8	0.370			
31	31						76						
32	32						39	77	2.40				
33	33						78						
34	34						40	79	0.310				
35	35						80						
36	36						41	81					
37	37						82						
38	38						42	83					
39	39						84						
40	40						43	85					
41	41						86						
42	42						44	87					
43	43						88						
44	44						45	89					
45	45	0.200	0.120				90						

DATE 25 August 1956  
TIME 1730-1740 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 57

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
2	2					24	47					
3	3					48						
4	4					25	49					
5	5					50						
6	6					26	51					
7	7					52						
8	8					27	53					
9	9					54						
10	10					28	55					
11	11					56						
12	12					29	57					
13	13					58						
14	14					30	59					
15	15					60						
16	16					31	61					
17	17					62						
18	18					32	63					
19	19					64						
20	20					33	65					
21	21					66						
22	22					34	67					
23	23					68						
24	24					35	69					
25	25					70						
26	26					36	71					
27	27					72						
28	28					37	73					
29	29					74						
30	30					38	75					
31	31					76						
32	32					39	77	0.145				
33	33					78						
34	34					40	79	0.260				
35	35					80						
36	36					41	81	0.550				
37	37					82						
38	38					42	83	2.31				
39	39					84						
40	40					43	85	3.27				
41	41					86						
42	42					44	87	5.69	0.145			
43	43					88						
44	44					45	89	6.68	0.550			
45	45					90						

DATE 25 August 1956  
TIME 1730-1740 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 57

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	15.6	2.96	0.590			136					
47	92						69	0.060				
48	93	32.7	M	1.41	0.020		137					
49	94						70	139				
50	95	58.5	9.00	4.19	0.520		140					
51	96						71	141				
52	97	81.9	15.3	5.04	1.37		72	142				
53	98						73	143				
54	99	132	29.1	7.35	1.53	0.110	74	144				
55	100					0.335	75	145				
56	101	171	44.7	11.0	2.49	0.690	76	146				
57	102					0.740	77	147				
58	103	224	57.8	18.2	3.60	0.910	78	148				
59	104					1.13	79	149				
60	105	270	74.6	30.0	6.16	1.25	80	150				
61	106					1.79	81	151				
62	107	282	79.4	29.2	8.82	1.96	82	152				
63	108					2.27	83	153				
64	109	281	75.3	26.4	7.33	1.93	84	154				
65	110					1.33	85	155				
66	111	243	59.6	20.4	4.40	0.910	86	156				
67	112					0.730	87	157				
68	113	201	51.6	17.5	3.36	0.590	88	158				
69	114					0.590	89	159				
70	115	159	47.9	12.6	2.78	0.630	90	160				
71	116					0.640	91	161				
72	117	142	37.2	12.6	2.94	0.820	92	162				
73	118					0.930	93	163				
74	119	118	28.7	8.61	2.73	0.660	94	164				
75	120					0.460	95	165				
76	121	86.7	17.7	5.27	2.16	0.320	96	166				
77	122					0.100	97	167				
78	123	54.0	8.70	4.28	1.19		98	168				
79	124						99	169				
80	125	42.2	7.37	2.54	0.250		100	170				
81	126						101	171				
82	127	24.6	4.47	0.510	0.045		102	172				
83	128						103	173				
84	129	10.7	1.37	0.035	0.020		104	174				
85	130						105	175				
86	131	4.82	1.28	0.020			106	176				
87	132						107	177				
88	133	0.850	0.030				108	178				
89	134						109	179				
90	135	0.165					110	180				
91	136						111	181				

DATE 25 August 1956  
TIME 1930-1940 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.58

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
	2					24	47					
2	3					48						
	4					25	49					
3	5					50						
	6					26	51					
4	7					52						
	8					27	53					
5	9					54						
	10					28	55					
6	11					56						
	12					29	57					
7	13					58						
	14					30	59					
8	15					60						
	16					31	61					
9	17					62						
	18					32	63					
10	19					64						
	20					33	65					
11	21					66						
	22					34	67					
12	23					68						
	24					35	69					
13	25					70						
	26					36	71					
14	27					72						
	28					37	73					
15	29					74						
	30					38	75					
16	31					76						
	32					39	77					
17	33					78						
	34					40	79	0.020				
18	35					80						
	36					41	81	0.560				
19	37					82						
	38					42	83	6.68				
20	39					84						
	40					43	85	60.2	2.96	0.035		
21	41					86					0.040	
	42					44	87	279	48.9	4.34	0.800	3.10
22	43					88					24.5	
	44					45	89	557	293	80.9	43.8	59.4
23	45					90					48.2	

DATE 25 August 1956  
TIME 1930 - 1940 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.58

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	1000	660	311	140	12.0						136
	92					0.215	69	137				
47	93	794	575	221	27.1							138
	94						70	139				
48	95	633	318	37.9	0.090							140
	96						71	141				
49	97	410	52.1	0.550								142
	98						72	143				
50	99	150	2.93	0.020								144
	100						73	145				
51	101	21.6										146
	102						74	147				
52	103	1.10										148
	104						75	149				
53	105	0.090										150
	106						76	151				
54	107											152
	108						77	153				
55	109											154
	110						78	155				
56	111											156
	112						79	157				
57	113											158
	114						80	159				
58	115											160
	116						81	161				
59	117											162
	118						82	163				
60	119											164
	120						83	165				
61	121											166
	122						84	167				
62	123											168
	124						85	169				
63	125											170
	126						86	171				
64	127											172
	128						87	173				
65	129											174
	130						88	175				
66	131											176
	132						89	177				
67	133											178
	134						90	179				
68	135											180
							91	181				

DATE 25 August 1956  
TIME 2230-2240 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 59

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					46						
2	2					24	47					
3	3					48						
4	4					25	49					
5	5					50						
6	6					26	51					
7	7					52						
8	8					27	53					
9	9					54						
10	10					28	55					
11	11					56						
12	12					29	57					
13	13					58						
14	14					30	59					
15	15					60						
16	16					31	61					
17	17					62						
18	18					32	63					
19	19					64						
20	20					33	65					
21	21					66						
22	22					34	67					
23	23					68						
24	24					35	69	0.110				
25	25					70						
26	26					36	71	0.165				
27	27					72						
28	28					37	73	0.330				
29	29					74						
30	30					38	75	1.36				
31	31					76						
32	32					39	77	14.3	0.300			
33	33					78						
34	34					40	79	100	7.01	0.090		
35	35					80						
36	36					41	81	332	77.0	7.43	0.325	
37	37					82					0.165	
38	38					42	83	567	303	88.8	22.1	3.43
39	39					84					20.3	
40	40					43	85	723	524	239	101	39.4
41	41					86					22.3	
42	42					44	87	707	419	134	26.4	3.55
43	43					88					0.295	
44	44					45	89	552	174	22.1	0.835	0.030
23	45					90						

DATE 25 August 1956  
TIME 2230 - 2240 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 59

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	239	23.6	0.870		69	136					
47	92					137						
48	93	67.2	2.51			70	138					
49	94					139						
50	95	11.8	0.305			140						
51	96					71	141					
52	97	4.43	0.055			142						
53	98					72	143					
54	99	0.265				144						
55	100					73	145					
56	101					146						
57	102					74	147					
58	103					148						
59	104					75	149					
60	105					150						
61	106					76	151					
62	107					152						
63	108					77	153					
64	109					154						
65	110					78	155					
66	111					156						
67	112					79	157					
68	113					158						
69	114					80	159					
70	115					160						
71	116					81	161					
72	117					162						
73	118					82	163					
74	119					164						
75	120					83	165					
76	121					166						
77	122					84	167					
78	123					168						
79	124					85	169					
80	125					170						
81	126					86	171					
82	127					172						
83	128					87	173					
84	129					174						
85	130					88	175					
86	131					176						
87	132					89	177					
88	133					178						
89	134					90	179					
90	135					180						
91	181					181						

DATE 26 August 1956  
TIME 0030-0040 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 60

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						
2	2						24	47					
3	3						48						
4	4						25	49					
5	5						50						
6	6						26	51					
7	7						52						
8	8						27	53					
9	9						54						
10	10						28	55					
11	11						56						
12	12						29	57					
13	13						58						
14	14						30	59					
15	15						60						
16	16						31	61					
17	17						62						
18	18						32	63					
19	19						64						
20	20						33	65					
21	21						66						
22	22						34	67					
23	23						68						
24	24						35	69					
25	25						70						
26	26						36	71					
27	27						72						
28	28						37	73					
29	29						74						
30	30						38	75					
31	31						76						
32	32						39	77					
33	33						78						
34	34						40	79					
35	35						80						
36	36						41	81					
37	37						82						
38	38						42	83					
39	39						84						
40	40						43	85					
41	41						86						
42	42						44	87	0.015	0.010			
43	43						88						
44	44						45	89	0.045	0.070			
45	45						90						

DATE 26 August 1956  
TIME 0030 - 0040 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 60

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91	0.125	0.515				69	136					
47	92						137						
48	93	0.210	0.480				70	138					
49	94						139						
50	95	0.870	0.375	0.070			71	140					
51	96						141						
52	97	4.07	0.470	0.120			72	142					
53	98						143						
54	99	22.5	1.73	0.275			73	144					
55	100						145						
56	101	65.0	8.12	0.795	0.030		74	146					
57	102						147						
58	103	130	33.2	6.40	0.540		75	148					
59	104					0.085	149						
60	105	237	83.1	26.4	5.18	0.545	150						
61	106					1.79	76	151					
62	107	302	118	43.6	15.1	4.15	77	152					
63	108					6.07	78	153					
64	109	281	114	40.2	10.8	4.75	79	154					
65	110					2.44	80	155					
66	111	212	53.4	13.3	3.20	0.815	81	156					
67	112					0.135	82	157					
68	113	110	27.2	2.98	0.270	0.050	83	158					
69	114						84	159					
70	115	44.7	4.94	0.330			85	160					
71	116						86	161					
72	117	10.6	0.415				87	162					
73	118						88	163					
74	119	1.76	0.060				89	164					
75	120						90	165					
76	121	0.220	0.045				91	166					
77	122						92	167					
78	123	0.140					93	168					
79	124						94	169					
80	125	0.110					95	170					
81	126						96	171					
82	127						97	172					
83	128						98	173					
84	129						99	174					
85	130						100	175					
86	131						101	176					
87	132						102	177					
88	133						103	178					
89	134						104	179					
90	135						105	180					
91	136						106	181					

DATE 27 August 1956  
TIME 1100-1110 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.61

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
1	1					24	46					
2	2					47						
3	3					48						
4	4					25	49					
5	5					50						
6	6					26	51					
7	7					52						
8	8					27	53					
9	9					54						
10	10					28	55					
11	11					56						
12	12					29	57					
13	13					58						
14	14					30	59					
15	15					60						
16	16					31	61					
17	17					32	62					
18	18					33	63					
19	19					64						
20	20					33	65					
21	21					66						
22	22					34	67					
23	23					68						
24	24					35	69					
25	25					70						
26	26					36	71					
27	27					72						
28	28					37	73					
29	29					74						
30	30					38	75					
31	31					76						
32	32					39	77					
33	33					78						
34	34					40	79	0.325				
35	35					80						
36	36					41	81	4.53				
37	37					82						
38	38					42	83	9.57				
39	39					84						
40	40					43	85	18.9	0.095			
41	41					86						
42	42					44	87	20.9	1.85			
43	43					88						
44	44					45	89	19.8	4.85	0.075		
45	45					90						

DATE 27 August 1956  
TIME 1100 - 1110 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 61

POST NO.	Inner Arcs 800m arc	ARC					POST NO.	Inner Arcs 800m arc	ARC				
		50m	100m	200m	400m	800m			50m	100m	200m	400m	800m
46	91	29.3	6.36	0.870	0.025		136						
47	93	46.2	9.03	3.75	0.070		69	137	18.2	5.22	1.38	0.085	
48	95	60.9	17.3	3.34	1.04	0.030		138					
49	96					0.080	70	139	22.7	5.37	1.37		
50	97	72.9	21.8	4.08	1.15	0.125		140					
51	98					0.265	71	141	17.1	5.67	0.780		
52	99	87.3	25.4	7.13	1.89	0.390		142					
53	100					0.625	72	143	12.3	4.05	0.140		
54	101	104	32.0	9.73	3.19	0.955		144					
55	102					0.845	73	145	8.09	0.865			
56	103	133	35.3	12.2	3.39	0.685		146					
57	104					0.615	74	147	2.24	0.055			
58	105	201	41.3	12.4	3.05	0.595		148					
59	106					0.545	75	149	0.050				
60	107	161	42.6	14.5	3.16	0.555		150					
61	108					0.600	76	151	0.045				
62	109	161	48.8	16.1	3.65	0.775		152					
63	110					0.905	77	153					
64	111	159	55.7	17.3	4.33	0.955		154					
65	112					0.845	78	155					
66	113	143	54.3	15.5	3.21	0.735		156					
67	114					0.595	79	157					
68	115	148	43.8	10.4	2.31	0.510		158					
69	116					0.450	80	159					
70	117	128	39.6	9.83	2.05	0.425		160					
71	118					0.320	81	161					
72	119	106	30.0	9.23	2.36	0.420		162					
73	120					0.280	82	163					
74	121	85.4	29.4	8.42	2.09	0.230		164					
75	122					0.185	83	165					
76	123	71.1	19.5	7.39	1.11	0.180		166					
77	124					0.170	84	167					
78	125	59.0	16.7	4.93	1.05	0.085		168					
79	126					0.080	85	169					
80	127	42.5	13.3	4.83	1.10	0.080		170					
81	128					0.105	86	171					
82	129	40.2	11.7	4.26	0.925	0.145		172					
83	130					0.145	87	173					
84	131	35.6	8.87	2.66	0.665	0.135		174					
85	132					0.060	88	175					
86	133	26.1	6.08	1.50	0.480			176					
87	134						89	177					
88	135	21.3	4.67	1.29	0.445			178					
89							90	179					
90								180					
91							91	181					

DATE 27 AUGUST 1956  
TIME 1400-1410 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 62

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
46	91						69	136					
47	92						69	137	29.1	4.11	0.045		
47	93						70	138					
48	94						70	139	14.6	2.60			
48	95	0.160					71	141	7.20	0.615			
49	96						71	142					
49	97	0.780					72	143	4.05	0.390			
49	98						72	144					
50	99	2.66	0.065				73	145	3.39	0.170			
50	100						73	146					
51	101	6.89	1.03				74	147	2.24	0.095			
52	102						74	148					
52	103	14.2	3.68				75	149	1.32	0.160			
53	104						75	150					
53	105	50.1	6.03	0.245		0.015	76	151	0.380	0.105			
54	106					0.040	76	152					
54	107	99.6	15.2	1.21		0.075	77	153	0.065	0.070			
54	108					0.185	77	154					
55	109	145	28.2	3.93	0.050	0.330	78	155	0.230				
55	110					0.220	78	156					
56	111	179	49.4	8.78	0.588	0.210	79	157	0.170				
56	112					0.210	79	158					
57	113	231	76.4	16.2	1.45	0.430	80	159	0.175				
57	114					0.645	80	160					
58	115	296	88.4	21.5	3.71	0.745	81	161	0.165				
58	116					1.06	81	162					
59	117	335	113	32.9	7.33	1.45	82	163	0.180				
59	118					1.50	82	164					
60	119	378	115	33.8	8.08	1.93	83	165	0.160				
60	120					1.46	83	166					
61	121	333	98.4	31.4	7.63	1.72	84	167	0.120				
61	122					1.44	84	168					
62	123	266	81.0	25.5	7.94	1.27	85	169	0.115				
62	124					0.855	85	170					
63	125	170	67.7	16.0	7.66	0.605	86	171					
63	126					0.350	86	172					
64	127	168	45.0	9.79	1.75	0.190	87	173					
64	128					0.125	87	174					
65	129	144	31.7	5.82	0.745	0.075	88	175					
65	130					0.075	88	176					
66	131	113	16.4	2.92	0.320	0.095	89	177					
66	132					0.085	89	178					
67	133	80.3	7.01	1.79	0.050	0.075	90	179					
67	134					0.090	90	180					
68	135	54.2	6.59	0.445		0.090	91	181					

DATE 29 August 1956  
TIME 1930-1940 CST  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO. 65

POST NO.		ARC					POST NO.		ARC				
Inner Arcs	800m arc	50m	100m	200m	400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m	800m
1	1						46						
2	2						24	47					
3	3						24	48					
4	4						25	49					
5	5						26	50					
6	6						26	51					
7	7						27	52					
8	8						27	53					
9	9						28	54					
10	10						28	55					
11	11						29	56					
12	12						29	57					
13	13						30	58					
14	14						30	59	0.045				
15	15						31	60					
16	16						31	61	0.065				
17	17						32	62					
18	18						32	63	0.150				
19	19						33	64					
20	20						33	65	0.215				
21	21						34	66					
22	22						34	67	0.370				
23	23						35	68					
24	24						35	69	0.945				
25	25						36	70					
26	26						36	71	2.94	0.045			
27	27						37	72					
28	28						37	73	12.3	0.550			
29	29						38	74					
30	30						38	75	39.3	5.81	0.170		
31	31						39	76					
32	32						39	77	93.5	19.4	2.17	0.120	
33	33						40	78					0.015
34	34						40	79	174	60.9	14.8	2.37	0.290
35	35						41	80					1.47
36	36						41	81	281	116	37.8	12.7	3.42
37	37						42	82					6.12
38	38						42	83	354	153	56.2	21.1	7.02
39	39						43	84					6.08
40	40						43	85	312	118	38.7	11.4	3.32
41	41						44	86					0.925
42	42						44	87	213	63.0	13.7	1.70	0.185
43	43						45	88					0.030
44	44						45	89	118	20.3	2.09	0.095	
45	45						90						

DATE 29 August 1956  
TIME 1930-1940 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.65

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
46	91	49.4	3.90	0.145			136							
	92						69	137						
47	93	16.2	0.415					138						
	94						70	139						
48	95	2.36						140						
	96						71	141						
49	97	0.310						142						
	98						72	143						
50	99							144						
	100						73	145						
51	101							146						
	102						74	147						
52	103							148						
	104						75	149						
53	105							150						
	106						76	151						
54	107							152						
	108						77	153						
55	109							154						
	110						78	155						
56	111							156						
	112						79	157						
57	113							158						
	114						80	159						
58	115							160						
	116						81	161						
59	117							162						
	118						82	163						
60	119							164						
	120						83	165						
61	121							166						
	122						84	167						
62	123							168						
	124						85	169						
63	125							170						
	126						86	171						
64	127							172						
	128						87	173						
65	129							174						
	130						88	175						
66	131							176						
	132						89	177						
67	133							178						
	134						90	179						
68	135							180						
	136						91	181						

DATE 29 August 1956  
TIME 2130-2140 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.66

POST NO.	ARC					POST NO.	ARC							
	Inner Arcs	800m arc	50m	100m	200m		400m	800m	Inner Arcs	800m arc	50m	100m	200m	400m
1	1						46							
	2						24	47	0.430					
2	3							48						
	4						25	49	0.445					
3	5							50						
	6						26	51	0.365	0.055				
4	7							52						
	8						27	53	0.305	0.100				
5	9							54						
	10						28	55	0.280	0.205				
6	11							56						
	12						29	57	0.315	0.245				
7	13							58						
	14						30	59	0.885	0.270	0.150			
8	15							60						
	16						31	61	4.64	0.495	0.080			
9	17							62						
	18						32	63	24.9	1.64	0.555			
10	19							64						
	20						33	65	76.4	28.8	4.58	0.190		
11	21							66						
	22						34	67	158	78.9	28.1	5.85	0.025	
12	23							68						0.130
	24						35	69	159	106	45.9	17.1	1.08	
13	25							70						4.80
	26						36	71	218	82.1	29.9	13.1	7.72	
14	27							72						6.88
	28						37	73	203	60.0	19.8	6.24	5.21	
15	29							74						4.13
	30						38	75	215	64.4	20.5	7.00	2.68	
16	31							76						2.85
	32						39	77	278	98.9	31.6	11.2	3.29	
17	33							78						4.88
	34						40	79	359	155	57.7	23.2	7.50	
18	35	0.050						80						7.17
	36						41	81	390	176	66.9	19.3	2.61	
19	37	0.130						82						0.445
	38						42	83	321	138	30.0	2.86	0.035	
20	39	0.200						84						
	40						43	85	234	47.3	4.34	0.030		
21	41	0.275						86						
	42						44	87	114	9.41	0.225			
22	43	0.350						88						
	44						45	89	37.2	0.960	0.060			
23	45	0.395						90						





DATE 30 August 1956  
TIME 0030-0040 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.67

Inner Arcs	800m arc	ARC					Inner Arcs	800m arc	ARC				
		50m	100m	200m	400m	800m			50m	100m	200m	400m	800m
46	91	150	52.1	13.0	2.27	0.410	69	136					
47	93	222	78.8	25.0	8.46	2.77	70	138					
48	95	281	124	41.1	13.8	4.37	71	141					
49	97	306	126	48.3	17.3	6.10	72	143					
50	99	275	109	36.3	10.4	4.61	73	145					
51	101	186	55.2	14.8	1.78	0.120	74	147					
52	103	105	21.0	2.61	0.065		75	149					
53	105	40.8	4.55	0.195			76	151					
54	107	14.5	0.545				77	153					
55	109	3.75	0.110				78	155					
56	111	0.935	0.105				79	157					
57	113	0.165	0.235				80	159					
58	115						81	161					
59	117						82	163					
60	119						83	165					
61	121						84	167					
62	123						85	169					
63	125						86	171					
64	127						87	173					
65	129						88	175					
66	131						89	177					
67	133						90	179					
68	135						91	181					

DATE 30 August 1956  
TIME 0230-0240 CST  
Table 5.2 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)  
RUN NO.68

Inner Arcs	800m arc	ARC					Inner Arcs	800m arc	ARC				
		50m	100m	200m	400m	800m			50m	100m	200m	400m	800m
1	1						24	46					
2	2						25	48					
3	3						26	50					
4	4						27	52					
5	5						28	54					
6	6						29	56					
7	7						30	58					
8	8						31	60					
9	9						32	62					
10	10						33	64					
11	11						34	66					
12	12						35	68					
13	13						36	70					
14	14						37	72					
15	15						38	74					
16	16						39	76					
17	17						40	78					
18	18						41	80					
19	19						42	82					
20	20						43	84					
21	21						44	86					
22	22						45	88					
23	23						46	90					
24	24						47	92					
25	25						48	94					
26	26						49	96					
27	27						50	98					
28	28						51	100					
29	29						52	102					
30	30						53	104					
31	31						54	106					
32	32						55	108					
33	33						56	110					
34	34						57	112					
35	35						58	114					
36	36						59	116					
37	37						60	118					
38	38						61	120					
39	39						62	122					
40	40						63	124					
41	41						64	126					
42	42						65	128					
43	43						66	130					
44	44						67	132					
45	45						68	134					
46	46						69	136					
47	47						70	138					
48	48						71	140					
49	49						72	142					
50	50						73	144					
51	51						74	146					
52	52						75	148					
53	53						76	150					
54	54						77	152					
55	55						78	154					
56	56						79	156					
57	57						80	158					
58	58						81	160					
59	59						82	162					
60	60						83	164					
61	61						84	166					
62	62						85	168					
63	63						86	170					
64	64						87	172					
65	65						88	174					
66	66						89	176					
67	67						90	178					
68	68						91	180					
69	69						92	182					
70	70						93	184					
71	71						94	186					
72	72						95	188					
73	73						96	190					
74	74						97	192					
75	75						98	194					
76	76						99	196					
77	77						100	198					
78	78						101	200					
79	79						102	202					
80	80						103	204					
81	81						104	206					
82	82						105	208					
83	83						106	210					
84	84						107	212					
85	85						108	214					
86	86						109	216					
87	87						110	218					
88	88						111	220					
89	89						112	222					
90	90						113	224					
91	91						114	226					
92	92						115	228					
93	93						116	230					
94	94						117	232					
95	95						118	234					
96	96						119	236					
97	97						120	238					
98	98						121	240					
99	99						122	242					
100	100						123	244					
101	101						124	246					
102	102						125	248					
103	103						126	250					
104	104						127	252					
105	105						128	254					
106	106						129	256					
107	107						130	258					
108	108						131	260					
109	109						132	262					
110	110						133	264					
111	111						134	266					
112	112						135	268					
113	113						136	270					
114	114						137	272					
115	115						138	274					
116	116						139	276					
117	117						140	278					
118	118						141	280					
119	119						142	282					
120	120						143	284					
121	121						144	286					
122	122						145	288					
123	123						146	290					
124	124						147	292					
125	125						148	294					
126	126						149	296					
127	127						150	298					
128	128						151	300					
129	129						152	302					
130	130												

DATE 30 August 1956  
 TIME 0230-0240 CST  
 Table 5.2 (Continued)  
 CONCENTRATION (mg m<sup>-3</sup>) RUN NO. 68

POST NO.	ARC					POST NO.	ARC					
	Inner Arcs 800m arc	50m	100m	200m	400m		800m	Inner Arcs 800m arc	50m	100m	200m	400m
46	91	146	23.4	4.45	0.935							
	92					69	136					
47	93	57.0	3.60	0.220	0.015		137					
	94					70	138					
48	95	14.6	0.355	0.020			139					
	96					71	140					
49	97	3.11					141					
	98					72	142					
50	99	0.390					143					
	100					73	144					
51	101						145					
	102					74	146					
52	103						147					
	104					75	148					
53	105						149					
	106					76	150					
54	107						151					
	108					77	152					
55	109						153					
	110					78	154					
56	111						155					
	112					79	156					
57	113						157					
	114					80	158					
58	115						159					
	116					81	160					
59	117						161					
	118					82	162					
60	119						163					
	120					83	164					
61	121						165					
	122					84	166					
62	123						167					
	124					85	168					
63	125						169					
	126					86	170					
64	127						171					
	128					87	172					
65	129						173					
	130					88	174					
66	131						175					
	132					89	176					
67	133						177					
	134					90	178					
68	135						179					
						91	180					
							181					

Table 5.3

Ten-minute average gas concentrations measured along the vertical during Project Prairie Grass; entries are in units of mg m<sup>-3</sup>. Samplers were located at nine levels on each of six towers positioned along the 100-m arc of the horizontal sampling network. Individual towers were located equidistant between the pairs of fence posts listed below:

TOWER NO.	POST NOS.
1	28-29
2	35-36
3	42-43
4	49-50
5	56-57
6	63-64

Remarks

The vertical sampling network was first placed in operation during Run No. 13 on 22 July 1956. No data are available for Runs No. 23, 28, 35, 53, 63, and 64. All towers were outside the time-mean plume during Runs No. 23, 35, and 53. The letter "M" indicates missing data, and blank spaces in the table signify no measurable concentration. The value of the concentration at the 0.5-m level on Tower No. 4 for Run No. 13 was estimated.

Table 5.3 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

Tower No.	Height (m)	Run No.									
		13	14	15	16	17	18	19	20	21	
1	17.5							0.250			
	13.5							1.43			
	10.5							2.42			
	7.5							3.09			
	4.5							3.80			
	2.5							5.91			
	0.5							7.34			
2	17.5				0.025			3.12	0.130		
	13.5				0.045			5.40	0.385		
	10.5				0.140			7.11	0.975		
	7.5				0.275			14.2	3.26		
	4.5		0.175		0.055			25.1	7.58		
	2.5		8.34		0.035			35.0	11.9		
	0.5		23.0		0.095			40.7	13.1		
3	17.5			0.280	0.085	8.87	0.280		1.07	0.440	0.090
	13.5			0.580	6.57	M			3.89	2.01	0.720
	10.5			0.330	0.175	6.56	6.09		8.21	5.19	4.29
	7.5			0.170	10.9	18.9		0.250	15.9	13.3	15.3
	4.5			2.22	0.360	18.9	55.4	2.04	29.8	26.1	42.9
	2.5			76.2	0.245	25.4	92.6	5.16	41.4	39.9	70.8
	0.5			42.9	174	0.285	28.5	115	6.02	M	45.6
4	17.5			0.415	2.84	13.6		0.085	0.030	1.29	
	13.5			1.46	4.16	16.5	0.040	1.23	0.095	3.33	
	10.5			0.095	7.46	15.9	0.130	2.76	0.215	5.87	0.080
	7.5			0.090	7.29	17.1	0.580	3.59	0.726	7.52	0.255
	4.5			0.070	9.24	22.8	2.66	41.0	1.25	10.7	0.585
	2.5		28.7	0.860	11.3	23.4	3.45	101	1.47	14.1	0.835
	0.5		239	1.97	10.6	23.1	3.66	135	1.31	15.9	1.05
5	17.5			0.070	5.21	1.55					
	13.5				11.8	2.73					
	10.5				19.2	3.81					
	7.5				30.2	7.37					
	4.5			0.100	58.8	9.17					
	2.5		1.14	0.540	74.7	8.56					
	0.5		83.3	1.56	83.1	10.4					
6	17.5			0.145	4.67	1.53					
	13.5			0.105	8.22	2.44					
	10.5			0.090	8.39	7.10					
	7.5				14.5	11.0					
	4.5				19.8	12.1					
	2.5			0.100	29.0	14.3					
	0.5			0.085	36.3	13.7					

\*ESTIMATED VALUE

Table 5.3 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

Tower No.	Height (m)	Run No.									
		22	24	25	26	27	29	30	31	32	
1	17.5			0.110	0.195						
	13.5			1.00	0.650						
	10.5			3.71	0.230						
	7.5			10.7	0.630						
	4.5			25.8	0.565						
	2.5			38.9	0.525						
	0.5			44.3	0.970						
2	17.5	0.040		6.51	0.015	0.005					
	13.5	0.080		5.61	0.035	0.150					
	10.5	0.130		11.5	0.065	0.225					
	7.5	0.225		15.5	0.170	0.370					
	4.5	0.325		17.9	0.130	0.580					
	2.5	0.215		20.3	0.035	3.92					0.150
	0.5	0.340		20.7	0.035	5.37					0.190
3	17.5	0.200		10.4	1.20	1.68				1.09	
	13.5	1.33		14.0	3.24	4.40				2.22	
	10.5	4.31		21.3	6.20	7.05				3.56	
	7.5	12.6		24.2	7.85	16.8				5.16	0.375
	4.5	33.6		28.2	15.3	30.9				7.98	38.1
	2.5	60.8		29.6	22.2	44.6				10.6	330
	0.5	86.9		28.7	25.2	54.6				10.4	651
4	17.5			3.38	0.920	1.33				1.16	
	13.5			6.35	2.39	M				4.17	
	10.5			7.94	3.54	M				7.11	
	7.5			8.90	10.2	12.8				15.0	
	4.5			9.32	22.4	25.8				23.1	
	2.5			15.9	35.6	39.3				29.3	0.055
	0.5			19.1	44.1	44.7				32.4	0.200
5	17.5			1.64	0.400	0.145				1.36	
	13.5			2.30	1.16	M				2.22	
	10.5			2.01	1.94	M	0.120			6.11	
	7.5			7.38	4.37	2.34	1.07			14.3	0.150
	4.5			9.74	7.59	2.55	5.36			28.5	0.705
	2.5			13.0	11.7	2.55	8.89			39.2	2.90
	0.5			13.4	15.5	2.84	11.9			46.4	4.64
6	17.5			2.00	0.115	M				1.91	
	13.5			4.04	0.045	M	0.095			4.56	
	10.5			5.69	0.040	M	0.110			8.19	
	7.5			8.15	0.695	M	0.895			13.8	
	4.5			13.4	1.45	M	2.72			21.5	
	2.5			20.1	2.51	M	57.6			4.43	32.7
	0.5			29.3	2.85	M	67.7			5.64	33.8

Table 5.3 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

Tower No.	Height (m)	Run No.								
		33	34	35	36	37	38	39	40	41
1	17.5		1.59					0.335		
	13.5		2.40	0.070				1.76		
	10.5		5.88	1.04				28.2		
	7.5		17.4	3.92				8.91		
	4.5		38.1	16.8				11.3		
	2.5		59.3	30.2				61.8		
	1.5		69.7	36.2				67.1		
	1.0		73.2	38.7				66.3		
	0.5		78.6	41.3						
2	17.5		0.085							
	13.5	0.045	0.730				0.035			
	10.5	0.175	2.60				0.180			
	7.5	0.310	4.38		0.590		0.815			
	4.5	0.530	6.98		54.8		2.15			
	2.5	1.50	8.10		296		2.13			
	1.5	1.67	8.78		492		2.36			
	1.0	1.70	9.08		584		2.36			
	0.5	1.19	8.94		660		2.43			
3	17.5	0.295					0.055		0.005	
	13.5	1.10					0.580		0.150	
	10.5	2.00				0.315	2.55		1.88	
	7.5	5.19				0.880	8.99		12.7	
	4.5	8.36				1.94	29.1		38.1	
	2.5	13.3				2.96	49.7		67.7	
	1.5	16.5				3.18	58.1		86.0	
	1.0	18.9				3.18	61.8		95.1	
	0.5	20.0				3.27	61.4		104	
4	17.5	0.710				0.180				
	13.5	2.56				0.710				
	10.5	6.81						0.610		
	7.5	15.9				13.0		4.65	0.020	
	4.5	35.3				35.4		22.4	0.420	
	2.5	56.1				57.2		47.4	0.510	
	1.5	64.7				64.8		59.9	0.780	
	1.0	69.0				71.9		65.4	0.660	
	0.5	73.2				75.6		68.3	0.780	
5	17.5									
	13.5									
	10.5	0.045							0.585	
	7.5	0.195							3.45	
	4.5	0.260				0.065			17.1	
	2.5	0.350				0.110			31.5	
	1.5	0.260				0.110			36.3	
	1.0	0.200				0.070			36.5	
	0.5	0.190				0.075			36.8	
6	17.5									
	13.5									
	10.5									
	7.5									
	4.5									
	2.5									
	1.5									
	1.0									
	0.5									

Table 5.3 (Continued)  
CONCENTRATION (mg m<sup>-3</sup>)

Tower No.	Height (m)	Run No.								
		42	43	44	45	46	47	48	48	49
1	17.5		0.630	1.01						
	13.5		2.42	3.54	0.340	0.135				
	10.5		3.95	7.08	0.440	0.730				
	7.5		5.04	13.1	0.670	3.66				
	4.5		5.87	17.6	1.91	12.6				
	2.5		6.05	22.5	1.58	24.2				
	1.5		5.97	25.1	1.44	32.1				
	1.0		6.29	27.2	1.45	37.7				
	0.5		6.57	29.7	1.64	41.0				
2	17.5		2.27	0.600	0.135				0.950	
	13.5		5.49	3.03	1.32				0.740	
	10.5		8.85	6.02	4.50				1.27	
	7.5		13.8	11.6	14.0				1.91	
	4.5		17.0	24.2	41.3	0.020			2.00	
	2.5		18.3	36.0	75.5	0.035			2.37	
	1.5		19.5	43.2	96.9	0.045			2.42	
	1.0		21.2	48.2	107	0.035			2.46	
	0.5		21.5	48.5	113	0.060			2.13	
3	17.5		2.88	1.37	0.355				7.50	0.020
	13.5		6.38	1.89	0.835				9.05	0.055
	10.5		11.4	4.71	1.50				9.71	0.040
	7.5		19.5	8.27	4.67				11.8	0.345
	4.5		38.5	12.7	12.5				11.4	1.10
	2.5		51.9	14.7	19.7				11.8	2.96
	1.5		54.6	15.0	24.2				10.7	3.99
	1.0		57.8	14.9	26.0				10.9	4.88
	0.5		60.6	14.6	27.0				11.3	5.07
4	17.5		0.150	0.160					3.35	0.630
	13.5		0.930	0.320					4.01	1.71
	10.5		2.49	0.270					4.59	4.85
	7.5		4.61	0.070					3.75	9.42
	4.5		12.8	0.015					4.41	17.6
	2.5		19.2	0.020					3.33	21.8
	1.5		23.0	0.035					3.36	24.3
	1.0		24.2	0.015					3.24	25.1
	0.5		25.1	0.050					3.24	24.8
5	17.5								5.42	0.070
	13.5		0.185						4.95	0.580
	10.5		1.32						5.42	1.74
	7.5		3.06						6.36	4.76
	4.5		8.28						6.18	7.10
	2.5		12.9						8.73	9.15
	1.5		15.5						8.43	10.6
	1.0		15.9						8.31	10.8
	0.5		16.4						8.69	11.3
6	17.5		0.050						0.065	6.32
	13.5		0.345						0.375	6.65
	10.5		1.86						0.460	6.41
	7.5		7.13						0.865	6.56
	4.5		18.9						0.530	4.19
	2.5		32.9						0.155	5.18
	1.5		37.4						0.260	5.70
	1.0		39.5						0.440	6.06
	0.5		43.1						0.410	6.32

Table 5.3 (Continued)  
CONCENTRATION (ng m<sup>-3</sup>)

Tower No.	Height (m)	Run No.								
		50	51	52	54	55	56	57	58	59
1	17.5			6.29						
	13.5			10.9		0.025	0.250			
	10.5			15.2	0.125	0.339	1.28			
	7.5			17.5	0.945	1.14	6.05			
	4.5			22.1	2.84	2.40	13.8			
	2.5			25.2	6.78	3.29	16.2			
	1.5			24.9	6.63	3.26	26.3			
	1.0			25.5	7.10	3.30	26.9			
	0.5			24.3	7.10	3.00	27.3			
2	17.5			1.10		0.200	0.030			
	13.5			1.58		1.07	0.160			
	10.5			1.64		3.86	1.43			
	7.5			4.50		10.4	5.24			
	4.5			5.28		25.0	12.5			
	2.5			5.54		44.4	19.7			
	1.5			3.48		54.0	23.1			
	1.0			3.48		58.4	23.7			
	0.5			4.55		60.5	20.7			
3	17.5									
	13.5									
	10.5									1.40
	7.5									0.225
	4.5									47.6
	2.5									0.500
	1.5									0.420
	1.0									0.295
	0.5									0.235
4	17.5									0.175
	13.5									1.62
	10.5									3.56
	7.5									6.81
	4.5									14.6
	2.5									21.5
	1.5									27.6
	1.0									31.1
	0.5									32.7
5	17.5		0.840							0.795
	13.5		2.81							2.33
	10.5		5.86							6.27
	7.5		8.70							15.0
	4.5		13.4							35.6
	2.5		18.3							55.5
	1.5		20.7							87.1
	1.0		20.9							69.3
	0.5		21.3							72.6
6	17.5		0.700							0.055
	13.5		2.13							0.455
	10.5		6.39	0.320						0.090
	7.5		15.2	0.805						1.76
	4.5		29.1	2.27						3.12
	2.5		41.1	2.68						7.16
	1.5		46.4	2.78						8.19
	1.0		49.1	2.75						8.70
	0.5		53.4	2.69						9.18

Table 5.3 (Continued)  
CONCENTRATION (ng m<sup>-3</sup>)

Tower No.	Height (m)	Run No.								
		60	61	62	65	66	67	68		
1	17.5									
	13.5									
	10.5									
	7.5									
	4.5									0.065
	2.5									0.230
	1.5									0.185
	1.0									0.225
	0.5									0.210
2	17.5									
	13.5									
	10.5									
	7.5									2.04
	4.5									0.115
	2.5									25.5
	1.5									76.5
	1.0									106
	0.5									118
3	17.5									
	13.5									
	10.5									0.020
	7.5									0.220
	4.5									4.80
	2.5									0.205
	1.5									0.205
	1.0									0.300
	0.5									0.250
4	17.5									0.925
	13.5									4.80
	10.5									3.21
	7.5									0.120
	4.5									7.23
	2.5									64.2
	1.5									30.0
	1.0									0.275
	0.5									71.7
5	17.5									0.070
	13.5									120
	10.5									73.5
	7.5									0.805
	4.5									200
	2.5									145
	1.5									93.9
	1.0									0.855
	0.5									281
6	17.5									158
	13.5									100
	10.5									0.955
	7.5									330
	4.5									164
	2.5									103
	1.5									1.17
	1.0									362
	0.5									
7	17.5									0.245
	13.5									0.025
	10.5									0.400
	7.5									1.62
	4.5									0.065
	2.5									4.37
	1.5									0.080
	1.0									9.29
	0.5									0.145
8	17.5									0.745
	13.5									22.1
	10.5									0.985
	7.5									23.7
	4.5									0.940
	2.5									23.4
	1.5									23.4
	1.0									129
	0.5									143
9	17.5									0.005
	13.5									0.165
	10.5									2.09
	7.5									4.80
	4.5									0.705
	2.5									4.83
	1.5									1.97
	1.0									2.69
	0.5									9.53
10	17.5									8.00
	13.5									8.63
	10.5									15.6
	7.5									23.0
	4.5									25.2
	2.5									21.8
	1.5									38.3
	1.0									42.9
	0.5									50.1
11	17.5									47.4
	13.5									54.0
	10.5									60.9
	7.5									54.0
	4.5									59.3
	2.5									67.7
	1.5									49.7
	1.0									M
	0.5									71.9
12	17.5									0.070
	13.5									5.46
	10.5									0.200
	7.5									8.89
	4.5									0.950
	2.5									14.6
	1.5									2.16
	1.0									21.0
	0.5									7.61
13	17.5									37.5
	13.5									13.5
	10.5									57.6
	7.5									14.7
	4.5									61.8
	2.5									15.5
	1.5									61.8
	1.0									17.0
	0.5									63.0

Table 5.4. Correction factors by which concentration data presented in Tables 5.2 and 5.3 should be multiplied to compensate for evaporational loss of impinger solution during aspiration. Tower data corrections are the same as those for the 100-m arc. Blank spaces signify missing data.

RUNNO.	ARC (m)				
	50	100	200	400	800
1	0.97	0.96	0.90	0.93	0.96
2			0.92	0.93	0.96
3	0.99	1.00	0.99	0.98	1.00
4	0.98	0.99	0.98	0.99	1.00
5	0.93	0.93	0.90	0.91	0.91
6	0.93	0.93	0.90	0.89	0.92
7	0.95	0.93	0.91	0.90	0.92
8	0.94	0.93	0.90	0.89	0.92
9	0.93	0.94	0.92	0.93	0.93
10	0.95	0.94	0.92	0.92	0.93
11	0.96	0.96	0.95	0.95	0.95
12	0.95	0.95	0.93	0.93	0.92
13	0.97	0.97	0.95	0.95	0.95
14	0.99	0.99	0.97	0.97	0.98
15	0.94	0.95	0.95	0.95	0.96
16	0.96	0.96	0.94	0.94	0.95
17	0.95	0.95	0.93	0.92	0.93
18	0.98	0.97	0.97	0.95	0.97
19	0.93	0.93	0.91	0.90	0.91
20	0.92	0.93	0.89	0.88	0.89
21	0.98	0.97	0.94	0.95	0.93
22	0.99	0.98	0.95	0.96	0.94
23	0.95	0.94	0.93	0.93	0.94
24	0.94	0.95	0.94	0.93	0.94
25	0.94	0.94	0.94	0.94	0.94
26	0.95	0.95	0.93	0.93	0.93
27	0.94	0.94	0.92	0.92	0.92
28	0.99	1.00	0.97	0.98	0.97
29	0.97	0.98	0.97	0.97	0.97
30					
31					0.93
32	0.97	0.93	0.93	0.92	0.93
33	0.94	0.94	0.93	0.93	0.93
34	0.93	0.93	0.89	0.91	0.91
35	0.94	0.94	0.94	0.94	0.94
35S	0.96	0.98	0.98	0.97	0.98
36	0.96	0.96	0.95	0.94	0.96
37	0.99	0.99	0.97	0.98	0.98
38	0.98	0.99	0.98	0.98	0.98
39	0.94	0.95	0.93	0.93	0.95

Table 5.4 (Continued)

RUNNO.	ARC (m)				
	50	100	200	400	800
40	0.96	0.98	0.96	0.94	0.94
41	0.97	0.97	0.96	0.95	0.96
42	0.96	0.97	0.96	0.97	0.97
43	0.91	0.90	0.87	0.87	0.87
44	0.91	0.92	0.87	0.85	0.88
45	0.92	0.92	0.88	0.87	0.88
46	0.92	0.93	0.92	0.92	0.92
47	0.93	0.94	0.93	0.93	0.93
48	0.96	0.96	0.95	0.96	0.96
48S	0.93	0.94	0.92	0.93	0.93
49	0.97	0.95	0.94	0.93	0.94
50	0.92	0.93	0.93	0.92	0.92
51	0.96	0.95	0.92	0.91	0.91
52	0.93	0.93	0.90	0.89	0.90
53	0.99	0.97	0.96	0.95	0.96
54	0.98	0.96	0.96	0.95	0.96
55	0.95	0.97	0.96	0.98	0.97
56	0.99	0.98	0.98	0.98	0.98
57	0.91	0.93	0.93	0.93	0.91
58	0.95	0.96	0.93	0.93	0.92
59	0.97	0.97	0.93	0.92	0.93
60	0.95	0.94	0.93	0.92	0.92
61	0.89	0.92	0.88	0.88	0.92
62		0.91	0.87	0.88	0.96
63					
64					
65	0.94	0.95	0.93	0.93	
66	0.94	0.98	0.97	0.94	0.95
67	0.97	0.97	0.95	0.95	
68	0.96	0.97	0.96	0.96	0.94

## CHAPTER 6 SLOW-RESPONSE METEOROLOGICAL OBSERVATIONS DURING PROJECT PRAIRIE GRASS

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### 6.1 Introduction

During the Project Prairie Grass diffusion experiments, mean wind speed and fluctuations in azimuth wind direction were measured at a height of 2 m above the ground at two locations. Closely-matched cup anemometers of conventional design were used to obtain wind speed data; fluctuations in wind direction were measured by means of airfoil-type vanes (subsequently replaced by flat-plate vanes). One pair of these instruments was installed along the base line of the sulfur-dioxide sampling network; the cup anemometer was mounted on a wood post set in the ground at a point 25 m directly west of the release-point for the tracer; the azimuth vane and recorder were similarly located directly east of the release-point. The second pair of instruments was located about 450 m north (downwind) of the release-point and approximately 30 m directly west of the center line of the horizontal sampling network; the lateral separation between the two posts supporting the instruments was about 10 meters. The recorder was mounted on a panel, located on the center line of the sampling network at 450 m, with the manual switches for operating the vacuum-pump motors. The cup anemometer and azimuth vane assemblies are shown in Figures 6.1 and 6.2. The azimuth vane and recorder installed along the base line of the sampling network appear in Figure 6.3. Detailed descriptions of the instrumentation and the treatment of the observations are presented in the remaining sections.

### 6.2 Description of Instrumentation

The cup anemometers are almost identical with those used previously in the Great Plains Turbulence Field Program.<sup>1</sup> The cup

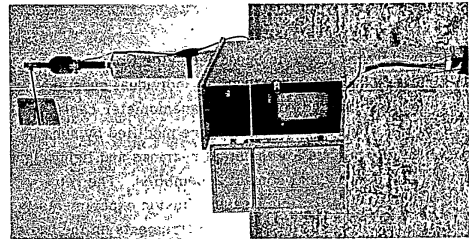


Figure 6.3 Azimuth wind-direction vane and recorder installation along base line of sulfur-dioxide sampling network.

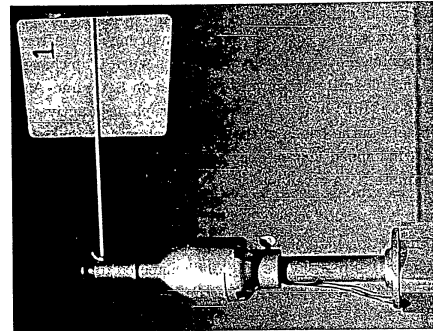


Figure 6.2 Azimuth vane assembly.

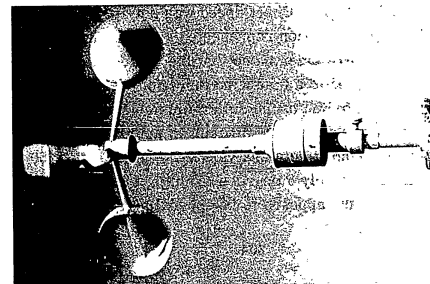


Figure 6.1 Cup anemometer assembly.



wheels, manufactured by the Electric Speed Indicator Company, are 11.3 inches in diameter and weigh 370 grams. Individual cups are conically shaped and have beaded edges. The anemometer cases, manufactured by the H. J. Green Company, were modified by substituting powdered bronze bearings for the steel bearings and lightweight electrical contacts for the original contact assemblies. The two anemometers used during the Prairie Grass diffusion experiments were selected from a total of eleven similar instruments on the basis of extensive field-matching tests. Results of these tests indicated an average difference in calibration of about 0.25 percent, over a wide range of mean wind speeds, between the two instruments. After the first twenty experiments, the two anemometers were interchanged. Passage of each 1/60-mile of air was recorded on Esterline-Angus chart rolls (Type 4310E) by means of chronograph pens activated by electrical contacts in the bases of the anemometers. The relationship between mean wind speed  $\bar{V}$  in  $\text{m sec}^{-1}$  and the average number of contacts per minute  $\bar{N}$  is given by

$$\bar{V} = 0.538 + 0.507 \bar{N}.$$

The wind direction instruments comprised airfoil-type vanes (later replaced by flat-plate types) rigidly connected to 360-degree potentiometers. The latter, purchased from the Technology Instrument Company (Type ST-20), were center-tapped and had an internal resistance of 5000 ohms. Data were recorded on portable Esterline-Angus center-zero milliammeters. Chart speed was set at 12 inches per minute and full-scale deflection represented an azimuth range of 200 degrees. The vanes were oriented so that the center of the recorder chart-rolls corresponded to a true wind direction of 180 degrees, the orientation of the center line of the sulfur-dioxide sampling network. Exact correspondence proved very difficult to achieve. Despite careful adjustments, subsequent data analysis indicates that the 450 m vane tended to read approximately 8 degrees too high; the absolute orientation of the base-line vane appears to be approximately correct.

Accessory electrical components included a Raytheon voltage-regulator transformer (Type VR-6111) and a 25-v rectifier power supply adjustable for any desired output within 14 to 25 volts. Critical damping was provided by a 1,250-ohm resistor in series with the galvanometer coil of the recorder. To ensure synchronous operation of the wind speed and wind direction instruments, both recorders were activated by a master switch located in the instrument truck at the northern end of the field site. An additional marking pen was used in the base-line recorder to provide information on the rate of release of the tracer. Wiring diagrams for this instrumentation are presented in Figures 6.4 and 6.5.

During the first 34 diffusion experiments, airfoil-type vanes were used to measure fluctuations in azimuth wind direction. These were constructed of balsa wood ribs covered with model airplane fabric. Due to repeated exposure to strong winds and light rain showers, the airfoils became asymmetrical; this deformation introduced an uncertainty of 3 to 6 degrees depending upon the wind speed, in the indicated mean wind direction. After Experiment No. 34 these airfoils were replaced with flat metal plates (see Figure 6.2). At the conclusion of the Prairie Grass field experiments, reduction of the data revealed the response of the potentiometers in the azimuth vanes was not linear over the 200-degree range; this occurred as a result of shunting effects in the galvanometer coils. Calibration curves for each vane assembly were subsequently determined in laboratory tests and these were used in evaluating the data abstracted from the chart rolls.

### 6.3 Data Abstraction and Analysis

The slow-response meteorological instrumentation was operated for 20-minute sampling periods centered on the midpoint of the 10-minute gas release. Values of mean wind speed, mean wind direction, and standard deviations of wind direction have been calculated both for the 20-minute sampling periods and for the 10-minute periods identified with the release of the tracer. The 10-minute observations at 450 m have been adjusted to correspond as closely as possible to the time that

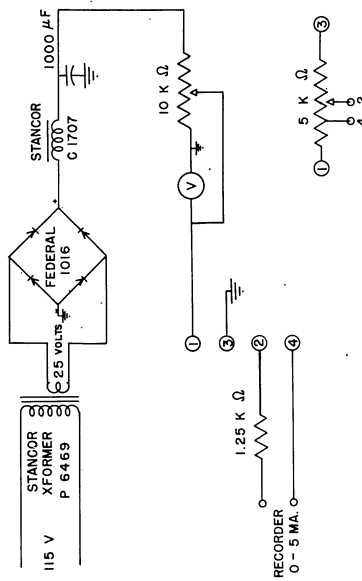


Figure 6.4 Wiring diagram for azimuth wind-direction assembly.

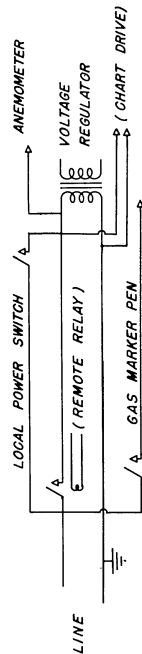


Figure 6.5 Wiring diagram for remote operation of recorders used in obtaining slow-response meteorological observations.

the tracer was actually present; this was accomplished by delaying the start of the 10-minute period by  $450/\bar{V}$  sec, where  $\bar{V}$  is the mean wind speed at the base line in  $\text{m sec}^{-1}$ . When  $\bar{V}$  was less than  $1.5 \text{ m sec}^{-1}$ , the last 10 minutes of chart record at 450 m were utilized. Mean wind speed values were determined by substituting the average number of pips per minute, obtained from the chart records, in the calibration equation given above. Azimuth wind-direction data were abstracted from the charts at 2.5-sec intervals; these data were then grouped in 2-degree class intervals identified with the angular positions of sampling stations in the first four arcs of the sulfur-dioxide sampling network. The results comprise frequency distributions of azimuth wind direction for both 10- and 20-minute sampling periods.

Mean wind speeds, azimuth wind directions, and standard deviations of azimuth wind direction for both 10- and 20-minute sampling periods are summarized in Table 6.1. Frequency distributions of azimuth wind direction for both 10- and 20-minute periods are presented in Table 6.2. It is felt that the wind speed data are accurate to within 2 to 5 percent for mean wind speeds greater than  $2.0 \text{ m sec}^{-1}$ ; for lower mean wind speeds, particularly during nighttime experiments in the presence of stable thermal stratification, the uncertainty is greatly increased (the starting speed of the anemometers is approximately  $0.8 \text{ m sec}^{-1}$ ). The relative accuracy of the mean wind directions is thought to be of the order of 2 to 5 degrees; the absolute values obtained for wind direction, as noted above, may be in error by 10 degrees. Standard deviations of azimuth wind direction are considered accurate within 10 percent, except in the case of mean wind speeds below  $2 \text{ m sec}^{-1}$  where the uncertainty is considerably larger. In about 40 percent of the cases, the 20-minute standard deviation of azimuth wind direction is slightly lower than the 10-minute value; these small differences are not considered statistically significant. For the few cases in which the 20-minute standard deviations are more than 10 percent lower than the 10-minute values, inspection of the original chart records reveals the presence of long-period inhomogeneities in the turbulent structure.

## REFERENCE

1. Cramer, H. E., G. C. Gill, and F. A. Record, "Standard Cup Anemometers - Massachusetts Institute of Technology" in "Exploring the Atmosphere's First Mile," Pergamon Press, N. Y., Vol. 1, 145-148, 1957.

Table 6.1

Summary of slow-response meteorological measurements made by the Massachusetts Institute of Technology during the Project Prairie Grass diffusion experiments

Tabular entries comprise mean wind speeds ( $\text{m sec}^{-1}$ ), mean wind directions (degree), and standard deviations of azimuth wind direction (degree); data are based on measurements made at height of 2 m along base line of sulfur-dioxide sampling network and at travel distance of 450 m from the release-point for the tracer. Results are presented for 10- and 20-minute sampling periods. With respect to the measurements made along the base line, the duration of the 10-minute period coincides with that of the gas release. At 450 m, the start of the 10-minute period was delayed by  $450/\bar{V}$  sec, as explained in the text. Entries marked with asterisks are estimates based on incomplete records; these are explained below. Blank spaces signify missing data. It appears that the mean wind directions obtained from the 450-m vane are about 8 degrees too large; more reasonable values may be secured by subtracting this amount from each of the tabular entries.

Explanation of incomplete or missing data

Experiment No.	Explanation
1	No wind direction data and no wind speed data for 450 m. First 5 min of record at base line missing; portions of remainder of record on slow speed.
2	No wind direction data available.
3	No slow-response data - light, variable winds.
6	Base-line chart records missing.
25	Last 9 1/2 min of chart record missing at 450 m.
27	Last 2 1/2 min of chart record missing at 450 m.
29	No data available at 450 m.
36	Last 4 min of record missing at base line.
40	First 5 min of wind speed record at 450 m is missing.
48S	No wind direction data presented - off scale.
52	No wind direction data at 450 m - off scale.
58	First 3-1/2 min of record during gas release missing from base-line chart.
63, 64	No slow-response data available - light, variable winds.

Table 6.1 (Continued)

Gas release No.	1	2	3	4	5	6	7
Date	3 July		5 July	6 July	1355	1655	10 July
Time (CST)	1055	1455	2155	0055			1355
Wind speed (m/sec)							
Source (10 min)	2.62*	2.01		1.40	6.47		4.19
450 m (10 min)		2.57		1.65	5.96	5.86	4.14
Source (20 min)	2.40*	2.14		1.58	6.57		4.19
450 m (20 min)		2.19		1.76	6.45	6.65	4.55
Wind direction (deg)							
Source (10 min)				216	176		188
450 m (10 min)				223	186	191	194
Source (20 min)				207	176		197
450 m (20 min)				226	184	190	200
Standard deviation of wind direction (deg)							
Source (10 min)				7.4	9.5		25.6
450 m (10 min)				7.6	9.1	7.1	27.1
Source (20 min)				9.7	11.1		31.7
450 m (20 min)				9.2	9.7	7.7	23.9
Gas release No.	8	9	10	11	12	13	14
Date	10 July	11 July	14 July	14 July	0955	22 July	1955
Time (CST)	1655	0955	1155	0755			2155
Wind speed (m/sec)							
Source (10 min)	4.85	6.88	4.60	7.03	8.35	1.25	1.91
450 m (10 min)	4.75	7.13	4.65	7.74	8.25	1.81	1.81
Source (20 min)	4.70	6.93	4.52	7.61	8.07	1.37	1.75
450 m (20 min)	4.80	7.13	4.65	7.76	8.14	1.85	1.81
Wind direction (deg)							
Source (10 min)	184	204	225	184	194	190	170
450 m (10 min)	193	214	214	196	200	206	186
Source (20 min)	176	206	217	185	192	192	172
450 m (20 min)	181	214	217	196	199	206	186
Standard deviation of wind direction (deg)							
Source (10 min)	10.2	10.2	16.8	7.2	7.9	3.2	3.6
450 m (10 min)	9.6	10.2	14.1	6.8	5.1	2.4	3.1
Source (20 min)	16.3	9.5	18.3	6.9	9.9	5.0	4.3
450 m (20 min)	19.1	9.1	15.4	6.7	6.9	2.5	5.9

Table 6.1 (Continued)

Gas release No.	15	16	17	18	19	20	21
Date	23 July				25 July		
Time (CST)	0755	0955	1955	2155	1055	1255	2155
Wind speed (m/sec)							
Source (10 min)	3.43	3.23	3.33	3.53	5.81	8.60	6.12
450 m (10 min)	3.43	3.28	3.48	3.43	5.76	8.35	5.76
Source (20 min)	3.25	3.02	3.33	3.45	5.81	8.52	5.53
450 m (20 min)	3.40	3.12	3.48	3.50	5.79	8.42	5.73
Wind direction (deg)							
Source (10 min)	209	192	184	187	166	178	181
450 m (10 min)	211	216	198	195	174	184	186
Source (20 min)	209	201	182	189	166	177	179
450 m (20 min)	212	212	186	186	174	183	185
Standard deviation of wind direction (deg)							
Source (10 min)	12.8	18.5	5.6	5.3	11.6	8.3	6.6
450 m (10 min)	11.0	18.9	5.2	4.7	10.1	7.9	5.7
Source (20 min)	12.4	23.4	5.5	5.7	12.4	8.3	6.2
450 m (20 min)	9.6	18.7	5.4	4.9	9.5	8.2	5.9
Gas release No.	22	23	24	25	26	27	28
Date	25 July	29 July		1 Aug.	2 Aug.		
Time (CST)	2355	2055	2255	1255	1155	1355	2355
Wind speed (m/sec)							
Source (10 min)	6.42	5.91	6.22	2.77	6.77	6.57	2.62
450 m (10 min)	6.78	6.27	5.76	2.92*	6.57	6.57	2.62
Source (20 min)	6.67	6.12	5.91	2.90	6.37	6.67	2.77
450 m (20 min)	6.82	6.22	5.81	2.91*	6.29	6.39*	2.67
Wind direction (deg)							
Source (10 min)	176	128	141	177	190	184	174
450 m (10 min)	184	134	150	188*	197	190	183
Source (20 min)	176	128	141	176	186	185	174
450 m (20 min)	184	133	150	187*	192	190*	181
Standard deviation of wind direction (deg)							
Source (10 min)	5.8	7.3	7.1	24.8	13.2	9.2	6.4
450 m (10 min)	5.1	5.2	6.2	16.0*	10.2	8.6	5.9
Source (20 min)	5.6	7.2	6.4	21.4	12.1	9.2	6.0
450 m (20 min)	4.7	5.5	6.2	15.5*	11.2	8.5*	5.3

Table 6.1 (Continued)

Gas release No.	29	30	31	32	33	34	35
Date	3 Aug.			6 Aug.	7 Aug.		
Time (CST)	0155	1255	1455	1955	1255	1455	2257
Wind speed (m/sec)							
Source (10 min)	3.48	6.82	7.33	2.21	8.50	9.00	4.04
450 m (10 min)		6.72	7.43	2.01	8.30	9.26	3.99
Source (20 min)	3.68	6.65	7.64	2.19	7.89	8.30	3.99
450 m (20 min)		6.55	7.76	2.24	7.99	9.36	3.91
Wind direction (deg)							
Source (10 min)	220	196	225	171	181	146	135
450 m (10 min)		209	223	185	190	161	150
Source (20 min)	222	201	216	170	179	145	136
450 m (20 min)		211	221	185	189	156	149
Standard deviation of wind direction (deg)							
Source (10 min)	8.0	10.3	10.9	3.6	10.5	7.3	5.0
450 m (10 min)		11.5	7.7	5.8	9.0	8.7	5.4
Source (20 min)	12.7	12.3	14.2	5.2	9.2	7.5	6.4
450 m (20 min)		10.8	10.7	3.4	8.9	9.6	5.9
Gas release No.	35	36	37	38	39	40	41
Date	11 Aug.		12 Aug.		13 Aug.	14 Aug.	
Time (CST)	2125	2325	0255	0455	2225	0025	0255
Wind speed (m/sec)							
Source (10 min)	1.86	1.86	4.64	4.14	3.12	3.08	4.04
450 m (10 min)		1.75	2.06	4.70	4.49	2.21	2.39
Source (20 min)	1.86	1.87*	4.57	4.09	3.10	3.15	4.06
450 m (20 min)		1.65	1.88	4.62	4.39	2.46	2.45*
Wind direction (deg)							
Source (10 min)	132	160	187	170	140	180	198
450 m (10 min)		105	169	190	175	131	166
Source (20 min)	131	158*	186	170	139	179	198
450 m (20 min)		109	167	190	175	133	182
Standard deviation of wind direction (deg)							
Source (10 min)	3.3	3.8	7.0	5.0	5.8	9.0	5.0
450 m (10 min)		5.1	4.2	7.0	4.5	6.8	10.4
Source (20 min)	3.6	4.2*	6.8	5.6	8.8	10.5	5.0
450 m (20 min)		7.1	4.4	6.6	4.7	6.7	11.8

Table 6.1 (Continued)

Gas release No.	42	43	44	45	46	47	48
Date	14 Aug.	15 Aug.				20 Aug.	
Time (CST)	0455	1155	1355	1655	1840	0955	1225
Wind speed (m/sec)							
Source (10 min)	5.81	4.95	5.71	6.12	5.15	3.58	3.38
450 m (10 min)		6.88	5.10	6.01	6.12	5.26	3.58
Source (20 min)	5.99	4.95	5.71	5.66	5.20	3.45	3.17
450 m (20 min)		6.32	5.05	6.14	5.89	5.38	3.48
Wind direction (deg)							
Source (10 min)	212	170	158	163	134	243	
450 m (10 min)		215	179	167	168	133	225
Source (20 min)	212	170	158	161	134	236	
450 m (20 min)		215	177	161	167	135	235
Standard deviation of wind direction (deg)							
Source (10 min)	6.6	12.2	12.7	6.9	7.7	13.9	
450 m (10 min)		5.9	10.3	14.0	7.2	8.2	12.6
Source (20 min)	6.6	13.7	13.7	8.2	7.6	20.0	
450 m (20 min)		5.3	11.7	18.1	8.4	8.6	18.0
Gas release No.	48	49	50	51	52	53	54
Date	21 Aug.				24 Aug.		
Time (CST)	0855	1055	1355	1525	1110	1955	2155
Wind speed (m/sec)							
Source (10 min)	8.04	6.27	6.57	6.12	4.29	2.51	4.04
450 m (10 min)		8.55	6.67	6.78	6.67	4.75	2.41
Source (20 min)	7.94	6.39	6.47	5.96	4.32	2.46	4.11
450 m (20 min)		8.40	6.85	6.77	6.77	4.75	2.39
Wind direction (deg)							
Source (10 min)	214	199	215	245	132	132	140
450 m (10 min)		213	202	214	237	131	142
Source (20 min)	212	198	216	244	129	133	140
450 m (20 min)		213	201	217	243	132	143
Standard deviation of wind direction (deg)							
Source (10 min)	8.1	11.9	10.9	10.8	17.7	3.9	5.9
450 m (10 min)		6.9	10.9	9.0	11.4	2.5	6.1
Source (20 min)	8.1	11.1	10.7	12.6	16.5	3.6	5.7
450 m (20 min)		6.7	10.9	10.4	12.5	2.7	5.8

Table 6.1 (Continued)

Gas release No.	55	56	57	58	59	60	61
Date	25 Aug.			26 Aug.			
Time (CST)	0055	0255	1725	1925	2225	0135	1055
Wind speed (m/sec)							
Source (10 min)	5.41	4.34	6.67	1.91*	2.62	4.90	7.99
450 m (10 min)	5.86	4.75	6.82	2.35	2.67	5.00	7.64
Source (20 min)	5.28	4.44	6.90	1.96*	2.52	4.87	7.64
450 m (20 min)	5.94	4.70	6.98	2.39	2.72	4.87	7.61
Wind direction (deg)							
Source (10 min)	156	153	200	178*	174	198	203
450 m (10 min)	162	156	206	185	181	202	204
Source (20 min)	155	152	198	179*	173	199	205
450 m (20 min)	162	154	205	186	180	202	209
Standard deviation of wind direction (deg)							
Source (10 min)	5.8	6.1	8.0	4.1*	5.2	5.9	11.0
450 m (10 min)	6.0	7.2	7.8	3.3	3.6	6.5	9.0
Source (20 min)	6.1	7.8	8.2	4.1*	4.6	5.5	10.9
450 m (20 min)	5.5	8.6	8.1	3.3	3.5	5.3	9.5
Gas release No.	62			65	66	67	68
Date	26 Aug.			29 Aug.		30 Aug.	
Time (CST)	1355			1925	2125	0025	0225
Wind speed (m/sec)							
Source (10 min)	5.15			4.44	3.08	4.34	2.82
450 m (10 min)	5.41			4.44	3.33	4.70	2.77
Source (20 min)	5.00			4.24	3.17	4.42	2.82
450 m (20 min)	5.30			4.37	3.43	4.67	2.95
Wind direction (deg)							
Source (10 min)	212			178	166	185	174
450 m (10 min)	214			174	171	190	181
Source (20 min)	213			173	165	182	173
450 m (20 min)	215			177	172	187	179
Standard deviation of wind direction (deg)							
Source (10 min)	8.8			5.0	6.9	5.4	5.3
450 m (10 min)	6.9			5.4	5.1	5.2	5.3
Source (20 min)	9.4			5.4	6.4	6.6	6.2
450 m (20 min)	7.6			4.8	5.0	6.2	5.9

Table 6.2

Frequency distributions of azimuth wind direction obtained by the Massachusetts Institute of Technology during Project Prairie Grass diffusion experiments

Frequency distributions of azimuth wind direction are based on measurements at height of 2 m along base line of sampling network and at travel distance of 450 meters. Data were read from chart records at intervals of 2.5 seconds; entries are total number of cases occurring within 2-degree class intervals expressed in terms of post numbers for horizontal sampling network. For example, Post No. 1 includes wind directions from 089 to 090 degrees; Post No. 46 includes wind directions from 179 to 180 degrees; Post No. 91 includes wind directions from 269 to 270 degrees. Selection of 10-minute sampling periods is explained in the text. As noted in the text and in the explanatory material for Table 6.1, the 450-m data should probably be shifted about 8 degrees or four post numbers towards lower values. Explanation of incomplete or missing data is presented in Table 6.1.

Explanation of incomplete or missing data

Gas Release No.

- 1,2,3 No wind direction data are available.
- 6 No wind direction data for the source.
- 25 No frequency distributions at 450 m - short record.
- 27 Last 2-1/2 min of chart record at 450 m is missing.
- 29 No frequency distributions at 450 m - short record.
- 36 20-min frequency distribution at source is based on 16 min of record (last 4 min missing).
- 52 No wind direction data available at 450 m - off scale.

Gas Release No.

58 Wind direction distributions at source are based on 16-1/2 min of record - 3-1/2 min missing at start of gas release.  
 63,64 No frequency distributions presented - light and variable winds.

Table 6.2 (Continued)

DATE 6 July 1956 TIME 0055-0115 CST RUN NO. 4

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47			1	
2					48				
3					49				
4					50				
5					51			3	
6					52			13	
7					53			27	
8					54			23	
9					55			32	
10					56	2		44	
11					57	8		35	
12					58	18	2	49	2
13					59	9	1	24	1
14					60	29	3	45	3
15					61	10	6	14	6
16					62	21	4	22	4
17					63	9	41	11	41
18					64	16	10	17	14
19					65	14	7	15	30
20					66	19	32	19	52
21					67	54	30	54	42
22					68	25	14	25	35
23					69	5	6	5	32
24					70		29		55
25					71		12		12
26					72		14		26
27					73		21		30
28					74		9		26
29					75				17
30					76				10
31					77				4
32					78				4
33					79				32
34					80				2
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 6 July 1956 TIME 1355-1415 CST RUN NO. 5

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	23	21	39	42
2					48	17	18	29	22
3					49	19	24	27	45
4					50	13	13	26	30
5					51	6	18	12	23
6					52	9	16	12	32
7					53	1	11	7	18
8					54	4	15	6	27
9					55	1	8	3	15
10					56	1	6	3	9
11					57		5	1	8
12					58		5	1	8
13					59		2		2
14					60		2		2
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29	1				75				
30			1		76				
31	1		3		77				
32			5	2	78				
33	1		11		79				
34	2		8	5	80				
35	4		20	1	81				
36	4		9	1	82				
37	9		21	2	83				
38	8		18	4	84				
39	5	4	19	5	85				
40	6	2	18	5	86				
41	10	6	32	11	87				
42	24	2	47	16	88				
43	14	8	18	21	89				
44	15	16	22	26	90				
45	18	20	31	41	91				
46	25	18	36	43					

Table 6.2 (Continued)

DATE 6 July 1956 TIME 1655-1715 CST RUN NO. 6

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48			24	48
3					49			23	31
4					50			14	46
5					51			26	35
6					52			22	45
7					53			29	45
8					54			25	42
9					55			19	27
10					56			7	24
11					57			9	13
12					58			3	6
13					59			4	4
14					60			1	6
15					61			1	1
16					62				
17					63				
18					64				1
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									



Table 6.2 (Continued)

DATE 10 July 1956 TIME 1355-1415 CST RUN NO. 7

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	17	6	24	5
2					48	9	3	12	11
3					49	6	11	14	15
4					50	6	4	16	9
5					51	3	6	7	9
6					52	4	8	9	12
7					53	3	2	10	9
8					54	5	6	7	9
9					55	9	4	12	11
10					56	7	7	10	16
11					57	5	9	9	16
12					58	9	11	12	24
13					59	5	8	12	14
14					60	7	8	14	24
15					61	4	5	7	18
16					62	8	8	11	20
17					63	6	14	10	35
18					64	3	7	8	17
19					65	4	3	7	10
20	1	1		1	66	13	2	21	6
21	1	3	1	3	67	6	2	13	14
22	1		1		68	2	4	9	13
23	4	2	4	2	69	2	6	6	18
24	2	3	2	3	70	2	5	4	13
25	1	1	1	1	71	3	7	5	12
26	2	1	2	1	72	2	4	2	12
27	2	3	2	3	73	1	5	1	6
28	2	1	2	1	74	1		3	1
29	2	1	3	1	75	1	1	3	1
30	4	1	5	2	76		1		1
31	2	4	7	4	77	1	2	4	2
32	1	5	4	6	78		1	2	1
33	2	2	9	2	79		3		3
34	2	1	5	1	80			1	
35	4	1	8	2	81			3	
36	1	1	7	1	82		1	5	1
37	6	2	13	3	83				
38	4	5	9	8	84			4	
39	6	1	8	5	85			4	
40	1	4	2	7	86			3	
41	6		11	2	87				
42	11	4	13	9	88			6	
43	4	4	5	7	89			3	
44	8	7	10	11	90			3	
45	6	4	8	7	91			4	
46	3	3	8	3					

Table 6.2 (Continued)

DATE 10 July 1956 TIME 1655-1715 CST RUN NO. 8

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	23	12	46	22
2					48	13	15	25	22
3					49	27	9	32	15
4					50	15	8	26	18
5					51	14	13	25	23
6					52	14	17	15	32
7					53	10	15	19	19
8					54	8	16	13	22
9					55	3	32	6	37
10					56	8	14	7	17
11					57		20	4	24
12					58	2	20	1	21
13					59	2	6	1	7
14					60		6	1	6
15					61	2	2	2	2
16					62		1		1
17					63	2		2	
18					64				
19					65		1		
20					66		1		
21					67		1		
22					68		5		
23					69		3		
24					70		1		
25					71		7		
26					72		5		
27					73		6		
28					74		4		
29					75		9		
30					76		6		
31					77		11		
32					78		11		
33					79		8		
34					80		6		
35					81		9		
36					82		3		
37					83		8		
38					84		7		
39					85		7		
40					86		3		
41					87		1		
42					88		21		
43					89		32		
44					90		15		
45					91		28		
46							18		

Table 6.2 (Continued) RUN NO. 9

DATE 11 July 1956		TIME 0955-1015 CST				RUN NO. 9			
Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48	4		4	
3					49	2	1	4	1
4					50	4		5	
5					51	7	1	9	1
6					52	7	4	12	4
7					53	17		26	1
8					54	15	5	19	5
9					55	15	6	20	6
10					56	18	6	27	7
11					57	15	17	35	28
12					58	28	17	61	30
13					59	29	13	47	28
14					60	14	8	42	34
15					61	9	7	24	27
16					62	13	19	36	40
17					63	5	28	16	33
18					64	5	14	19	24
19					65	5	14	21	26
20					66	5	15	13	31
21					67	6	9	11	19
22					68	7	22	12	38
23					69	3	10	5	13
24					70	5	8	7	14
25					71		11	1	21
26					72		4		8
27					73		1		4
28					74	1		1	
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89		1		
44					90				
45					91				
46	1		1						

Table 6.2 (Continued)

DATE 11 July 1956		TIME 1155-1215 CST				RUN NO. 10			
Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48	1	2	6	4
3					49	2	2	8	2
4					50	3	2	9	2
5					51	5	6	13	10
6					52		3	7	7
7					53	6	5	12	9
8					54	3	5	12	8
9					55	4	3	13	7
10					56	7	11	14	11
11					57	2	8	13	17
12					58	3	9	11	15
13					59	4	9	11	12
14					60	7	12	19	22
15					61	3	14	14	18
16					62	8	13	16	29
17					63	7	19	14	33
18					64	6	18	19	27
19					65	7	11	21	25
20					66	8	9	22	23
21					67	8	8	15	24
22					68	12	10	23	31
23					69	17	9	28	21
24					70	13	10	23	20
25					71	11	8	13	13
26					72	15	7	18	18
27					73	6	4	7	8
28					74	16	2	19	6
29					75	9	7	9	10
30					76	6	6	6	7
31					77	12	5	13	8
32					78	8		9	1
33					79	4	1	6	5
34					80	2		3	1
35					81	8		8	1
36					82	2		6	2
37					83	2		2	
38					84	2		2	7
39					85				1
40					86	1		1	4
41					87				
42					88	1		1	
43					89				
44					90				1
45					91				
46	1		3	1					

Table 6.2 (Continued)

DATE 14 July 1956 TIME 0755-0815 CST RUN NO. 11

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	25	3	63	7
2					48	21	9	50	16
3					49	23	10	52	24
4					50	23	7	45	26
5					51	16	22	32	44
6					52	22	25	33	49
7					53	13	26	28	53
8					54	6	18	12	44
9					55	3	35	16	60
10					56	3	17	6	38
11					57	1	24	1	36
12					58	16			29
13					59		15		24
14					60		9		16
15					61		2		4
16					62				2
17					63		1		2
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40			1		86				
41	5		5		87				
42	14		20		88				
43	6		15		89				
44	16		28		90				
45	19	1	29	1	91				
46	24		42	2					

Table 6.2 (Continued)

DATE 14 July 1956 TIME 0955-1015 CST RUN NO. 12

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	8		33	6
2					48	12		26	4
3					49	9		23	4
4					50	14	1	23	9
5					51	25	10	41	21
6					52	31	9	42	28
7					53	11	24	28	46
8					54	29	27	41	44
9					55	17	32	26	63
10					56	19	37	30	58
11					57	21	36	28	53
12					58	18	31	26	36
13					59	4	17	7	30
14					60	4	8	17	14
15					61	3	4	2	17
16					62	2	2	2	11
17					63		2	2	9
18					64			1	
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 22 July 1956 TIME 1955-2015 CST RUN NO. 13

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48			1	
3					49	18		46	
4					50	74		80	
5					51	67		162	
6					52	21		56	
7					53	34		43	
8					54	26		35	2
9					55			10	5
10					56			12	9
11					57		38	4	49
12					58		81	23	114
13					59		74	9	179
14					60		22	6	82
15					61		19		41
16					62		6		4
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 22 July 1956 TIME 2155-2215 CST RUN NO. 14

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47			13	44
2					48			2	82
3					49			68	75
4					50			46	53
5					51			19	33
6					52			7	17
7					53			4	21
8					54			1	24
9					55				14
10					56				6
11					57				4
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46	1		6		15		47		

Table 6.2 (Continued)

DATE 23 July 1956 TIME 1755-1815 CST RUN NO. 15

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	7		12	
2					48	4	1	8	1
3					49	1	2	3	3
4					50	5	3	7	3
5					51	3	4	9	5
6					52	3	9	13	10
7					53	3	6	9	10
8					54	5	9	16	9
9					55	2	9	12	7
10					56	5	9	8	31
11					57	8	5	15	36
12					58	5	8	27	30
13					59	13	4	31	43
14					60	25	28	45	37
15					61	12	11	27	27
16					62	18	13	39	55
17					63	15	23	26	30
18					64	15	15	31	28
19					65	16	15	29	15
20					66	15	13	27	20
21					67	16	17	21	29
22					68	7	16	12	18
23					69	17	12	19	12
24					70	11	3	15	8
25					71	1	2	3	8
26					72	1	1	3	2
27					73	1		1	
28					74				
29					75	1	1	1	
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42	1		1		88				
43					89				
44	1		2		90				
45	3		4		91				
46		1	2	1					

Table 6.2 (Continued)

DATE 23 July 1956 TIME 0955-1015 CST RUN NO. 16

Post No.	10 - min		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	12	1	15	13
2					48	8	2	12	5
3					49	12	1	16	12
4					50	15	3	22	6
5					51	13		17	6
6					52	14	8	19	11
7					53	11	4	13	7
8					54	10	6	15	13
9					55	7	3	12	6
10					56	4	3	8	7
11					57	3	11	3	16
12					58	3	10	9	18
13					59	4	4	10	5
14					60	8	15	14	28
15					61		12	3	17
16					62	3	12	8	20
17					63		13	5	37
18					64	4	3	11	16
19					65	10	17	18	29
20					66	12	13	22	17
21					67	9	11	19	26
22					68	5	14	15	28
23					69	4	5	14	17
24					70		7	12	20
25					71		5	6	7
26					72	1	6	11	10
27					73	1	11	4	11
28					74	1	3	2	3
29					75		4	5	4
30					76		1	7	1
31					77	1	2	2	2
32					78		2	11	3
33					79		3	3	5
34					80		2	2	2
35	1				81		2	2	1
36	3				82		1	3	2
37	4	1			83				
38	4	1	4	1	84		2		3
39	5				85			1	
40	6	2	9	2	86		3		3
41	13	1	15	2	87				
42	4	1	10	1	88		1		1
43	6	3	8	6	89		2		2
44	5	1	12	4	90				
45	6		7	6	91				
46	8	3	19	6					

Table 6.2 (Continued)

DATE 23 July 1956 TIME 1955-2015 CST RUN NO. 17

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	46	23	90	80
2					48	36	33	68	87
3					49	28	41	39	84
4					50	24	37	35	59
5					51	17	34	26	49
6					52	8	20	13	39
7					53	7	22	8	31
8					54	4	7	4	12
9					55	2	5	2	6
10					56				
11					57		2		4
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38	1		2		84				
39			2		85				
40					86				
41	2		9	3	87				
42	4	1	12	1	88				
43	6	2	18	7	89				
44	13	2	41	9	90				
45	13	5	47	17	91				
46	31	6	63	29					

Table 6.2 (Continued)

DATE 23 July 1956 TIME 1955-2015 CST RUN NO. 18

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	28		41	
2					48	25		42	1
3					49	31	7	60	12
4					50	32	13	59	22
5					51	38	19	64	31
6					52	25	32	51	58
7					53	17	36	45	68
8					54	8	48	29	77
9					55	7	30	39	72
10					56	1	19	11	43
11					57		27	2	50
12					58		7	4	26
13					59				8
14					60		2		10
15					61			1	
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44	4				90	4			
45	6				91	7			
46	18					20			

Table 6.2 (Continued)

DATE 25 July 1956 TIME 1055-1115 CST RUN NO. 19

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	13	13	18	43
2					48	8	6	13	16
3					49	3	7	11	20
4					50	6	8	10	17
5					51	1	4	3	10
6					52	1	3	1	4
7					53	1		1	
8					54		2		2
9					55		1		1
10					56	1		1	
11					57				
12					58		2		2
13					59				
14					60		1		1
15					61				
16					62				
17					63				
18					64				
19			1		65				
20					66				
21			2		67				
22					68				
23			1		69				
24			3		70				
25					71				
26	1		7		72				
27	1		3	1	73				
28	2		8		74				
29	3		7	1	75				
30	10		13	3	76				
31	6	4	13	7	77				
32	12	3	20	5	78				
33	4	1	11	2	79				
34	14	2	18	8	80				
35	17	8	26	8	81				
36	12	2	24	5	82				
37	25	11	31	15	83				
38	5	13	20	21	84				
39	26	7	41	7	85				
40	7	19	23	32	86				
41	8	30	27	48	87				
42	13	14	45	32	88				
43	11	22	17	48	89				
44	15	21	33	39	90				
45	9	23	16	51	91				
46	6	14	11	33					

Table 6.2 (Continued)

DATE 25 July 1956 TIME 1255-1315 CST RUN NO. 20

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	19	34	32	56
2					48	16	18	22	33
3					49	11	17	21	50
4					50	7	18	15	29
5					51	8	16	11	30
6					52	5	14	12	24
7					53	3	11	6	17
8					54	2	12	4	21
9					55	4	7	5	8
10					56	1	3	2	4
11					57				
12					58	1		1	6
13					59	1		2	
14					60				1
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37	1		3	1	83				
38	1	1	8	2	84				
39	15	4	30	7	85				
40	7	3	15	7	86				
41	19	6	38	12	87				
42	19	2	50	17	88				
43	17	11	19	27	89				
44	33	12	63	27	90				
45	24	25	54	55	91				
46	25	25	42	41					

Table 6.2 (Continued)

DATE 25 July 1956 TIME 2155-2215 CST RUN NO. 21

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	30	25	55	70
2					48	23	28	33	55
3					49	24	47	33	74
4					50	18	28	24	48
5					51	4	31	5	48
6					52	7	19	8	28
7					53	6	12	7	20
8					54	1	5	1	9
9					55	1	4	1	5
10					56		1		1
11					57	1		1	1
12					58		2		2
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35			2		81				
36					82				
37	1		4		83				
38	1		2		84				
39	3		7	1	85				
40	2		4	2	86				
41	11		19	1	87				
42	11	2	33	10	88				
43	12	5	36	14	89				
44	27	6	88	14	90				
45	31	10	61	34	91				
46	26	14	55	43					

Table 6.2 (Continued)

DATE 25 July 1956 TIME 2355-0015 CST RUN NO. 22

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	23	37	53	75
2					48	17	32	29	78
3					49	4	43	13	97
4					50	3	24	9	42
5					51	1	27	1	40
6					52	1	9	2	12
7					53		5		7
8					54		3		3
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37	1				83				
38	6				84				
39	6				85				
40	21	1	41	1	86				
41	21				87				
42	35				88				
43	14	3	27	10	89				
44	41	8	81	15	90				
45	24	26	57	52	91				
46	31	20	60	40					



Table 6.2 (Continued)

DATE 29 July 1956. TIME 2055-2115 CST RUN NO. 23

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8			1		54				
9					55				
10					56				
11	1		4		57				
12	2		3		58				
13	2		5		59				
14	8		16	1	60				
15	3		8	1	61				
16	31	1	51	5	62				
17	13	1	22	4	63				
18	24	6	50	21	64				
19	29	12	56	30	65				
20	32	9	73	18	66				
21	27	17	53	59	67				
22	16	55	24	99	68				
23	20	32	49	50	69				
24	11	44	16	74	70				
25	1	31	7	55	71				
26	7	11	12	17	72				
27	5	11	13	19	73				
28	4	3	5	7	74				
29		4		8	75				
30	2		3		76				
31			1		77				
32	1	1	1	1	78				
33					79				
34	1	1	1	1	80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 29 July 1956 TIME 2255-2315 CST RUN NO. 24

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19	1			4	65				
20	9			13	66				
21	11			20	1	67			
22	7			11	1	68			
23	25	1		40	2	69			
24	27	2		51	4	70			
25	14	5		28	6	71			
26	31	8		69	14	72			
27	22	17		61	36	73			
28	31	10		62	23	74			
29	15	23		24	52	75			
30	15	39		40	63	76			
31	12	36		17	73	77			
32	9	32		13	62	78			
33	3	11		4	25	79			
34	4	23		6	48	80			
35	1	17		2	36	81			
36	2	6		2	11	82			
37		6			9	83			
38		1			5	84			
39		1			5	85			
40					2	86			
41		1			1	87			
42						88			
43						89			
44						90			
45						91			
46									

Table 6.2 (Continued)

DATE 1 August 1956 TIME 1255-1315 CST RUN NO. 25

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	4		19	
2					48	17		15	
3					49	6		9	
4					50	2		9	
5					51	6		16	
6					52	3		10	
7					53	7		5	
8					54	4		9	
9					55	2		10	
10					56	9		4	
11					57	2		4	
12					58	17		19	
13					59	6		8	
14					60	9		14	
15					61	5		7	
16					62	5		6	
17	2		2		63	9		11	
18					64	3		6	
19					65				
20	1		1		66	1		3	
21	3		3		67				
22	1		2		68	1		1	
23	2		3		69				
24	4		4		70				
25	2		2		71				
26	2		3		72				
27	1		1		73				
28	8		11		74				
29	4		8		75				
30	5		8		76				
31	5		10		77				
32	5		14		78				
33	8		13		79				
34	1		5		80				
35	11		18		81				
36	6		10		82				
37	9		21		83				
38	8		19		84				
39	4		9		85				
40	3		21		86				
41	9		24		87				
42	10		20		88				
43	6		16		89				
44	7		15		90				
45	6		10		91				
46	1		8						

Table 6.2 (Continued)

DATE 2 August 1956 TIME 1155-1215 CST RUN NO. 26

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	17		10	
2					48	8		5	
3					49	11		11	
4					50	19		7	
5					51	12		23	
6					52	17		15	
7					53	12		17	
8					54	12		24	
9					55	9		16	
10					56	8		9	
11					57	8		14	
12					58	11		21	
13					59	5		11	
14					60	3		17	
15					61	3		3	
16					62	3		3	
17					63	4		5	
18					64			5	
19					65	4		2	
20					66	4		1	
21					67	2			
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36	2				82				
37					83				
38					84				
39	4				85				
40	4				86				
41	7				87				
42	6		1		88				
43	6		1		89				
44	15		1		90				
45	14		4		91				
46	10		8						

Table 6.2 (Continued)

DATE 2 August 1956

TIME 1355-1415 CST

RUN NO. 27

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	24	22	52	36
2					48	17	25	38	38
3					49	24	18	34	41
4					50	22	18	37	34
5					51	16	12	37	25
6					52	17	21	32	37
7					53	14	18	26	25
8					54	9	22	14	23
9					55	5	14	14	23
10					56	4	9	9	13
11					57	5	13	8	24
12					58	2	5	3	11
13					59	1	6	3	7
14					60		6	4	7
15					61	1		3	2
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35	1		1		81				
36	1		1		82				
37	2		2		83				
38	2		3		84				
39	3		5		85				
40	2	1	5	1	86				
41	6	1	10	3	87				
42	12	2	21	4	88				
43	13	6	14	12	89				
44	13	3	36	5	90				
45	8	4	25	13	91				
46	18	14	35	22					

Table 6.2 (Continued)

DATE 2 August 1956

TIME 1255-0015 CST

RUN NO. 28

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	19	42	19	41
2					48	11	19	9	60
3					49	5	33	4	34
4					50	3	21	1	15
5					51	1	13	2	11
6					52	1	8	7	7
7					53		2	3	
8					54		1	1	
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35	1		1		81				
36	4		4		82				
37	6		15		83				
38	3		8		84				
39	9		27	2	85				
40	17		38	1	86				
41	40	3	72	7	87				
42	29	4	72	12	88				
43	18	10	39	28	89				
44	34	18	70	35	90				
45	20	33	37	82	91				
46	19	24	32	52					

Table 6.2 (Continued)

DATE 3 August 1956 TIME 0155-0215 CST RUN NO. 29

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55			3	
10					56			5	
11					57	1		7	
12					58	6		15	
13					59	3		15	
14					60	10		31	
15					61	12		28	
16					62	19		39	
17					63	25		34	
18					64	16		24	
19					65	23		32	
20					66	19		19	
21					67	26		26	
22					68	21		23	
23					69	14		14	
24					70	9		10	
25					71	10		11	
26					72	13		22	
27					73	5		11	
28					74	4		28	
29					75	3		24	
30					76	1		10	
31					77			22	
32					78			11	
33					79			8	
34					80			6	
35					81				
36					82			1	
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 3 August 1956 TIME 1255-1315 CST RUN NO. 30

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	8	2	12	2
2					48	13	5	15	6
3					49	8	4	12	4
4					50	9	2	11	3
5					51	13	3	23	4
6					52	18	7	28	7
7					53	16	11	26	13
8					54	22	7	23	12
9					55	16	7	30	14
10					56	26	3	40	12
11					57	13	15	19	36
12					58	12	14	37	34
13					59	16	6	26	20
14					60	3	25	24	51
15					61	6	12	19	28
16					62	6	18	19	32
17					63	6	25	21	49
18					64	4	15	16	30
19					65	2	10	11	20
20					66		8	8	15
21					67		19	7	32
22					68	1	5	12	16
23					69		7	5	16
24					70		1	4	5
25					71		4	1	8
26					72		2	1	4
27					73		2	1	4
28					74				
29					75			1	
30					76			1	3
31					77		1		2
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43	2				89				
44	2				90				
45	4				91				
46	10								

Table 6.2 (Continued)

DATE 3 August 1956 TIME 1455-1515 CST RUN NO. 31

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47			2	
2					48			1	1
3					49			3	1
4					50			4	4
5					51			6	
6					52			11	1
7					53			8	3
8					54			10	6
9					55	1		17	4
10					56	2		23	1
11					57	1		9	5
12					58	6	2	27	8
13					59	6	2	13	6
14					60	8	5	23	12
15					61	5	6	18	21
16					62	8	5	25	13
17					63	13	13	23	31
18					64	12	12	34	29
19					65	12	20	21	31
20					66	12	19	19	34
21					67	11	33	17	45
22					68	16	39	24	62
23					69	15	21	20	46
24					70	13	21	16	27
25					71	19	11	22	22
26					72	20	7	22	16
27					73	9	10	9	14
28					74	20		20	2
29					75	17	8	17	10
30					76	3	1	3	4
31					77	5	3	5	12
32					78	2	1	2	5
33					79	2	1	3	1
34					80			1	2
35					81	1		1	1
36					82	1		1	
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46			1						

Table 6.2 (Continued)

DATE 6 August 1956 TIME 1955-2015 CST RUN NO. 32

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47			38	2
2					48			47	97
3					49			55	115
4					50			43	81
5					51			23	39
6					52			1	1
7					53			2	2
8					54				1
9					55				1
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 7 August 1956 TIME 1255-1310 CST RUN NO. 33

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	20	13	40	36
2					48	15	17	27	31
3					49	22	17	34	30
4					50	16	22	26	34
5					51	20	15	25	42
6					52	12	20	15	34
7					53	9	16	12	35
8					54	10	18	11	38
9					55	5	23	6	39
10					56	3	14	3	19
11					57	5	14	0	31
12					58	2	9	2	16
13					59		2		2
14					60		2		3
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32	1		1		78				
33	2		2		79				
34	2		2		80				
35	5		5		81				
36	8		8		82				
37	2		7		83				
38	1		3		84				
39	5		17		85				
40	4	2	11	3	86				
41	5	1	19	1	87				
42	9	8	43	11	88				
43	10	2	24	14	89				
44	16	8	53	18	90				
45	17	6	37	16	91				
46	21	11	45	24					

Table 6.2 (Continued)

DATE 7 August 1956 TIME 1455-1515 CST RUN NO. 34

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19	1		2		65				
20	2		7		66				
21	4		10		67				
22	5		7	2	68				
23	7		24	2	69				
24	12		29	7	70				
25	6	4	17	11	71				
26	15	1	51	9	72				
27	25	6	49	15	73				
28	32		62	11	74				
29	11	6	22	32	75				
30	24	6	41	20	76				
31	36	13	57	34	77				
32	20	14	33	45	78				
33	20	5	26	13	79				
34	7	25	17	48	80				
35	7	17	16	36	81				
36	2	19	3	32	82				
37	2	16	2	28	83				
38	1	24	1	34	84				
39	1	17	1	23	85				
40		24	1	31	86				
41		17		18	87				
42		13		14	88				
43		7		8	89				
44		5		5	90				
45				1	91				
46									

Table 6.2 (Continued)

DATE 7 August 1956 TIME 2255-2315 CST RUN NO. 35-S

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16	1		5		62				
17	2		4		63				
18	4		10		64				
19	4		18		65				
20	15		32		66				
21	30		53		67				
22	13		24	1	68				
23	58		86		69				
24	41	1	62	4	70				
25	14	3	28	15	71				
26	33	5	72	18	72				
27	12	17	24	35	73				
28	8	12	28	24	74				
29	3	40	9	88	75				
30	1	36	9	63	76				
31	1	38	12	60	77				
32		29	3	50	78				
33		12	2	28	79				
34		20		40	80				
35		14		23	81				
36		9		17	82				
37		2		11	83				
38		1			84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 11 August 1956 TIME 2125-2145 CST RUN NO. 35

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1			3		3				
2			5		11				
3			3		6				
4			8		14				
5			11		12				
6			5		9				
7			30		30				
8			26		28				
9			3		3				
10			108		108				
11			25		25				
12			12		121				
13					10				
14					17				
15	1			1	52				
16	2			3	28				
17				4					
18				28	1				
19	4			48					
20	30			46					
21	52			88					
22	50			173					
23	77			31					
24	17			38					
25	5			18					
26	2								
27				1					
28									
29									
30									
31									
32									
33									
34									
35									
36									
37									
38									
39									
40									
41									
42									
43									
44									
45									
46									

Table 6.1 (Continued)

DATE 11 August 1956 TIME 2325-2345 CST RUN NO. 36

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27			1		73				
28					74				
29					75				
30			2		76				
31	2		14		77				
32	8		18	2	78				
33	10		41		79				
34	26		50	5	80				
35	72	1	105	12	81				
36	35	3	46	24	82				
37	50	9	63	32	83				
38	18	23	23	76	84				
39	10	37	11	84	85				
40	4	37	6	104	86				
41		57		55	87				
42	2	35	3	43	88				
43		18		22	89				
44		16	1	16	90				
45		2		2	91				
46		2		2					

Table 6.2 (Continued)

DATE 12 August 1956 TIME 0255-0315 CST RUN NO. 37

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	24	13	58	24
2					48	26	22	53	38
3					49	26	33	49	61
4					50	26	20	60	45
5					51	29	18	54	58
6					52	19	27	36	56
7					53	23	22	30	45
8					54	7	23	14	39
9					55	13	23	15	36
10					56	4	5	8	15
11					57	1	3	3	12
12					58	2	2	3	2
13					59	1	2	1	3
14					60		2		
15					61				1
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41	3	2		5	87				
42	2	1		10	88				
43	7	1		10	89				
44	8	1		20	90				
45	6	9		22	91				
46	13	11		28	14				



Table 6.2 (Continued)

DATE 12 August 1956 TIME 0455-0515 CST RUN NO. 38

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	5	9	9	18
2					48	1	9	3	15
3					49		5	1	10
4					50				2
5					51			1	1
6					52			1	
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32			2		78				
33					79				
34			2		80				
35	4		9		81				
36	8		8		82				
37	16		33	1	83				
38	11	1	34	4	84				
39	28	1	52	8	85				
40	29	17	49	40	86				
41	48	22	89	42	87				
42	35	29	83	71	88				
43	30	51	31	97	89				
44	18	31	50	68	90				
45	9	42	14	73	91				
46	1	23	7	31					

Table 6.2 (Continued)

DATE 13 August 1956 TIME 2225-2245 CST RUN NO. 39

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9		1		1	55				
10					56				
11					57				
12	1	1	1	1	58				
13					59				
14		3		3	60				
15		1	1	1	61				
16		10		11	62				
17		1	1	1	63				
18		30	11	30	64				
19	2	22	11	27	65				
20	2	33	40	41	66				
21	9	25	34	46	67				
22	8	34	19	89	68				
23	39	18	61	47	69				
24	21	28	25	76	70				
25	21	12	28	44	71				
26	38	2	41	5	72				
27	33	7	43	23	73				
28	30	1	48	5	74				
29	6	5	13	10	75				
30	16	2	31	7	76				
31	6	3	26	6	77				
32	2	1	13	1	78				
33	3		14	1	79				
34			8	1	80				
35	1		5		81				
36			2		82				
37	1		2		83				
38				1	84				
39	1		1		85				
40			1		86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 14 August 1956 TIME 0025-0045 CST RUN NO. 40

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	20	16	29	21
2					48	17	10	28	15
3					49	15	15	31	18
4					50	12	7	29	11
5					51	13	13	32	19
6					52	3	8	16	17
7					53	8	14	26	27
8					54	6	17	12	28
9					55	4	20	6	23
10					56	5	21	8	24
11					57		12	1	15
12					58	1	6	2	7
13					59		1		1
14					60		1		1
15					61		1		1
16					62				1
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30				1	76				
31			1		77				
32					78				
33					79				
34	1		2		80				
35			4	3	81				
36	2		3	1	82				
37	2		17	3	83				
38	2		7	8	84				
39	7	3	26	17	85				
40	4	1	21	24	86				
41	22	7	45	34	87				
42	18	7	50	37	88				
43	20	6	11	29	89				
44	26	15	33	32	90				
45	17	19	20	36	91				
46	15	20	18	25					

Table 6.2 (Continued)

DATE 14 August 1956 TIME 0255-0315 CST RUN NO. 41

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	1		2	
2					48	2		2	1
3					49	2		3	3
4					50	7		15	2
5					51	11		22	4
6					52	7	3	17	10
7					53	27	8	59	26
8					54	27	16	65	31
9					55	44	19	94	75
10					56	42	44	74	61
11					57	34	27	58	90
12					58	20	51	34	99
13					59	11	40	19	34
14					60	5	15	10	23
15					61		14	1	12
16					62		2	1	5
17					63		1	1	2
18					64			1	
19					65			1	1
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46							1		

Table 6.2 (Continued)

DATE 14 August 1956 TIME 0455-0515 CST RUN NO. 42

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50			1	
5					51				
6					52			1	
7					53	2	1	2	1
8					54	2	1	3	1
9					55	3		4	
10					56	6	1	9	2
11					57	5	2	11	3
12					58	19	9	34	13
13					59	14	5	28	11
14					60	28	9	52	25
15					61	25	12	52	31
16					62	33	27	66	50
17					63	26	48	56	108
18					64	26	28	41	69
19					65	17	34	42	59
20					66	16	24	34	45
21					67	7	20	18	28
22					68	4	13	9	22
23					69	4	3	7	4
24					70	1	1	4	2
25					71	1		2	1
26					72	1	1	1	1
27					73		1		1
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 15 August 1956 TIME 1155-1215 CST RUN NO. 43

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	24	20	41	33
2					48	7	13	14	21
3					49	6	14	8	31
4					50	3	9	10	21
5					51	6	8	10	14
6					52	2	4	3	11
7					53	1	4	2	12
8					54	2	5	3	10
9					55	1	1	3	3
10					56	1	1	2	1
11					57		2	1	2
12					58		5	1	8
13					59		1	1	1
14					60	1	1	3	1
15					61		1	2	1
16					62				
17					63				
18					64				
19					65			1	
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 15 August 1956 TIME 1355-1415 CST RUN NO. 44

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	3	9	6	14
2					48	2	5	2	6
3				1	49		11	2	12
4					50		2	1	4
5					51		1		1
6				1	52				2
7					53		1		1
8				1	54		3		3
9				1	55				1
10				1	56				
11					57		1		1
12				1	58		1		1
13				1	59		1		1
14				1	60				
15					61				
16			1	2	62				
17			0	3	63		1		1
18			3	6	64				
19		1	0	5	65				
20					66				
21	5	1	2	8	67				
22	2	3	9	13	68				
23	5	1	16	4	69				
24	2		8	7	70				
25	4	1	4	9	71				
26	5	3	7	8	72				
27	4	3	10	8	73				
28	14	4	23	7	74				
29	4	1	8	7	75				
30	14	6	20	16	76				
31	10	13	21	26	77				
32	12	6	19	14	78				
33	16	5	27	6	79				
34	9	10	15	21	80				
35	18	3	32	12	81				
36	12	12	21	17	82				
37	11	10	18	22	83				
38	13	16	23	20	84				
39	17	10	39	16	85				
40	5	20	13	40	86				
41	21	15	41	28	87				
42	10	15	27	22	88				
43	4	9	12	17	89				
44	10	13	24	18	90				
45	5	15	11	26	91				
46	3	8	6	11					

Table 6.2 (Continued)

DATE 15 August 1956 TIME 1655-1715 CST RUN NO. 45

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	2	5	2	7
2					48			3	4
3					49			3	4
4					50				1
5					51				
6					52				
7					53			1	2
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 15 August 1956 TIME 1840-1900 CST RUN NO. 46

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12	1		1		58				
13					59				
14	1	3	2	3	60				
15	1	2	2	3	61				
16	5	7	14	12	62				
17	4	3	12	6	63				
18	8	15	24	27	64				
19	22	36	23	51	65				
20	16	15	43	18	66				
21	23	23	45	40	67				
22	39	30	32	45	68				
23	19	17	65	33	69				
24	14	12	40	35	70				
25	24	19	26	39	71				
26	15	8	53	23	72				
27	25	12	40	39	73				
28	2	10	27	21	74				
29	8	17	5	38	75				
30	1	3	6	20	76				
31	3	3	6	12	77				
32	4	4	8	8	78				
33	3		4	3	79				
34	1		1	2	80				
35	1	1		1	81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 20 August 1956 TIME 0955-1015 CST RUN NO. 47

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49		1	4	1
4					50		1	7	1
5					51			6	
6					52		2	4	2
7					53		2	4	2
8					54		2	5	2
9					55		1	7	1
10					56			6	
11					57		5	3	6
12					58	3		4	4
13					59		2	3	4
14					60		8	2	9
15					61	3	3	5	5
16					62	1	2	4	5
17					63	3	9	7	14
18					64	3	8	6	12
19					65	3	9	9	11
20					66		9	5	11
21					67	4	14	11	18
22					68	4	21	6	26
23					69	2	15	9	18
24					70	9	18	18	20
25					71	6	24	13	31
26					72	16	24	25	34
27					73	4	10	10	25
28					74	11	4	21	8
29					75	12	15	36	26
30					76	4	11	12	21
31					77	16	5	32	20
32					78	16	2	31	9
33					79	13	5	20	28
34					80	5	1	6	15
35					81	20		24	8
36					82	25		29	14
37					83			4	5
38					84	25	1	34	6
39					85	6		7	3
40					86	7		9	3
41					87	6		4	5
42					88	2		1	9
43					89			8	6
44					90	7		1	7
45					91	1		3	4
46					Off Scale	2	1	1	16

Table 6.2 (Continued)

DATE 21 August 1956 TIME 0855-0915 CST RUN NO. 48

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48			1	
3					49				
4					50				
5					51				
6					52	2		4	1
7					53	1		6	2
8					54	4	2	7	5
9					55	3	2	10	4
10					56	8	6	25	8
11					57	2	10	15	15
12					58	9	18	29	29
13					59	13	9	32	26
14					60	29	23	58	42
15					61	9	26	31	44
16					62	32	19	53	40
17					63	14	42	29	89
18					64	35	30	59	53
19					65	17	20	30	39
20					66	14	14	26	36
21					67	15	3	24	15
22					68	13	8	16	17
23					69	7	2	10	6
24					70	7	3	7	4
25					71	5	1	6	1
26					72	1	1	1	1
27					73		1		1
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 21 August 1956 TIME 1055-1115 CST RUN NO. 49

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	10	6	18	14
2					48	6	5	19	10
3					49	6	6	16	12
4					50	8	9	12	12
5					51	13	6	24	17
6					52	8	10	17	20
7					53	8	15	28	27
8					54	3	11	19	21
9					55	22	16	39	34
10					56	15	14	37	31
11					57	14	19	24	44
12					58	20	23	49	48
13					59	19	13	26	25
14					60	20	18	38	30
15					61	12	18	20	28
16					62	14	9	25	16
17					63	7	15	10	29
18					64	6	5	8	12
19					65	4	3	5	8
20					66	2	9	5	10
21					67	3	2	4	2
22					68		2	3	3
23					69		2		2
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 21 August 1956

TIME 1355-1415 CST

RUN NO. 50

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48	1			1
3					49				1
4					50				
5					51	2			1
6					52			3	2
7					53	2	1	2	2
8					54	4	5	4	4
9					55	10	4	14	7
10					56	7	5	13	8
11					57	7	10	13	14
12					58	13	16	25	26
13					59	9	8	21	13
14					60	16	27	31	13
15					61	17	27	24	29
16					62	15	16	35	25
17					63	10	21	21	37
18					64	15	9	30	29
19					65	14	18	29	28
20					66	11	12	34	25
21					67	16	13	28	29
22					68	17	16	31	50
23					69	18	9	34	24
24					70	13	13	30	32
25					71	5	8	13	18
26					72	10		23	9
27					73	4	1	6	5
28					74	1		4	1
29					75			4	2
30					76	1		1	4
31					77			2	1
32					78			1	2
33					79				3
34					80				
35					81				1
36					82				1
37					83				1
38					84				1
39					85				1
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46					92				

Table 6.2 (Continued)

DATE 21 August 1956

TIME 1525-1545 CST

RUN NO. 51

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				1
13					59				
14					60				
15					61				
16					62				
17					63				2
18					64	3	4	5	4
19					65	1	4	7	4
20					66	1	7	6	8
21					67	3	8	8	8
22					68	2	19	9	13
23					69	3	12	11	15
24					70	4	10	6	19
25					71	6	19	9	19
26					72	12	15	22	31
27					73	8	17	13	20
28					74	11	7	29	28
29					75	22	21	33	36
30					76	6	13	18	13
31					77	14	18	30	27
32					78	14	9	39	32
33					79	17	8	26	31
34					80	15	8	21	13
35					81	18	4	28	28
36					82	25	11	37	26
37					83	10	9	15	14
38					84	17	5	32	25
39					85	9	5	13	7
40					86	6	2	10	24
41					87	4	3	8	5
42					88	4	1	18	9
43					89	1	1	3	4
44					90	2	1	10	10
45					91	1		4	1
46					92			4	4

Table 6.2 (Continued)

DATE 24 August 1956 TIME 1110-1130 CST RUN NO. 52

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1			2		47				
2			1		48				
3					49				
4	2		2		50				
5	1		2		51				
6			2		52				
7	1		3		53				
8	6		9		54				
9	5		9		55				
10	7		8		56				
11	9		25		57				
12	10		27		58				
13	5		15		59				
14	9		21		60				
15	3		12		61				
16	12		34		62				
17	8		18		63				
18	8		26		64				
19	6		14		65				
20	16		35		66				
21	12		24		67				
22	5		9		68				
23	15		27		69				
24	8		21		70				
25	2		2		71				
26	13		20		72				
27	5		10		73				
28	6		12		74				
29	3		4		75				
30	6		19		76				
31	14		16		77				
32	6		10		78				
33	4		4		79				
34	6		9		80				
35	3		9		81				
36	8		5		82				
37	6		9		83				
38	3		5		84				
39	5		5		85				
40	2		3		86				
41			1		87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 24 August 1956 TIME 1955-2015 CST RUN NO. 53

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16	1			1	62				
17	1			2	63				
18	3	1		5	2	64			
19	7	15		12	20	65			
20	30	31		41	29	66			
21	61	92		112	137	67			
22	27	83		63	123	68			
23	65	11		128	72	69			
24	26	7		67	90	70			
25	8			21	5	71			
26	9			21	1	72			
27	1			2		73			
28				1		74			
29				1		75			
30	1			1		76			
31						77			
32						78			
33						79			
34						80			
35						81			
36						82			
37						83			
38						84			
39						85			
40						86			
41						87			
42						88			
43						89			
44						90			
45						91			
46									



Table 6.2 (Continued)

DATE 24 August 1956 TIME 2155-2215 CST RUN NO. 54

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16	1		1		62				
17					63				
18			1		64				
19	1		1		65				
20	5		8	1	66				
21	11	6	20	8	67				
22	9	11	14	14	68				
23	24	10	51	11	69				
24	25	21	55	38	70				
25	18	32	30	50	71				
26	45	24	30	47	72				
27	36	32	72	67	73				
28	41	21	74	48	74				
29	4	28	17	75	75				
30	9	16	22	48	76				
31	4	12	11	31	77				
32	1	11	4	19	78				
33	2	2	9	8	79				
34	2	5	5	8	80				
35		2	5	5	81				
36					82				
37			1		83				
38	2		2		84				
39			1		85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 25 August 1956 TIME 0055-0115 CST RUN NO. 55

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49			1	1
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27	3	2	6	2	73				
28	6		17		74				
29	3		6		75				
30	10	4	22	7	76				
31	21	5	40	8	77				
32	22	9	55	19	78				
33	38	5	62	12	79				
34	34	22	67	46	80				
35	39	28	76	55	81				
36	18	23	40	45	82				
37	23	40	36	83	83				
38	10	37	15	77	84				
39	9	24	15	52	85				
40	2	21	6	35	86				
41	1	11	3	23	87				
42	1	2	2	5	88				
43	1	3	2	6	89				
44	1	2	1	2	90				
45		1		1	91				
46		1		1					

Table 6.2 (Continued)

DATE 25 August 1956 TIME 0255-0315 CST RUN NO.56

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49				
4					50				
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18			1		64				
19					65				
20		1	2	1	66				
21		1	1	1	67				
22					68				
23	1		8	3	69				
24	2		14	7	70				
25		4	2	15	71				
26	5		19	8	72				
27	3	3	18	18	73				
28	8	3	24	16	74				
29	9	8	13	32	75				
30	18	13	31	26	76				
31	49	24	78	46	77				
32	26	26	41	36	78				
33	36	12	47	15	79				
34	27	29	52	50	80				
35	22	33	50	46	81				
36	10	24	16	37	82				
37	11	22	34	43	83				
38	6	20	8	35	84				
39	4	6	13	14	85				
40	1	5	3	15	86				
41	2	3	4	8	87				
42		3		5	88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 25 August 1956 TIME 1725-1745 CST RUN NO. 57

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	1		7	
2					48	1			
3					49	9	1	23	3
4					50	5	-	11	12
5					51	14	3	36	9
6					52	15	6	32	13
7					53	18	8	40	18
8					54	19	7	39	21
9					55	19	19	42	40
10					56	30	17	49	34
11					57	13	22	30	41
12					58	37	30	60	50
13					59	15	12	28	27
14					60	18	26	30	57
15					61	6	22	12	38
16					62	5	17	8	28
17					63	4	16	5	35
18					64	5	14	6	19
19					65	6		1	16
20					66		4	1	6
21					67	2	6	2	7
22					68				5
23					69	1	4	1	
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46	3								

Table 6.2 (Continued)

DATE 25 August 1956 TIME 1925-1945 CST RUN NO. 58

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	24	36	71	53
2					48	6	56	22	78
3					49	4	79	17	137
4					50	2	35	5	89
5					51		11	2	63
6					52		6	2	25
7					53	2	2	3	11
8					54				
9					55		2		5
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41	4		7		87				
42	7		15		88				
43	19		34		89				
44	46		88		90				
45	25	6	63	9	91				
46	27	7	75	7					

Table 6.2 (Continued)

DATE 25 August 1956 TIME 2225-2245 CST RUN NO. 59

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	16	61	23	102
2					48	4	25	4	47
3					49	4	16	5	28
4					50	1	6	1	12
5					51	1	3	1	4
6					52				
7					53	1	1	1	1
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41	25		68	3	87				
42	34	2	111	9	88				
43	46	7	72	17	89				
44	57	15	86	44	90				
45	12	60	21	123	91				
46	9	44	22	88					

Table 6.2 (Continued)

DATE 25 August 1956 TIME 0135-0155 CST RUN NO. 60

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	3	1	3	2
2					48	4		5	2
3					49	8	1	9	2
4					50	8	1	13	4
5					51	22	7	35	9
6					52	19	11	29	16
7					53	35	13	53	24
8					54	37	32	78	60
9					55	34	21	79	41
10					56	18	50	56	98
11					57	26	47	64	96
12					58	12	20	24	38
13					59	5	20	12	50
14					60	2	8	8	17
15					61	3	2	4	5
16					62		5		9
17					63				2
18					64		1	1	2
19					65				1
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45	1		1		91				
46									

Table 6.2 (Continued)

DATE 26 August 1956 TIME 1055-1115 CST RUN NO. 61

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	3		4	
2					48	4		4	
3					49	6	4	9	5
4					50	9		10	2
5					51	3	8	5	8
6					52	12	9	15	7
7					53	16	10	24	14
8					54	11	16	16	19
9					55	23	30	40	36
10					56	16	7	32	11
11					57	19	23	38	32
12					58	23	36	41	46
13					59	19	11	23	18
14					60	17	24	50	47
15					61	10	12	22	21
16					62	6	12	22	30
17					63	8	12	25	62
18					64	5	5	18	24
19					65	5	3	18	27
20					66	3		10	16
21					67	5	6	9	24
22					68	4	3	10	15
23					69	5	4	11	7
24					70	2	3	7	6
25					71	2		4	1
26					72	2	1	4	1
27					73			1	
28					74	2		3	
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 26 August 1956 TIME 1355-1415 CST RUN NO. 62

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47				
2					48				
3					49	1		1	
4					50	1		1	
5					51				
6					52	4		4	
7					53	5	1	7	4
8					54	3		5	1
9					55	5	2	10	8
10					56	9	3	18	5
11					57	6	10	12	17
12					58	23	11	39	17
13					59	17	10	29	16
14					60	21	28	31	40
15					61	15	19	32	29
16					62	21	27	41	50
17					63	21	33	40	63
18					64	20	21	31	37
19					65	17	21	48	41
20					66	23	12	37	34
21					67	9	16	26	38
22					68	8	18	20	38
23					69	6	6	18	17
24					70		2	7	13
25					71	4		7	7
26					72			5	3
27					73			1	
28					74			3	
29					75	1		4	
30					76				
31					77			1	
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38					84				
39					85				
40					86				
41					87				
42					88				
43					89				
44					90				
45					91				
46									

Table 6.2 (Continued)

DATE 29 August 1956 TIME 1925-1945 CST RUN NO. 65

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	34	7	10	53
2					48	11	7	9	18
3					49	8	4	4	13
4					50	5	1	3	7
5					51	5	1	1	6
6					52				1
7					53				
8					54			1	
9					55	1			1
10					56	1			1
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34					80				
35					81				
36					82				
37					83				
38	1				84				
39	1	17			85				
40	5	10			86				
41	2	30			87				
42	17	44			88				
43	23	25			89				
44	30	39			90				
45	56	17			91				
46	34	20							

Table 6.2 (Continued)

DATE 29 August 1956 TIME 2125-2145 CST RUN NO. 66

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	2			6
2					48		1		4
3					49				3
4					50				1
5					51				
6					52				
7					53				
8					54				
9					55				
10					56				
11					57				
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29	1		2		75				
30	1		3		76				
31	1		1		77				
32	7		12		78				
33	7		14		79				
34	9		22		80				
35	18		50		81				
36	16	6	39	7	82				
37	22	9	65	13	83				
38	17	23	39	31	84				
39	29	22	55	25	85				
40	25	24	39	42	86				
41	31	33	59	66	87				
42	23	32	38	73	88				
43	13	32	18	77	89				
44	12	35	14	73	90				
45	3	15	4	38	91				
46	3	5	3	20					

Table 6.2 (Continued)

DATE 30 August 1956 TIME 0025-0045 CST RUN NO. 67

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.		
	Source	450 m	Source	450 m		Source	450 m	Source	450 m	
1					47	34	12		53	47
2					48	34	19		63	41
3					49	42	21		56	62
4					50	27	25		35	47
5					51	26	50		36	77
6					52	14	33		18	45
7					53	9	32		10	39
8					54	7	22		7	27
9					55	2	12		2	15
10					56	2	2		4	4
11					57		1			2
12					58		2			2
13					59					
14					60					
15					61					
16					62		1			1
17					63					
18					64					
19					65					
20					66					
21					67					
22					68					
23					69					
24					70					
25					71					
26					72					
27					73					
28					74					
29					75					
30					76					
31					77					
32					78					
33					79					
34					80					
35					81					
36					82					
37	1				83					
38					84					
39					85					
40					86					
41	1				87					
42	2				88					
43	4				89					
44	8	1			90					
45	9	4			91					
46	20	3								

Table 6.2 (Continued)

DATE 30 August 1956 TIME 0025-0245 CST RUN NO. 68

Post No.	10 - min.		20 - min.		Post No.	10 - min.		20 - min.	
	Source	450 m	Source	450 m		Source	450 m	Source	450 m
1					47	6	42	23	60
2					48	7	28	12	43
3					49	3	27	7	40
4					50		15	3	21
5					51	2	8	2	12
6					52		3		3
7					53		4		4
8					54				
9					55				
10					56				
11					57		1		1
12					58				
13					59				
14					60				
15					61				
16					62				
17					63				
18					64				
19					65				
20					66				
21					67				
22					68				
23					69				
24					70				
25					71				
26					72				
27					73				
28					74				
29					75				
30					76				
31					77				
32					78				
33					79				
34			1		80				
35			7	1	81				
36			9		82				
37	8		24	1	83				
38	2	1	11	2	84				
39	16		24	2	85				
40	8	1	26	9	86				
41	35	2	65	25	87				
42	41	5	86	43	88				
43	36	12	50	41	89				
44	44	20	63	47	90				
45	21	36	35	70	91				
46	11	35	31	55					

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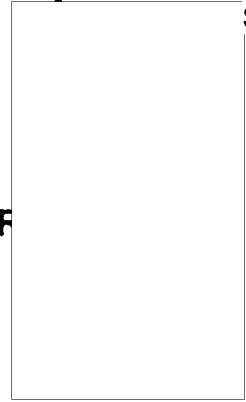
<p>AD 152572 Air Force Cambridge Research Center Geophysics Research Directorate Bedford, Mass.</p> <p>PROJECT PRAIRIE GRASS, A FIELD PROGRAM IN DIFFUSION (Vol. I), Unclassified Report July 1958, 270 p. incl. illus. tables (Geophysical Research Papers No. 59; AFRCR-TR-58-235 (I))</p> <p>Unclassified Report</p> <p>Project Prairie Grass was a field program designed to provide experimental data on the diffusion of a tracer gas over a range of 800 meters. In each of 70 experiments the gas was released continuously for 10 minutes at a source located near flat prairie in Nebraska under a variety of meteorological conditions during July and August of 1956. This paper includes a brief description of the tracer technique and the meteorological equipment employed in the field program. Tabulations of the diffusion data</p>	<p>AD 152572 Air Force Cambridge Research Center Geophysics Research Directorate Bedford, Mass.</p> <p>PROJECT PRAIRIE GRASS, A FIELD PROGRAM IN DIFFUSION (Vol. II), Unclassified Report July 1958, 270 p. incl. illus. tables (Geophysical Research Papers No. 59; AFRCR-TR-58-235 (II))</p> <p>Unclassified Report</p> <p>Project Prairie Grass was a field program designed to provide experimental data on the diffusion of a tracer gas over a range of 800 meters. In each of 70 experiments the gas was released continuously for 10 minutes at a source located near flat prairie in Nebraska under a variety of meteorological conditions during July and August of 1956. This paper includes a brief description of the tracer technique and the meteorological equipment employed in the field program. Tabulations of the diffusion data</p>	<p>AD 152572 Air Force Cambridge Research Center Geophysics Research Directorate Bedford, Mass.</p> <p>PROJECT PRAIRIE GRASS, A FIELD PROGRAM IN DIFFUSION (Vol. III), Unclassified Report July 1958, 270 p. incl. illus. tables (Geophysical Research Papers No. 59; AFRCR-TR-58-235 (III))</p> <p>Unclassified Report</p> <p>Project Prairie Grass was a field program designed to provide experimental data on the diffusion of a tracer gas over a range of 800 meters. In each of 70 experiments the gas was released continuously for 10 minutes at a source located near flat prairie in Nebraska under a variety of meteorological conditions during July and August of 1956. This paper includes a brief description of the tracer technique and the meteorological equipment employed in the field program. Tabulations of the diffusion data</p>	<p>AD 152572 Air Force Cambridge Research Center Geophysics Research Directorate Bedford, Mass.</p> <p>PROJECT PRAIRIE GRASS, A FIELD PROGRAM IN DIFFUSION (Vol. I), Unclassified Report July 1958, 270 p. incl. illus. tables (Geophysical Research Papers No. 59; AFRCR-TR-58-235 (I))</p> <p>Unclassified Report</p> <p>Project Prairie Grass was a field program designed to provide experimental data on the diffusion of a tracer gas over a range of 800 meters. In each of 70 experiments the gas was released continuously for 10 minutes at a source located near flat prairie in Nebraska under a variety of meteorological conditions during July and August of 1956. This paper includes a brief description of the tracer technique and the meteorological equipment employed in the field program. Tabulations of the diffusion data</p>	<p>UNCLASSIFIED</p> <p>1. Gas diffusion - Measurement 2. Micrometeorology - Measurement I. edited by M. L. Barad</p>	<p>UNCLASSIFIED</p> <p>1. Gas diffusion - Measurement 2. Micrometeorology - Measurement I. edited by M. L. Barad</p>	<p>UNCLASSIFIED</p> <p>1. Gas diffusion - Measurement 2. Micrometeorology - Measurement I. edited by M. L. Barad</p>	<p>UNCLASSIFIED</p> <p>1. Gas diffusion - Measurement 2. Micrometeorology - Measurement I. edited by M. L. Barad</p>
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<p>AD 152572</p> <p>and the meteorological data collected during the gas releases under a variety of meteorological conditions during other selected periods during the Summer of 1956.</p>	<p>UNCLASSIFIED</p>	<p>AD 152572</p> <p>and the meteorological data collected during the gas releases under a variety of meteorological conditions during other selected periods during the Summer of 1956.</p>	<p>UNCLASSIFIED</p>
<p>AD 152572</p> <p>and the meteorological data collected during the gas releases under a variety of meteorological conditions during other selected periods during the Summer of 1956.</p>	<p>UNCLASSIFIED</p>	<p>AD 152572</p> <p>and the meteorological data collected during the gas releases under a variety of meteorological conditions during other selected periods during the Summer of 1956.</p>	<p>UNCLASSIFIED</p>

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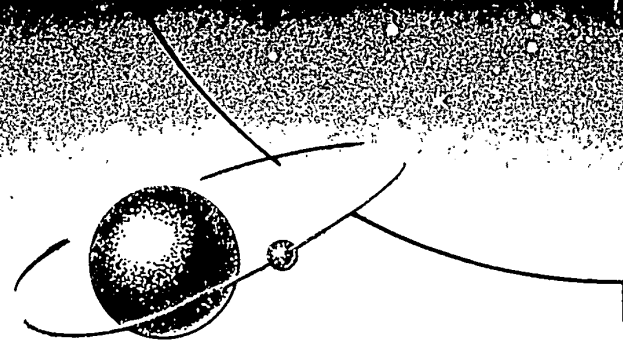
**GEOPHYSICAL RESEARCH PAPER  
No. 59**

**PROJECT PRAIRIE GRASS, A FIELD PROGRAM  
IN DIFFUSION.  
VOLUME II**

**EDITED BY  
MORTON L. BARAD**

**JULY 1958**

**GRD**



**GEOPHYSICS RESEARCH DIRECTORATE  
AIR FORCE CAMBRIDGE RESEARCH CENTER  
AIR RESEARCH AND DEVELOPMENT COMMAND  
UNITED STATES AIR FORCE  
BEDFORD, MASSACHUSETTS**

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PROJECT PRAIRIE GRASS,  
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Volume II

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Project 7657

Atmospheric Analysis Laboratory  
GEOPHYSICS RESEARCH DIRECTORATE  
AIR FORCE CAMBRIDGE RESEARCH CENTER  
AIR RESEARCH AND DEVELOPMENT COMMAND  
UNITED STATES AIR FORCE  
Bedford, Mass.

## ABSTRACT

Project Prairie Grass was a field program designed to provide experimental data on the diffusion of a tracer gas over a range of 800 meters. In each of 70 experiments the gas was released continuously for 10 minutes at a source located near ground level. The gas releases were made over a flat prairie in Nebraska under a variety of meteorological conditions during July and August of 1956.

This paper, published in two volumes, includes a brief history of the project and detailed descriptions of the tracer technique and the meteorological equipment employed in the field program. Tabulations of the diffusion data and the meteorological data collected during the gas releases are also presented. In addition this paper contains data on the heat budget at the air-earth interface during other selected periods during the Summer of 1956.

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CHAPTER 7  
INSTRUMENTATION USED BY THE TEXAS A&M GROUP

R.L. Richman\* and W. Covey  
Texas A&M Research Foundation

7.1 The Mobile Micrometeorological Station

The mobile micrometeorological station of the Texas A&M group was installed at the extreme west end of the observation line (Figure 7.1). Figure 7.2 shows the relative locations of the component elements of the station. The station consisted of (a) a slender aluminum pipe mast supporting six anemometers at heights of 8, 4, 2, 1, 0.5, and 0.25 meters, (b) a similar mast supporting seven temperature measuring, radiation shielded, copper-constantan thermocouple junctions at heights of 8, 4, 2, 1, 0.5, 0.25, and 0.125 meters, (c) a similar mast supporting seven polyethylene air sampling tubes at heights of 8, 4, 1, 0.5, 0.25, and 0.125 meters, (d) a triangular section, tubular steel, fold-over type tower supporting at a height of 16 meters an air sampling tube, an anemometer, a shielded thermocouple, a wind vane and a radioactive point collector, (e) a U. S. Signal Corps instrument shelter housing maximum and minimum thermometers and a thermograph, (f) an 8-inch rain gauge and a weighing type recording rain gauge, (g) a wind vane supported at a height of 1 meter by an iron pipe stake, (h) a Gier and Dunkle net exchange radiometer supported at a height of 1 meter, (i) an inverted Eppley thermoelectrical pyrliometer supported by an iron pipe standard at a height of 2 meters to receive reflected short-wave radiation, (j) an instrument trailer which housed indicating and recording apparatus, (k) an Eppley pyrliometer mounted on the roof of the trailer, (l) two differentially connected shielded thermocouple measuring junctions supported by a pipe stake at heights of 1/2 and 1 meter, and (m) six copper-constantan temperature measuring junctions at depths of 3.125, 6.25, 12.5, 25, 50, and 100 cm in the

\*Present affiliation: U. S. Navy Electronics Laboratory

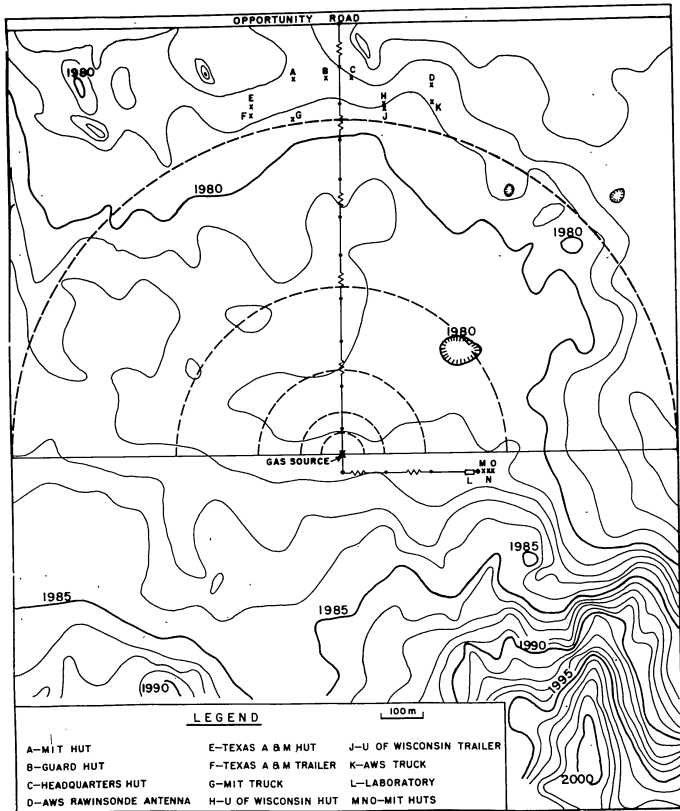


Figure 7.1 Topography of field site and layout of equipment

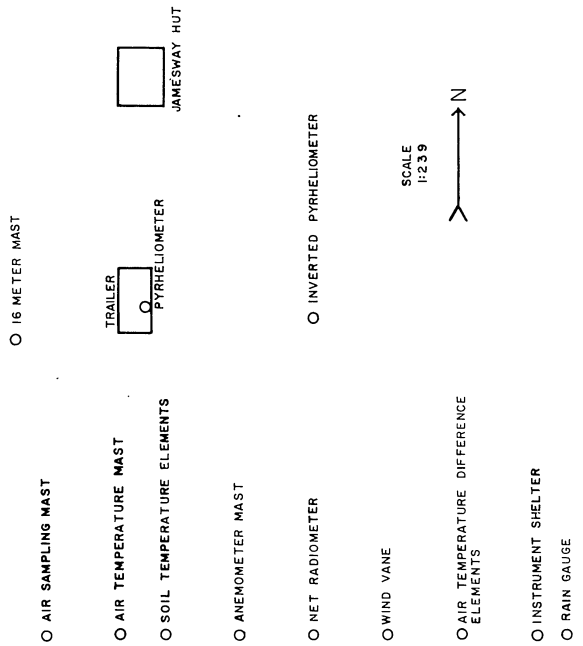


Figure 7.2 The micrometeorological station (Texas A and M)

soil. Figure 7.3 illustrates the vertical distribution of the sensing elements.

The instrument trailer was a 15-foot house trailer shell, the interior of which was designed to accommodate the recording and indicating equipment associated with the exposed sensing elements.<sup>5</sup> Figures 7.4 and 7.5 illustrate the assignment of space in the trailer. The principal instruments were (a) a Thornthwaite dew-point hygrometer and associated air sampling apparatus, (b) a group of six recording milliammeters with modulated-carrier-type d-c amplifiers for recording insolation, reflected short-wave radiation, net radiation, temperature differences, wind direction, and absolute temperatures, (c) a temperature indicating system with a switch for selecting thermocouple measuring junctions, and (d) a counting system for indicating the number of turns of the anemometers, that is, for recording wind profiles. These instruments will be discussed individually and described in detail. In addition, space was provided for computing and plotting data, storing spare parts, and storing the sensing elements and supporting structures during transit.

#### 7.2 Observation Procedure

Most of the observations were made during periods which centered about five minutes after the hour Central Standard Time. The procedure during such observations is listed below. A similar procedure was followed for periods centered about other times.

1. Ten minutes before the hour: measurement of soil temperature at 6 depths.
2. Five minutes before the hour: start of the anemometer counting period; start of the air sampling period; start of the recording period for insolation, net radiation, reflected short-wave radiation, temperature difference, and wind direction; start of the air temperature measurements. (Eight measurements of air temperature, one at each height, were made each minute for a 20-minute period.)
3. Fifteen minutes after the hour: ending of observation period which was started at five minutes before the hour.

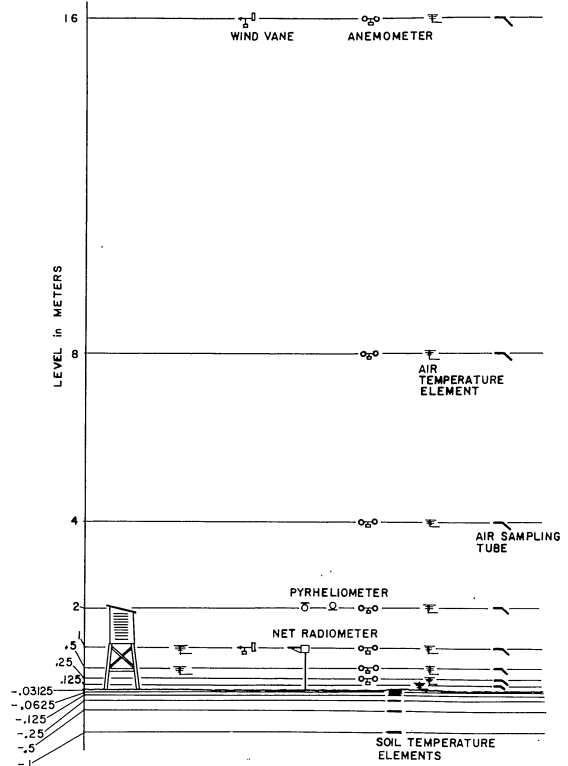
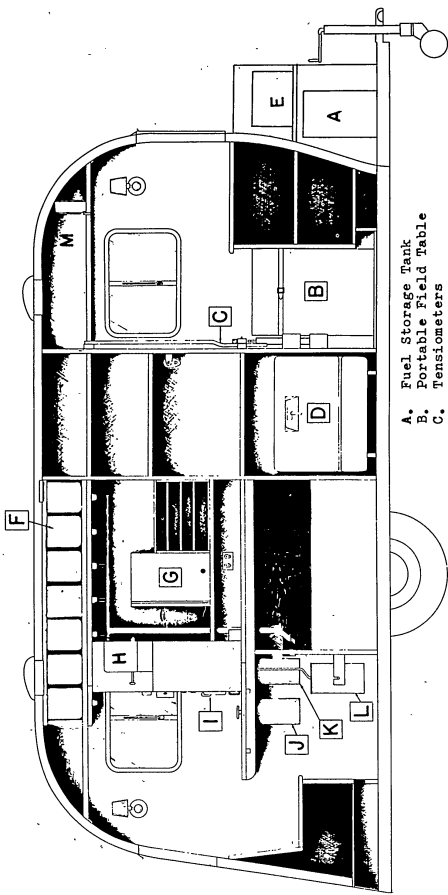
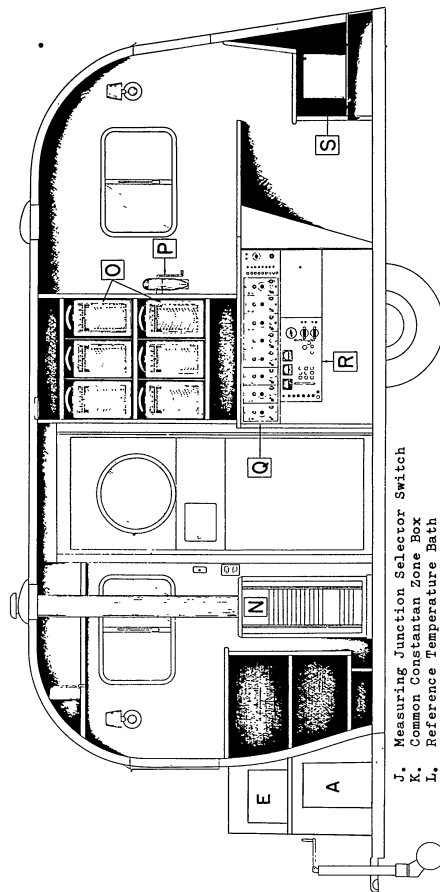


Figure 7.3 Vertical distribution of the sensing elements



- A. Fuel Storage Tank
- B. Portable Field Table
- C. Tensionometers
- D. Refrigerator
- E. A-C Power Regulator
- F. Air Sample Storage Jugs
- G. Dew-Point Hygrometer
- H. Dew-Point Control Unit
- I. Main Instrument Panel

Figure 7.4 Instrument trailer interior



- J. Measuring Junction Selector Switch
- K. Common Constantan Zone Box
- L. Reference Temperature Bath
- M. Power Monitoring Meters
- N. Kerosene Stove
- O. Esterline-Angus Recorders
- P. Ice Crusher
- Q. Bank of Amplifiers for Recorders
- R. 10 Unit Power Supply for Amplifiers
- S. Wind Speed Counting Unit

Figure 7.5 Instrument trailer interior

4. Seventeen minutes after the hour: second measurement of soil temperatures.

5. Twenty minutes after the hour: measurement of the dew-points of the 8 air samples obtained during the air sampling period. (One sample was obtained for each height.)

All data reported are average values for the observation period.

### 7.3 Individual Elements

7.3.1 Insolation Incoming short-wave radiation was measured by an Eppley pyrliometer (Weather Bureau 10-junction type). The output of the pyrliometer was continuously recorded by a modulated-carrier-type d-c amplifier (Figure 7.11) and an Esterline-Angus graphic ammeter. The amplifier was equipped with a gain selector switch so that the recording sensitivity could be changed. Three recording scales were thus provided, 0 to 0.025 cal cm<sup>-2</sup> sec<sup>-1</sup>, 0 to 0.01 cal cm<sup>-2</sup> sec<sup>-1</sup>, and 0 to 0.0025 cal cm<sup>-2</sup> sec<sup>-1</sup>.

The calibration factor for the pyrliometer was determined by the manufacturer and assumed to be correct. The amplifier and recorder combined were calibrated by supplying an input voltage from a calibrated voltage source. The voltage source had been calibrated by a Leeds and Northrup potentiometer (Type K).

The calibrated voltage source (Figure 7.6) is extremely stable and was used in the field for periodic checks of the calibrations of the various amplifier-recorder systems.

7.3.2 Reflected Short-Wave Radiation Short-wave radiation reflected by the surface was measured and recorded by a system which was identical to that used for insolation measurements. In measuring reflected radiation, the Eppley pyrliometer was mounted at a height of 2 meters and inverted so that this radiation was incident on the sensitive element.

The calibration of this system was determined in the same manner as that of the insolation system.

7.3.3 Net Radiation A Beckman and Whitley thermal radiometer, Model N188-1 (Gier and Dunkle net exchange radiometer), was used in measuring the net radiation.<sup>3</sup> A continuous record of the net radiometer

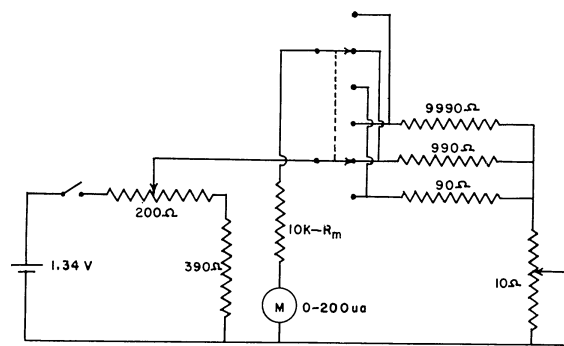


Figure 7.6 Calibrated d-c voltage source

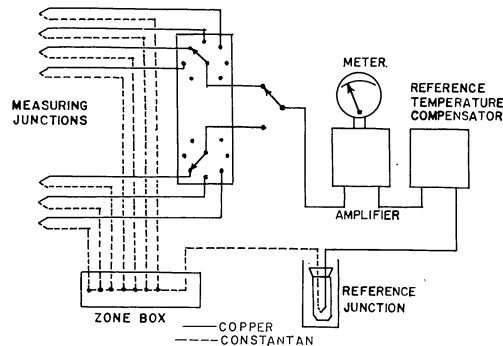


Figure 7.7 Temperature measuring system

output was obtained by means of an amplifier and recorder similar to that used for insolation measurements. Two recording scales were provided;  $-0.00125$  to  $+0.005 \text{ cal cm}^{-2} \text{ sec}^{-1}$ , and  $-0.005$  to  $+0.02 \text{ cal cm}^{-2} \text{ sec}^{-1}$ .

The calibration of this system was determined in the same manner as that of the insolation system.

**7.3.4 Air and Soil Temperature Profiles** All temperature measurements were made by means of copper-constantan thermocouples. The temperature measuring system (Figure 7.7) consisted of (a) shielded air temperature measuring junctions, (b) soil temperature measuring junctions, (c) measuring junction selector switches, (d) a modulated-carrier-type d-c amplifier, (e) a milliammeter, (f) a reference temperature compensator (calibrated microvolt source), (g) a constantan junction zone box, and (h) a reference junction.<sup>2</sup>

A radiation-shielded thermocouple assembly is shown in Figure 7.8. The shield consisted of four aluminum plates held together by small screws and plastic spacers. "Alzak" aluminum 0.032 inches thick was used for the shield plates because it is highly reflective in the portion of the spectrum between 0.4 and 7.5 microns. The thermocouple junction formed by No. 36 B&S gauge copper and constantan wire was positioned in the center space of the shield plate stack. The surfaces of the plates faced toward the junction were coated with flat black paint so that heat transfer by radiation would assist in keeping the shield stack at air temperature.

The lead wires were No. 16 B&S gauge rubber-covered copper and constantan in a twisted pair which was encased by a weather-proof neoprene covering.

Hollow brass tubes formed the supporting arms for the shield assembly. The lead wires entered the base fitting and the copper lead was threaded through one arm and the constantan through the other. As shown in Figure 7.8, the ends of the No. 36 B&S gauge copper and constantan wires which formed the junction were secured to the corresponding lead wires by means of firm-fitting plastic sleeves.

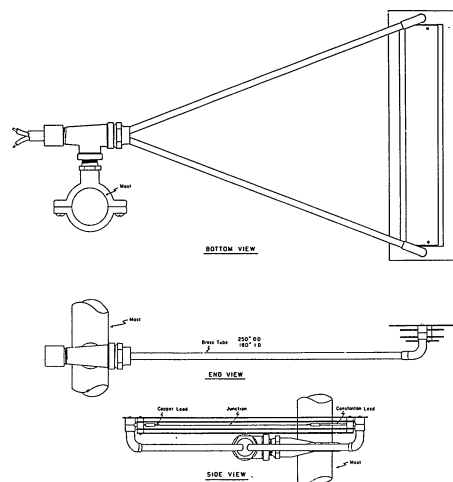


Figure 7.8 Shielded thermocouple assembly

The thermocouple junctions were made by tinning the ends of No. 36 B&S gauge copper and constantan wires, bringing them into end-to-end contact with the aid of a glass capillary tube, and soldering them.<sup>8</sup> Junctions formed in this manner are uniform and not significantly larger in diameter than the wires themselves. A thermocouple of this type has a low heat capacity and relatively low thermal conductivity.

A set of eight shielded thermocouple assemblies was used as shown in Figure 7.3. The supporting structures could be lowered to facilitate cleaning the shields and replacing the thermocouples.

The thermocouple measuring junctions used to obtain soil temperatures were of two types<sup>4</sup> as shown in Figure 7.9. The junctions which were placed at depths of 12.5, 25, 50, and 100 cm were formed by No. 16 B&S gauge copper and constantan lead wire. This type of junction was encased in a copper tube 6.5 inches long and 5/16-inch outside diameter. The copper tube was sealed at one end by a brass bullet-shaped cap. The junction was electrically insulated from the copper sheath by "Glyptal" lacquer and plastic tape. The junctions which were placed at depths of 3.125 and 6.25 cm were formed by No. 36 B&S gauge copper and constantan wires. The wires were insulated by means of thin glass capillary tubes and inserted in a brass sheath 6.5 inches long and 0.095 inches outside diameter. One end of the sheath was sealed by a pointed brass cap and the other end was connected to a 1.5-inch length of 5/16-inch outside diameter copper tubing which served as a housing for the splices of the No. 36 B&S gauge wires to No. 16 B&S gauge lead wires. The junction was electrically insulated from the sheath by "Glyptal" lacquer.

Care was taken during installation of the soil temperature elements to disturb as little as possible the soil which would surround the junctions. A triangular pit slightly more than one meter deep was excavated. The sod was cut and removed and successive layers of soil were removed and piled separately. In order to maintain accurate spacing between the junctions, a wooden template (5 cm x 2 cm x 105 cm) in which appropriate holes had been drilled was used. The wooden support was accurately positioned vertically at the apex of the pit. Holes which were slightly

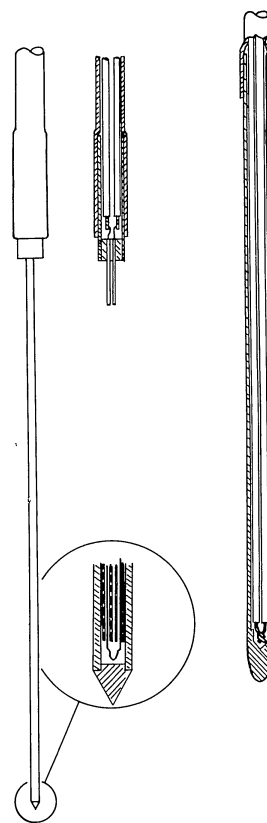


Figure 7.9 Soil temperature thermocouple elements

smaller in diameter than the temperature elements were drilled into the side of the pit at each level. The temperature elements were then inserted horizontally through the wooden support and into the holes in the soil. The layers of soil were replaced at their original depths as the pit was filled. To minimize the effect of thermal conduction along the lead wires, each lead was buried at the same depth as its corresponding element for a horizontal distance of approximately one meter from the element. Figure 7.10 illustrates the arrangement of the soil temperature measuring junctions.

All constantan leads from the measuring junctions were connected to the constantan lead to the reference junction at the constantan junction zone box. (See Figure 7.7.) The lead ends were held in contact with the common lead by means of plastic clamps. Each lead could be easily disconnected from the circuit for checking purposes.

The copper leads from the measuring junctions were connected to the individual positions of a two-gang rotary selector switch. A copper knife switch permitted selection of a gang. Since the rotary selector switch had silver contacts, it was mounted in a thermos flask which insured isothermal conditions and prevented the occurrence of spurious voltages due to the copper-silver junctions.

The reference junction was formed by No. 16 B&S gauge copper and constantan wires and was electrically insulated and water-proofed by a thin coating of polyethelene. The reference junction was immersed in a pint thermos flask filled with a mixture of distilled water and crushed distilled water ice. To prevent conduction of heat to the junction by the lead wires, approximately one foot of the lead wires was looped and immersed with the junction. The thermos flask was mounted in a cork-lined metal container to further reduce the melting rate of the ice. The metal container was mounted near the floor on a pair of horizontal pivots. The operator could impart a rocking motion to the container with his foot. In this way the reference bath was agitated to minimize thermal stratification. The mixture of ice and water was assumed to be at 0°C.

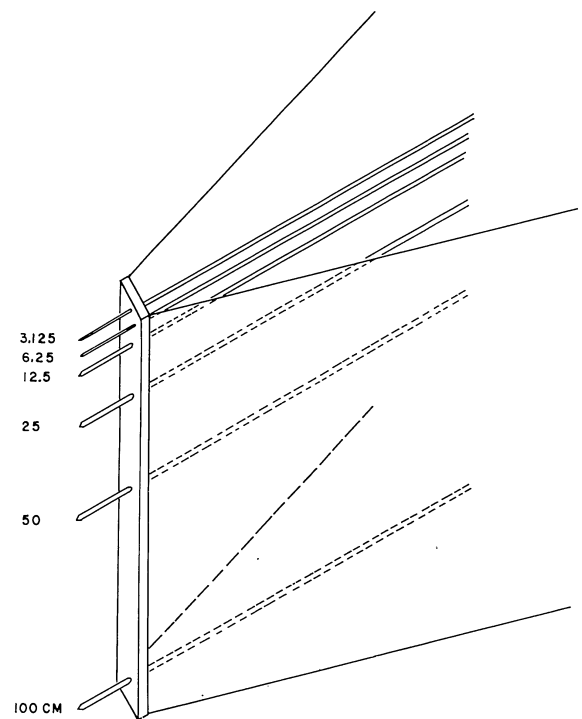


Figure 7.10 Installation of soil temperature elements



The circuit diagram for the modulated-carrier-type d-c amplifier is shown in Figure 7.11. The prominent characteristics of this amplifier are high sensitivity, virtually no zero drift, high gain stability, relatively high input impedance, and a high degree of linearity. The amplifier used for temperature measurements had a nominal input range of 0 to 400 microvolts which corresponds to the output of copper-constantan thermocouples for a 10°C temperature difference. A control was provided for precise setting of the amplifier gain.

The amplifier output was indicated on a meter (Weston, Model 271) which had a range of 0 to 1 milliampere and an internal resistance of 1400 ohms. The meter scale was 5.8 inches (147 mm) in length, had 100 divisions, and was marked to read a temperature range of 0° to 100°. This meter was equipped with a knife-edge pointer and a mirror scale which eliminated reading errors due to parallax.

The reference temperature compensator circuit is shown in Figure 7.12. This unit is a calibrated variable microvoltage source. By setting the dial of the 5000-ohm precision variable resistor and regulating the voltage across the precision divider consisting of the 1-ohm, 250-ohm, and nominal 5000-ohm series-connected resistors; a microvoltage equivalent to that produced by copper-constantan thermocouples for any temperature difference in the ranges of 0° to 45°C and 0° to 45°C could be obtained. In this circuit, the output microvoltage is made dependent only on the setting of the 5000-ohm resistor by maintaining a constant voltage across the divider. This is accomplished by comparing the voltage across the divider with the emf of a standard cell and varying the 100K ohm resistor in series with the 1.5-volt dry cell until a condition of balance is obtained as indicated by the microammeter.

Since the input range of the amplifier was limited to a 10° increment and the reference thermocouple junction was maintained at 0°C, the reference temperature compensator was employed in measuring temperatures which exceeded 10°C. The connection of the compensator in the measuring circuit was such that its output voltage was subtracted from the voltage

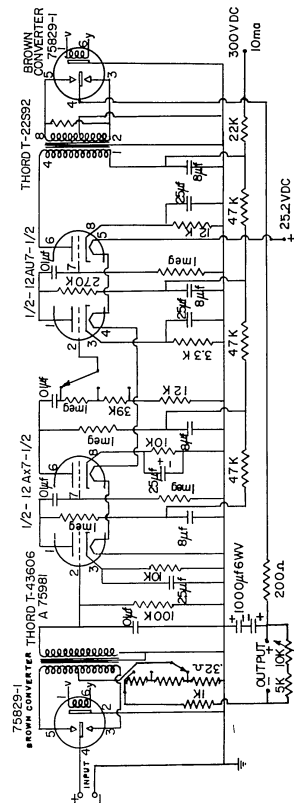


Figure 7.11 Thermocouple amplifier

produced by the thermocouples. The net voltage was then amplified and indicated on the meter. The following example illustrates the operation of the temperature measuring system:

To measure the temperature (assumed to be between 20° and 30°C) at the 50-cm depth in the soil:

- (1) Set the selector switch for the -50 cm soil-measuring junction,
- (2) Set the reference temperature compensator dial for 20°C compensation and adjust the balance control,
- (3) Set the amplifier gain dial for the 20° to 30°C increment, and
- (4) Read the meter (assume a reading of 6.35 is obtained)
- (5) Apply a meter correction, in this case +0.02.

The temperature (26.37) is the compensation (20°C) plus the meter reading (6.35°C) plus the meter correction (+0.02).

A platinum resistance thermometer (Leeds and Northrup), which had been calibrated by the National Bureau of Standards, and a Mueller Bridge (Rubicon) were used to calibrate the copper-constantan thermocouple wire. A thermocouple circuit was constructed from a length of No. 16 B&S gauge copper-constantan lead wire. One junction was placed in a 0°C reference bath with water (approximately five gallons). A Beckman differential thermometer and the resistance thermometer were immersed in this calibrating bath. The thermocouple junction, Beckman thermometer bulb and resistance thermometer bulb, were placed in close proximity near the center of the bath. A motor-driven stirring mechanism was used to agitate the water. The thermocouple wires were connected in a circuit with an amplifier, meter, and reference temperature compensator as shown in Figure 7.13. The amplifier and meter merely served as a sensitive null indicator, hence their calibrations had no influence on the wire calibration.

The temperature of the calibrating bath was varied through the range of -20°C to 50°C and 15 evenly-distributed calibrations points were obtained. Methanol antifreeze was added to the bath water for temperatures less than 0°C. The temperature of the bath was determined by the resistance

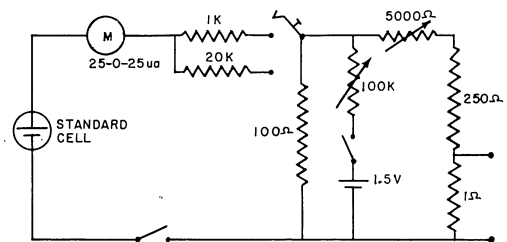


Figure 7.12 Reference temperature compensator

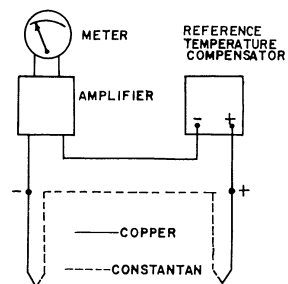


Figure 7.13 Thermocouple wire calibrating circuit

thermometer, and the rate of change of temperature was monitored by the Beckman differential thermometer. At each calibration point, a reference temperature compensator setting was determined which produced zero current flow in the measuring circuit as indicated by the amplifier meter null detector; that is, a setting was determined which caused the compensator output to be equal in magnitude to the emf produced by the thermocouple junctions. The emf temperature characteristic of the copper-constantan wire was then determined by measuring the output of the compensator for each of the dial settings. A potentiometer (Leeds and Northrup Type K), a precision voltage divider, an amplifier-meter null detector, and an auxiliary emf source were used for this measurement as shown in Figure 7.14. The amplifier and meter were calibrated by means of the circuit shown in Figure 7.15. In this circuit, the compensator serves as a calibrated microvoltage source which simulates the output of a thermocouple circuit. With the auxiliary microvoltage source set at zero output, the compensator was set for 10°C and the setting of the amplifier gain control which produced full-scale meter deflection was determined. The output of the auxiliary microvoltage source was then adjusted until it was equal in magnitude to the compensator output. Since the two microvoltage sources were connected so that their polarities were in opposition, a condition of equality was indicated by a reading of zero on the meter. (The zero reading, of course, is independent of the amplifier-meter calibration.) The setting of the compensator was then changed to 20°C and the amplifier gain setting for full-scale meter deflection was determined. The auxiliary microvoltage source was again adjusted for a condition of equality and the process was repeated. By this method, amplifier gain settings were established for a series of overlapping operating ranges, that is, 0° to 10°C, 5° to 15°C, 10° to 20°C, etc. The transfer characteristic of the amplifier-meter combination was determined and it was found that deviations from linearity were due primarily to meter movement and scale irregularities. Corrections to be applied to meter readings were established which corrected for the irregularities in the amplifier-meter transfer characteristic and the curvature of the emf temperature characteristic of the thermocouple wire.

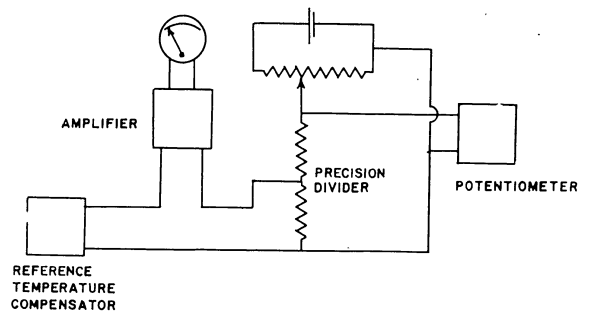


Figure 7.14 Calibrating circuit

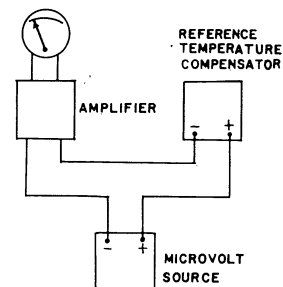


Figure 7.15 Amplifier calibrating circuit

The emf temperature characteristic of the No. 36 B&S gauge copper-constantan thermocouple wire had been established to be virtually the same as that of the No. 16 B&S gauge thermocouple wire by the Leeds and Northrup Company. This was verified by experimentation. A series circuit was constructed from lengths of No. 16 B&S gauge copper wire, No. 16 B&S gauge constantan wire, No. 36 B&S gauge copper wire, and No. 36 B&S gauge constantan wire.

Four junctions were formed: (1) No. 16 B&S gauge copper to No. 36 B&S gauge copper, (2) No. 36 B&S gauge copper to No. 36 B&S gauge constantan, (3) No. 36 B&S gauge constantan to No. 16 B&S gauge constantan and (4) No. 16 B&S gauge constantan to No. 16 B&S gauge copper. This circuit was connected to an amplifier-meter null detector. The No. 16 B&S gauge copper-constantan junction and the No. 36 B&S gauge copper-constantan junction were maintained at the same temperature by immersing them in a thermos flask filled with water. The No. 16 B&S gauge to No. 36 B&S gauge copper junction and constantan junction were heated separately. No thermoelectrical emf was obtained.

An overall statement of the accuracy of the temperature measurements cannot be made. The accuracy of the air temperature measurements is a function of the prevailing atmospheric conditions at the time the measurements were made. Errors inherent in thermal measurements further complicate an assessment of accuracy. It is possible, however, to designate the sources of error and to estimate, in some cases, the magnitude.

Absolute accuracy can be defined as the deviation of a measurement from true temperature. Relative accuracy can be defined as the deviation of a measured difference from true temperature difference. The significant errors in air temperature measurements are calibration error, radiation error, and sampling error.

The calibration of the thermocouple wire is the basis of the calibration of the temperature measuring system. The accuracy of the wire calibration is difficult to evaluate. However, the calibration was conducted with extreme care and several determinations of each measured value

showed the calibration to be reproducible. A conservative estimate of the error due to calibration inaccuracies is 0.05°C for an absolute measurement and 0.02°C for a relative measurement. Error caused by loss of calibration due to change in characteristics of the system components (in particular, a change in the emf temperature characteristic of the thermocouple wire) can be considered insignificant. A comparison of this wire calibration (conducted in April 1956) with a calibration conducted in May 1953 shows an average difference of 0.05°C. An unknown fraction (believed to be small) of this difference is probably due to a change in the emf temperature characteristic of the wire. Frequent checks of the amplifier calibration were made by the method illustrated in Figure 7.15 to insure no loss in accuracy due to this component.

Probably the most detrimental effect on the accuracy of the air temperature measurements was produced by radiative transfer at the measuring junctions. The magnitude of the radiation error is difficult to determine since it is a function of atmospheric conditions, time, height, and vertical distribution of wind velocity. In the daytime with a clear sky and low wind velocity this error would be greatest. All measured air temperatures would be higher than true air temperature. Air movement decreases the effect of radiation. The measurement nearest the ground would have the greatest error since the wind speed there is less than the wind speed aloft. At night with a clear sky the radiation error would produce measured temperatures lower than real, and variable with height and wind speed. Under cloudy and windy conditions, the radiation error would be less significant. Under isothermal conditions with zero net radiation at the surface, the radiation error would be completely absent. It is conceivable that the radiation error could be as high as 2°C; however, for most of the observations made at O'Neill it probably did not exceed 0.1°C.

A handy means of checking the relative accuracy of air temperature measurements independent of sampling error makes use of Nature's heat bath which exists with adiabatic thermal stratification. At these times, the thermocouples on the mast are exposed to the same constant potential

temperature.\* That is, since the potential temperature is constant throughout the depth of measurement, and over the time of measurement, no breath of air of different potential temperature can come along to introduce sampling error. Since meteorological sampling error is missing, only radiational error and calibration error remain.

Adiabatic thermal stratification near the ground occurs typically twice a day, shortly after sunrise and a while before sunset. However, these are also times of rapid heating in the morning and cooling in the afternoon, so that the length of time that adiabatic stratification exists may be very short. On some occasions the entire 16-meter depth of measurement will not be at uniform potential temperature at any one time. Adiabatic profiles may be caused at other times by high turbulence if the turbulent heat flux is relatively small.

Analyses were made of six adiabatic or nearly adiabatic air temperature profiles (20-minute periods) obtained during the 3-day observation period 6-9 August 1956. Profiles of mean temperature and mean potential temperature were plotted for each of the six runs (see Figures 7.16, 7.17, 7.18, 7.19, 7.20 and 7.21). It was assumed that the logarithmic profile equation holds:

$$\theta = \theta_0 + n\Delta\theta,$$

where  $\Delta\theta$  does not vary with height in the lowest 16 meters. Logarithmic profiles were fitted-by-eye, and the standard error of mean potential temperature for the 20-minute period was estimated as 1.25 times the average deviation of the points from the fitted line. The values are given in Table 7.1. This standard error ranges from 0.0048°C to 0.031°C, with an average value of 0.020°C. Since some meteorological sampling

\*More precisely, to the same value of  $\theta = T + \frac{g}{C_p} z$  where  $z$  is measured from the surface of the ground.

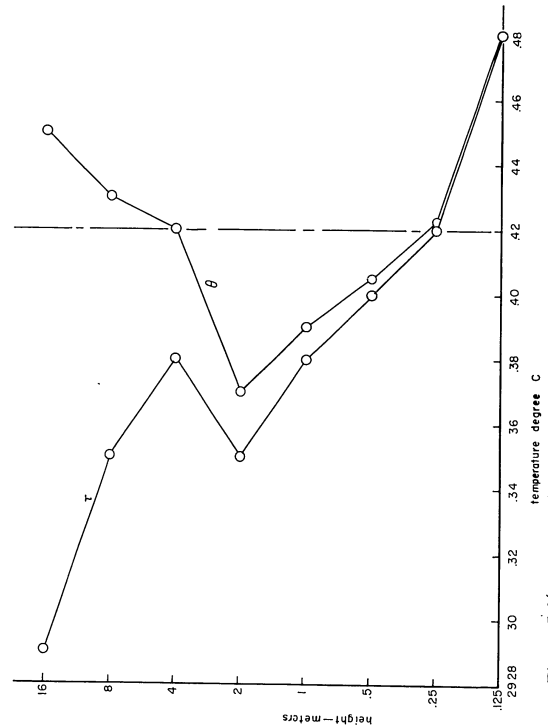


Figure 7.16 Twenty-minute profiles of temperature and potential temperature for conditions of nearly adiabatic stratification, 6 August 1956, 1805 CST

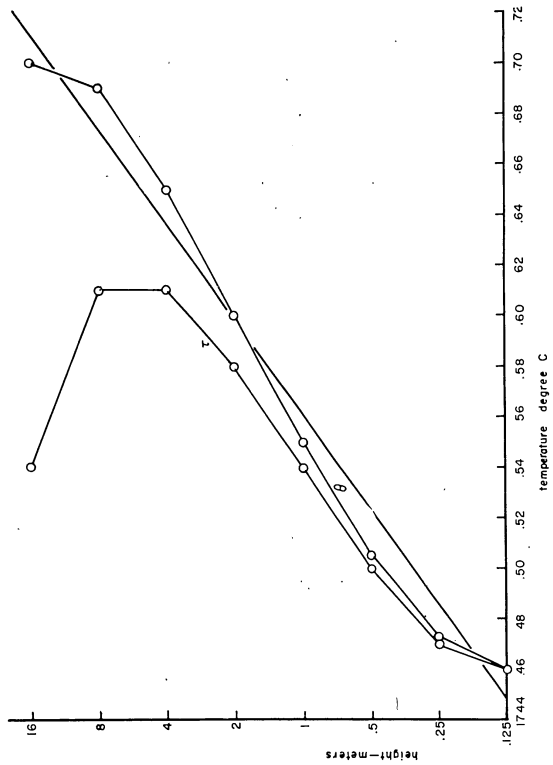


Figure 7.17 Twenty-minute profiles of temperature and potential temperature for conditions of nearly adiabatic stratification, 7 August 1956, 0305 CST

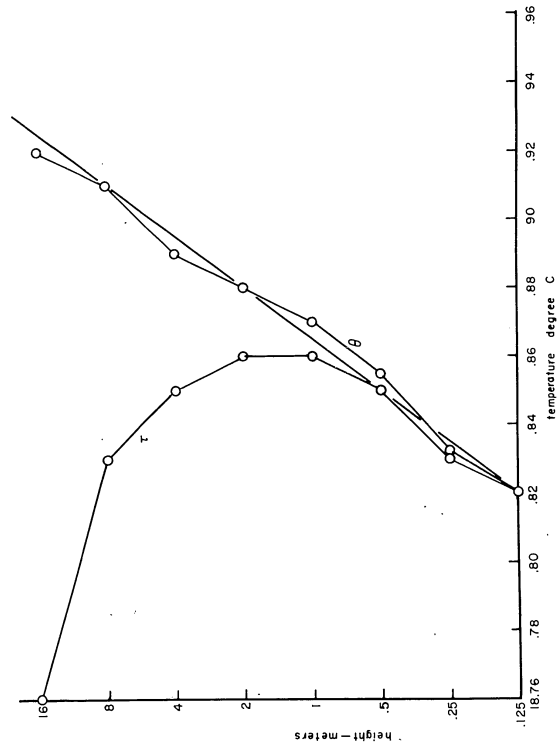


Figure 7.18 Twenty-minute profiles of temperature and potential temperature for conditions of nearly adiabatic stratification, 8 August 1956, 0205 CST

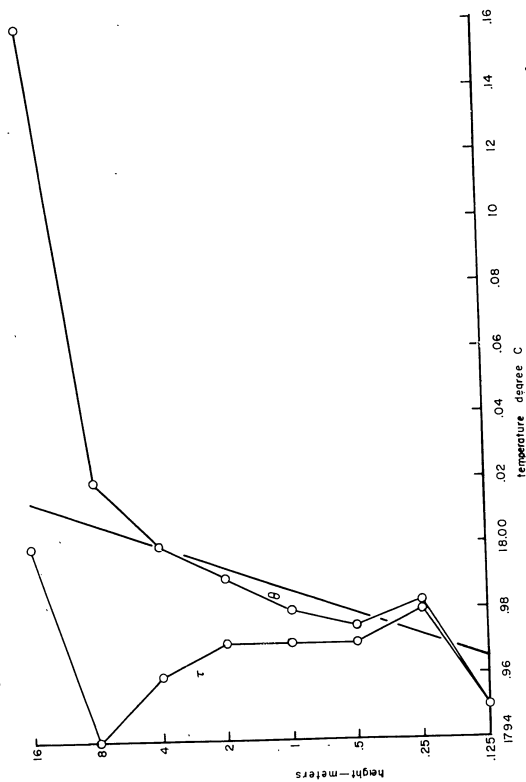


Figure 7.19 Twenty-minute profiles of temperature and potential temperature for conditions of nearly adiabatic stratification, 8 August 1956, 0805 CST

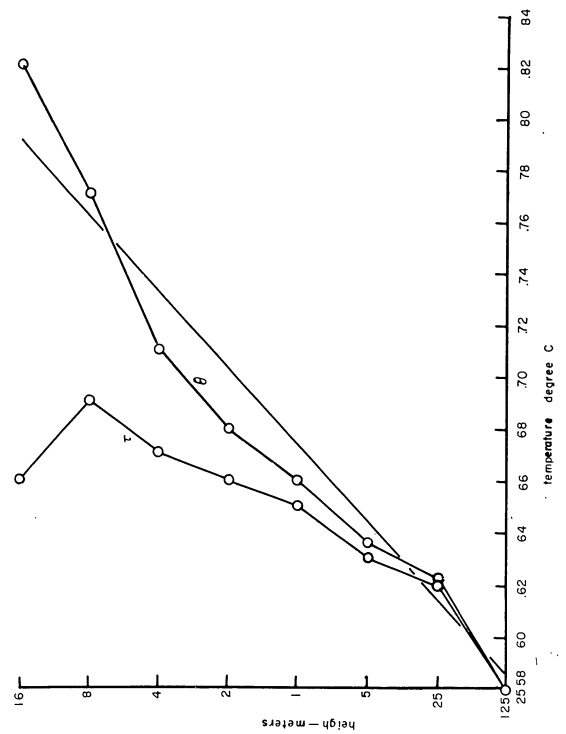
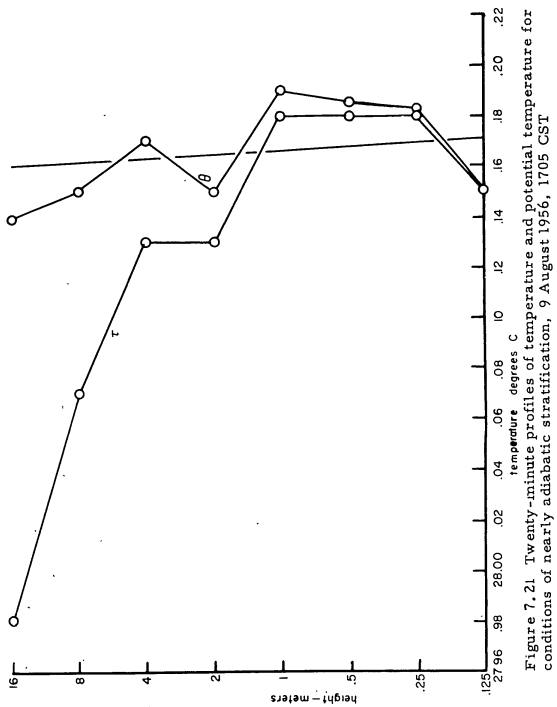


Figure 7.20 Twenty-minute profiles of temperature and potential temperature for conditions of nearly adiabatic stratification, 8 August 1956, 1905 CST



error still exists, and possibly a very small radiational error, these values are considered outside limits for the calibration standard error.

Table 7.1 Values of standard error of mean potential temperature

Date	Time	Type	$\Delta\theta^*$ (°C)	Wind Velocity (cm/sec)	Dir (deg)	S, E, T (°C)	Remarks
6 Aug	1755-1805	Cooling	.00	537	160	.031	.1 Cs
7 Aug	0255-0315	Dynamic	.04	574	65	.016	.4 low cloud Was raining previous two hrs
8 Aug	0155-0205	Dynamic	.015	812	20	.0048	Thunderstorms to north last few hrs
8 Aug	0755-0805	Warming	.01	314	330	.030	Overcast Raining one hr. ago
8 Aug	1855-1905	Cooling	.03	527	0	.017	.2 Cu
9 Aug	1655-1705	Cooling	.002	416	30	.019	Huge thunder-storm to west, advancing on us for last 3 hrs

\*  $\Delta\theta = \frac{8\theta}{8n}$ , where n ("number of doubled levels") is the logarithmic, non-dimensional height scale  $n = \frac{\ln z/z_0}{\ln 2}$ .



The importance of the meteorological sampling error still remaining can be appreciated by taking a closer look at the data for two of the runs: that of 0205 CST on 8 August, an ideal case, and that of 1805 CST on 6 August, a less than ideal case. The thing sought is the nature of trends during the 20-minute periods. To this end, simplified profiles of potential temperature for the first and last five minutes of each run were obtained. The data of the lowest two heights, middle two heights, and top two heights were combined, giving profiles of only three points. These profiles are plotted in Figures 7.22 and 7.23. The latter 20-minute profile was obtained when shelter-height temperature dropped 1.0°C in 15 minutes, and the potential temperature profile quickly passed from daytime type to nighttime type during the run.

On the other hand, the ideal 20-minute profile was obtained with high turbulent mixing and small, nearly constant, heat flux downward. The drop in shelter-height temperature was only 0.4°C in 15 minutes, and the slope of the potential temperature profiles changed very little during the run. Meteorological sampling error was therefore much less in this period of observation than in that of 1805 CST on 6 August 1956.

Errors in the 20-minute profiles of mean temperature due to sampling may be evaluated by simple statistical techniques. The magnitude of these errors is least (nearly zero) when thermal stratification is adiabatic. It is also usually small with calm conditions at night. These errors are greatest in the heat of the day when no steady breeze is blowing.

A computation was made to evaluate sampling error in the temperature profiles. Data are from the 1455-1515 observation period of 8 August. This was a time of strong solar heating (clear sky above, bank of cumulus clouds in the distant southeast) and "very light" winds from the southwest. In the computations, the standard deviations are in all cases estimated at 5/4 of the average deviation.

The standard deviation of the 20 temperature measurements at each height varied from 1.06 degrees ( $Z = 0.125$  m) to 0.44 degrees ( $Z = 16$  m). Since the serial correlation is negligible, the standard error of the mean temperature is  $(1/20)^{1/2}$  times the standard deviation. The mean

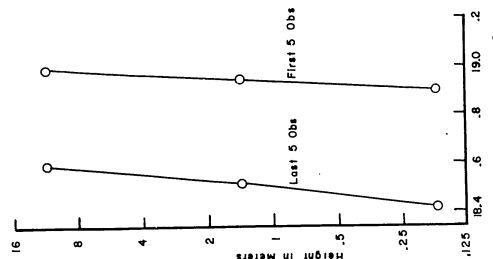


Figure 7.23 Temperature profile, 8 August 1956, 0205 CST

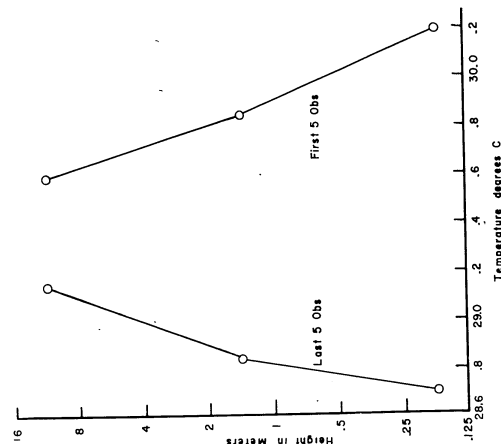


Figure 7.22 Temperature profile, 6 August 1956, 1805 CST

temperatures at the various heights are found to have standard errors of 0.10 to 0.24 degrees. Figure 7.24 shows the profile of  $\bar{T}$  plus or minus S.E. $\bar{T}$  as a function of height.

The accuracy of mean temperature differences within the profile is increased by a small positive correlation between temperature observations at various heights. In this example, the difference in mean temperature at 1 m height and at all other heights is between 0.18 degrees and 0.24 degrees.

The means, standard deviations, and correlation coefficients are given in Table 7.2.

Table 7.2. Statistical measures of temperature

Height (Cm)	$\bar{T}$	$\sigma_T$	S.E. $\bar{T}$	$\bar{T}_z - \bar{T}_{1m}$	$\sigma(T_z - T_{1m})$	SE( $T_z - T_{1m}$ ) *	$r(T_z, T_{1m})$
1600	28.86	0.44	0.10	-1.83	0.93	0.21	0.20
800	29.37	.57	.13	-1.32	.92	.21	.22
400	29.76	.75	.17	-0.93	.91	.20	.25
200	30.31	.68	.15	-0.38	.91	.20	.23
100	30.69	.80	.18				
50	31.40	.93	.21	+0.71	0.82	.18	.27
25	32.54	0.92	.21	+1.85	1.06	.24	.27
12	33.55	1.06	0.24	+2.86	1.03	0.23	0.30

\* - Value that S.E.( $T_z - T_{1m}$ ) would have if correlation were zero.

$$\bar{T} = \frac{1}{N} \sum_{i=1}^N T_i$$

$$\sigma_T^2 = \frac{1}{N} \sum_{i=1}^N (T_i - \bar{T})^2 ; \quad \sigma_T = \frac{1}{\sqrt{N}} \sum_{i=1}^N |T_i - \bar{T}|$$

$$S.E._T = \frac{1}{\sqrt{N}} \sigma_T$$

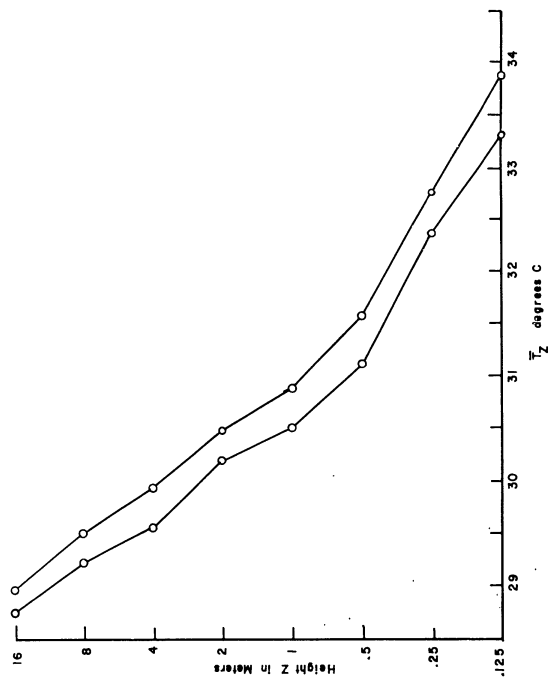


Figure 7.24 Mean temperature plus or minus its standard error, 8 August 1956, 1505 CST

$$\sigma^2(T_z - T_{1m}) = \frac{1}{N} \sum_{i=1}^N \left[ (T_{z,i} - T_{1m,i}) - (\bar{T}_z - \bar{T}_{1m}) \right]^2$$

$$\text{S.E.}(\bar{T}_z - \bar{T}_{1m}) = \frac{1}{\sqrt{N}} \sigma(T_z - T_{1m})$$

$$\sigma^2(T_z - T_{1m}) = \sigma_{T_z}^2 + \sigma_{T_{1m}}^2 - 2r(T_z, T_{1m})\sigma_{T_z}\sigma_{T_{1m}}$$

The accuracy of the soil temperature measurements is 0.05°C for absolute measurements and 0.02°C for relative measurements since the only significant error is that due to calibration inaccuracy.

Malfunctioning of the temperature measuring system could be easily recognized by observing the hourly change in temperature at the 1-meter depth in the soil. Large scale change or rapid fluctuations in this reading usually indicated shorts or leakage to ground, electric and magnetic field pickup, or component failures. Difficulties could also be recognized by reading the 1-meter soil temperature using two overlapping reference temperature compensator ranges.

**7.3.5 Air Temperature Difference.** The air temperature difference between the 1-meter and the 1/2-meter levels was measured by means of two radiation-shielded thermocouple junctions of the same type as that used for air temperature profile measurements. The two junctions were differentially connected and the output was recorded by a modulated-carrier-type d-c amplifier and an Esterline-Angus graphic ammeter.

A recording scale of -5° to +5°C was used; hence, the temperature at one level relative to the other was determined in addition to the temperature difference.

**7.3.6 Vapor Pressure Profiles.** The measurement of the amount of water vapor in the air was accomplished by means of an air sampling system and a dew-point hygrometer. During the 20-minute observation periods, air samples were obtained at each level as shown in Figure 7.3.

The dew point of each sample was then measured using a Thornthwaite automatic dew-point hygrometer.<sup>6</sup> The data reported are in units of vapor pressure (millibars) which were obtained by conversion of the measured data which were in terms of dew-point temperature (degrees Centigrade).

The air sampling system shown schematically in Figure 7.25 consisted of (a) polyethylene sampling tubes, (b) sample storage jugs, (c) sample selector valves, (d) a variable speed pump, and (e) a pump speed control. Polyethylene tubing having an inside diameter of 0.25-in. was used since this material is virtually non-hygroscopic. One gallon glass jugs were used as reservoirs for the air samples in order to obtain average samples (that is, samples which did not exhibit small scale fluctuations) simultaneously from all levels. The sample selector valves permitted extraction of the samples from the reservoirs for measurement. A modified vacuum cleaner was used as an air pump. The rate of pumping could be changed by varying the input voltage to the pump motor. Two pump speeds were used and were conveniently obtained by switching the motor input to full line voltage or to the voltage at a tap on an auto-transformer.

The dew-point hygrometer is shown in Figure 7.26. This is a condensation type hygrometer which utilizes a mirror surface on which moisture is caused to condense. By measuring the temperature of the mirror at the time of incipient condensation the dew point is obtained.

The instrument which was used consisted of (a) a mirror assembly, (b) a sample chamber, (c) a photoelectric dew-film detection system, (d) a dry-ice heat sink, (e) a control circuit, and (f) a radio frequency induction-heating unit. The mirror assembly was formed by copper foil chrome plated on one surface and soldered to the end of a steel rod 0.25-in. in diameter which, in turn, was connected to a copper slug 1-inch in diameter and 5 inches long. The chrome surface served as the mirror and a copper-constantan thermocouple junction was held in contact with the under or copper surface by a second piece of copper foil. This junction

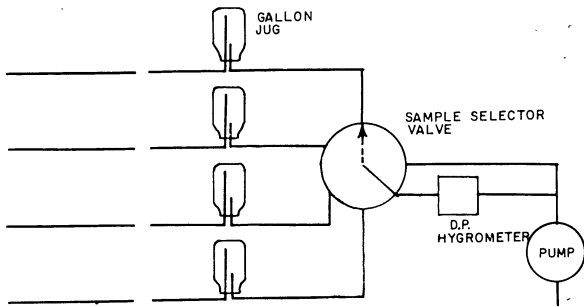


Figure 7.25 Air sampling system

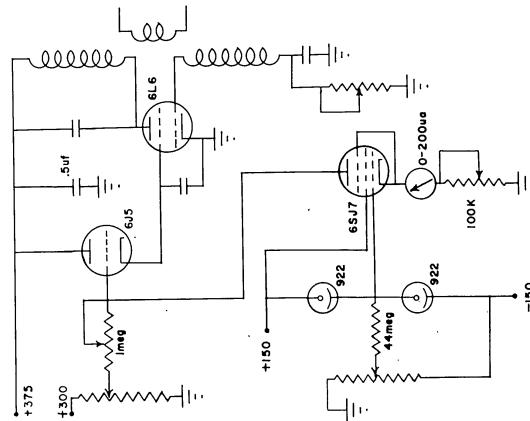
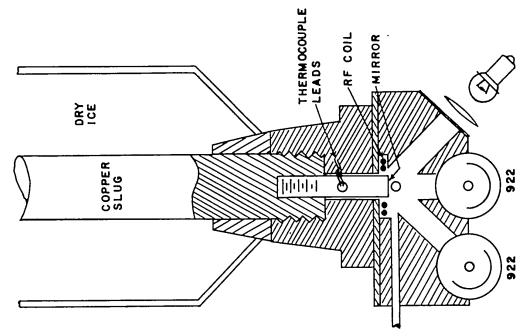


Figure 7.26 Dew point hygrometer

was connected to the temperature measuring system (see Figure 7.7). The thermocouple wire was the same type, No. 36 B&S gauge, as that used for the air temperature measuring junctions.

The copper slug of the mirror assembly was inserted in a thermos flask filled with crushed dry ice and the steel mirror stem was inserted in a hole in the sample chamber. A radio frequency induction heating coil concentric with the hole in the sample chamber then encircled the steel mirror stem. The sample chamber was a hollow, airtight, plastic block with air sample intake and exhaust ports, windows for two photocells, and a window for the admission of a light beam.

The photoelectric dew-film detection system was connected to an amplifier (control circuit) which, in turn, controlled a radio frequency oscillator (R-F induction heating unit).

In operation the mirror surface was cooled by the dry ice and heated by the R-F induction heater. By controlling the heating, the mirror temperature could be varied. Three heat controls were available: (1) a quick-heat button, (2) a manual control, and (3) an automatic control. By manually depressing the quick-heat button, rapid heating of the mirror was obtained. The manual control enabled the operator to vary the mirror temperature to obtain a dew-film of proper thickness. The automatic control was provided by the photoelectric dew-film detection system. Light which was incident at an angle of 45 degrees on the mirror was reflected to one photocell. A second photocell positioned directly below the mirror surface (that is, on a line normal to the mirror surface) received scattered light when a dew-film was present. An increase in dew-film thickness caused a decrease in reflected light and an increase in scattered light. This change was sensed by the photocells which produced a control voltage causing an increase in R-F induction heating. Conversely a decrease in dew-film thickness was sensed and the heat supply to the mirror decreased. In this way the automatic control aided the operator in maintaining a constant dew-film thickness on the mirror.

In addition to providing automatic control, the photoelectric dew-film detection system produced a meter indication of dew-film thickness. The dew-film thickness meter permitted establishing a standard dew-film thickness for all measurements.

The following procedure was used for measuring dew-point profiles. With the sample selector valves set in the simultaneous sample position and the pump set for high speed, air samples were drawn into the storage jugs. The pump was set for low speed and the valves were set so that air which was a mixture of all the samples was passed through the sample chamber. In this way an initial setting of the manual control was made to produce a dew-film and the proper reference temperature compensator range setting was determined for the temperature measuring system. The quick-heat button was then depressed to clear the dew-film from the mirror and the zero or clear mirror reading of the dew-film thickness meter was checked. Valve settings were made for selection of the first sample. The pump was operated at high speed for 3 to 5 seconds to scavenge the sample chamber and connecting tubes of the initial air. With the pump operating at low speed, the manual control was set to produce a dew-film of the proper thickness as indicated by the dew-film thickness meter. The temperature of the mirror was then read by means of the temperature measuring system. The second sample was selected and the first sample scavenged by operating the pump at high speed. The process was then repeated. Slow speed operation of the air sample and mechanical disturbance of the dew-film by the air passing over its surface.

Because of the number of manual adjustments and switch settings, and complexity of the procedure, considerable skill was required of the operator in measuring dew-point profiles.

Prior to Project Prairie Grass, the dew-point hygrometer was calibrated by an air saturating chamber as shown in Figure 7.27. The chamber was formed by two sheet-copper boxes one within the other

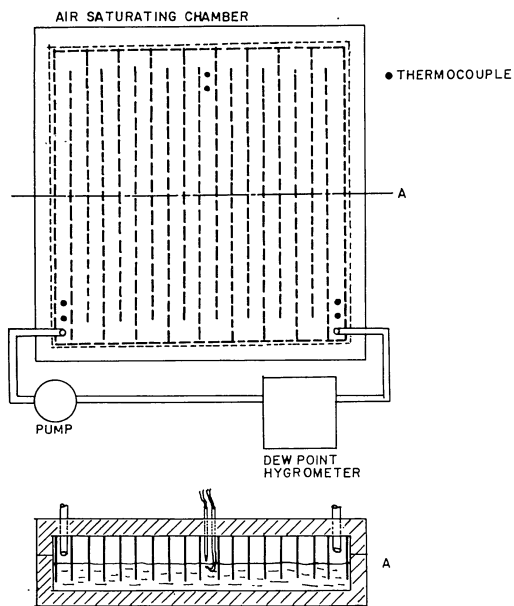


Figure 7.27 Air saturating chamber

and separated by insulating material 1-inch thick. The box was constructed in two sections to permit access to the chamber. The bottom section formed a pan 18 inches by 18 inches by 1.5 inches deep. The top section contained a labyrinth of baffle plates. The pan formed by the top section was 1.5 inches deep and the baffle plates were 2 inches in width. The bottom section was filled with distilled water and the top section was positioned in such a way that the lower edges of the baffle plates were immersed to a depth of 0.5 inches. In this way an enclosed and baffled air space 1.5 inches high was formed over the water surface. Glass tubing inserted through the top section of the chamber provided intake and exhaust ports. Air entering the chamber was confined to a path formed by the baffle plates. Between the intake and exhaust ports, the air path length was 27 feet. The air temperature and water temperature were measured by means of copper-constantan thermocouple junctions at three stations along the air path: at the intake port, at the exhaust port, and at the midpoint of the air path. The dew-point hygrometer, a pump, and the chamber were connected in a closed circuit by means of polyethylene tubing. The pump circulated air through the chamber and dew-point hygrometer at a speed sufficiently high to produce turbulent flow in the saturating chamber. The difference between air and water temperature at each station was observed. A condition of temperature equilibrium between air and water was used as an indication of saturation. The temperature at which saturation occurred was then taken as the actual dew point of the air. The condensation temperature or dew point as indicated by the dew-point hygrometer when operating with various dew-film thicknesses was compared with the saturation temperature. By repeated tests a dew-film thickness was established which produced agreement of saturation temperature and dew point as indicated by the dew-point hygrometer. To prevent condensation from occurring in the connecting polyethylene tubes which were virtually at room temperature, saturation temperatures less than room temperature were used. This was accomplished by using

water in the chamber having a temperature a few degrees below that of the room.

The accuracy of the dew-point measurements is at best equal to the accuracy of the calibration of the temperature measuring system. In addition there are sampling errors, and small random errors introduced in setting the dew-film thickness. Sampling errors are difficult to evaluate but are suspected to exist when a smooth profile is not obtained. Excluding sampling errors, absolute measurements are probably accurate to 0.06°C and relative measurements are probably accurate to 0.03°C.

Malfunctioning of the dew-point hygrometer was readily recognized by observing the behavior of the dew-film thickness meter. The presence of water in the sampling tubes could be detected by the behavior of the instrument and by readings of dew point which were greater than ambient temperature. Water in the sampling tubes sometimes occurred as a result of rain, fog or an inversion under humid conditions. The sampling tubes were necessarily cleared of water before resuming measurements. During the observation periods, moisture measurements were made by means of a sling psychrometer. These measurements were used as a check for gross error in the dew-point system.

7.3.7 Wind Profiles. Wind profiles were measured by a set of matched three-cup anemometers. Nineteen Rikoken\* anemometers were modified, compared, and grouped in sets of seven matched units.

When received from the manufacturer, the Rikoken anemometers were equipped with gear trains and contact systems for counting the

\*Manufactured by the Sanoya Iron Works,  
1064 Nakata-machi, Kanuma-shi  
Tochigi-ken, Japan

turns of the cups. The modification consisted of replacing the gear train and contact system with a photoelectric counting system. The latter system utilized a cadmium sulfide photoconductive cell and a No. 51 light bulb. The light reflected to the photocell by the mirror was interrupted by a shutter blade connected to the shaft which was turned by the cup assembly. In this way the photocell was illuminated and shaded once for each revolution of the cup assembly. The photoelectric counting system had several advantages not afforded by the gear train and contact system: (a) Friction due to the gear train and contacts was eliminated by use of the photoelectric system. Since this was the major portion of the friction in the instrument, its elimination resulted in lower starting speed. Also, the magnitude of this portion of the friction was not the same in each anemometer so its absence tended to make the anemometer characteristics more nearly alike. (b) The resolution (counts per revolution or counts per meter of air passage) obtained by using a photoelectric system which counted each revolution of the anemometer cups was 6.9 times as large as that provided by the gear train and contact system. Since the anemometer output was in digital or pulse form and was recorded by means of a digital counter (step function integrator), wind measurements having a resolution commensurate with accuracy could be obtained for a shorter time interval using the photoelectric system than by using the gear train and contact system. (c) Gear train and contact systems often produce spurious counts caused by contact bounce and intermittent conduction at the instant of make or break. The photoelectric system produced no spurious counts. (d) Contacts become pitted with use requiring that they be burnished or replaced. The photoelectric system required little and infrequent maintenance.

A unit having 8 counting channels (one for each anemometer and one spare) was used to register the number of revolutions of the anemometers. The circuit of a counting channel is shown in Figure 7.28. The circuit consists of a pulse-shaping stage, three bi-stable multivi-

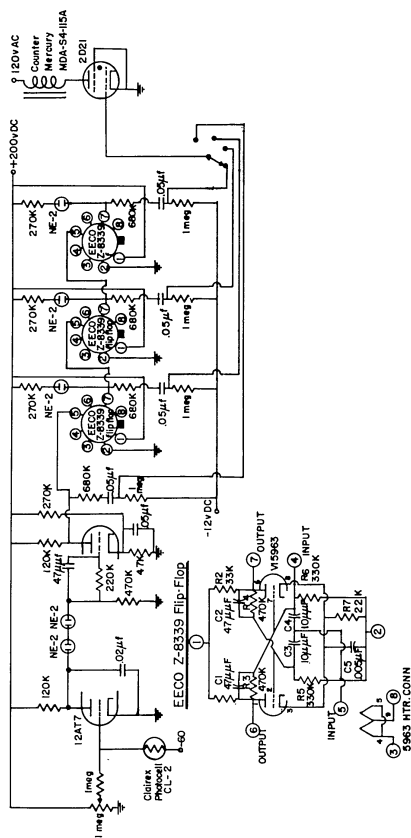


Figure 7.28 Counting circuit

brators, and a thyatron-driven electromechanical counter. Input pulses from the anemometer were converted to short rise time rectangular pulses. The output of the pulse-shaping stage was then fed to the three bi-stable multivibrators which were connected as a binary frequency divider. By means of a selector switch, the thyatron driven electromechanical counter could be connected to the output of the pulse-shaping stage or the output of any multivibrator. In this way the electromechanical counter was caused to register either each, every other, every fourth, or every eighth revolution of the anemometer. The electromechanical counter (mercury four-digit reset type) was rated at 10 counts per second. Since the anemometer speed could exceed this rate, the binary frequency divider was employed. In addition to enabling the counting circuit to accommodate a maximum input rate of 80 counts per second, the binary frequency divider reduced wear of the electromechanical counter when wind measurements were made which did not require the maximum available resolution.

The counting unit was constructed in three assemblies. The electronic portion of the counting channels was built on a single chassis. The threshold controls and count-down (frequency division) selector switches were located on this chassis. Two banks of electromechanical counters, a counter start-stop switch and a bank selector switch were mounted on a panel. One bank of counters could be read and reset while the other was registering counts. In this way successive profile measurements could be made without loss of data during the reading and reset periods. The power supply for the system was contained on a single chassis.

Prior to Project Prairie Grass, the anemometers were matched by means of a whirling device having four horizontal arms each eight feet long.<sup>7</sup> The anemometers were matched at O'Neill by mounting them at the same level on a horizontal support approximately two meters above the ground in an open field as far as possible from obstructions.<sup>1</sup> The support could accommodate 10 anemometers



having a horizontal spacing of approximately 1 foot.

An anemometer which was representative of the matched set was selected as a standard and its calibration was determined. This anemometer was calibrated in a wind tunnel\* against a pitot tube which had been calibrated by the Bureau of Standards. Several trial calibrations were run to investigate the characteristics of the calibrating procedure and equipment. Four independent calibrations were then made and the average was taken as the true calibration. A check of this calibration was made using a different procedure and different calibrating apparatus.\*\* The calibrating apparatus consisted of an airtight room (located in the laboratory building) having an air intake nozzle (9-inch throat diameter) in one wall and a volumetric flow rate-measuring exhaust nozzle in the opposite wall. By measuring the rate of flow out of the airtight room, the speed of the air entering the room through the intake nozzle could be determined. The anemometer was placed in the throat of the intake nozzle and its calibration determined. In the velocity range of 1 to 4.5 meters per second this calibration was virtually the same as the previous calibration. At higher velocities a difference was obtained. The calibrations differed by 2 percent at 5 meters per second and increased to 8 percent at 15 meters per second. A pitot tube was recognized to be most accurate at high velocities. The second calibrating technique was recognized to have an accuracy deficiency at high velocities. Both calibration techniques were unsatisfactory at velocities less than 1 meter per second since the air flow could not be maintained constant and the zero error and drift of the manometers became large compared to their readings. The calibration using the pitot tube, therefore, was accepted for the velocity

\*Massachusetts Institute of Technology portable wind tunnel at O'Neill, Nebraska.

\*\*This calibration was performed at the Fan Test Laboratory, Engineering Experiment Station, Texas A&M campus, October 1956.

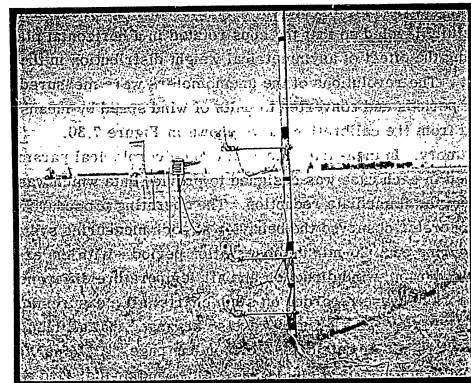


Figure 7.29 View of Rikoken anemometers installed at heights of 25, 50, and 100 cm

range of 1 to 15 meters per second. A third method was employed to obtain a calibration point at a velocity less than 1 meter per second. Under conditions of steady low velocity, virtually laminar flow at a height of 0.5 meters in the atmosphere\* the wind velocity was measured by observing the time required for smoke from a cigarette to travel a measured distance, and the corresponding anemometer indication was obtained.

In measuring wind profiles, the anemometers were installed at the heights shown in Figure 7.3. The three lowest anemometers,

\*These conditions existed at 2100 CST, 22 July 1956 at O'Neill.

those at 25, 50, and 100 cm, are shown in Figure 7.29. Each anemometer was carefully leveled so that the cups rotated in a horizontal plane thus minimizing the effect of asymmetrical weight distribution in the cup assembly.<sup>1</sup> The revolutions of the anemometers were measured for 20-minute periods and converted to units of wind speed by means of tables derived from the calibration curve shown in Figure 7.30.

7.3.8 Summary. In measuring these micrometeorological parameters, the method used in each case was designed to provide data which was in a convenient form for immediate reduction. The operating procedure was such that the operator observed the behavior of each measuring system at least once during each 20-minute observation period. With the exception of the radiation, wind direction and air temperature difference measurements which were recorded on strip charts, all measurements were recorded on data forms. These were so arranged that all tabulations and computations per data class were on one page. All computations were made from prepared tables, slide rule, and or standard desk calculator. This enabled the operator to reduce the data immediately after the measurements were made; hence, gross errors due to malfunctioning of the measuring equipment were noted and remedial action could be taken before measurements were resumed.

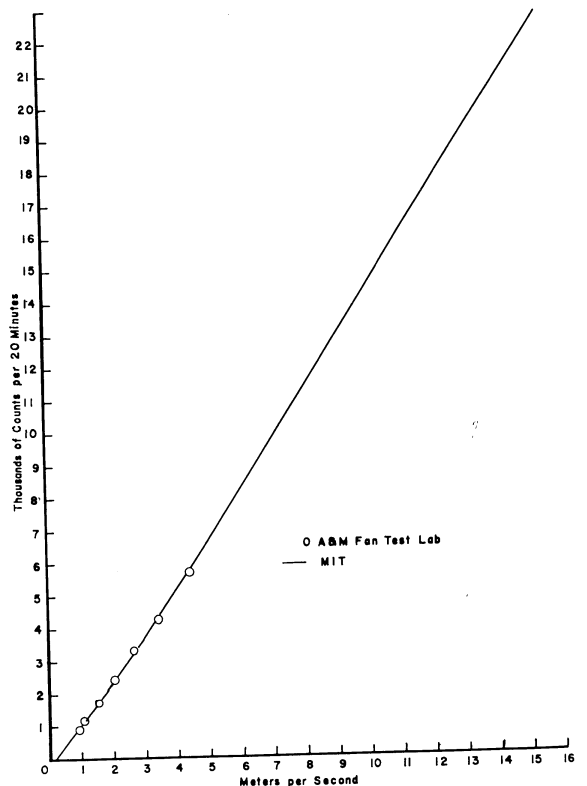


Figure 7.30 Anemometer calibration curve

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#### CHAPTER 8

##### MICROMETEOROLOGICAL DATA COLLECTED BY TEXAS A&M

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This section contains three groups of data collected during Project Prairie Grass. In the first group (Table 8.1) are micrometeorological data collected during the 68 regular and the two special gas releases. These observations covered a period of 20 minutes each, starting 5 minutes before and ending 5 minutes after the 10-minute period during which the gas was released.

The second group (Table 8.2) includes similar observations, but at times other than the 70 gas release times. 177 observational periods are included in this group.

The third group (Table 8.3) contains soil moisture and soil density data on four days during July and August.

\*Present affiliation: U. S. Navy Electronics Laboratory

Table 8.1

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA					
GAS RELEASE NO.	1	2	3	4	5	6	7	8	9	10	11	12
JULY (1956)	3	3	5	6	6	6	10	10	11	11	14	14
CST	1105	1505	2205	0105	1405	1705						
RADIATION (cal/cm <sup>2</sup> sec)												
Insolation	.0080	.0048	--	--	.0205	.0120						
Reflected	--	--	--	--	--	--						
Net Radiation	.0050	.0029	-.0013	-.0010	.0145	.0060						
AIR and SOIL TEMPERATURES (°C)												
Height (m)	--	--	--	--	--	--						
16.00	--	--	--	--	--	--						
8.00	21.08	23.78	22.41	20.09	29.18	30.19						
4.00	21.00	23.79	21.12	18.55	29.72	30.50						
2.00	22.12	23.87	19.53	17.50	30.17	30.80						
1.00	22.32	23.99	18.45	16.75	30.71	31.09						
.50	22.95	24.18	17.24	16.00	31.44	31.32						
.25	23.22	24.54	16.89	15.63	32.05	31.63						
.12	23.84	24.85	16.55	15.33	--	31.82						
-.03	24.06	25.39	--	--	--	--						
-.06	23.11	24.53	--	--	--	--						
-.12	21.71	23.20	--	--	--	--						
-.25	21.61	21.58	--	--	--	--						
-.50	20.53	20.38	--	--	--	--						
-1.00	18.21	18.18	--	--	--	--						
VAPOR PRESSURE (mb)												
16.00	--	--	--	--	--	--						
8.00	18.43	18.62	18.34	16.43	17.19	16.53						
4.00	18.73	18.73	18.44	16.52	17.39	16.84						
2.00	18.86	18.88	18.46	16.53	17.73	16.88						
1.00	19.04	19.10	18.58	16.58	18.11	17.07						
.50	19.51	19.38	18.58	16.64	18.46	17.24						
.25	--	19.77	18.49	16.65	18.73	17.30						
.12	19.95	20.21	18.96	17.29	19.27	17.41						
WIND SPEED (cm/sec)												
16.00	--	--	--	--	--	--						
8.00	321	233	211	304	703	846						
4.00	289	216	113	202	651	765						
2.00	258	190	44	123	593	680						
1.00	239	174	66	91	515	599						
.50	206	154	39	52	448	523						
.25	173	122	16	17	378	439						
WIND DIRECTION (deg)												
1.00	150	100	150	200	160	180						
SOIL TEMPERATURE CHANGE (°C)												
Initial Time	--	1450	--	--	--	--						
Run Time (min)	--	29	--	--	--	--						
-.03	--	-10	--	--	--	--						
-.06	--	00	--	--	--	--						
-.12	--	-11	--	--	--	--						
-.25	--	-03	--	--	--	--						
-.50	--	-02	--	--	--	--						
-1.00	--	-01	--	--	--	--						
Precipitation (cm)	--	--	--	--	--	--						

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA					
GAS RELEASE NO.	7	8	9	10	11	12	13	14	15	16	17	18
JULY (1956)	10	10	11	11	14	14	10	10	11	11	14	14
CST	1405	1705	1005	1205	0805	1005						
RADIATION (cal/cm <sup>2</sup> sec)												
Insolation	.0212	.0115	.0180	.0200	.0105	.0185						
Reflected	.0039	.0023	.0035	.0040	--	--						
Net Radiation	.0128	.0057	.0114	.0128	.0060	.0117						
AIR and SOIL TEMPERATURES (°C)												
Height (m)	28.71	29.90	25.76	28.42	--	--						
16.00	29.04	30.15	26.25	28.98	24.16	28.83						
8.00	29.46	30.57	26.61	29.58	24.64	29.25						
4.00	30.27	31.10	27.39	30.45	25.01	29.67						
2.00	31.21	31.47	28.19	31.47	25.42	30.53						
1.00	31.99	32.01	28.75	32.11	25.92	31.18						
.50	31.99	32.01	28.75	32.11	25.92	31.18						
.25	33.10	32.58	29.53	33.14	26.34	31.94						
.12	34.23	33.06	29.82	33.78	26.68	32.65						
-.03	34.90	33.74	26.64	31.79	24.23	28.66						
-.06	30.53	31.77	24.46	27.91	23.46	25.98						
-.12	24.23	26.77	23.14	23.93	24.25	24.16						
-.25	21.11	21.84	22.47	22.27	24.14	23.65						
-.50	20.03	19.99	20.42	20.34	21.49	21.34						
-1.00	18.22	18.22	18.28	18.20	18.75	18.68						
VAPOR PRESSURE (mb)												
16.00	12.06	13.16	20.60	22.84	--	--						
8.00	12.97	13.87	20.88	23.10	--	--						
4.00	13.02	13.72	20.92	23.14	--	--						
2.00	13.05	13.75	21.10	23.27	--	--						
1.00	13.18	13.85	21.14	23.40	--	--						
.50	13.50	13.98	21.20	23.43	--	--						
.25	13.85	14.16	21.39	23.59	--	--						
.12	14.15	14.32	21.92	23.62	--	--						
WIND SPEED (cm/sec)												
16.00	560	611	884	579	--	--						
8.00	508	540	842	536	944	973						
4.00	481	498	769	506	850	892						
2.00	444	452	700	468	761	799						
1.00	402	406	611	415	677	721						
.50	352	350	533	376	579	617						
.25	295	288	450	312	490	522						
WIND DIRECTION (deg)												
1.00	204	171	199	200	185	175						
SOIL TEMPERATURE CHANGE (°C)												
Initial Time	1351	1651	0950	1150	0750	0950						
Run Time (min)	27	26	16	26	28	27						
-.03	-1.80	-7.6	1.01	.79	.80	.23						
-.06	.53	-.29	.59	.70	-.16	.72						
-.12	.53	.20	.06	.23	-.08	.10						
-.25	.07	.13	-.08	-.03	-.11	-.08						
-.50	00	-.03	-.01	-.01	-.03	-.01						
-1.00	00	00	-.01	00	-.01	-.01						
Precipitation (cm)	--	--	--	--	--	--						

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA						
GAS RELEASE NO.		14	15	16	17	16							
JULY (1956)		22	23	23	23	23							
CST		2005	2205	0805	1005	2005	2205						
RADIATION (cal/cm <sup>2</sup> sec)													
Insolation	.0001	.0000	.0101	.0103	.0001	.0000							
Reflected	--	--	--	--	--	--							
Net Radiation	-.0011	-.0010	.0050	.0100	-.0011	-.0014							
AIR and SOIL TEMPERATURES (°C)													
Height (m)	22.34	21.04	20.32	24.61	27.91	25.11							
16.00	22.34	21.04	20.32	24.61	27.91	25.11							
8.00	21.64	19.76	20.51	24.82	27.83	24.30							
4.00	21.04	17.87	20.78	25.10	27.62	23.83							
2.00	20.39	16.25	21.44	25.61	27.44	23.52							
1.00	19.56	15.31	22.05	26.07	27.32	23.23							
.50	18.72	14.66	22.58	27.79	27.19	23.03							
.25	18.15	14.31	23.32	28.64	27.08	22.83							
.12	17.76	13.99	23.95	29.63	27.00	22.66							
-.03	26.48	23.10	20.75	26.71	29.49	26.39							
-.06	27.02	24.62	20.48	23.55	29.53	27.08							
-.12	25.50	24.95	21.44	21.62	27.26	26.51							
-.25	22.17	22.60	22.12	21.79	22.96	23.20							
-.50	20.36	20.48	20.72	20.68	20.32	20.28							
-1.00	18.95	19.02	19.04	18.99	18.54	18.62							
VAPOR PRESSURE (mb)													
16.00	16.13	14.91	17.19	17.66	--	--							
8.00	16.47	14.20	17.39	18.14	--	--							
4.00	16.74	14.21	17.41	18.21	--	--							
2.00	16.60	14.20	17.43	18.30	--	--							
1.00	16.02	14.25	17.52	18.40	--	--							
.50	15.86	14.27	17.63	18.57	--	--							
.25	15.71	14.32	17.65	18.81	--	--							
.12	15.71	14.99	17.77	19.08	--	--							
WIND SPEED (cm/sec)													
16.00	343	445	--	378	555	656							
8.00	264	348	--	362	455	488							
4.00	198	225	354	346	402	375							
2.00	146	139	322	331	341	322							
1.00	92	74	290	286	287	268							
.50	46	41	261	265	237	229							
.25	18	16	215	225	209	186							
WIND DIRECTION (deg)													
1.00	--	--	193	202	172	188							
SOIL TEMPERATURE CHANGE (°C)													
Initial Time	1952	2150	0752	0950	1950	2155							
Run Time (min)	25	30	24	27	26	22							
-.03	-1.08	-.68	.79	1.54	-.76	-.83							
-.06	-.63	-.60	-.32	-.92	-.59	-.70							
-.12	-.07	-.18	-.04	-.17	-.10	-.25							
-.25	.04	.04	-.04	-.02	.05	-.07							
-.50	-.05	.04	00	.01	00	-.04							
-1.00	-.04	.02	00	-.02	00	-.01							

Precipitation (cm) -- -- -- -- --

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA						
GAS RELEASE NO.		20	21	22	23	24							
JULY (1956)		25	25	25	26	29							
CST		1105	1305	2205	0005	2105	2305						
RADIATION (cal/cm <sup>2</sup> sec)													
Insolation	.0140	.0218	--	--	--	--							
Reflected	.00290	.00415	--	--	--	--							
Net Radiation	.0081	.0137	-.0009	-.0014	-.0014	-.00115							
AIR and SOIL TEMPERATURES (°C)													
Height (m)	27.26	30.14	28.91	26.75	23.62	22.07							
16.00	27.26	30.14	28.91	26.75	23.62	22.07							
8.00	27.77	30.88	28.84	26.70	23.52	21.99							
4.00	28.04	31.87	28.74	26.60	23.49	21.96							
2.00	28.59	32.49	28.60	26.42	23.40	21.89							
1.00	29.28	33.34	28.50	26.32	23.31	21.83							
.50	29.75	34.31	28.42	26.22	23.21	21.74							
.25	30.56	35.16	28.32	26.05	23.11	21.71							
.12	31.06	35.98	28.19	25.93	23.04	21.63							
-.03	28.52	33.60	27.70	26.32	27.92	25.85							
-.06	24.91	28.89	27.65	26.57	28.14	26.38							
-.12	22.80	23.92	26.76	26.11	26.63	26.16							
-.25	22.74	22.56	23.90	24.06	23.98	24.10							
-.50	21.21	21.12	21.14	21.17	21.63	21.65							
-1.00	19.00	18.94	19.04	19.08	19.62	19.62							
VAPOR PRESSURE (mb)													
16.00	14.91	14.19	14.56	15.81	--	--							
8.00	15.22	14.33	14.65	15.87	--	--							
4.00	15.24	14.99	14.66	15.81	--	--							
2.00	15.30	14.41	14.60	15.82	--	--							
1.00	15.41	14.47	14.62	15.80	20.7*	20.9*							
.50	15.60	14.51	14.64	15.81	--	--							
.25	15.60	14.57	14.65	15.77	--	--							
.12	15.73	14.71	14.59	15.75	--	--							
WIND SPEED (cm/sec)													
16.00	752	1211	859	1041	883	865							
8.00	721	1130	772	933	784	764							
4.00	627	1017	675	814	685	662							
2.00	--	938	611	739	605	586							
1.00	533	826	531	639	537	521							
.50	475	727	462	557	471	461							
.25	393	594	376	454	389	382							
WIND DIRECTION (deg)													
1.00	162	188	167	170	132	146							
SOIL TEMPERATURE CHANGE (°C)													
Initial Time	1050	1250	2154	2350	2050	2250							
Run Time (min)	26	27	23	26	26	27							
-.03	.91	.67	-.16	-.24	-.53	-.78							
-.06	.96	.64	-.20	-.11	-.43	-.77							
-.12	.13	.37	-.21	-.11	-.12	-.33							
-.25	-.04	-.01	.02	.05	.06	.12							
-.50	-.02	-.01	-.01	.00	.00	.00							
-1.00	-.01	.00	-.01	.01	.00	-.03							

Precipitation (cm) -- -- -- -- --  
\* Sling Psychrometer

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA		
GAS RELEASE NO.	25	26	27	28	29	30			
AUGUST (1956)	1	2	2	3	3	3			
CST	1305	1205	1405	0005	0205	1305			
RADIATION (cal/cm <sup>2</sup> sec)									
Insolation	.0092	.0180	.0183	--	--	.0202			
Reflected	.00185	.00305	--	--	--	.00329			
Net Radiation	.0052	.0125	.0123	--	-.0003	.0129			
AIR and SOIL TEMPERATURES (°C)									
Height (m)									
16.00	22.87	--	--	25.24	26.24	31.88			
8.00	22.92	27.93	30.28	24.76	25.81	32.39			
4.00	23.26	28.57	30.84	24.38	25.72	32.86			
2.00	23.62	29.21	31.43	24.22	25.36	33.53			
1.00	24.09	29.91	31.96	24.07	25.14	34.00			
.50	24.77	30.42	32.62	23.92	24.78	34.73			
.25	25.32	31.15	33.45	23.72	24.58	35.42			
.12	25.72	31.74	34.25	23.53	24.33	36.10			
-.03	27.41	27.41	29.97	23.68	22.92	33.29			
-.06	25.32	25.42	27.84	24.64	23.78	30.50			
-.12	22.91	22.96	23.93	25.25	24.60	25.03			
-.25	22.50	22.94	22.31	23.74	23.08	22.94			
-.50	21.73	21.38	21.31	21.59	21.52	21.58			
-1.00	19.82	19.70	19.65	19.82	19.82	19.71			
VAPOR PRESSURE (mb)									
16.00	--	--	--	--	--	18.67			
8.00	22.57	22.43	21.72	--	--	18.27			
4.00	22.40	22.69	21.86	--	--	19.48			
2.00	22.63	23.02	22.02	--	--	19.74			
1.00	--	23.40	22.29	--	--	20.07			
.50	--	23.72	22.44	--	--	20.53			
.25	23.28	23.92	22.57	--	--	20.65			
.12	23.75	24.31	22.82	--	--	21.04			
WIND SPEED (cm/sec)									
16.00	328	851	849	508	606	885			
8.00	318	775	755	388	529	852			
4.00	297	721	694	321	441	775			
2.00	275	648	613	255	394	697			
1.00	248	568	540	212	340	628			
.50	221	511	483	177	296	540			
.25	173	422	402	154	241	455			
WIND DIRECTION (deg)									
1.00	183	171	176	167	208	196			
SOIL TEMPERATURE CHANGE (°C)									
Initial Time	1252	1150	1350	2357	0150	1250			
Run Time (min)	26	27	26	20	27	26			
-.03	.04	1.35	1.10	-.51	-.21	.72			
-.06	.21	1.09	.69	-.61	-.17	.74			
-.12	.07	.14	.36	-.45	-.10	.02			
-.25	-.04	-.06	.11	-.27	-.01	.05			
-.50	-.03	-.07	.05	-.20	.02	.00			
-1.00	-.03	-.04	.06	-.31	.00	.02			
Precipitation (cm)	--	--	--	--	--	--			

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA		
GAS RELEASE NO.	31	32	33	34	35 <sub>s</sub>	36			
AUGUST (1956)	3	6	7	7	7	11			
CST	1505	2005	1305	1505	2305	2135			
RADIATION (cal/cm <sup>2</sup> sec)									
Insolation	.0152	.0000	.0164	.0174	--	--			
Reflected	.00284	--	--	--	--	--			
Net Radiation	.0092	-.0013	.0100	.0113	-.0007	-.00091			
AIR and SOIL TEMPERATURES (°C)									
Height (m)									
16.00	33.23	27.21	21.71	29.00	23.03	23.57	20.74		
8.00	33.44	25.33	27.88	29.21	22.68	22.30	19.81		
4.00	33.79	23.71	28.16	29.58	22.47	21.04	19.32		
2.00	34.25	22.93	28.73	30.19	22.28	19.73	18.84		
1.00	34.85	22.45	29.16	30.99	22.17	19.13	18.63		
.50	35.37	22.06	29.64	31.45	22.05	18.47	18.10		
.25	35.81	21.66	30.07	32.13	21.94	18.34	18.19		
.12	36.11	21.38	30.61	32.62	21.79	18.21	17.98		
-.03	34.04	25.35	29.57	31.07	23.42	24.85	23.15		
-.06	32.10	26.42	27.07	28.86	24.41	26.02	24.41		
-.12	26.80	26.18	23.43	24.86	25.22	26.27	25.49		
-.25	23.11	24.00	22.58	22.73	23.93	23.78	24.01		
-.50	21.50	22.02	21.80	21.82	21.91	21.63	21.74		
-1.00	19.69	19.94	19.89	19.93	20.08	19.99	20.08		
VAPOR PRESSURE (mb)									
16.00	18.49	13.82	16.64	17.00	19.99	19.08	18.30		
8.00	18.65	14.39	16.97	17.21	20.12	18.93	18.43		
4.00	18.76	15.08	17.16	17.38	20.17	19.06	18.44		
2.00	18.79	15.54	17.41	17.51	20.17	18.91	18.44		
1.00	19.07	15.85	17.62	17.76	20.23	18.84	18.52		
.50	19.20	16.01	17.77	17.97	20.27	19.32	18.83		
.25	19.34	16.09	18.09	18.10	20.27	18.59	18.59		
.12	19.33	16.12	18.36	18.28	20.33	18.59	18.83		
WIND SPEED (cm/sec)									
16.00	1013	609	1063	1214	639	421	464		
8.00	--	412	--	1128	520	318	342		
4.00	887	288	848	1052	434	253	243		
2.00	787	213	756	920	373	180	186		
1.00	691	160	690	846	340	110	137		
.50	617	136	580	706	281	88	116		
.25	527	95	484	587	231	45	81		
WIND DIRECTION (deg)									
1.00	204	168	171	140	164	97	154		
SOIL TEMPERATURE CHANGE (°C)									
Initial Time	1450	1950	1250	1450	2255	2120	2320		
Run Time (min)	28	27	27	28	21	26	30		
-.03	-.06	-.70	.10	.14	-.38	-.47	-.35		
-.06	.25	-.55	.64	.31	-.39	-.42	-.38		
-.12	.25	-.09	.22	.25	-.19	-.12	-.23		
-.25	.10	.05	-.12	.02	-.04	.12	.00		
-.50	.00	.01	-.11	-.04	.05	.04	.01		
-1.00	.00	.01	-.08	-.03	-.04	.04	.00		
Precipitation (cm)	--	--	--	--	--	--	--		

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA							
GAS RELEASE NO.		37	38	39	40	41	42							
AUGUST (1956)		12	12	13	14	14	14							
CST		0305	0505	2235	0035	0305	0505							
RADIATION (cal/cm <sup>2</sup> sec)														
Insolation	--	--	--	--	--	--	--							
Reflected	--	--	--	--	--	--	--							
Net Radiation	-0.0067	-0.0085	-0.0135	-0.014	-0.0123	-0.0192								
AIR and SOIL TEMPERATURES (°C)														
Height (m)														
16.00	21.02	20.07	23.68	21.91	21.63	21.92								
8.00	20.90	19.93	22.39	21.11	20.82	21.68								
4.00	20.79	19.84	21.28	20.69	20.43	21.61								
2.00	20.65	19.82	20.47	20.29	20.20	21.49								
1.00	20.55	19.65	20.61	19.95	20.03	21.30								
.50	20.41	19.34	19.55	19.52	19.90	21.16								
.25	20.33	19.48	19.35	19.29	19.62	21.03								
.12	20.22	19.37	19.06	19.08	19.43	20.90								
-.03	21.68	21.59	25.09	23.54	22.26	21.92								
-.06	22.69	22.37	26.52	24.88	23.53	22.82								
-.12	24.21	23.62	27.42	26.41	25.28	24.56								
-.25	23.83	23.62	24.83	24.89	24.80	24.47								
-.50	21.80	21.81	21.87	21.92	22.06	22.06								
-1.00	20.08	20.05	20.03	20.02	20.09	22.03								
VAPOR PRESSURE (mb)														
16.00	19.61	19.77	12.82	13.11	14.93	14.13								
8.00	19.62	19.77	12.91	13.15	15.03	14.14								
4.00	19.63	19.82	12.92	13.18	15.08	14.19								
2.00	19.62	19.75	12.92	13.19	15.07	14.16								
1.00	19.63	19.73	12.94	13.21	15.08	14.20								
.50	20.11	20.00	12.95	13.22	15.08	14.23								
.25	19.68	19.72	12.93	13.23	15.09	14.22								
.12	19.84	19.73	12.99	13.31	15.09	14.23								
WIND SPEED (cm/sec)														
16.00	726	679	542	486	671	828								
8.00	608	585	419	343	550	751								
4.00	528	504	291	250	435	673								
2.00	459	428	229	208	369	594								
1.00	400	370	169	158	316	527								
.50	344	317	152	137	267	452								
.25	281	258	112	99	216	380								
WIND DIRECTION (deg)														
1.00	176	161	122	165	185	199								
SOIL TEMPERATURE CHANGE (°C)														
Initial Time	0250	0450	2220	0020	0250	0450								
Run Time (min)	30	26	28	28	28	28								
-.03	.06	-.12	-.46	-.27	-.10	-.05								
-.06	-.13	-.09	-.45	-.30	-.18	-.01								
-.12	-.29	-.11	-.25	-.25	-.15	-.14								
-.25	-.04	-.08	.02	-.04	-.03	-.06								
-.50	00	-.01	00	.01	.01	.01								
-1.00	-.01	-.01	-.02	00	.02	00								

Precipitation (cm) -- -- -- -- --

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA							
GAS RELEASE NO.		43	44	45	46	47	48s	48s	48s	48s	48s	48s	48s	
AUGUST (1956)		15	15	15	15	20	20	20	20	20	20	20	21	
CST		1205	1405	1705	1850	1005	1205	1255	0905					
RADIATION (cal/cm <sup>2</sup> sec)														
Insolation	.0178	.0164	.00443	.00035	.0187	.0125	--	.0142						
Reflected	.0030	.0028	.00090	--	.00313	.00215	--	.00253						
Net Radiation	.0108	.0097	.0014	-.0014	.0108	.0070	--	.0081						
AIR and SOIL TEMPERATURES (°C)														
Height (m)														
16.00	31.63	33.92	34.59	33.12	16.81	18.55	18.29	17.18						
8.00	32.00	34.37	34.75	33.01	17.10	18.77	19.71	17.70						
4.00	32.60	34.73	34.91	32.90	17.47	19.04	20.11	18.05						
2.00	33.05	35.43	35.04	32.74	17.73	19.45	20.72	18.40						
1.00	34.17	36.06	35.28	32.57	18.46	19.91	21.31	18.96						
.50	34.92	36.92	35.59	32.44	19.20	20.52	22.10	19.43						
.25	35.76	37.69	35.82	32.32	20.13	21.12	23.15	19.97						
.12	36.64	38.64	35.95	32.20	21.30	22.02	24.44	20.46						
-.03	33.60	37.31	35.56	32.50	18.27	25.66	--	17.12						
-.06	28.82	32.25	33.03	31.67	17.79	22.57	--	16.89						
-.12	24.63	26.11	27.99	28.32	18.21	19.07	--	18.40						
-.25	23.75	23.72	24.11	24.49	20.24	19.97	--	20.52						
-.50	22.29	22.25	22.12	22.09	20.96	20.78	--	20.73						
-1.00	20.13	20.11	20.08	20.05	20.28	20.13	--	20.04						
VAPOR PRESSURE (mb)														
16.00	11.83	10.64	11.30	11.41	--	9.73	--	12.53						
8.00	12.28	11.17	12.17	11.51	--	10.09	--	12.78						
4.00	12.36	11.16	12.18	11.57	--	10.26	--	12.81						
2.00	12.46	11.15	12.21	11.63	--	10.35	--	12.93						
1.00	12.50	11.19	12.26	11.64	--	10.49	--	13.03						
.50	12.61	11.30	12.31	11.64	--	10.58	--	13.17						
.25	12.74	11.33	12.39	11.68	--	10.86	--	13.27						
.12	12.95	11.41	12.34	11.70	--	11.33	--	13.38						
WIND SPEED (cm/sec)														
16.00	641	760	788	787	384	356	376	1027						
8.00	606	719	735	707	374	347	365	961						
4.00	565	680	665	625	356	329	342	--						
2.00	522	--	602	556	332	307	321	784						
1.00	468	539	531	486	302	277	2.94	691						
.50	411	468	480	428	270	249	2.96	606						
.25	343	397	378	364	--	210	2.23	505						
WIND DIRECTION (deg)														
1.00	168	156	153	134	--	216	--	189						
SOIL TEMPERATURE CHANGE (°C)														
Initial Time	1150	1350	1650	1835	0950	1150	--	0850						
Run Time (min)	27	28	26	27	26	28	--	27						
-.03	.67	.21	-.57	-.77	1.87	.47	--	.96						
-.06	.60	.52	-.25	-.40	.70	1.03	--	.52						
-.12	-.22	-.36	.13	-.05	.03	.34	--	.00						
-.25	-.09	-.03	.08	.05	.03	-.06	--	-.06						
-.50	-.03	-.02	-.02	-.04	-.04	-.03	--	-.02						
-1.00	-.02	-.01	00	-.07	-.04	-.01	--	-.02						

Precipitation (cm) -- -- -- -- --

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA						
GAS RELEASE NO.	55	56	57	58	59	60							
AUGUST (1956)	25	25	25	25	25	26							
CST	0105	0305	1735	1935	2235	0035							
RADIATION (cal/cm <sup>2</sup> sec)													
Insolation	--	--	.0054	--	--	--							
Reflected	--	--	.00087	--	--	--							
Net Radiation	-.0015	-.0014	.0013	-.0013	-.0014	-.0014							
AIR and SOIL TEMPERATURES (°C)													
Height (m)	17.17	15.88	33.54	29.50	26.61	26.49							
16.00	17.08	15.70	33.76	28.49	25.34	26.17							
8.00	16.90	15.47	33.91	27.16	24.31	25.91							
4.00	16.75	15.29	34.11	23.64	23.00	25.75							
2.00	16.65	15.15	34.19	25.04	23.13	25.49							
1.00	16.48	15.03	34.33	25.13	22.82	25.35							
.50	16.37	14.91	34.52	24.82	22.58	25.14							
.25	16.20	14.77	34.61	24.58	22.29	24.98							
-.03	20.56	19.42	31.70	28.09	24.52	23.28							
-.06	21.43	20.85	29.54	27.97	25.12	23.87							
-.12	23.58	22.75	25.51	25.90	25.10	24.46							
-.25	23.04	22.82	22.19	22.49	22.99	23.09							
-.50	21.02	21.02	20.89	20.78	20.89	20.94							
-1.00	19.71	19.68	19.46	19.51	19.59	19.60							
VAPOR PRESSURE (mb)													
16.00	11.72	12.37	12.39	--	12.82	11.89							
8.00	11.73	12.21	12.59	--	12.99	11.96							
4.00	11.73	12.29	12.55	--	13.05	11.97							
2.00	11.73	12.39	12.55	--	13.11	11.97							
1.00	11.74	12.39	12.59	--	13.10	12.01							
.50	11.73	12.36	12.61	--	13.14	12.04							
.25	11.73	12.36	12.63	--	13.15	12.06							
.12	11.72	12.30	12.65	--	13.15	12.08							
WIND SPEED (cm/sec)													
16.00	830	704	989	572	628	723							
8.00	755	619	879	433	462	595							
4.00	679	546	824	311	342	533							
2.00	594	475	720	224	261	457							
1.00	517	415	642	165	202	404							
.50	446	361	556	131	168	349							
.25	374	299	469	103	134	294							
WIND DIRECTION (deg)													
1.00	143	138	185	158	160	182							
SOIL TEMPERATURE CHANGE (°C)													
Initial Time	0050	0250	1722	1923	2227	0028							
Run Time (min)	26	26	25	25	19	18							
-.03	-.24	-.21	-.37	-.86	-.39	-.10							
-.06	-.21	-.22	-.22	-.51	-.24	-.17							
-.12	-.17	-.22	-.16	-.03	-.13	-.13							
-.25	-.01	-.04	.08	.11	.03	-.03							
-.50	00	00	.01	.03	.01	00							
-1.00	00	-.02	-.01	.02	.01	00							
Precipitation (cm)	--	--	--	--	--	--							

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA						
GAS RELEASE NO.	49	50	51	52	53	54							
AUGUST (1956)	21	21	21	24	24	24							
CST	1105	1405	1535	1120	2005	2205							
RADIATION (cal/cm <sup>2</sup> sec)													
Insolation	.0209	.0202	.0158	.0204	--	--							
Reflected	.00303	.00309	.00259	.00289	--	--							
Net Radiation	.0129	.0128	.0088	.0110	-.0015	-.0017							
AIR and SOIL TEMPERATURES (°C)													
Height (m)	21.45	27.14	28.36	23.17	21.32	19.56							
16.00	21.94	27.68	29.13	23.59	20.26	19.31							
8.00	22.64	27.90	29.40	24.08	18.77	18.94							
4.00	23.29	28.64	29.80	24.96	17.39	18.68							
2.00	24.05	29.20	30.50	25.98	16.56	18.45							
1.00	25.00	30.95	31.07	26.74	15.76	18.25							
.50	25.72	31.23	31.97	27.55	15.37	18.04							
.25	26.38	31.95	32.52	29.19	14.90	17.89							
-.03	22.77	29.55	30.45	27.56	25.07	22.48							
-.06	20.34	26.18	27.78	23.69	26.32	23.92							
-.12	18.86	21.20	22.45	21.12	25.65	24.68							
-.25	20.15	19.99	20.12	21.57	22.66	22.96							
-.50	20.60	20.45	20.34	20.91	20.82	20.60							
-1.00	19.92	19.83	19.73	19.58	19.56	19.64							
VAPOR PRESSURE (mb)													
16.00	14.03	14.09	12.94	9.22	10.64	11.40							
8.00	13.84	14.95	13.21	10.72	10.79	11.42							
4.00	13.77	14.39	13.23	10.69	10.75	11.42							
2.00	13.60	14.49	13.34	10.79	10.74	11.40							
1.00	13.47	14.58	13.53	11.19	10.78	11.42							
.50	13.29	14.68	13.57	11.10	10.86	11.41							
.25	13.20	14.75	13.65	11.21	10.84	11.39							
.12	12.87	14.93	13.92	11.49	10.84	11.42							
WIND SPEED (cm/sec)													
16.00	868	819	863	521	594	641							
8.00	802	796	804	508	446	537							
4.00	752	764	766	496	320	464							
2.00	674	673	682	442	228	394							
1.00	603	606	618	404	156	340							
.50	522	--	547	--	137	299							
.25	444	448	475	308	101	248							
WIND DIRECTION (deg)													
1.00	185	197	226	--	119	147							
SOIL TEMPERATURE CHANGE (°C)													
Initial Time	1050	1350	1520	1150	1950	2150							
Run Time (min)	28	28	25	26	26	27							
-.03	1.44	.56	-.02	1.21	-.90	-.35							
-.06	.97	.60	.20	.89	-.61	-.44							
-.12	.22	.40	.34	.20	-.12	-.21							
-.25	-.06	-.02	.04	-.06	.07	.04							
-.50	-.03	-.02	-.03	-.02	-.01	00							
-1.00	-.01	-.03	-.02	-.02	-.01	00							
Precipitation (cm)	--	--	--	--	--	--							



Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA			
GAS RELEASE NO.	61	62	63	64	65	66				
AUGUST (1956)	27	27	27	27	29	29				
CST	1105	1405	2005	2235	1930	2135				
RADIATION (cal/cm <sup>2</sup> sec)										
Insolation	.0190	.0110	--	--	--	--				
Reflected	.0030	.00174	--	--	--	--				
Net Radiation	.0019	-.0072	-.0011	-.0005	-.0022	-.0018				
AIR and SOIL TEMPERATURES (°C)										
Height (m)	29.80	29.77	29.52	26.77	25.98	22.02				
16.00	30.41	30.00	27.27	23.85	25.61	21.22				
8.00	31.00	30.49	25.54	22.16	25.22	20.65				
4.00	31.63	30.75	24.07	20.30	24.86	20.19				
2.00	32.29	31.15	21.41	19.00	24.76	19.88				
1.00	33.20	31.58	19.24	18.70	24.57	19.57				
.50	34.10	32.10	18.17	18.16	24.30	19.27				
.25	34.61	32.35	17.57	17.83	24.04	18.99				
.12	30.12	30.02	20.04	23.49	--	--				
-.03	25.86	28.56	27.33	24.68	--	--				
-.06	23.60	25.44	26.30	25.54	--	--				
-.12	23.19	23.01	23.77	23.98	--	--				
-.25	21.49	21.39	21.55	21.59	--	--				
-.50	19.66	19.61	19.56	19.78	--	--				
-1.00										
VAPOR PRESSURE (mb)										
16.00	11.64	12.41	15.09	15.33	--	--				
8.00	12.15	12.56	15.04	15.68	--	--				
4.00	12.10	12.67	14.88	15.87	--	--				
2.00	12.20	12.83	14.13	15.58	--	--				
1.00	12.20	12.91	13.64	15.16	--	--				
.50	12.28	13.13	13.20	14.86	--	--				
.25	12.36	13.30	12.75	14.69	--	--				
.12	12.44	13.47	12.20	14.51	--	--				
WIND SPEED (cm/sec)										
16.00	980	632	287	307	768	650				
8.00	926	603	195	269	626	506				
4.00	--	583	139	169	530	392				
2.00	782	518	116	130	455	314				
1.00	700	461	26	48	393	256				
.50	614	405	--	25	339	217				
.25	520	343	--	--	277	177				
WIND DIRECTION (deg)										
1.00	190	189	--	159	153					
SOIL TEMPERATURE CHANGE (°C)										
Initial Time	1050	1353	1950	2220	--	--				
Run Time (min)	26	23	27	27	--	--				
-.03	1.40	.46	-.89	-.24	--	--				
-.06	.82	-.27	-.54	-.31	--	--				
-.12	.11	.15	-.03	-.19	--	--				
-.25	-.08	.03	.08	.01	--	--				
-.50	-.05	.01	.04	.00	--	--				
-1.00	-.03	.00	.05	.00	--	--				
Precipitation (cm)	--	--	--	--	--	--				

Table 8.1 (Continued)

HOURLY OBSERVATIONS							O'NEILL, NEBRASKA			
GAS RELEASE NO.	07	68								
AUGUST (1956)	30	30								
CST	0035	0235								
RADIATION (cal/cm <sup>2</sup> sec)										
Insolation	--	--								
Reflected	--	--								
Net Radiation	-.0011	-.0009								
AIR and SOIL TEMPERATURES (°C)										
Height (m)	21.12	21.97								
16.00	20.88	21.36								
8.00	20.66	20.94								
4.00	20.55	20.65								
2.00	20.38	20.38								
1.00	20.21	20.24								
.50	20.19	20.08								
.25	20.02	19.88								
.12	--	--								
-.03	--	--								
-.06	--	--								
-.12	--	--								
-.25	--	--								
-.50	--	--								
-1.00	--	--								
VAPOR PRESSURE (mb)										
16.00	--	--								
8.00	--	--								
4.00	--	--								
2.00	--	--								
1.00	--	--								
.50	--	--								
.25	--	--								
.12	--	--								
WIND SPEED (cm/sec)										
16.00	748	558								
8.00	615	427								
4.00	521	331								
2.00	444	269								
1.00	385	219								
.50	336	188								
.25	274	149								
WIND DIRECTION (deg)										
1.00	168	159								
SOIL TEMPERATURE CHANGE (°C)										
Initial Time	--	--								
Run Time (min)	--	--								
-.03	--	--								
-.06	--	--								
-.12	--	--								
-.25	--	--								
-.50	--	--								
-1.00	--	--								
Precipitation (cm)	--	--								

Table 8.2

HOURLY OBSERVATIONS							July 10, 1956						O'NEILL, NEBRASKA		
CST	1305	1405	1505	1605	1705	1805									
RADIATION (cal/cm <sup>2</sup> sec)															
Insolation	.0225	.0212	.0187	.0150	.0115	.0066									
Reflected	.0040	.0039	.0036	.0027	.0023	.0015									
Net Radiation	.0138	.0128	.0108	.0085	.0057	.0025									
AIR and SOIL TEMPERATURES (°C)															
Height (m)	28.55	28.71	29.22	29.85	29.90	29.89									
16.00	29.09	29.04	29.57	30.18	30.15	30.12									
8.00	29.21	29.46	29.75	30.61	30.57	30.34									
4.00	29.84	30.27	30.34	30.73	31.10	30.52									
2.00	30.50	31.21	31.10	31.61	31.47	30.79									
1.00	32.01	31.99	32.01	32.30	32.01	31.00									
.50	32.93	33.10	33.39	33.22	32.58	31.16									
-.25	33.92	34.33	34.27	34.16	33.06	31.38									
-.50	33.68	34.89	35.41	35.22	33.74	31.75									
-.75	29.89	30.53	31.58	32.08	31.77	30.82									
-1.00	23.25	24.23	25.34	26.16	26.77	27.19									
	21.01	21.11	21.27	21.55	21.64	22.17									
	20.07	20.03	19.97	20.00	19.89	19.97									
	18.23	18.22	18.19	18.22	18.22	18.20									
VAPOR PRESSURE (mb)															
16.00	11.90	12.06	12.12	13.28	13.16	13.41									
8.00	13.06	12.97	13.07	13.81	13.87	13.59									
4.00	13.03	13.02	13.10	13.87	13.72	13.53									
2.00	13.12	13.05	13.16	13.92	13.75	13.69									
1.00	13.32	13.18	13.42	14.15	13.85	13.78									
.50	13.71	13.50	13.63	14.52	13.98	13.88									
.25	14.26	13.85	13.94	14.65	14.16	13.93									
.12	14.81	14.15	14.31	15.12	14.32	14.02									
WIND SPEED (cm/sec)															
16.00	362	560	479	506	611	827									
8.00	314	508	433	461	540	710									
4.00	324	481	408	427	488	647									
2.00	298	444	379	390	452	572									
1.00	277	402	350	353	406	503									
.50	246	352	309	308	350	432									
.25	203	295	257	253	288	362									
WIND DIRECTION (deg)															
1.00	--	295	--	--	171	--									
SOIL TEMPERATURE CHANGE (°C)															
Initial Time	1253	--	1452	1550	1757	--									
Run Time (min)	26	--	29	29	21	--									
-.03	.85	--	.02	-.37	--	--									
-.06	.85	--	.40	-.06	--	--									
-.12	.55	--	.39	.35	--	--									
-.25	.02	--	-.08	.12	--	--									
-.50	-.05	--	-.04	-.01	--	--									
-1.00	0	--	-.01	0	--	--									
Precipitation (cm)	--	--	--	--	--	--									

Table 8.2 (Continued)

HOURLY OBSERVATIONS							July 10, 1956						O'NEILL, NEBRASKA		
CST	1905	2005	2105	0005*	0105*	0205*									
RADIATION (cal/cm <sup>2</sup> sec)															
Insolation	.0002	--	--	--	--	--									
Reflected	.0004	--	--	--	--	--									
Net Radiation	-.0004	-.0017	-.0016	-.0014	-.0013	-.0013									
AIR and SOIL TEMPERATURES (°C)															
Height (m)	29.15	26.90	25.72	--	--	--									
16.00	29.12	26.36	25.06	23.29	21.99	21.92									
8.00	29.07	25.90	24.47	23.03	21.61	21.50									
4.00	29.03	25.50	24.13	22.86	21.38	21.24									
2.00	28.99	25.26	23.81	22.63	21.12	21.04									
1.00	28.96	25.02	23.45	22.47	20.96	20.86									
.50	28.91	24.78	23.20	22.29	20.74	20.64									
.25	28.89	24.58	23.03	22.13	20.58	20.39									
.12	30.34	28.48	26.89	24.10	23.47	22.91									
-.03	27.20	27.06	26.84	25.54	25.16	24.86									
-.06	22.42	22.72	23.00	23.30	23.33	23.34									
-.12	19.99	20.01	20.10	20.20	20.26	20.34									
-.50	18.20	18.25	18.32	18.39	18.34	18.35									
-1.00															
VAPOR PRESSURE (mb)															
16.00	14.08	14.63	14.06	--	15.76	16.07									
8.00	14.24	14.80	14.20	15.70	16.06	16.04									
4.00	14.35	14.84	14.24	15.73	16.00	16.07									
2.00	14.43	14.83	14.28	15.76	16.02	16.09									
1.00	14.54	14.98	14.34	15.78	16.01	16.09									
.50	14.58	15.02	14.36	15.78	16.03	16.11									
.25	14.63	15.02	14.43	15.80	16.08	16.11									
.12	14.70	15.02	14.54	15.80	16.00	16.13									
WIND SPEED (cm/sec)															
16.00	729	627	660	801	1368	632									
8.00	639	478	501	640	1061	491									
4.00	569	380	397	554	900	416									
2.00	497	307	322	484	775	352									
1.00	432	260	279	415	661	305									
.50	373	222	230	362	576	262									
.25	299	161	173	294	457	201									
WIND DIRECTION (deg)															
1.00	--	--	--	--	--	--									
SOIL TEMPERATURE CHANGE (°C)															
Initial Time	1850	1950	2050	2353	0058	0155									
Run Time (min)	28	28	28	28	26	22									
-.03	-.84	-.87	-.68	-.27	-.20	.20									
-.06	-.51	-.52	-.53	-.30	-.17	.20									
-.12	-.02	-.09	-.17	-.19	-.08	.11									
-.25	.15	.14	.06	0	+.06	.01									
-.50	.02	.01	0	-.02	+.09	0									
-1.00	.01	.05	0	-.04	0	.02									
Precipitation (cm)	--	--	--	--	--	--									
* July 11, 1956															



Table 8.2 (Continued)

HOURLY OBSERVATIONS							July 23, 1956							O'NEILL, NEBRASKA						
CST	0905	1105	1205	1305	1405	1605														
RADIATION (cal/cm <sup>2</sup> sec)																				
Insolation	.0148	.0205	.0219	.0217	.0201	.0148														
Reflected	--	--	--	--	--	--														
Net Radiation	.0080	.0118	.0130	.0130	.0117	.0076														
AIR and SOIL TEMPERATURES (°C)																				
Height (m)	22.67	26.10	27.43	28.56	30.54	30.92														
16.00	23.18	26.83	27.89	28.83	30.91	31.22														
8.00	23.65	26.89	28.30	29.52	31.76	31.61														
4.00	24.19	27.81	29.11	30.45	32.47	32.03														
2.00	25.04	28.73	29.88	30.96	32.85	32.80														
1.00	25.81	29.59	31.02	31.85	33.62	33.68														
.50	26.80	30.92	32.17	33.05	34.90	34.62														
.25	27.44	31.97	33.06	34.21	35.80	35.22														
.12	23.44	30.35	33.22	35.40	37.20	36.63														
-.03	21.69	25.86	28.20	30.24	32.72	33.05														
-.06	21.37	22.10	22.81	23.74	25.72	26.48														
-.12	21.93	21.64	21.57	21.60	21.68	21.98														
-.25	20.65	20.60	20.54	20.54	20.36	20.37														
-.50	19.01	18.92	18.92	18.85	18.74	18.56														
-.100																				
VAPOR PRESSURE (mb)																				
16.00	18.21	--	13.77	--	13.00	--														
8.00	18.47	--	--	--	13.91	--														
4.00	18.50	17.57	--	--	13.83	--														
2.00	18.54	17.57	--	--	13.84	--														
1.00	18.61	17.77	14.89	--	13.82	--														
.50	18.80	18.04	14.68	--	13.99	--														
.25	18.86	18.34	--	--	14.07	--														
.12	19.09	18.83	15.30	--	14.11	--														
WIND SPEED (cm/sec)																				
16.00	516	410	442	512	546	521														
8.00	489	378	424	483	511	485														
4.00	464	359	397	452	472	455														
2.00	425	342	373	428	457	423														
1.00	379	305	334	387	410	382														
.50	338	275	303	343	369	336														
.25	281	234	255	289	303	287														
WIND DIRECTION (deg)																				
1.00	186	180	170	170	200	210														
SOIL TEMPERATURE CHANGE (°C)																				
Initial Time	0850	1057	1154	1254	1354	1555														
Run Time (min)	27	25	27	20	25	30														
-.03	1.40	1.38	.89	.63	-.10	-.36														
-.06	-.74	1.03	-.74	.72	.36	.16														
-.12	-.07	-.22	-.30	.49	.21	-.16														
-.25	-.05	-.09	-.04	.13	.17	.25														
-.50	0	-.08	-.04	.08	-.02	.12														
-1.00	.01	-.01	-.03	0	-.02	-.01														

Precipitation (cm) -- -- -- -- --

Table 8.2 (Continued)

HOURLY OBSERVATIONS							July 23, 1956							O'NEILL, NEBRASKA						
CST	1705	1805	1905	2105	2305	0005*														
RADIATION (cal/cm <sup>2</sup> sec)																				
Insolation	.0099	.0060	.0018	--	--	--														
Reflected	--	--	--	--	--	--														
Net Radiation	.0042	.0017	-.0007	-.0011	-.0014	-.0014														
AIR and SOIL TEMPERATURES (°C)																				
Height (m)	31.21	31.05	29.96	26.83	23.68	24.82														
16.00	31.48	31.27	30.04	26.49	23.13	24.26														
8.00	31.93	31.52	30.04	26.18	22.69	23.93														
4.00	32.37	31.77	30.01	26.01	22.34	23.55														
2.00	32.65	31.99	30.02	25.70	22.07	23.15														
1.00	33.16	32.26	30.01	25.58	21.74	22.59														
.50	33.61	32.50	30.01	25.40	21.51	22.27														
.25	34.06	32.69	30.03	25.22	21.33	21.99														
-.12	34.40	33.20	31.31	27.98	26.27	24.66														
-.03	32.77	31.84	30.68	28.31	26.20	25.69														
-.06	26.98	27.30	27.28	26.95	26.16	25.07														
-.12	22.19	22.52	22.74	23.17	23.44	23.75														
-.25	20.31	20.38	20.32	20.32	20.38	20.65														
-.50	18.58	18.54	18.54	18.54	18.65	18.93														
-1.00																				
VAPOR PRESSURE (mb)																				
16.00	--	--	--	15.33	15.17	16.64														
8.00	--	--	--	15.38	15.17	16.46														
4.00	--	--	--	16.26	15.17	16.50														
2.00	--	--	--	15.74	15.12	16.43														
1.00	--	--	--	15.81	15.09	16.34														
.50	--	--	--	15.53	15.13	16.30														
.25	--	--	--	15.71	15.16	16.11														
.12	--	--	--	15.58	15.15	16.11														
WIND SPEED (cm/sec)																				
16.00	637	776	731	532	575	437														
8.00	600	706	635	410	474	398														
4.00	537	667	568	341	385	341														
2.00	487	--	--	278	330	288														
1.00	449	505	437	233	279	241														
.50	390	442	377	176	241	207														
.25	326	368	310	160	174	168														
WIND DIRECTION (deg)																				
1.00	190	180	170	180	200	250														
SOIL TEMPERATURE CHANGE (°C)																				
Initial Time	1657	1753	1850	2050	2252	2352														
Run Time (min)	20	13	27	27	33	25														
-.03	-.85	-.62	-.76	-.68	-.49	-.33														
-.06	-.35	-.38	-.48	-.58	-.43	-.31														
-.12	-.37	-.22	0	-.26	-.24	-.17														
-.25	-.04	.10	.12	.06	.07	0														
-.50	-.15	-.01	0	0	.07	.01														
-1.00	-.12	0	0	0	.01	-.01														

Precipitation (cm) -- -- -- -- --  
\* July 24, 1956

Table 8.2 (Continued)

HOURLY OBSERVATIONS							July 24, 1956							O'NEILL, NEBRASKA						
CST	0105	0205	0305	0405	0505	0605														
RADIATION (cal/cm <sup>2</sup> sec)																				
Insolation	--	--	--	--	.0001	.0013														
Reflected	--	--	--	--	.0000	.0003														
Net Radiation	-.0014	-.0017	-.0016	-.0017	-.0018	-.0008														
AIR and SOIL TEMPERATURES (°C)																				
Height (m)	24.34	22.55	20.96	19.83	19.64	18.74														
16.00	24.17	22.18	20.62	19.47	19.52	18.70														
8.00	23.98	21.93	20.35	19.27	19.41	18.68														
4.00	23.85	21.73	20.19	19.08	19.25	18.60														
2.00	23.65	21.47	19.96	18.95	19.13	18.50														
1.00	23.30	21.23	19.62	18.68	18.95	18.43														
.50	23.05	20.91	19.32	18.49	18.89	18.34														
.25	22.80	20.64	19.02	18.33	18.62	18.26														
.12	24.23	23.71	22.92	22.37	21.91	21.60														
-.03	25.04	24.56	24.02	23.50	23.00	22.64														
-.06	25.65	25.28	24.96	24.66	24.32	23.99														
-.12	23.76	23.75	23.70	23.70	23.62	23.52														
-.25	20.70	20.74	20.80	20.84	20.88	20.91														
-.50	18.93	18.92	18.93	18.94	18.94	18.95														
-1.00																				
VAPOR PRESSURE (mb)																				
16.00	18.43	17.77	17.97	18.23	18.32	17.99														
8.00	18.47	17.74	17.98	18.05	18.35	18.05														
4.00	18.44	17.70	17.97	18.09	18.42	18.03														
2.00	18.41	17.61	17.88	18.17	18.45	18.05														
1.00	18.36	17.57	18.01	18.19	18.51	18.07														
.50	18.36	17.57	18.07	18.21	18.56	18.12														
.25	18.31	17.48	18.09	18.23	18.61	18.13														
.12	18.31	17.43	18.14	18.25	18.71	18.11														
WIND SPEED (cm/sec)																				
16.00	669	605	530	637	642	584														
8.00	559	472	418	495	542	532														
4.00	487	415	371	435	483	505														
2.00	375	358	319	378	411	420														
1.00	321	307	270	328	378	380														
.50	294	287	229	287	330	336														
.25	246	222	197	244	281	289														
WIND DIRECTION (deg)																				
1.00	320	320	320	320	320	320														
SOIL TEMPERATURE CHANGE (°C)																				
Initial Time	0051	0157	0238	0350	0450	0651														
Run Time (min)	25	19	20	27	27	25														
-.03	-.12	-.26	-.31	-.20	-.12	-.11														
-.06	-.17	-.21	-.18	-.19	-.12	-.15														
-.12	-.15	-.13	-.11	-.11	-.10	-.14														
-.25	-.01	-.01	-.03	-.03	0	-.06														
-.50	.02	.03	.01	.03	.06	-.02														
-1.00	0	.01	0	0	.03	-.02														
Precipitation (cm)	--	--	--	--	--	--														

Table 8.2 (Continued)

HOURLY OBSERVATIONS							July 24, 1956							O'NEILL, NEBRASKA						
CST	0705	0805	0905	1005	1105	1205														
RADIATION (cal/cm <sup>2</sup> sec)																				
Insolation	.0048	.0095	.0143	.0182	.0212	.0225														
Reflected	.0012	.0022	.0030	.0035	.0039	.0041														
Net Radiation	.0015	.0051	.0094	.0115	.0133	.0144														
AIR and SOIL TEMPERATURES (°C)																				
Height (m)	19.75	21.48	22.78	24.58	25.64	26.77														
16.00	20.95	21.87	23.09	24.90	26.05	27.03														
8.00	20.05	22.13	23.56	25.26	26.60	27.87														
4.00	20.20	22.48	24.02	26.04	27.23	28.66														
2.00	20.35	22.73	24.56	26.91	28.16	29.74														
1.00	20.42	23.20	25.08	27.68	29.11	30.38														
.50	20.59	23.66	25.77	28.44	29.80	31.31														
.25	20.87	23.98	26.30	28.83	30.52	32.02														
.12	21.70	22.75	24.72	27.44	30.20	32.65														
-.03	22.38	22.66	23.47	24.84	26.57	28.38														
-.06	23.66	23.43	23.30	23.38	23.74	24.30														
-.12	23.37	23.29	23.16	23.04	22.90	22.85														
-.25	29.90	20.97	20.98	21.00	21.00	20.98														
-.50	18.94	18.96	18.95	18.84	18.87	18.85														
-1.00																				
VAPOR PRESSURE (mb)																				
16.00	17.96	18.21	17.91	18.33	15.96	12.24														
8.00	18.05	18.36	18.00	17.10	15.96	12.74														
4.00	18.00	18.34	18.04	17.15	16.12	12.74														
2.00	18.03	18.37	18.01	17.14	16.08	12.68														
1.00	18.09	18.43	18.07	17.25	16.19	12.70														
.50	18.13	18.48	18.19	17.39	16.23	12.71														
.25	18.12	18.48	18.21	17.48	16.20	12.83														
.12	18.21	18.57	18.30	17.68	16.17	12.88														
WIND SPEED (cm/sec)																				
16.00	843	905	929	959	974	918														
8.00	763	828	856	904	889	863														
4.00	708	719	723	756	745	765														
2.00	609	608	614	662	658	679														
1.00	552	532	540	585	585	613														
.50	501	475	492	537	538	569														
.25	426	412	416	455	455	502														
WIND DIRECTION (deg)																				
1.00	340	340	340	340	340	340														
SOIL TEMPERATURE CHANGE (°C)																				
Initial Time	0651	0750	0851	0951	1050	1150														
Run Time (min)	25	27	26	25	29	30														
-.03	.20	.70	.97	1.05	1.27	.88														
-.06	-.03	.29	.46	.61	.75	.74														
-.12	-.14	-.06	.03	.09	.21	.29														
-.25	-.06	-.02	-.04	-.05	-.05	-.04														
-.50	-.01	+.06	.02	0	0	-.01														
-1.00	-.01	.01	0	-.02	-.02	-.02														
Precipitation (cm)	--	--	--	--	--	--														

Table 8.2 (Continued)

HOURLY OBSERVATIONS							July 24, 1956							O'NEILL, NEBRASKA						
CST		1305	1405	1505	1605	1805	1905													
RADIATION (cal/cm <sup>2</sup> sec)																				
Insolation		.0222	.0208	.0183	.0150	.0063	.0019													
Reflected		.0041	.0039	.0034	.0030	.0017	--													
Net Radiation		.0142	.0127	.0109	.0080	.0014	-.0011													
AIR and SOIL TEMPERATURES (°C)																				
Height (m)		27.71	28.60	28.92	29.04	29.09	28.45													
16.00		28.11	28.83	29.39	29.63	29.19	28.51													
8.00		28.75	29.50	30.07	30.12	29.54	28.54													
4.00		29.93	30.08	30.74	30.83	29.82	28.56													
2.00		30.35	31.11	31.44	31.24	30.08	28.59													
1.00		31.32	32.05	32.17	31.84	30.36	28.60													
.50		32.54	32.94	33.08	32.42	30.72	28.65													
.25		33.36	33.77	33.98	33.26	31.17	28.63													
.12		34.60	35.12	35.74	35.43	33.54	31.58													
-.03		30.03	31.45	32.52	32.95	32.03	30.99													
-.06		24.98	25.77	26.47	27.17	28.04	28.08													
-.12		22.84	22.94	23.03	23.20	23.45	23.69													
-.25		20.98	21.03	21.01	20.99	20.87	20.85													
-.50		18.82	18.84	18.80	18.75	18.87	18.87													
-1.00																				
VAPOR PRESSURE (mb)																				
16.00		11.17	10.96	11.29	11.51	11.66	12.26													
8.00		11.82	11.65	11.89	11.88	11.61	12.38													
4.00		11.94	11.68	12.00	11.88	11.51	12.38													
2.00		11.66	11.65	11.76	11.84	11.45	12.36													
1.00		11.78	11.68	11.79	11.76	11.44	12.35													
.50		11.90	12.19	11.93	11.81	11.46	12.36													
.25		12.24	12.76	11.93	11.92	11.57	12.35													
.12		12.93	12.84	12.21	11.14	11.57	12.36													
WIND SPEED (cm/sec)																				
16.00		856	790	825	657	487	503													
8.00		793	797	745	588	433	427													
4.00		736	688	704	565	426	398													
2.00		657	611	618	501	376	359													
1.00		595	540	554	444	337	291													
.50		540	485	507	401	296	259													
.25		477	420	434	353	264	224													
WIND DIRECTION (deg)																				
1.00		340	340	--	--	--	--													
SOIL TEMPERATURE CHANGE (°C)																				
Initial Time		1250	1350	1450	1554	1752	1850													
Run Time (min)		27	27	26	27	25	25													
-.03		.64	.45	.01	-.43	-.63	-.93													
-.06		.74	.46	.30	.06	-.33	-.52													
-.12		.32	.30	.30	.28	.05	-.02													
-.50		.01	.02	.03	.09	.10	+0.06													
-1.00		-.01	0	-.02	0	.01	0													

Precipitation (cm) -- -- -- -- --

Table 8.2 (Continued)

HOURLY OBSERVATIONS							July 24, 1956							O'NEILL, NEBRASKA						
CST		2005	2105	2205	2305	0005*	0105*													
RADIATION (cal/cm <sup>2</sup> sec)																				
Insolation		.0002	--	--	--	--	--													
Reflected		--	--	--	--	--	--													
Net Radiation		-.0015	-.0012	-.0011	-.0010	-.0011	-.0009													
AIR and SOIL TEMPERATURES (°C)																				
Height (m)		27.19	26.40	25.42	23.66	22.44	21.26													
16.00		26.47	24.39	23.13	22.37	21.29	19.58													
8.00		25.28	22.98	21.83	20.73	19.43	17.15													
4.00		23.83	21.71	19.63	19.17	17.62	15.94													
2.00		22.94	20.23	17.27	16.31	16.54	14.54													
1.00		21.68	18.52	16.01	14.68	15.76	13.05													
.50		21.02	17.49	15.42	13.73	15.26	12.13													
.25		20.26	16.30	14.81	13.02	14.77	11.56													
-.03		20.13	26.72	25.05	23.70	22.64	21.70													
-.06		29.62	28.04	26.68	25.49	24.48	23.62													
-.12		27.94	27.63	27.21	26.69	26.14	--													
-.25		23.95	24.19	24.33	24.42	24.44	24.46													
-.50		20.95	21.05	21.08	21.10	21.15	21.24													
-1.00		18.91	18.95	19.00	19.04	19.08	19.16													
VAPOR PRESSURE (mb)																				
16.00		12.36	12.40	12.40	13.18	13.74	13.16													
8.00		12.28	12.64	12.46	13.18	13.58	12.89													
4.00		12.26	12.42	12.46	13.29	13.55	12.76													
2.00		12.22	12.28	12.38	13.25	13.56	12.71													
1.00		12.20	12.19	12.22	13.10	13.52	12.87													
.50		12.33	12.08	11.99	13.08	13.34	12.66													
.25		12.22	11.98	11.96	13.08	13.15	12.64													
.12		12.18	11.97	11.94	13.13	12.98	12.36													
WIND SPEED (cm/sec)																				
16.00		417	442	448	478	512	521													
8.00		317	270	387	395	414	378													
4.00		250	172	301	291	302	230													
2.00		146	115	216	217	202	178													
1.00		65	69	130	126	137	116													
.50		36	21	79	69	92	48													
.25		26	18	27	16	45	16													
WIND DIRECTION (deg)																				
1.00		--	--	--	--	--	180													
SOIL TEMPERATURE CHANGE (°C)																				
Initial Time		1951	2052	2150	2250	2353	0053													
Run Time (min)		26	25	27	27	25	31													
-.03		-1.19	-.83	-.66	-.57	-.34	-.49													
-.06		-.73	-.64	-.57	-.50	-.39	-.47													
-.12		-.19	-.16	-.20	-.28	-.22	--													
-.25		.17	.04	.05	-.01	-.01	-.11													
-.50		.11	-.01	.03	0	0	-.03													
-1.00		0	.01	.02	-.01	.02	.02													

Precipitation (cm) -- -- -- -- --

\* July 25, 1956

Table 8.2 (Continued)

HOURLY OBSERVATIONS July 25, 1956 O'NEILL, NEBRASKA							
CST	0205	0305	0405	0505	0605	0705	
RADIATION (cal/cm <sup>2</sup> sec)							
Insolation	--	--	--	.0000	.0017	.0057	
Reflected	--	--	--	.0000	.0006	.0016	
Net Radiation	-.0009	-.0008	-.0012	-.0011	-.0004	.0022	
AIR and SOIL TEMPERATURES (°C)							
Height (m)	20.05	18.35	18.15	17.65	17.14	19.22	
16.00	18.51	15.34	16.34	15.56	16.67	19.40	
8.00	15.78	14.13	15.07	14.04	16.52	19.56	
4.00	14.60	13.73	14.47	13.25	16.41	19.75	
2.00	13.61	13.38	14.00	12.86	16.36	20.09	
1.00	12.56	11.91	13.66	12.45	16.27	20.33	
.50	11.77	10.73	13.34	12.13	16.24	20.69	
.25	11.04	9.86	13.01	11.89	16.19	20.87	
-.03	21.24	19.94	19.47	19.21	18.99	19.82	
-.06	22.78	22.04	21.40	20.90	20.31	20.84	
-.12	25.06	24.56	24.07	23.60	23.14	22.82	
-.25	24.30	24.18	24.06	23.90	23.69	23.57	
-.50	21.24	21.26	21.30	21.29	21.32	21.34	
-1.00	19.15	19.16	19.18	19.16	19.08	19.09	
VAPOR PRESSURE (mb)							
16.00	13.27	13.13	--	--	--	14.65	
8.00	12.33	12.01	--	--	--	14.87	
4.00	12.23	11.95	--	--	--	14.79	
2.00	12.20	11.82	--	--	--	14.86	
1.00	12.28	11.79	--	--	--	14.87	
.50	12.30	11.83	--	--	--	14.92	
.25	12.36	11.89	--	--	--	14.98	
-.12	12.63	12.27	--	--	--	15.05	
WIND SPEED (cm/sec)							
16.00	521	458	559	538	646	521	
8.00	398	217	442	414	514	512	
4.00	229	118	301	297	426	466	
2.00	153	79	230	191	365	429	
1.00	95	55	174	137	322	390	
.50	32	45	140	97	279	335	
.25	16	16	94	55	220	271	
WIND DIRECTION (deg)							
1.00	180	180	190	190	180	190	
SOIL TEMPERATURE CHANGE (°C)							
Initial Time	0152	0252	0352	0453	0550	0650	
Run Time (min)	32	24	24	24	28	26	
-.03	-.51	-.25	-.06	-.14	.11	+5.6	
-.06	-.43	-.32	-.12	-.17	-.58	-.12	
-.12	-.30	-.21	-.22	-.14	-.16	-.18	
-.25	-.05	-.07	-.05	-.01	-.06	-.10	
-.50	.01	-.01	.03	.0	.03	-.01	
-1.00	0	0	.03	.01	0	-.01	
Precipitation (cm)	--	--	--	--	--	--	

Table 8.2 (Continued)

HOURLY OBSERVATIONS July 25, 1956 O'NEILL, NEBRASKA							
CST	0805	0905	1005	1205	1405	1505	
RADIATION (cal/cm <sup>2</sup> sec)							
Insolation	.0085	.0055	(.0126)	.0230	.0203	.0180	
Reflected	.0020	.0012	.0025	.0044	.0038	.0033	
Net Radiation	.0042	.0023	.0069	.0142	.0128	.0108	
AIR and SOIL TEMPERATURES (°C)							
Height (m)	21.95	23.96	25.37	28.91	31.40	32.63	
16.00	22.27	24.25	25.82	29.72	32.15	33.35	
8.00	22.68	24.39	26.27	30.44	32.87	34.01	
4.00	22.96	24.64	26.90	31.13	33.63	34.70	
2.00	23.17	24.83	27.43	31.75	34.40	35.31	
1.00	23.64	24.95	27.98	32.80	35.18	35.80	
.50	24.06	25.17	28.55	34.06	36.07	36.55	
.25	24.27	25.35	28.81	34.96	36.82	37.35	
-.03	21.41	23.58	25.58	31.46	35.05	35.69	
-.06	21.19	22.30	23.38	26.50	30.32	31.22	
-.12	22.52	22.44	22.57	23.24	24.66	25.58	
-.25	23.31	23.09	22.91	22.62	22.56	22.60	
-.50	21.31	21.27	21.85	21.15	21.11	21.02	
-1.00	19.05	19.01	19.02	18.97	18.92	18.89	
VAPOR PRESSURE (mb)							
16.00	14.69	15.09	15.20	13.22	13.75	13.28	
8.00	14.79	15.23	15.37	13.68	13.95	13.44	
4.00	14.83	15.24	15.38	13.76	13.99	13.48	
2.00	14.89	15.32	15.42	13.97	14.05	13.54	
1.00	14.89	15.38	15.48	14.04	14.11	13.58	
.50	14.96	15.46	15.51	14.30	14.17	13.64	
.25	15.00	15.47	15.60	14.38	14.21	13.67	
-.12	15.09	15.50	15.73	14.57	14.30	13.70	
WIND SPEED (cm/sec)							
16.00	786	819	776	1053	1289	1135	
8.00	717	753	--	1009	1217	1103	
4.00	652	684	662	878	1073	994	
2.00	547	524	518	841	975	901	
1.00	522	550	545	732	864	785	
.50	460	474	--	648	749	688	
.25	375	388	393	534	614	563	
WIND DIRECTION (deg)							
1.00	180	180	170	160	165	180	
SOIL TEMPERATURE CHANGE (°C)							
Initial Time	0750	0854	0951	1151	1350	1450	
Run Time (min)	26	24	28	27	28	26	
-.03	-.73	.45	.90	1.03	.78	.02	
-.06	-.30	.52	.63	.75	.58	.27	
-.12	-.13	.02	.07	.21	.33	.31	
-.25	-.11	-.08	-.09	-.05	.01	.05	
-.50	-.02	0	-.01	-.02	-.02	0	
-1.00	-.04	.02	-.01	-.02	0	0	
Precipitation (cm)	--	--	--	--	--	--	

Table 8.2 (Continued)

HOURLY OBSERVATIONS							July 25, 1956							O'NEILL, NEBRASKA						
CST		1605	1705	1805	1905	2005	2105													
RADIATION (cal/cm <sup>2</sup> sec)																				
Insolation	.0145	.0090	.0045	.0011	.0001	--	--													
Reflected	.0028	.0020	.0010	--	--	--	--													
Net Radiation	.0080	.0040	.0006	-.0015	-.0017	-.0011														
AIR and SOIL TEMPERATURES (°C)																				
Height (m)																				
16.00	32.66	33.42	33.14	31.97	29.63	28.91														
8.00	33.32	33.68	33.26	31.87	29.52	28.86														
4.00	33.79	34.01	33.36	31.79	29.42	28.76														
2.00	34.45	34.38	33.40	31.68	29.21	28.68														
1.00	34.96	34.72	33.49	31.61	29.03	28.62														
.50	35.40	35.02	33.56	31.50	28.85	28.52														
.25	36.17	35.34	33.62	31.38	28.66	28.34														
.12	36.78	35.62	33.68	31.28	28.50	28.25														
-.03	35.28	34.46	32.69	31.28	29.64	28.34														
-.06	31.64	31.71	31.10	30.26	29.30	28.28														
-.12	26.22	26.84	27.14	27.22	27.18	26.96														
-.25	22.70	22.99	23.17	23.37	23.60	23.78														
-.50	20.98	21.06	21.04	21.04	21.06	21.10														
-1.00	18.88	18.99	18.98	18.98	19.01	19.04														
VAPOR PRESSURE (mb)																				
16.00	14.01	13.05	13.13	13.80	14.37	14.51														
8.00	14.20	13.12	13.27	13.94	14.43	14.61														
4.00	14.24	13.21	13.26	13.85	14.49	14.60														
2.00	14.31	13.26	13.28	13.94	14.58	14.53														
1.00	14.39	13.29	13.35	13.66	14.48	14.62														
.50	14.39	13.33	13.32	13.97	14.45	14.59														
.25	14.42	13.40	13.32	13.94	14.49	14.59														
.12	14.49	13.46	13.33	13.84	14.39	14.59														
WIND SPEED (cm/sec)																				
16.00	1260	1236	1174	948	920	972														
8.00	1179	1193	1073	821	803	863														
4.00	1046	1044	944	727	714	770														
2.00	955	959	853	650	614	663														
1.00	830	826	744	565	541	587														
.50	722	789	652	490	475	520														
-.25	591	588	534	405	386	419														
WIND DIRECTION (deg)																				
1.00	170	180	170	160	160	160														
SOIL TEMPERATURE CHANGE (°C)																				
Initial Time	1550	1650	1752	1851	1951	2053														
Run Time (min)	26	26	24	25	26	27														
-.03	-.12	-.63	-.74	-.74	-.50	-.30														
-.04	.03	-.12	-.33	-.32	-.39	-.31														
-.12	.26	-.13	.09	+.02	-.05	-.07														
-.25	+.07	+.10	.10	.08	.10	.07														
-.50	-.02	-.02	.01	0	.04	.01														
-1.00	-.01	0	.03	.02	.04	0														

Precipitation (cm) -- -- -- -- --

Table 8.2 (Continued)

HOURLY OBSERVATIONS							July 25, 1956							O'NEILL, NEBRASKA						
CST		2305	0005*	0205*	0305*	0405*	0505*													
RADIATION (cal/cm <sup>2</sup> sec)																				
Insolation	--	--	--	--	--	--	.0000													
Reflected	--	--	--	--	--	--	.0000													
Net Radiation	-.0014	-.0014	-.0009	-.0012	-.0011	-.0007														
AIR and SOIL TEMPERATURES (°C)																				
Height (m)																				
16.00	27.72	26.75	26.37	25.65	25.07	24.02														
8.00	27.63	26.70	26.38	25.56	24.83	23.48														
4.00	27.51	26.60	26.34	25.30	24.63	22.79														
2.00	27.43	26.42	26.23	25.16	24.45	22.03														
1.00	27.35	26.32	26.16	24.89	24.20	21.31														
.50	27.23	26.22	26.09	24.69	24.07	20.65														
.25	27.11	26.05	26.00	24.42	23.94	20.27														
.12	27.03	25.93	25.91	24.25	23.78	20.02														
-.03	27.16	26.32	25.44	25.26	24.75	24.02														
-.06	27.14	26.57	25.69	25.44	25.09	24.67														
-.12	26.46	26.11	25.78	25.48	25.26	25.07														
-.25	23.98	24.06	24.17	24.15	24.10	24.05														
-.50	21.14	21.17	21.33	21.34	21.37	21.42														
-1.00	19.05	19.08	19.19	19.19	19.20	19.21														
VAPOR PRESSURE (mb)																				
16.00	15.29	15.81	17.73	15.75	15.38	14.55														
8.00	15.23	15.87	17.75	15.84	15.48	14.99														
4.00	15.24	15.81	17.75	15.88	15.46	15.05														
2.00	15.28	15.82	17.73	15.87	15.50	15.16														
1.00	15.31	15.80	17.73	15.88	15.48	15.16														
.50	15.22	15.81	17.75	15.98	15.54	15.18														
.25	15.26	15.77	17.77	15.92	15.48	15.13														
.12	15.28	15.75	17.84	15.97	15.60	15.18														
WIND SPEED (cm/sec)																				
16.00	1084	1041	968	591	607	341														
8.00	931	933	954	527	550	287														
4.00	864	814	853	432	457	238														
2.00	724	739	757	400	411	191														
1.00	636	639	655	342	351	150														
.50	561	557	576	295	299	120														
-.25	463	454	469	236	242	72														
WIND DIRECTION (deg)																				
1.00	150	170	190	215	210	250														
SOIL TEMPERATURE CHANGE (°C)																				
Initial Time	2253	2350	0150	0250	0350	0450														
Run Time (min)	23	26	26	26	25	26														
-.03	-.23	-.24	.01	-.27	-.17	-.38														
-.06	-.18	-.11	-.13	-.14	-.13	-.20														
-.12	-.11	-.11	.01	-.12	-.06	-.08														
-.25	.02	.05	.03	-.04	-.01	-.02														
-.50	0	0	.01	0	0	0														
-1.00	.02	.01	0	0	-.01	0														

Precipitation (cm) -- -- -- -- --  
\* July 26, 1956



Table 8.2 (Continued)

HOURLY OBSERVATIONS July 26, 1956 O'NEILL, NEBRASKA						
CST	0605	0705	0805	0905	1005	1805*
RADIATION (cal/cm <sup>2</sup> sec)						
Insolation	.0016	.0050	.0060	.0150	.0155	.0035
Reflected	.0006	.0013	.0013	.0030	.0030	--
Net Radiation	-.0002	.0019	.0027	.0080	.0090	.0009
AIR and SOIL TEMPERATURES (°C)						
Height (m)	23.44	24.78	26.74	29.84	32.45	29.29
16.00	22.52	24.90	26.85	30.07	32.68	29.35
8.00	21.78	25.10	26.98	30.26	33.21	29.38
4.00	21.23	25.28	27.19	30.83	33.63	29.35
2.00	20.93	25.45	27.57	31.42	34.18	29.38
1.00	20.74	25.74	27.93	32.10	34.98	29.40
.50	20.78	25.99	28.25	33.08	35.00	29.42
.25	20.78	26.22	28.57	33.81	36.82	29.46
.12	23.41	23.71	24.76	26.58	30.15	28.71
-.03	24.21	23.96	24.24	24.89	26.68	28.68
-.06	24.88	24.62	24.38	24.26	24.29	26.38
-.12	24.03	23.94	23.83	23.70	23.54	23.76
-.25	21.45	21.45	21.44	21.42	21.36	22.06
-.50	19.21	19.21	19.20	19.19	19.15	19.91
-.100						
VAPOR PRESSURE (mb)						
16.00	15.05	14.49	14.39	13.88	13.38	14.34
8.00	15.27	14.55	14.45	14.02	13.57	14.89
4.00	15.38	14.59	14.50	14.04	13.56	15.07
2.00	15.50	14.63	14.66	14.11	13.63	15.21
1.00	15.54	14.67	14.77	14.21	13.77	15.44
.50	15.58	14.72	14.89	14.37	14.09	15.58
.25	15.62	14.79	15.01	14.68	14.22	15.71
.12	15.73	14.96	15.26	15.16	14.33	15.76
WIND SPEED (cm/sec)						
16.00	306	364	311	430	319	726
8.00	264	372	320	415	328	680
4.00	212	346	301	374	308	612
2.00	179	324	281	371	277	537
1.00	146	287	248	331	253	471
.50	121	272	180	296	234	411
.25	86	206	174	246	198	332
WIND DIRECTION (deg)						
1.00	180	210	200	235	320	160
SOIL TEMPERATURE CHANGE (°C)						
Initial Time	0550	0650	0750	0852	0952	1750
Run Time (min)	25	28	28	24	26	27
-.03	-.24	.46	.49	1.20	1.46	-.74
-.06	-.20	.05	.17	.40	.85	-.43
-.12	-.10	-.15	-.08	-.02	.06	.05
-.25	-.01	-.04	-.04	-.05	-.05	.05
-.50	0	0	0	-.03	-.03	-.01
-.100	0	0	0	0	0	00

Precipitation (cm) -- -- -- -- --  
\* August 6, 1956

Table 8.2 (Continued)

HOURLY OBSERVATIONS August 6, 1956 O'NEILL, NEBRASKA						
CST	1905	2105	2205	2305	0005*	0305*
RADIATION (cal/cm <sup>2</sup> sec)						
Insolation	.0015	--	--	--	--	--
Reflected	--	--	--	--	--	--
Net Radiation	.0007	-.0012	-.0011	rain	-.0007	-.0013
AIR and SOIL TEMPERATURES (°C)						
Height (m)	28.18	24.70	22.25	21.67	21.06	17.54
16.00	28.00	23.67	22.10	21.63	21.05	17.61
8.00	27.94	22.85	21.99	21.58	21.09	17.61
4.00	27.78	22.44	21.87	21.53	21.03	17.58
2.00	27.56	21.97	21.77	21.44	21.02	17.54
1.00	27.42	21.54	21.59	21.34	20.96	17.50
.50	27.25	21.25	21.45	21.26	20.90	17.47
.25	27.14	21.01	21.28	21.20	20.88	17.46
.12	27.12	23.88	22.96	22.84	22.71	20.57
-.03	27.64	25.22	24.90	23.80	23.52	21.86
-.06	26.38	25.86	25.49	25.13	24.70	23.73
-.12	26.39	24.07	24.15	24.22	24.18	23.83
-.25	22.06	22.06	22.11	22.16	22.06	22.06
-.50	19.93	19.96	20.00	20.11	20.02	20.01
-.100						
VAPOR PRESSURE (mb)						
16.00	13.47	15.06	22.93	rain	rain	20.27
8.00	13.85	15.54	22.55	rain	rain	19.59
4.00	14.02	15.90	22.58	rain	rain	19.59
2.00	14.14	16.11	22.51	rain	rain	19.51
1.00	14.24	16.31	22.45	rain	rain	19.50
.50	14.32	16.42	22.45	rain	rain	19.59
.25	14.38	16.52	22.33	rain	rain	19.27
.12	14.45	16.58	22.39	rain	rain	19.63
WIND SPEED (cm/sec)						
16.00	630	492	651	549	779	780
8.00	528	387	544	457	697	700
4.00	464	308	498	425	660	638
2.00	404	244	437	374	565	574
1.00	354	196	386	327	491	--
.50	305	166	337	286	428	437
.25	247	131	281	235	360	371
WIND DIRECTION (deg)						
1.00	165	80	50	75	50	
SOIL TEMPERATURE CHANGE (°C)						
Initial Time	1850	2050	2150	2250	2350	0250
Run Time (min)	27	28	27	27	26	26
-.03	-.65	-.50	-.31	-.04	.11	-.29
-.06	-.45	-.46	-.41	-.14	.00	-.29
-.12	-.05	-.14	-.22	-.18	-.14	-.19
-.25	-.04	.06	.00	-.01	.06	-.14
-.50	-.01	.02	.00	.00	.09	-.06
-.100	00	.03	+.03	.02	00	-.02

Precipitation (cm) -- -- -- -- --

\* August 7, 1956

Table 8.2 (Continued)

HOURLY OBSERVATIONS								August 7, 1956				O'NEILL, NEBRASKA			
CST	0405	0505	0605	0705	0805	0905									
RADIATION (cal/cm <sup>2</sup> sec)															
Insolation	--	.0000	.0005	.0048	.0092	.0125									
Reflected	--	--	--	--	--	--									
Net Radiation	-.0014	-.0012	-.0009	.0019	.0055	.0068									
AIR and SOIL TEMPERATURES (°C)															
Height (m)	17.76	17.19	16.82	18.28	20.67	22.60									
16.00	17.83	17.11	16.70	18.41	20.96	22.93									
8.00	17.75	17.00	16.57	18.55	21.22	23.15									
4.00	17.69	16.90	16.45	18.66	21.49	23.41									
2.00	17.62	16.80	16.37	18.75	21.73	23.74									
1.00	17.51	16.69	16.24	18.84	22.03	23.96									
.50	17.40	16.57	16.18	18.98	22.34	24.25									
.25	17.57	16.53	16.13	19.08	22.70	24.57									
.12	20.17	19.51	19.92	19.04	20.14	21.64									
-.03	21.41	20.91	20.38	20.09	20.41	21.31									
-.06	23.40	23.09	22.75	22.41	22.16	22.06									
-.12	23.75	23.67	23.56	23.42	23.28	23.13									
-.25	22.06	22.10	22.08	22.06	22.04	22.04									
-.50	20.03	20.03	20.04	20.02	20.01	20.00									
-1.00															
VAPOR PRESSURE (mb)															
16.00	18.64	17.60	17.43	17.86	17.75	18.07									
8.00	18.62	17.53	18.02	18.14	18.11	18.19									
4.00	18.56	17.53	18.13	18.23	18.23	18.32									
2.00	18.64	17.56	18.08	18.37	18.42	18.49									
1.00	18.67	17.61	18.07	18.56	18.61	18.66									
.50	18.75	17.72	18.06	18.77	18.94	18.91									
.25	18.76	17.75	17.98	19.12	19.22	19.25									
.12	19.02	17.94	17.82	19.21	19.52	19.47									
WIND SPEED (cm/sec)															
16.00	698	623	589	583	694	1218									
8.00	617	553	509	535	660	1134									
4.00	577	511	455	512	606	1040									
2.00	498	436	385	456	542	915									
1.00	439	--	--	431	500	835									
.50	410	331	289	370	420	693									
.25	319	279	242	299	349	603									
WIND DIRECTION (deg)															
1.00	75	85	85	50	110	140									
SOIL TEMPERATURE CHANGE (°C)															
Initial Time	0355	0450	0551	0652	0751	0851									
Run Time (min)	21	26	25	24	25	25									
-.03	-.30	-.14	-.06	.18	.72	.51									
-.06	-.19	.78	-.08	-.05	.27	.41									
-.12	-.11	-.13	-.07	-.11	-.05	00									
-.25	00	-.06	-.01	-.05	-.04	-.06									
-.50	.01	.01	.04	-.02	.02	-.02									
-1.00	.01	00	.10	-.04	.03	-.03									
Precipitation (cm)	--	--	--	--	--	--									

Table 8.2 (Continued)

HOURLY OBSERVATIONS								August 7, 1956				O'NEILL, NEBRASKA			
CST	1005	1105	1205	1405	1605	1705									
RADIATION (cal/cm <sup>2</sup> sec)															
Insolation	.0145	.0192	.0150	.0199	.0150	.0097									
Reflected	--	--	--	--	--	--									
Net Radiation	.0102	.0130	.0110	.0135	.0103	.0054									
AIR and SOIL TEMPERATURES (°C)															
Height (m)	23.95	25.97	27.47	27.74	29.83	28.58									
16.00	24.24	26.34	27.89	28.38	30.26	28.86									
8.00	24.58	26.82	28.34	28.92	30.52	29.23									
4.00	24.94	27.49	28.66	29.37	31.00	29.62									
2.00	25.32	28.24	29.27	29.93	31.36	29.85									
1.00	25.83	28.77	29.84	30.78	31.85	30.46									
.50	26.39	29.25	30.39	31.62	32.47	30.73									
.25	26.67	30.30	30.89	32.02	32.90	31.15									
.12	23.09	25.80	27.62	30.24	31.12	30.65									
-.03	21.71	23.80	25.54	28.18	29.48	29.53									
-.06	22.13	22.32	22.81	24.24	25.52	25.97									
-.12	22.94	22.76	22.70	22.68	22.96	23.12									
-.25	21.99	21.92	21.92	21.86	21.88	21.87									
-.50	19.98	19.92	19.96	19.94	19.98	19.98									
-1.00															
VAPOR PRESSURE (mb)															
16.00	18.48	17.77	18.80	17.42	17.12	19.50									
8.00	18.97	18.17	19.14	17.80	17.38	19.82									
4.00	19.10	18.19	19.13	17.97	17.54	20.02									
2.00	19.42	18.34	19.25	18.12	17.69	20.16									
1.00	19.62	18.63	19.64	18.29	17.85	20.27									
.50	19.96	18.91	19.79	18.59	18.02	20.44									
.25	20.33	19.36	20.14	18.79	18.24	20.60									
.12	20.59	19.65	20.64	18.97	18.46	20.87									
WIND SPEED (cm/sec)															
16.00	991	838	665	1348	1379	902									
8.00	874	754	773	1251	1290	923									
4.00	878	707	718	1135	1165	841									
2.00	764	609	651	1004	1025	739									
1.00	710	554	595	908	923	669									
.50	404	470	500	768	773	500									
.25	340	385	405	640	630	464									
WIND DIRECTION (deg)															
1.00	145	155	175	155	150	155									
SOIL TEMPERATURE CHANGE (°C)															
Initial Time	0952	1052	1150	1350	1550	1650									
Run Time (min)	24	25	27	27	26	28									
-.03	-.61	1.00	.61	.43	-.19	-.38									
-.06	1.41	.79	.54	.27	.07	-.04									
-.12	.07	.13	.24	.36	.21	.18									
-.25	-.05	-.08	-.07	.02	.07	.11									
-.50	-.02	-.03	-.04	.00	.01	.04									
-1.00	.01	-.03	-.04	.01	.01	.04									
Precipitation (cm)	--	--	--	--	--	--									

Table 8.2 (Continued)

HOURLY OBSERVATIONS August 7, 1956 O'NEILL, NEBRASKA						
CST	1805	1905	2005	2105	2205	0005*
RADIATION (cal/cm <sup>2</sup> sec)						
Insolation	.0050	.0009	.0000	--	--	--
Reflected	--	--	--	--	--	--
Net Radiation	.0023	-.0009	-.0012	-.0010	-.0008	-.0014
AIR and SOIL TEMPERATURES (°C)						
Height (m)						
16.00	28.29	27.08	25.79	24.96	23.91	22.78
8.00	28.50	27.03	25.46	24.29	23.56	22.62
4.00	28.62	26.95	25.13	23.70	23.12	22.48
2.00	28.77	26.84	24.96	23.25	22.62	22.27
1.00	28.93	26.77	24.77	22.97	22.52	22.19
.50	29.12	26.65	24.57	22.59	22.17	22.03
.25	29.31	26.34	24.38	22.43	22.02	21.87
.12	29.50	26.48	24.22	22.33	21.88	21.75
-.03	29.33	27.82	26.28	25.11	24.15	22.98
-.06	28.96	28.09	27.02	26.02	25.16	23.94
-.12	26.23	26.29	26.19	25.93	25.59	24.89
-.25	23.30	23.50	23.64	23.80	23.90	23.96
-.50	21.85	21.89	21.86	21.90	21.91	21.93
-1.00	20.00	20.04	20.05	20.06	20.08	20.10
VAPOR PRESSURE (mb)						
16.00	19.62	19.84	19.31	19.89	19.75	18.42
8.00	19.77	20.00	19.50	20.01	20.06	18.59
4.00	19.94	20.01	19.60	20.12	20.25	18.60
2.00	19.89	20.10	19.62	20.11	20.26	18.62
1.00	20.02	20.13	19.64	20.13	20.27	18.66
.50	20.11	20.22	19.75	20.21	20.39	18.74
.25	20.22	20.22	19.76	20.14	20.36	18.74
.12	20.27	20.31	19.87	20.22	20.39	18.78
WIND SPEED (cm/sec)						
16.00	714	697	632	440	378	932
8.00	668	634	521	349	298	833
4.00	615	554	439	267	239	745
2.00	544	491	376	214	191	632
1.00	500	447	342	177	163	589
.50	423	378	280	139	128	491
.25	350	314	232	102	92	399
WIND DIRECTION (deg)						
1.00	145	135	145	105	75	150
SOIL TEMPERATURE CHANGE (°C)						
Initial Time	1750	1850	1950	2050	2155	2353
Run Time (min)	26	26	26	26	21	23
-.03	-47	-56	-53	-44	-28	-22
-.06	-31	-42	-42	-40	-31	-18
-.12	.07	-02	-09	-17	-15	-11
-.25	.08	.09	-.03	.06	.04	-.01
-.50	.02	00	-.09	00	00	-.02
-1.00	00	00	-.01	00	-.01	-.01

Precipitation (cm) -- -- -- -- --

\*August 8, 1956

Table 8.2 (Continued)

HOURLY OBSERVATIONS August 8, 1957 O'NEILL, NEBRASKA						
CST	0105	0205	0305	0405	0505	0605
RADIATION (cal/cm <sup>2</sup> sec)						
Insolation	--	--	--	--	.0000	.0005
Reflected	--	--	--	--	--	--
Net Radiation	-.0015	-.0007	-.0014	-.0015	-.0011	-.0004
AIR and SOIL TEMPERATURES (°C)						
Height (m)						
16.00	23.12	18.76	17.77	17.15	16.51	17.17
8.00	22.89	18.83	17.58	16.70	16.11	17.11
4.00	22.58	18.85	17.41	16.45	15.81	17.05
2.00	22.33	18.86	17.30	16.21	15.57	16.95
1.00	22.07	18.86	17.17	16.00	15.44	16.89
.50	21.73	18.85	17.00	15.77	15.22	16.81
.25	21.41	18.83	16.86	15.60	15.12	16.73
.12	21.20	18.82	16.77	15.43	15.02	16.65
-.03	22.37	21.89	21.08	20.12	19.16	19.10
-.06	23.52	22.96	22.43	21.75	21.00	20.48
-.12	24.74	24.34	24.02	23.70	23.29	22.84
-.25	23.94	23.87	23.81	23.73	23.62	23.44
-.50	21.95	21.95	21.95	21.96	21.95	21.90
-1.00	20.10	20.09	20.08	20.08	20.06	20.04
VAPOR PRESSURE (mb)						
16.00	17.30	15.20	15.21	15.21	15.71	16.40
8.00	17.43	15.29	15.25	14.89	15.52	16.42
4.00	17.51	15.30	15.30	14.95	15.54	16.49
2.00	17.59	15.31	15.31	14.99	15.52	16.62
1.00	17.59	15.32	15.31	15.01	15.55	16.71
.50	17.68	15.34	15.34	15.06	15.57	16.72
.25	17.74	15.35	15.36	15.06	15.58	16.76
.12	17.75	15.36	15.36	15.15	15.75	16.77
WIND SPEED (cm/sec)						
16.00	479	1190	547	532	470	558
8.00	438	997	451	445	377	494
4.00	395	815	397	375	310	440
2.00	340	812	344	311	255	379
1.00	313	729	311	283	229	349
.50	255	633	256	233	186	294
.25	214	533	201	191	142	238
WIND DIRECTION (deg)						
1.00	265	360	50	85	95	110
SOIL TEMPERATURE CHANGE (°C)						
Initial Time	0053	0154	0253	0351	0454	0550
Run Time (min)	23	22	23	25	21	27
-.03	-30	-28	-28	-37	-24	-01
-.06	-20	-17	-24	-31	-21	-16
-.12	-21	-14	-12	-15	-13	-16
-.25	-.02	-.04	-.03	-.05	-.04	-.05
-.50	00	01	00	-.01	00	-.01
-1.00	00	00	-.01	-.01	00	-.01

Precipitation (cm) -- -- -- -- --

Table 8.2 (Continued)

HOURLY OBSERVATIONS								August 8, 1956						O'NEILL, NEBRASKA					
CST	0805	0905	1005	1105	1205	1305													
RADIATION (cal/cm <sup>2</sup> sec)																			
Insolation	.0030	.0139	.0179	.0190	.0220	.0218													
Reflected	--	--	--	--	--	--													
Net Radiation	wet	.0088	.0113	.0110	.0150	.0150													
AIR and SOIL TEMPERATURES (°C)																			
Height (m)																			
16.00	18.00	20.84	23.76	25.28	26.74	27.54													
8.00	17.94	21.20	23.79	25.52	27.23	27.76													
4.00	17.96	21.45	24.17	25.60	27.74	28.13													
2.00	17.97	21.93	24.46	26.12	28.01	28.70													
1.00	17.97	22.19	25.09	26.63	28.61	29.70													
.50	17.97	22.62	25.88	27.52	29.64	30.74													
.25	17.98	23.07	26.85	28.33	30.83	31.41													
.12	17.95	23.55	27.68	29.97	31.67	32.71													
-03	19.30	20.78	24.27	27.44	29.85	31.89													
-06	20.19	20.56	21.76	24.62	26.71	28.46													
-12	22.22	22.00	21.94	22.38	23.06	23.93													
-25	23.18	22.98	22.82	22.75	22.41	22.61													
-50	21.90	21.88	21.82	21.87	21.87	21.83													
-100	20.04	20.02	19.99	20.04	20.06	20.05													
VAPOR PRESSURE (mb)																			
16.00	--	14.04	14.74	13.28	12.96	13.16													
8.00	--	14.41	15.05	13.55	13.42	13.83													
4.00	--	14.55	15.26	13.74	13.62	14.03													
2.00	--	14.83	15.35	13.85	13.85	14.18													
1.00	--	14.95	15.58	14.18	14.04	14.40													
.50	--	15.91	15.96	14.66	14.67	14.69													
.25	--	16.13	16.46	15.16	15.17	15.08													
.12	--	16.83	17.16	15.64	15.72	15.61													
WIND SPEED (cm/sec)																			
16.00	511	489	368	530	493	531													
8.00	440	466	349	505	487	541													
4.00	385	444	321	473	446	487													
2.00	314	409	298	436	413	452													
1.00	287	385	290	408	391	420													
.50	250	320	245	344	178	--													
.25	212	270	210	317	60	--													
WIND DIRECTION (deg)																			
1.00	330	45	5	40	110	150													
SOIL TEMPERATURE CHANGE (°C)																			
Initial Time	0750	0850	0950	1050	1155	1250													
Run Time (min)	28	27	28	28	21	26													
-03	-16	1.32	1.68	1.00	.83	.71													
-06	-02	.29	.06	1.01	.70	.70													
-12	-13	-.09	.06	.26	.34	.34													
-25	-.07	-.16	-.09	.04	-.55	.00													
-50	-.01	-.03	-.01	.02	-.02	-.03													
-100	-.01	-.01	-.02	.03	-.02	-.04													
Precipitation (cm)	--	--	--	--	--	--													

Table 8.2 (Continued)

HOURLY OBSERVATIONS								August 9, 1956						O'NEILL, NEBRASKA					
CST	1405	1505	1605	1705	1805	1905													
RADIATION (cal/cm <sup>2</sup> sec)																			
Insolation	.0200	.0178	.0138	.0082	.0052	.0012													
Reflected	--	.0033	.0029	.0018	.0013	--													
Net Radiation	.0133	.0110	.0077	.0041	.0018	-.0011													
AIR and SOIL TEMPERATURES (°C)																			
Height (m)																			
16.00	28.02	28.86	28.48	27.91	27.14	25.66													
8.00	28.44	29.37	29.00	28.28	27.35	25.69													
4.00	28.79	29.76	29.60	28.58	27.58	25.67													
2.00	29.28	30.31	30.04	28.90	27.80	25.66													
1.00	29.92	30.69	30.43	29.26	28.03	25.65													
.50	31.31	31.40	30.99	29.65	28.19	25.63													
.25	32.09	32.54	31.77	30.03	28.39	25.62													
.12	33.48	33.55	32.25	30.43	28.68	25.58													
-03	33.29	34.46	34.48	32.81	30.98	29.02													
-06	29.97	31.25	31.98	31.63	30.78	29.49													
-12	24.80	25.65	26.43	27.16	27.55	27.54													
-25	22.58	22.74	22.91	23.11	23.44	23.71													
-50	21.79	21.76	21.72	21.69	21.75	21.76													
-100	20.01	19.96	19.94	19.93	20.00	20.03													
VAPOR PRESSURE (mb)																			
16.00	12.79	13.58	15.40	17.08	17.40	17.51													
8.00	13.46	13.48	15.89	17.31	17.65	17.52													
4.00	13.66	13.57	15.95	17.39	17.73	17.52													
2.00	13.76	13.65	15.95	17.39	17.77	17.51													
1.00	14.04	13.85	16.98	17.43	17.64	17.53													
.50	14.50	14.20	16.40	17.58	17.92	17.57													
.25	14.89	14.47	16.66	17.73	17.86	17.57													
.12	15.58	14.96	16.98	17.80	17.99	17.62													
WIND SPEED (cm/sec)																			
16.00	411	295	595	685	744	794													
8.00	396	291	547	624	674	671													
4.00	366	269	508	572	587	601													
2.00	336	256	467	517	515	527													
1.00	317	249	438	483	480	494													
.50	272	218	378	408	418	419													
.25	228	173	318	346	360	351													
WIND DIRECTION (deg)																			
1.00	145	140	5	360	350	360													
SOIL TEMPERATURE CHANGE (°C)																			
Initial Time	1350	1450	1550	1650	1752	1853													
Run Time (min)	26	26	26	26	24	23													
-03	.52	.12	-.43	-.62	-.72	-.77													
-06	.60	.37	.06	-.26	-.50	-.51													
-12	.36	.30	.28	.15	.08	-.03													
-25	.14	.05	.05	.10	.09	.09													
-50	-.01	-.03	-.05	-.04	-.01	.00													
-100	-.01	-.09	-.02	-.02	-.02	.02													
Precipitation (cm)	--	--	--	--	--	--													

Table 8.2 (Continued)

HOURLY OBSERVATIONS							August 8, 1956					O'NEILL, NEBRASKA	
CST	2005	2105	2205	2305	0005*	0105*							
RADIATION (cal/cm <sup>2</sup> sec)													
Insolation	.0000	--	--	--	--	--							
Reflected	--	--	--	--	--	--							
Net Radiation	-.0015	-.0010	-.0010	-.00085	-.00031	-.00110							
AIR and SOIL TEMPERATURES (°C)													
Height (m)	24.26	23.43	22.45	22.44	21.83	19.68							
16.00	23.98	22.43	21.25	20.15	20.35	18.85							
8.00	22.65	21.15	19.74	18.00	18.86	18.34							
4.00	22.22	19.88	18.81	17.83	17.49	17.86							
2.00	21.82	19.08	17.19	16.46	16.38	17.64							
1.00	21.54	18.01	15.91	15.29	15.84	17.41							
.50	21.24	17.23	15.48	14.77	15.62	17.19							
.25	21.02	16.20	15.19	14.34	15.45	17.07							
.12	20.30	15.30	14.89	14.34	15.45	17.07							
-.03	20.07	14.81	14.30	13.77	14.81	16.54							
-.06	20.07	14.81	14.30	13.77	14.81	16.54							
-.12	20.07	14.81	14.30	13.77	14.81	16.54							
-.25	20.07	14.81	14.30	13.77	14.81	16.54							
-.50	20.07	14.81	14.30	13.77	14.81	16.54							
-1.00	20.07	14.81	14.30	13.77	14.81	16.54							
VAPOR PRESSURE (mb)													
16.00	18.14	17.63	16.77	15.45	18.65	18.84							
8.00	18.42	17.43	15.89	14.64	17.78	18.36							
4.00	18.41	17.49	15.94	14.65	17.78	18.34							
2.00	18.35	17.51	15.98	14.62	17.76	18.28							
1.00	18.35	17.54	16.01	14.68	17.77	18.28							
.50	18.35	17.58	16.01	14.67	17.77	18.34							
.25	18.28	17.58	16.09	15.63	17.71	18.23							
.12	18.29	17.89	16.53	15.00	17.62	18.44							
WIND SPEED (cm/sec)													
16.00	482	296	--	189	118	552							
8.00	343	225	156	179	82	423							
4.00	256	130	114	139	76	338							
2.00	197	85	174	109	85	249							
1.00	157	36	101	66	57	222							
.50	132	19	51	44	50	193							
.25	101	--	--	--	18	151							
WIND DIRECTION (deg)													
1.00	40	--	--	--	--	175							
SOIL TEMPERATURE CHANGE (°C)													
Initial Time	1953	2054	2152	2253	2350	0050							
Run Time (min)	23	25	24	23	28	27							
-.03	-.63	-.79	-.50	-.40	-.21	-.23							
-.06	-.52	-.56	-.48	-.40	-.37	-.20							
-.12	-.11	-.17	-.21	-.21	-.25	-.21							
-.25	-.01	.06	.03	.00	-.04	-.04							
-.50	.02	.01	.00	.03	.00	.00							
-1.00	.04	.01	.01	.00	-.01	-.01							
Precipitation (cm)	--	--	--	--	--	--							

\* August 9, 1956

Table 8.2 (Continued)

HOURLY OBSERVATIONS							August 9, 1956					O'NEILL, NEBRASKA	
CST	0205	0305	0405	0505	0605	0705							
RADIATION (cal/cm <sup>2</sup> sec)													
Insolation	--	--	--	--	.0000	.0011	.0052						
Reflected	--	--	--	--	.0000	.00038	.0015						
Net Radiation	-.00100	.00099	-.00101	-.00114	-.00038	.0026							
AIR and SOIL TEMPERATURES (°C)													
Height (m)	19.75	19.04	18.36	17.33	16.97	18.12							
16.00	18.69	17.61	16.97	16.91	16.92	19.20							
8.00	17.92	16.97	16.14	16.56	16.70	19.34							
4.00	16.96	16.38	15.46	16.25	16.17	19.34							
2.00	16.08	15.72	14.93	16.02	15.39	19.42							
1.00	15.29	15.08	14.47	15.66	14.85	19.53							
.50	14.75	14.81	14.30	15.44	14.98	19.77							
.25	14.39	14.60	14.13	15.22	15.10	19.84							
.12	21.18	20.22	19.68	19.40	19.00	19.51							
-.03	22.61	21.99	21.38	20.85	20.54	20.37							
-.06	24.56	24.16	23.68	23.28	22.93	22.63							
-.12	24.18	24.10	23.88	23.75	23.70	23.53							
-.25	21.90	21.92	21.91	21.92	22.00	21.98							
-.50	20.03	20.04	20.04	20.04	20.11	20.10							
-1.00	20.03	20.04	20.04	20.04	20.11	20.10							
VAPOR PRESSURE (mb)													
16.00	15.96	15.16	16.45	15.95	17.19	16.07							
8.00	15.25	14.67	15.41	15.70	16.45	17.30							
4.00	15.25	14.67	15.44	15.70	16.48	17.46							
2.00	15.22	14.68	15.39	15.70	16.51	17.49							
1.00	15.23	14.66	15.39	15.70	16.41	17.17							
.50	15.25	14.69	15.41	15.70	16.41	17.20							
.25	15.20	14.68	15.36	15.68	16.21	17.40							
.12	15.91	15.22	15.38	15.97	16.12	17.63							
WIND SPEED (cm/sec)													
16.00	293	404	470	425	147	308							
8.00	278	293	365	336	105	286							
4.00	204	227	289	250	76	263							
2.00	143	160	212	205	106	245							
1.00	96	107	157	160	82	214							
.50	71	88	135	145	62	194							
.25	19	41	98	116	29	161							
WIND DIRECTION (deg)													
1.00	--	--	--	300	160*	230							
SOIL TEMPERATURE CHANGE (°C)													
Initial Time	0150	0250	0350	0450	0550	0650							
Run Time (min)	27	27	28	28	26	26							
-.03	-.53	-.19	-.25	-.05	-.18	-.64							
-.06	-.24	-.29	-.39	-.16	-.18	-.08							
-.12	-.17	-.15	-.20	-.18	-.23	-.16							
-.25	-.03	-.03	-.06	-.06	-.07	-.06							
-.50	.01	+01	.00	.01	-.04	-.05							
-1.00	.00	+01	.01	.02	.00	-.02							
Precipitation (cm)	--	--	--	--	--	--							

\*Wind to light to turn vane

Table 8.2 (Continued)

HOURLY OBSERVATIONS August 9, 1956 O'NEILL, NEBRASKA						
CST	0805	0905	1005	1105	1205	1305
RADIATION (cal/cm <sup>2</sup> sec)						
Insolation	.0071	.0138	.0177	.0204	.0214	.0132
Reflected	.0015	.00265	.00315	.0035	.0037	.0023
Net Radiation	.0037	.0077	.0104	.0119	.0127	.0069
AIR and SOIL TEMPERATURES (°C)						
Height (m)						
16.00	21.33	23.22	24.75	26.46	27.36	28.05
8.00	21.66	23.66	25.13	26.75	27.71	28.29
4.00	21.82	23.92	25.58	27.08	28.14	28.74
2.00	21.92	24.20	25.90	27.21	28.26	29.24
1.00	22.04	24.67	26.35	28.03	29.41	29.56
.50	22.50	25.28	27.44	29.35	30.27	30.38
.25	22.91	26.47	28.33	30.67	31.52	30.94
.12	23.54	27.16	29.21	31.68	32.79	32.06
-.03	20.99	23.10	25.26	29.41	31.99	34.12
-.06	20.87	21.98	23.82	26.07	28.09	30.21
-.12	22.33	22.25	22.45	22.96	23.63	24.70
-.25	23.31	23.11	22.91	22.78	22.68	22.72
-.50	21.92	21.87	21.83	21.78	21.78	21.74
-1.00	20.03	19.96	19.99	19.93	19.91	19.95
VAPOR PRESSURE (mb)						
16.00	22.62	16.91	16.10	14.75	14.37	--
8.00	27.58	17.36	16.53	15.40	14.79	--
4.00	27.88	17.50	16.65	15.46	14.86	--
2.00	27.72	18.82	17.63	15.40	14.78	--
1.00	26.91	17.63	16.77	15.46	14.85	--
.50	19.11	17.76	17.08	15.78	15.05	--
.25	17.29	18.01	17.30	16.09	15.42	--
.12	17.29	18.34	18.17	16.64	15.98	--
WIND SPEED (cm/sec)						
16.00	174	338	322	400	393	313
8.00	176	339	290	373	391	306
4.00	148	323	273	360	351	286
2.00	153	300	256	330	332	268
1.00	136	(273)	230	306	309	235
.50	128	246	216	276	282	212
.25	102	204	182	235	239	182
WIND DIRECTION (deg)						
1.00	265	200	235	230	260	315
SOIL TEMPERATURE CHANGE (°C)						
Initial Time	0750	0850	0950	1050	1148	1251
Run Time (min)	26	26	26	20	28	23
-.03	.65	1.10	1.28	1.06	1.17	.22
-.06	.33	.64	.81	.87	.96	.77
-.12	-.04	.00	.17	.31	.42	.56
-.25	-.08	-.11	.09	-.07	.04	-.01
-.50	-.01	-.03	-.03	-.06	.07	-.04
-1.00	.00	-.12	-.03	-.02	-.02	-.03

Precipitation (cm) -- -- -- -- --

Table 8.2 (Continued)

HOURLY OBSERVATIONS August 9, 1956 O'NEILL, NEBRASKA						
CST	1405	1505	1605	1705	1805*	1605*
RADIATION (cal/cm <sup>2</sup> sec)						
Insolation	.0210	.0185	.0099	.0012	.0072	.0125
Reflected	.0038	.0033	.0016	--	.0013	.0021
Net Radiation	.0125	.0105	.0030	-.0006	.0038	.0060
AIR and SOIL TEMPERATURES (°C)						
Height (m)						
16.00	28.81	29.80	29.27	27.98	32.09	33.00
8.00	29.29	30.33	29.64	28.07	32.30	33.26
4.00	29.59	30.88	28.89	28.13	32.59	33.81
2.00	30.01	30.80	30.11	28.13	32.94	34.32
1.00	30.27	31.66	30.24	28.18	33.30	34.84
.50	31.03	32.88	30.75	28.18	33.52	35.61
.25	33.04	33.92	31.27	28.18	34.00	36.10
-.12	34.02	34.94	32.12	28.15	34.35	36.50
-.03	35.64	36.77	36.01	33.28	30.82	32.05
-.06	31.53	32.79	33.30	32.44	28.54	28.86
-.12	25.77	26.64	27.48	27.98	25.65	25.70
-.25	22.76	22.88	23.06	23.31	23.10	23.30
-.50	21.69	21.65	21.60	21.56	21.30	21.51
-1.00	19.91	19.87	19.82	19.84	19.62	19.47
VAPOR PRESSURE (mb)						
16.00	13.06	13.60	13.53	14.38	12.71	13.24
8.00	13.95	14.06	13.85	14.55	12.90	13.48
4.00	13.95	14.17	13.89	14.60	12.94	13.53
2.00	13.92	14.16	13.94	14.65	13.00	13.64
1.00	14.04	14.26	14.09	14.66	13.09	13.68
.50	14.32	14.59	14.27	14.74	13.13	13.71
.25	14.64	14.66	14.51	14.76	13.18	13.77
.12	15.05	14.87	14.88	14.85	13.23	13.82
WIND SPEED (cm/sec)						
16.00	246	277	154	573	753	889
8.00	261	279	153	501	727	843
4.00	244	261	141	463	664	764
2.00	230	244	144	416	590	678
1.00	217	228	133	370	522	603
.50	200	205	125	325	456	527
.25	166	175	101	276	383	440
WIND DIRECTION (deg)						
1.00	215	250	85	30	158	162
SOIL TEMPERATURE CHANGE (°C)						
Initial Time	1353	1454	1553	1653	1453	1553
Run Time (min)	25	24	25	23	24	23
-.03	.60	.32	-.56	-1.23	-.03	-.46
-.06	.56	.46	.17	-.50	.16	-.34
-.12	.39	.38	.33	.18	.08	.10
-.25	.03	.05	.11	.10	.03	.05
-.50	.07	.00	.00	-.01	.00	.00
-1.00	-.03	.60	.60	-.01	.02	-.02

Precipitation (cm) -- -- -- -- --

\* August 27, 1956

Table 8.2 (Continued)

HOURLY OBSERVATIONS August 27, 1956 O'NEILL, NEBRASKA							
CST	1705	1905	2105	2205	0005*	0105*	
RADIATION (cal/cm <sup>2</sup> sec)							
Insolation	.0070	.0003	.0000	.0000	.0000	.0000	
Reflected	.0014	--	.0000	.0000	.0000	.0000	
Net Radiation	.0027	-.0011	-.0010	-.0008	-.0006	-.0009	
AIR and SOIL TEMPERATURES (°C)							
Height (m)							
16.00	33.22	31.13	29.11	26.72	24.46	21.75	
8.00	33.32	30.55	26.72	24.90	21.38	20.03	
4.00	33.60	29.67	24.95	22.57	20.11	19.02	
2.00	33.95	28.94	22.59	20.69	18.83	18.37	
1.00	34.34	27.41	18.84	19.72	18.29	17.65	
.50	34.64	25.57	17.45	19.02	17.65	16.78	
.25	35.04	24.45	16.85	18.56	17.95	16.47	
-.12	35.38	23.85	16.28	18.09	16.94	16.06	
-.03	32.19	29.07	25.04	23.77	22.52	21.79	
-.06	29.40	28.58	26.26	25.04	23.67	23.14	
-.12	25.91	26.38	26.25	25.76	24.96	24.57	
-.25	23.36	23.65	23.98	23.96	23.99	23.82	
-.50	21.49	21.54	21.60	21.58	21.61	21.62	
-1.00	19.44	19.56	19.77	19.78	19.78	19.78	
VAPOR PRESSURE (mb)							
16.00	13.55	14.87	14.32	--	14.48	14.49	
8.00	13.70	15.00	15.10	--	15.20	14.84	
4.00	13.73	14.80	15.75	--	15.06	14.85	
2.00	13.76	14.88	15.55	--	14.82	14.77	
1.00	13.81	14.75	14.35	--	14.70	14.51	
.50	13.87	14.45	14.08	--	14.38	14.51	
.25	13.93	14.22	13.89	--	14.37	14.53	
.12	13.98	14.05	13.73	--	14.32	14.48	
WIND SPEED (cm/sec)							
16.00	825	230	213	320	167	337	
8.00	784	201	157	325	138	265	
4.00	706	163	136	262	103	206	
2.00	628	147	149	155	100	169	
1.00	555	83	70	76	66	113	
.50	490	49	33	59	70	99	
.25	403	--	--	30	52	74	
WIND DIRECTION (deg)							
1.00	165	--	--	--	--	--	
SOIL TEMPERATURE CHANGE (°C)							
Initial Time	1652	1850	2050	2150	0000	0050	
Run Time (min)	24	27	27	27	26	25	
-.03	-.25	-.96	-.60	-.30	-.27	-.37	
-.06	-.09	-.40	-.55	-.38	-.27	-.37	
-.12	-.12	.02	-.14	-.15	-.18	-.14	
-.25	.03	.06	-.03	.04	.00	-.02	
-.50	-.02	.02	.01	.02	.02	.00	
-1.00	-.01	.01	.00	.02	.00	.00	

Precipitation (cm) --  
\* August 28, 1956

Table 8.2 (Continued)

HOURLY OBSERVATIONS August 28, 1956 O'NEILL, NEBRASKA							
CST	0205	0305	0405	0505	0605	0705	
RADIATION (cal/cm <sup>2</sup> sec)							
Insolation	.0000	.0000	.0000	.0000	.0004	.0045	
Reflected	.0000	.0000	.0000	.0000	.0001	.0011	
Net Radiation	.0000	-.0004	-.0006	-.0008	-.0007	.0021	
AIR and SOIL TEMPERATURES (°C)							
Height (m)							
16.00	23.14	21.93	22.32	21.28	19.15	19.74	
8.00	21.83	21.04	21.37	20.04	17.71	19.95	
4.00	20.87	19.90	20.27	18.55	16.50	20.15	
2.00	19.97	18.95	19.01	17.99	15.65	20.28	
1.00	19.30	18.45	16.91	15.97	14.93	20.51	
.50	18.59	17.98	14.59	15.13	13.72	20.84	
.25	18.10	17.65	13.92	14.75	13.30	21.14	
-.12	17.76	17.47	13.38	14.43	13.02	21.41	
-.03	21.23	20.87	20.63	19.91	19.42	19.60	
-.06	22.63	22.15	21.88	21.41	20.94	20.63	
-.12	24.27	23.93	23.60	23.30	22.99	22.70	
-.25	23.91	23.83	23.73	23.61	23.50	23.38	
-.50	21.68	21.71	21.73	21.73	21.74	21.74	
-1.00	19.82	19.83	19.83	19.83	19.83	19.85	
VAPOR PRESSURE (mb)							
16.00	14.82	14.57	14.99	14.70	14.87	14.80	
8.00	15.04	14.78	14.90	14.90	13.83	14.87	
4.00	14.87	15.05	14.78	14.70	13.80	14.87	
2.00	14.69	15.05	14.69	14.68	13.58	14.85	
1.00	14.52	14.95	14.51	14.59	13.02	14.86	
.50	14.50	14.93	14.13	14.43	12.92	14.80	
.25	14.39	14.85	13.82	14.39	12.85	14.87	
.12	14.31	14.83	13.68	14.37	12.80	14.87	
WIND SPEED (cm/sec)							
16.00	289	99	314	422	223	400	
8.00	248	149	183	365	184	393	
4.00	192	144	112	301	99	366	
2.00	158	114	111	238	57	326	
1.00	106	61	81	164	41	290	
.50	90	51	32	124	46	256	
.25	64	36	--	97	31	205	
WIND DIRECTION (deg)							
1.00	--	--	--	--	340	151	
SOIL TEMPERATURE CHANGE (°C)							
Initial Time	0150	0250	0350	0450	0550	0650	
Run Time (min)	26	26	26	26	27	26	
-.03	-.16	.07	-.35	-.27	-.22	.63	
-.06	-.21	-.16	-.13	-.16	-.18	.00	
-.12	-.12	-.15	-.12	-.11	-.10	-.12	
-.25	-.02	-.02	-.03	-.07	-.08	-.08	
-.50	.03	.00	.01	.00	.00	-.01	
-1.00	.01	.01	.00	.00	.00	.00	

Precipitation (cm) --

Table 8.2 (Continued)

HOURLY OBSERVATIONS								August 28, 1956						O'NEILL, NEBRASKA					
CST		0805	0905	1005	1105	1205	1305												
RADIATION (cal/cm <sup>2</sup> sec)																			
Insolation	.0070	.0125	.0155	.0195	.0165	.0185													
Reflected	.0015	.0022	.0024	.0031	.0028	.0016													
Net Radiation	.0035	.0061	.0085	.0115	.0100	.0030													
AIR and SOIL TEMPERATURES (°C)																			
Height (m)	20.96	24.98	26.94	30.36	31.11	31.34													
16.00	21.09	25.34	27.25	30.86	31.51	31.71													
8.00	21.20	25.82	27.69	31.39	31.86	31.91													
4.00	21.29	26.02	28.07	32.26	32.43	32.27													
2.00	21.59	26.26	28.87	32.90	33.36	32.56													
1.00	22.04	26.78	29.63	33.63	33.97	33.41													
.50	22.65	27.74	30.77	34.42	34.99	34.28													
.25	23.20	28.51	31.45	34.98	35.90	34.98													
.12	21.41	24.46	27.96	31.28	33.95	35.24													
-.03	21.14	22.41	24.44	26.63	28.62	30.25													
-.06	22.40	22.34	22.52	22.95	23.76	24.61													
-.12	23.20	23.02	22.85	22.68	22.70	22.70													
-.25	21.73	21.70	21.68	21.58	21.64	21.61													
-.50	19.82	19.83	19.80	19.74	19.84	19.82													
-.100																			
VAPOR PRESSURE (mb)																			
16.00	15.80	17.96	17.19	15.44	14.76	12.31													
8.00	15.92	18.07	17.58	14.32	15.05	12.57													
4.00	16.00	18.07	17.60	14.37	15.05	12.57													
2.00	16.04	18.06	17.63	14.30	15.03	12.58													
1.00	16.10	18.09	17.65	14.21	15.08	12.59													
.50	16.20	18.18	17.72	14.48	15.11	12.66													
.25	16.43	18.36	17.80	14.63	15.16	12.71													
.12	16.51	18.54	17.88	14.78	15.19	12.86													
WIND SPEED (cm/sec)																			
16.00	159	185	331	546	637	464													
8.00	162	194	322	488	598	456													
4.00	148	183	307	475	553	433													
2.00	144	171	281	428	476	384													
1.00	114	137	253	385	438	339													
.50	117	135	235	348	403	307													
.25	94	117	207	303	367	269													
WIND DIRECTION (deg)																			
1.00	315	45	315	360	360	315													
SOIL TEMPERATURE CHANGE (°C)																			
Initial Time	0750	0850	0950	1050	1150														
Run Time (min)	20	26	26	25	27	27													
-.03	67	1.50	1.43	1.17	.74	.19													
-.06	32	.76	.87	.88	.83	.66													
-.12	-.08	-.04	.16	.22	.38	.42													
-.25	-.08	-.05	-.08	-.08	-.01	.01													
-.50	-.01	-.01	.00	-.04	.00	-.02													
-.100	.00	.01	.00	.00	-.01	-.04													

Precipitation (cm) -- -- -- -- --

Table 8.2 (Continued)

HOURLY OBSERVATIONS								August 28, 1956						O'NEILL, NEBRASKA					
CST		1405	1505	1805															
RADIATION (cal/cm <sup>2</sup> sec)																			
Insolation	.0175	.0157	--																
Reflected	.0029	.0027	--																
Net Radiation	.0097	.0083	--																
AIR and SOIL TEMPERATURES (°C)																			
Height (m)	31.87	29.63	32.96																
16.00	32.29	30.26	33.08																
8.00	33.01	30.67	33.16																
4.00	33.54	31.38	33.18																
2.00	34.01	32.23	33.22																
1.00	34.01	32.23	33.22																
.50	34.80	32.94	33.26																
.25	36.16	33.94	33.28																
.12	37.14	34.52	33.32																
-.03	35.59	36.25	31.00																
-.06	31.11	31.98	29.25																
-.12	25.44	26.14	26.24																
-.25	22.76	22.93	23.53																
-.50	21.60	21.59	21.52																
-.100	19.83	19.84	19.52																
VAPOR PRESSURE (mb)																			
16.00	13.80	17.16	15.92																
8.00	14.05	17.28	14.08																
4.00	14.07	17.28	14.11																
2.00	14.07	17.27	14.12																
1.00	14.08	17.29	14.20																
.50	14.17	17.31	14.23																
.25	14.24	17.30	14.30																
.12	14.39	17.31	14.32																
WIND SPEED (cm/sec)																			
16.00	746	954	567																
8.00	790	948	511																
4.00	744	893	466																
2.00	669	798	407																
1.00	593	711	356																
.50	532	626	315																
.25	451	542	261																
WIND DIRECTION (deg)																			
1.00	288	295	--																
SOIL TEMPERATURE CHANGE (°C)																			
Initial Time	1350	1450	1750																
Run Time (min)	27	28	27																
-.03	.72	-.06	-.57																
-.06	.36	.23	-.08																
-.12	-.33	.31	.10																
-.25	-.06	.06	.04																
-.50	.01	.02	.00																
-.100	.00	-.03	.01																

Precipitation (cm) -- -- -- -- --



Table 8.3 Soil moisture and soil density, O'Neill, Nebraska, 1956

Date:	July 10		July 16	
	Soil Moisture (% Dry Wt.)	Soil Density (Gr/cm <sup>3</sup> )	Soil Moisture (% Dry Wt.)	Soil Density (Gr/cm <sup>3</sup> )
0-10	7.2	1.06	6.8	.89
10-20	7.0	1.13	6.3	1.07
20-30	3.8	1.28	6.3	1.11
30-40	4.2	1.35	4.9	1.17
40-50	5.1	1.31	3.9	1.19
50-60	3.1	1.43	3.7	1.20
60-70	1.9	1.53*	3.4	1.27
70-80	1.8	1.53*	3.2	1.29
80-90	2.9	1.53*	4.8	1.40
90-100	5.7	1.53*	4.8	1.45

Date:	August 6		August 29	
	Soil Moisture (% Dry Wt.)	Soil Density (Gr/cm <sup>3</sup> )	Soil Moisture (% Dry Wt.)	Soil Density (Gr/cm <sup>3</sup> )
0-10	9.2	1.03	6.6	1.05
10-20	6.6	1.11	6.5	1.19
20-30	3.0	1.23	6.0	1.22
30-40	2.8	1.27	4.4	1.35
40-50	2.9	1.29	5.6	1.29
50-60	3.5	1.32	6.7	1.39
60-70	6.2	1.20	3.8	1.51
70-80	3.8	1.35	2.9	1.56
80-90	2.6	1.45	2.4	1.58
90-100	1.8	1.60	2.4	1.68

\*Mean value, 60-100cm.

## CHAPTER 9 EVALUATION OF THE FLUXES OF SENSIBLE AND LATENT HEAT FROM MEASUREMENTS OF WIND, TEMPERATURE, AND DEW POINT PROFILES

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Texas A&M Research Foundation

### 9.1 Introduction

Inasmuch as the macroparameters of meteorology are, in many cases, determinable by the microparameters in the near surface layers of the atmosphere, a great deal of study has been conducted by many investigators towards better evaluation of these microparameters. A basic attack on the problem lies in the determination of the surface energy budget; and it is the purpose of this paper to present a method of evaluating the various terms of the energy balance relationship from measurements of moisture, net radiation, and the vertical gradients of wind, temperature, and moisture at a particular site for a given time interval.

From conservation of energy requirements, the sum of energy fluxes entering or leaving the earth's surface must be zero. Or

$$R_n + q_c + q_e + q_s = 0 \quad (1)$$

where  $R_n$  = net radiative flux of heat,

$q_c$  = flux of sensible heat to the air,

$q_e$  = flux of latent heat from evaporation or condensation of water, and

$q_s$  = conductive heat flux into or out of the ground.

The net radiation is easily measurable directly and need not concern us here other than as a measure of the reliability of the other terms in Eq. (1).

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Measurements of soil heat flux, though not performed directly, are based on the Fourier conduction equation and the treatment shown in this paper is no different from that of previous authors (for example, Sutton<sup>5</sup>).

The essential difference between this and previous papers is based on a definition of turbulent flow first advanced by Halstead.<sup>2</sup> This, in turn, leads to evaluations of  $q_c$  and  $q_e$  in a turbulent regime different from those obtained through the classical concept of equivalence of exchange coefficients for heat and momentum.

The applicability of these evaluations is shown by heat budget computations based on data collected during Project Prairie Grass by personnel of Texas A&M Research Foundation.

### 9.2 The Flux of Momentum

The transfer rate of molecular momentum within a gas per unit time and area, in a direction perpendicular to the mean velocity of the gas (or tangential shear), is proportional to the vertical gradient of the velocity. That is,

$$\tau_z = \mu du/dz \quad (2)$$

where  $\mu$  is defined as the absolute viscosity of the gas. Equation (2), though first presented as an empirical concept, can easily be derived from kinetic theory.

This derivation shows that

$$\mu = \rho \bar{c} L/3 \quad (3)$$

where  $\bar{c}$  is the root-mean-square velocity of the molecules comprising the gas,  $\rho$  is the density, and  $L$  is the mean free path. If the scale of motion within the gas, as characterized by the product  $uz$ , where  $z$  is the distance from the bounding surface, exceeds the molecular scale of motion as shown by  $\bar{c}L$ , by a sufficient amount, the flow ceases to be laminar and becomes irregular or chaotic or, as usually described, turbulent.

The critical values of this ratio for tubes of various sizes were first investigated by Reynolds, who found that turbulent motion occurred

in a tube of diameter  $d$  when

$$R_e = 3ud/\bar{c}L = \rho ud/\mu > 2000. \quad (4)$$

Even though turbulent motion is present, a laminar sublayer adjacent to the boundary can still exist. The thickness of this layer is determinable from  $R_e$  for flow over smooth surfaces. Assuming a linear profile within the laminar layer, the surface friction is

$$\tau_o = .332 \rho u_o^2 / \sqrt{R_e}.$$

From integration of Eq. (2), assuming  $\tau \neq \tau(z)$ ,

$$\tau_o = \rho \bar{c} L u_o / 3\delta.$$

Thus, the localized Reynolds' number is

$$R_c = 3u_o \delta / \bar{c}L = 135. \quad (5)$$

It should be noted that the flow pattern at  $z = \delta$  will not be strictly laminar or turbulent. That is,  $z = \delta$  cannot be interpreted as a point but rather as a region. However, for purposes of discussion here,  $\delta$  will be regarded as the thickness of the laminar layer.

To apply Eq. (2) to a turbulent regime, the molecular viscosity must be replaced by a term, usually referred to as the eddy viscosity, which will be a function of the distance from the bounding surface.

Inasmuch as division between laminar and turbulent flow does not occur at a precise point, it appears reasonable that the eddy viscosity should be so defined that it reduces to the molecular viscosity. That is, Eq. (2) could be written as

$$\tau_z = K du/dz, \quad (6)$$

where  $K$  will be equal to  $\mu$  at  $z = \delta$ .

Consider a flow of gas over a smooth surface and assume  $n$  hypothetical surfaces inserted in the gas above the boundary, each a mean distance  $\delta$  units above the layer preceding it. That is, the first

surface is coincident with the top of the laminar sublayer. The effect of turbulence may be thought of as a factor of area distortion of a given surface. Hence, the area of the surface at elevation  $j$  will be greater than the area of the surface at  $j - \delta$  and less than the surface at elevation  $j + \delta$ . This is shown in Figure 9.1.

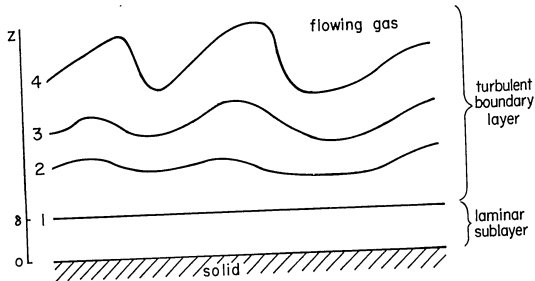


Figure 9.1 Distorted Area Pattern

The first surface has the same area as the smooth boundary itself inasmuch as below  $z = \delta$  the flow is laminar. Above  $z = \delta$ , a given surface becomes distorted due to the distortion of the preceding surface, plus any inherent distortion of the surface itself.

Let  $r$  be the ratio of areas of any two adjacent surfaces. Then

$$r = A_n / A_{n-1} \quad (7)$$

Hence, Eq. (6) may be written  $\tau_z = \mu A_n / A_0 \, du/dz$ .

Thus, the area of the  $n$ th layer at elevation  $z$  will be

$$A_n = A_1 r^n.$$

Since  $A_1 = A_0$ ,

$$A_n / A_0 = r z / \delta. \quad (8)$$

Substituting Eq. (8) in Eq. (7), we obtain,

$$\tau_z = r z \mu / \delta \, du/dz, \quad (9)$$

as applicable to turbulent flow.

The shearing stress  $\tau_z$  will vary with elevation, being a maximum at  $z = 0$ , and decreasing with elevation. For the atmosphere,  $\tau_z$  will vanish at  $z = H$ , where  $H$  is the geostrophic wind level.

Assuming a linear variation of shearing stress with height\*, we may write,

$$\tau_z = \tau (1 - z/H), \quad (10)$$

where  $\tau$  is the stress at the top of the laminar layer, which for all practical considerations for the atmosphere will equal the shear stress at the surface. Hence,

$$\tau_0 (1 - z/H) = \rho \bar{c} (Lr z / 3\delta) \, du/dz \quad (11)$$

Actually,  $\rho$  and  $\bar{c}$  and  $L$  will vary with height also, but for the lower layers of the atmosphere this variation will be small.

Separating variables and integrating from  $\delta$  to  $z$ , we obtain,

$$u_z = u_\delta + 3\delta \tau_0 (\ln z/\delta - z/H) / \rho \bar{c} Lr \quad (12)$$

From integration of Eq. (7) from  $z = 0$  to  $z = \delta$  ( $\tau_0 = \tau_z$ ,  $K = \mu$ ),

$$u_\delta = 3\tau_0 \delta / \rho \bar{c} L. \quad (13)$$

\*This is equivalent to assuming a unidirectional mean velocity, negligible Coriolis acceleration, and a uniform horizontal pressure gradient.

Thus,

$$u_z = u_0 [1 + (\ln z/\delta - z/H)/r]. \quad (14)$$

Inasmuch as the discussion is restricted to the region where  $z$  is of the order of a few meters, while  $H$  will be of the order of 500 meters,  $z/H$  of Eq. (14) will be insignificant with respect to  $\ln z/\delta$  and the former term may be neglected. Thus,

$$u_z = u_0 [1 + (\ln z/\delta) r]. \quad (15)$$

Equation (15) is analogous to the wind profile equation derived from mixing length concepts, that is,

$$u_z = u_* [A + (\ln u_* z/\nu)/k] \quad (16)$$

where  $u_* = \sqrt{\tau/\rho}$ ,  $k$  is von Karman's constant ( $k = 0.40$ ), and  $A$  is a constant. It is interesting to convert Eqs. (15) and (16) to identical form, inasmuch as  $A$  and  $k$  have been evaluated from empirical studies.

From Eqs. (5) and (13),

$$u_0 = R_c \nu / \delta = u_*^2 \delta / \nu. \quad (17)$$

Substituting in Eq. (15)

$$u_z = u_* [A + (\ln u_* z/\delta) k] \quad (18)$$

which is identical to Eq. (16) when

$$A = u_* \delta / \nu [1 - (\ln u_* \delta / \nu) / r] \quad (19)$$

and

$$k = \nu r / u_* \delta. \quad (20)$$

Using Nikuradse's (Sutton<sup>5</sup>) data for flow near a smooth surface,  $A = 5.5$  for  $k = .40$ ; hence,  $r = 4.65$ .

More recent work by Laufer at the Bureau of Standards affirms the Nikuradse data and leads to the same  $r$  value.

Substituting this value in Eq. (15),

$$u_z = u_0 [1 + (\ln z/\delta)/4.65], \quad z > \delta \quad (21)$$

for flow near a smooth bounding surface.

Within the laminar sublayer ( $z \leq \delta$ ),  $u$  is given from Eq. (17) and using  $\mu = 1.8 \times 10^{-4}$  gm/cm sec,  $\rho = 1.2 \times 10^{-3}$  gm/cm<sup>3</sup>,

$$u_0 = 20.3/\delta. \quad (22)$$

Figure 9.2 shows Eqs. (21) and (13) for several  $\tau$  values, plotted as velocity versus the logarithm of elevation. The turbulent and laminar regimes are separated by the line along which  $u_0 \delta = 20.3$ .

The applicability of Eq. (21) is limited to small elevations and smooth surfaces. We can rigorously define elevation but not a smooth surface. Aerodynamically speaking, a smooth surface means a surface that does not physically protrude through the laminar sublayer. However, since the thickness of this layer depends upon the velocity, a surface consisting of No. 4 sandpaper could be a smooth surface; and, under other flow conditions, a pane of glass could be a rough surface.

While a satisfactory theoretical treatment of the effect of surface roughness has yet to be developed, it is reasonable to think of the roughness elements as sinks of momentum which in total are equivalent to a "drag velocity." Hence, for the postulated type of flow over a rough surface, Eq. (21) can be modified to

$$u_z = u_0 [1 + (\ln z/\delta)/4.65] - u_s, \quad (23)$$

where  $u_s$  is the drag velocity corresponding to momentum transferred to surface roughness elements, assuming no modification of the roughness elements by the flow. Further, the length  $\delta$  must then represent, not the thickness of an actual sublayer, but more generally, the thickness of any layer which would give a distortion  $r$ . Since it is impossible to determine the sink strength of a surface theoretically or to

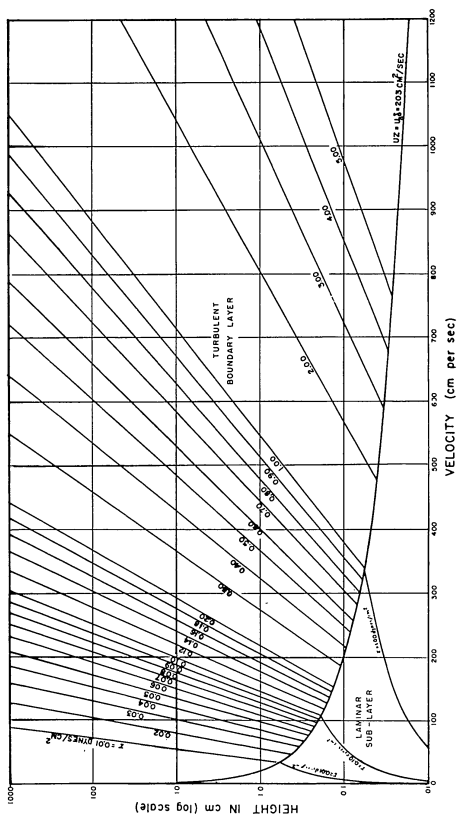


Figure 9.2 Wind profile grid for steady flow of air at constant temperature over aerodynamically smooth surfaces

measure  $u_s$  directly, it is necessary to eliminate the "drag velocity" by solving Eq. (23) simultaneously for more than one level.

In the presence of a vertical gradient of potential temperature, the modification of the flow pattern can be significant, as the density, mean free path, and root mean square velocity of the gas will change with elevation. That is, a buoyancy term will be present. This will be true in the laminar as well as in the turbulent region. For the lower layers of the atmosphere to which this discussion is restricted, the effects of buoyancy can be large, varying velocities and transfer rates through one or two orders of magnitudes. Fortunately, however, these effects do not appreciably influence the logarithmic nature of the profiles in the layers below one or two meters, hence need not be considered. Actually, this requires that  $z$  be no greater than the elevation for which  $u$  vs  $\ln z$  is linear.

In general, the argument presented implies that turbulent transfer is not a function of an exchange coefficient varying with lateral or vertical displacement but a rate of distortion of laminar flow area which will vary from case to case, but will remain constant for a given flow pattern.

In order to apply the development to measurements of momentum transfer to the surface, we require the difference in velocity between a height  $z$  and  $2z$ . From Eq. (23)

$$u_{2z} - u_z = (u_0 \ln 2)/r. \tag{24}$$

Substituting Eq. (23) in (13) and recalling that  $r = 4.65$ , then the total momentum flux at the surface (or any elevation,  $z$ , since Eq. (23) is essentially based on constancy of shearing stress with height) is given by

$$\tau_z = 1/3 \rho (u_{2z} - u_z)^2. \tag{25}$$

Inasmuch as this equation will be used again in the evaluation of the convective and evaporative fluxes of heat, it will be worthwhile to repeat the meaning of the various terms entering this equation.

These are listed below:

- $u_z$  = mean wind speed at elevation  $z$ ,
- $u_\delta$  = mean speed at the top of the laminar sublayer (fictional for flow over a rough surface),
- $r$  = 4.65, increase in surface area due to turbulent distortion of a single layer of mean thickness  $\delta$ ,
- $\delta$  = thickness of layer producing a constant distortion  $r$  (for flow over smooth surfaces, the thickness of the laminar sublayer).

### 9.3 The Flux of Sensible Heat

The rate of vertical transfer of heat ( $q_c$ ) per unit time and unit area within a gas is proportional to the density of the medium, the specific heat, and the gradient of potential temperature, or for non-turbulent flow,

$$q_c = \nu_c \rho c_p dT/dz, \quad (26)$$

where  $\rho$  is density,  $c_p$  is the specific heat at constant pressure,  $T$  is potential temperature, and  $\nu_c$  is a constant of proportionality related to the product of molecular mean free path and root-mean-square velocity, and generally referred to as the thermal diffusivity. It has the same units as kinematic viscosity,  $\text{cm}^2/\text{sec}$  in the cgs system.

If air is in turbulent motion, transfer of heat is still expressible by Eq. (26) but with a dependency on the scale of motion within the fluid. That is, heat is transferred by parcels of air as well as by individual molecules.

As in the case of flux of momentum, consider a flow of air over a smooth boundary with hypothetical, equally spaced surfaces separating layers of the moving air. For laminar flow, each surface will be parallel to every other surface, or each surface will have the same area. For turbulent flow, however, each surface will have a different area depending on the degree of turbulence. The first of this hypothetical group of surfaces will be parallel to the solid surface itself, if it is located at the top of the laminar layer, which is at a distance  $\delta$

above the solid boundary. Surface number two, at a mean distance  $\delta$  above number one, will be distorted to a degree depending on the scale of motion between the two surfaces. Surface number three (at a mean distance  $\delta$  above surface two) will be distorted according to the scale of motion between it and surface one, or between it and number two, plus the distortion between surfaces one and two.

The area of a surface at a given height,  $z$ , is a measure of the opportunity for energy transfer. This area  $A_n$ , divided by the area of surface number one (or the area of the boundary itself,  $A_0$ ), will be equal to  $rn$  where  $r$  is the fractional increase in area due to turbulent distortion and  $n$  is the number of surfaces, each a mean distance  $\delta$  apart, between the boundary and elevation  $z$ . Thus,

$$A_n = A_0 rz/\delta. \quad (27)$$

Hence, Eq. (26) may be written as

$$q_c = K_c \rho c_p dT/dz, \quad (28)$$

where

$$K_c = \nu_c \text{ for } z \leq \delta \text{ (laminar flow),}$$

and for turbulent flow (over smooth surfaces) as,

$$q_c = \nu_c rz \rho c_p / \delta dT/dz. \quad (29)$$

Restricting the application of Eq. (29) to small values of  $z$ , constancy of  $\nu_c$ ,  $\rho$ , and  $c_p$  may be assumed. This, in effect, means negligibility of any buoyancy terms.

For the same conditions given in the preceding section for stress varying linearly with elevation, we assume a linear variation of  $q$  with elevation, or

$$q_c = q_0 (1 - z/H), \quad (30)$$

where  $H$  is the thickness of the turbulent layer, or geostrophic wind level.

Substituting Eq. (30) in (29), separating variables, and integrating from the top of the laminar layer to an elevation  $z$ ,

$$T_z = T_\delta [1 + (\ln z/\delta - z/H)/r], \quad (31)$$

where

$$T_\delta = q_c \delta / \rho c_p \nu_c. \quad (32)$$

For small values of  $z$ , the term  $z/H$  will be negligible in comparison with  $\ln z/\delta$  and may be omitted. Thus,

$$T_z = T_\delta [1 + (\ln z/\delta)/r], \quad (33)$$

for flow over smooth surfaces.

For flow over aerodynamically rough surfaces, we parallel the previous view concerning momentum. That is, we will regard roughness elements to act as sources or sinks of heat, according to the temperature differences between the elements and the ambient, and postulate a potential temperature equivalent to the magnitude of the sources or sinks. In this view, Eq. (32) may be modified to

$$T_z = T_\delta [1 + (\ln z/\delta)/r] + T_s. \quad (34)$$

Generally,  $T_s$  will be unknown, but it is not involved when Eq. (34) is applied to potential difference between two levels. For the particular levels  $z$  and  $2z$ ,

$$T_{2z} - T_z = T_\delta (\ln 2)/r. \quad (35)$$

Combining Eqs. (17), (24), (32), and (35), we obtain

$$q_c = c_p r^2 \rho \nu_c (T_{2z} - T_z) (u_{2z} - u_z) / R_c \nu (\ln 2)^2, \quad (36)$$

for evaluation of the flux of sensible heat.

Using the values

$$\rho = 1.2 \times 10^{-3} \text{ gm/cm}^3,$$

$$c_p = 0.24 \text{ cal/gm deg C},$$

$$\nu_c = 0.21 \text{ cm}^2/\text{sec},$$

$$\nu = 0.15 \text{ cm}^2/\text{sec},$$

$$r = 4.65, \text{ and}$$

$$R_c = 135,$$

in Eq. (36)

$$q_c = .124 \times 10^{-3} (u_{2z} - u_z) (T_{2z} - T_z) \quad (37)$$

with  $q_c$  in  $\text{cal/cm}^2 \text{ sec}$ , velocity in  $\text{cm/sec}$ , and temperature in degrees Centigrade.

#### 9.4 The Flux of Water Vapor

Evaporation of a fluid is a measure of the difference of exchange rates of molecules of the fluid between the surface and the surrounding medium. For the case in which molecules escaping from the surface of the fluid are influenced only by their concentration and the molecular properties of the surrounding medium (for example, still air over water), the evaporation is given by,

$$E = \sigma d \rho' / dz, \quad (38)$$

where  $\sigma$  is the diffusion coefficient, and  $\rho'$  is the density of the fluid vapor. While  $\sigma$  will vary slightly with temperature, it may be considered constant for purposes of this discussion. Its value for  $15^\circ\text{C}$  is  $.250 \text{ cm}^2/\text{sec}$ .

If the air is in turbulent motion, Eq. (38) requires modification to allow for non-molecular transfer. As in the previous cases of transfer of momentum and heat, we will generalize the laminar flow

case to include turbulent flow by introducing a factor to allow for the increased area of contact between the turbulently distorted layers, or

$$E = \sigma r z / \delta \, d\rho' / dz. \quad (39)$$

Using the same reasoning that has been applied for the wind and temperature profiles with respect to variations in E with height, surface roughness, and thermal buoyancy, the evaporation is given as

$$E = \sigma (u_{2z} - u_z) (\rho'_{2z} - \rho'_z) / 3, \quad (40)$$

where E will be given in gm/cm<sup>2</sup> sec for  $\rho'$  in gm/cm<sup>3</sup>, and u in cm/sec.

In order to compute the flux of latent heat by evaporation, Eq. (40) must be multiplied by the latent heat of vaporization of water for the particular temperature concerned. Using 20°C as an average temperature and converting absolute humidity to an equivalent vapor pressure by use of

$$\rho' = eM/RT \quad (41)$$

where

- M = 18, molecular weight of water,
- R =  $8.31 \times 10^{-7}$  erg deg, universal gas constant,
- T = 293°K,
- e = vapor pressure (millibars), and
- $q_e$  = evaporative flux of heat,

we can write approximately,

$$q_e = .240 \times 10^{-3} (u_{2z} - u_z) (e_{2z} - e_z), \quad (42)$$

when  $q_e$  is given in cal/cm<sup>2</sup> sec.

### 9.5 Soil Heat Flux

Inasmuch as transfer of heat energy within the soil is by conduction, the equation for heat flux in the soil is given by the Fourier relation,

$$\partial T / \partial t = \nu_c \nabla^2 T \quad (43)$$

where T = temperature, and  $\nu_c$  = thermal diffusion coefficient. If  $\partial^2 T / \partial x^2 = \partial^2 T / \partial y^2 = 0$ , using Eq. (26) to define the heat flux, and considering z to increase positively with height,

$$q_o = q_z + \int_z^0 \rho c_p (\partial T / \partial t) dz. \quad (44)$$

Since it is desirable to determine the surface heat flux from soil temperature difference with time,  $q_z$  must equal zero. That is, measurements must cover the range from the surface to a point where  $\partial T / \partial z = 0$ . Hence,

$$q_o = \int_z^0 \rho c_p (\partial T / \partial t) dz. \quad (45)$$

### 9.6 Computation of Surface Heat Budgets

During the 70 gas releases of Project Prairie Grass, personnel of the Texas A&M Research Foundation made measurements of net radiation as well as of wind velocity, vapor pressure, air temperature, and soil temperature at several levels. These data have been used in the energy balance equation as a measure of the applicability of the expressions developed for evaluating the fluxes of sensible and evaporative heat.

The systems of measurement employed in the study are described in Chapter 7 of this report and need not be repeated here. The method of analysis of the data as pertinent to the various flux computations, however, is given below.

Referring to Eq. (37), evaluation of  $\Delta u = (u_{2z} - u_z)$  and  $\Delta T = (T_{2z} - T_z)$



is all that is required to evaluate the flux of sensible heat. These values, of course, are obtainable from profile measurements of wind speed and air temperature. Specifically, the mean values of  $u$  and  $T$  at 12.5, 25, 50, 100, 200, 400, 800, and 1600 centimeters were measured for a 20- to 30-minute interval surrounding the gas release intervals and plotted versus the logarithm of elevation. Inasmuch as the developed relationships apply in the region where  $u$  is linear with  $\ln z$ , the portions of the profiles significant to the study are straight lines, and the double-level variation is merely the abscissa increment between any two successive levels along the profile.

To minimize plotting and reading errors, the increments were read between four levels and divided accordingly. Of course, not all profiles were strictly linear. In such cases the "best sight" fit to a linear profile was used with greatest weight given to the lowest levels where deviation from linearity was a minimum.

In the  $u$  evaluation, extrapolation of the profile to  $u = 0$  gives the roughness parameter  $z_0$ , as can be seen from

$$u = (u_* \ln z / z_0) / k, \quad (46)$$

which is another form of Eq. (16). A value of 0.6 cm was found to be the  $z_0$  value for the measuring station location. This value represents the average value of the  $\ln z$  versus  $u$  intercepts of 16 profiles that were essentially linear at all levels. Hence, all wind profiles were drawn as straight lines from the point  $z = 0.6$  cm,  $u = 0$ , through the lower four points of  $u$  versus the logarithm of  $z$ .

The increment of vapor pressure  $\Delta e = (e_{2z} - e_z)$  was obtained similarly from measurements of vapor pressure at the same elevations used for wind speed and air temperature.

The soil heat flux at the surface is given by Eq. (45). Both  $\rho$  and  $c_p$  vary with depth but so slightly, for the interval considered, that they may be treated as constant. For the type of soil in question (O'Neill loam, upland phase),  $\rho c_p = 0.28$ , as determined from six

different soil tests performed during the period covered by the data.

Thus, the value of soil heat flux is proportional to the area between profiles of temperature versus depth at the beginning and the end of the sampling period. The above, of course, is based on the assumption that  $\partial T / \partial z = 0$  at some level  $z$ .

Soil temperatures were measured at 3.12, 6.25, 12.5, 25, 50, and 100 centimeters. If a maximum or minimum occurred at a depth of less than 100 centimeters, then the integral is represented by the area between the two profiles from the surface to the critical depth. If no maximum or minimum temperature occurred, then the integral was evaluated to 100 centimeters, provided the temperature at that depth did not vary significantly with time during the gas release period. Inasmuch as surface temperature was not measured, this point on the profile was obtained from a graph of surface temperature versus time of day for that location as given by an analog computer<sup>4</sup> from local input data.

Table 9.1 gives a summary of the analysis for 48 release periods for which complete data were available. The fluxes in this table are given in kilocalories per square centimeter per second. To facilitate comparison of these fluxes with values determined by the University of Wisconsin group, the fluxes are presented in calories per square centimeter per minute in Table 9.2.

The line of best fit\* of the data of Table 9.1 is  $y = .99x$ , where  $y$  represents the net radiation values and  $x$  is the negative of the sum of the fluxes of latent heat, sensible heat, and soil heat. The average error (that is, between the net radiation values and the sum of the fluxes) is  $0.43 \times 10^{-3}$  cal/cm<sup>2</sup> sec. If release No. 10, which is obviously suspect, is omitted, the line of best fit is  $y = 0.97x$  and average error is  $0.36 \times 10^{-3}$  cal/cm<sup>2</sup> sec.

\*Determined by the method of least squares. The second significant figure in the equation of best fit should not be taken to imply an accuracy of 1 percent, but is given only as a means of comparison with other equations based on different methods of evaluating heat fluxes.

Table 9.1. Heat budget data collected by the Texas A&amp;M Research Foundation

Gas	$\Delta u$	$\Delta \theta$	$\Delta e$	$q_c$	$q_e$	$q_s$	$\sum q_i$	$R_n$	$R_n + \sum q_i$
Rel. No.	cm/sec	$^{\circ}C$	mb	Kcal/cm <sup>2</sup> sec	Kcal/cm <sup>2</sup> sec	Kcal/cm <sup>2</sup> sec	Kcal/cm <sup>2</sup> sec	Kcal/cm <sup>2</sup> sec	Kcal/cm <sup>2</sup> sec
2	23	-.28	-.42	-.80	-2.32	.07	-3.05	2.90	.15
7	54	-1.07	-.33	-7.16	-4.28	-1.56	-13.02	12.80	.22
8	54	-.51	-.20	-3.41	-2.59	.23	-5.77	5.70	.07
9	84	-.53	-.23	-5.52	-4.64	-1.18	-11.34	11.40	-.06
10	57	-.90	-.13	-6.36	-1.78	-1.39	-9.53	12.80	-3.27
15	40	-.70	-.09	-3.47	-.86	-1.11	-5.44	5.00	.44
16	42	-1.03	-.23	-5.36	-2.32	-2.38	-10.06	10.00	.06
19	73	-.60	-.10	-5.43	-1.75	-1.08	-8.26	8.10	.16
20	112	-.83	-.05	-11.53	-1.34	-1.43	-14.30	13.70	.60
21	72	.10	-.01	.89	-.17	.22	.94	-.90	-.04
22	83	.15	-.02	1.54	-.40	.28	1.42	-1.40	-.02
25	34	-.52	-.48	-2.19	-3.92	.03	-6.09	6.20	-.12
26	79	-.63	-.30	-6.17	-5.69	-1.06	-12.92	12.60	.32
27	73	-.82	-.18	-7.42	-3.15	-2.68	-13.25	12.30	.95
30	83	-.70	-.25	-7.20	-4.98	-1.52	-13.70	12.90	.80
31	99	-.38	-.14	-4.66	-3.33	-.95	-8.94	9.20	-.26
32	20	.33	-.06	.82	-.29	.99	1.52	-1.30	-.22
33	90	-.48	-.30	-5.36	-6.48	.78	-11.06	10.90	.16
34	110	-.55	-.15	-7.50	-3.96	-.35	-11.81	11.30	.51
35s	44	.12	-.04	.65	-.42	.76	.99	-.70	-.29
35	10	.12	.00	.15	.00	.82	.97	-.91	-.06
36	16	.23	-.06	.46	-.23	.61	.84	-.85	.01
38	48	.10	.00	.60	.00	.35	.95	-.85	-.10
39	22	.26	-.02	.71	-.11	.78	1.38	-1.35	-.03
40	20	.23	-.04	.57	-.19	.70	1.08	-1.14	.06
41	42	.16	-.01	.83	-.10	.51	1.24	-1.23	-.01
42	70	.15	-.01	1.30	-.17	.26	1.39	-1.92	-.53
43	65	-.83	-.17	-6.69	-2.65	-.63	-9.97	10.80	-.63
44	71	-.85	-.07	-7.48	-1.19	-1.35	-10.02	9.70	.32
45	70	-.20	-.03	-1.74	-.50	.66	-1.58	1.40	.18
46	66	-.13	-.04	1.06	-.63	1.34	1.77	-1.40	-.37
48s	38	-.77	-.34	-3.63	-3.10	-1.54	-8.27	7.00	1.27
48	91	-.51	-.11	-5.75	-2.40	-1.01	-9.16	8.10	1.06
49	82	-.76	-.15	-7.73	-2.95	-1.67	-12.35	12.90	-.55
50	81	-.90	-.13	-9.04	-2.53	-1.33	-12.90	12.80	.10
51	82	-.87	-.13	-8.81	-2.56	-.52	-9.89	8.80	1.09
52	55	-1.25	-.19	-8.52	-2.51	-.68	-11.71	11.00	.71
53	21	.43	-.03	1.12	-.15	.98	1.95	-1.50	-.45
54	46	.17	.00	.97	.00	.67	1.64	-1.70	-.06
55	69	.15	.00	1.28	.00	.55	1.83	-1.50	-.33
56	56	.10	.04	.69	-.54	.64	1.87	-1.40	-.47
57	85	-.13	-.02	-1.37	-.41	.34	-1.44	1.30	.14
59	26	.26	-.01	.84	-.06	.58	1.36	-1.40	.04
60	54	.17	-.01	1.14	-.13	.52	1.53	-1.40	-.13
61	96	-.70	-.08	-8.33	-1.84	-1.21	-11.38	11.90	-.52
62	63	-.37	-.17	-2.89	-2.57	-.60	-6.06	7.20	-1.14
63	3	.83	.47	.31	.34	.95	1.60	-1.10	-.50
64	3	.43	.18	.16	.13	.96	1.25	-.50	-.75

Table 9.2. Heat budget data collected by the Texas A&amp;M Research Foundation

Gas	$q_c$	$q_e$	$q_s$	$R_n$
Release No.	cal/cm <sup>2</sup> min	cal/cm <sup>2</sup> min	cal/cm <sup>2</sup> min	cal/cm <sup>2</sup> min
2	-.048	-.139	.004	.174
7	-.430	-.257	-.095	.768
8	-.205	-.155	.014	.342
9	-.331	-.278	-.071	.684
10	-.382	-.107	-.003	.768
15	-.208	-.052	-.067	.300
16	-.322	-.139	-.143	.600
19	-.326	-.105	-.065	.486
20	-.692	-.080	-.086	.822
21	.053	-.010	.017	-.054
22	.092	-.024	.013	.372
25	-.131	-.235	.002	.756
26	-.370	-.341	-.064	.738
27	-.445	-.189	-.161	.774
30	-.432	-.299	-.091	.552
31	-.280	-.200	-.057	.678
32	.049	-.017	.059	-.078
33	-.322	-.389	.047	.654
34	-.450	-.238	-.021	.678
35s	.039	-.025	.046	-.042
35	.009	.000	.049	-.055
36	.028	-.014	.037	-.051
38	.036	.000	.021	-.051
39	.043	-.007	.047	-.031
40	.034	-.011	.042	-.068
41	.050	-.006	.031	-.074
42	.078	-.010	.016	-.115
43	-.401	-.159	-.038	.648
44	-.449	-.071	-.081	.582
45	-.104	-.030	.040	.084
46	.064	-.038	.080	-.084
48s	-.218	-.186	-.092	.420
48	-.345	-.144	-.061	.486
49	-.464	-.177	-.100	.774
50	-.542	-.152	-.080	.768
51	-.409	-.154	-.031	.528
52	-.511	-.151	-.041	.660
53	.067	-.009	.059	-.090
54	.058	.000	.040	-.102
55	.077	.032	.038	-.090
56	.041	.032	.020	-.084
57	-.082	-.025	.020	-.073
59	.050	-.004	.035	-.084
60	.068	-.008	.031	-.084
61	-.500	-.110	-.073	.714
62	-.173	-.154	-.036	.432
63	.019	.020	.057	-.066
64	.010	.008	.058	-.030

Figure 9.3 is a scatter diagram of the data of Table 9.1.

A comparison of Eq. (40) with the Thornthwaite-Holzman evaporation formula shows that the latter relation differs from the former by a constant factor. The equations are, respectively,

$$q_{1e} = \sigma/3\nu \Delta u \rho' \quad (46)$$

$$q_{2e} = (pk^2 \Delta u \Delta h)/(\ln 2)^2 \quad (47)$$

where  $\Delta h$  is the difference in specific humidity between elevations  $z$  and  $2z$ , and all other symbols have the meanings previously used. Replacing  $h$  in Eq. (47) by the ratio of absolute humidity to air density

$$q_{1e}/q_{2e} = \sigma/\nu (\ln 2)^2 / 3k^2 \quad (48)$$

That is,

$$q_{1e} \doteq \sigma/\nu q_{2e} \quad (49)$$

At 20°C, the ratio of  $\sigma/\nu$  is equal to 1.6 or

$$q_{1e} \doteq 1.6 q_{2e} \quad (50)$$

Hence, the evaporation amount and the flux of latent heat, as computed by the developments in this paper, are approximately 50 percent greater than the corresponding values obtained by the Thornthwaite-Holzman equation.

The sensible heat flux, according to the developments of this paper, also differs from the usual computations based on equivalence of the eddy conduction of heat and momentum by approximately 50 percent. That is,

$$q_{lh} = K_H c_p \rho d\theta/dz \quad (51)$$

where  $K_H$  is the eddy coefficient for heat. Assuming that  $K_m = K_H = ku_* z$ , where the subscript  $m$  refers to momentum, then

$$q_{lh} = ku_* z c_p \rho d\theta/dz \quad (52)$$

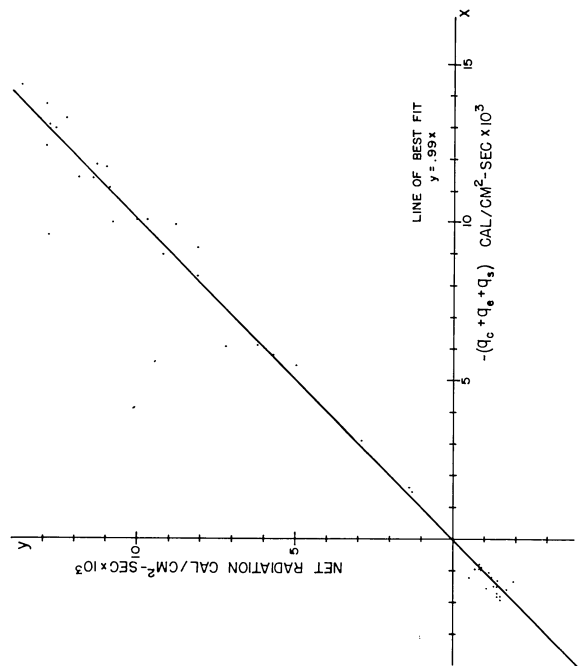


Figure 9.3 Net radiation vs. summation of heat fluxes, O'Neill, Nebraska, Summer of 1956,  $K_M \neq K_H \neq K_W$

Comparing this with Eq. (29)

$$q_{2h} = \nu_c \tau(z/\delta) \rho c_p d\theta/dz$$

and using Eq. (20) to evaluate  $ku_*$ ,

$$q_{lh}/q_{2h} = \nu/\nu_c = K_m/K_H, \quad (53)$$

which is the Prandtl number for air (.711). Hence,

$$q_{2h} = 1.4 q_{lh}, \quad (54)$$

or, as noted above, the sensible heat flux based on the reasoning of this paper is approximately one and one-half times the flux computations based on equivalence of the Austauch values for heat and momentum. Figure 9.4 is a scatter diagram of the O'Neill data based on the latter concept.

The supposition that the exchange coefficients for heat and momentum are equal or nearly so probably dates from the Reynolds' analogy, that is,

$$\tau/\rho = (\nu + K) du/dz = K_m du/dz \quad (55)$$

and

$$-q/c_p \rho = (\nu_c + K) d\theta/dz = K_H d\theta/dz. \quad (56)$$

Assuming that  $\nu$  and  $\nu_c$  represent insignificant contributions to the coefficients,  $K_H$  and  $K_m$  should be nearly equal.

The development used in this paper is equivalent to the postulate that

$$\tau/\rho = K du/dz = K_m du/dz, \quad (57)$$

and

$$-q/\rho c_p = \nu_c K d\theta/dz = K_H d\theta/dz, \quad (58)$$

hence, using Eqs. (9) and (29),

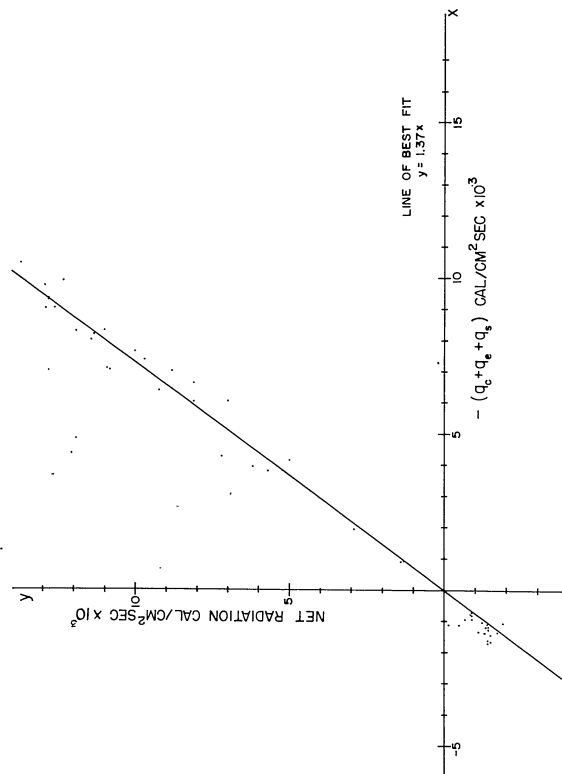


Figure 9.4 Net radiation vs summation of heat fluxes, O'Neill, Nebraska, Summer of 1956,  $K_M = K_H = K_W$

$$K_m/K_H = \nu/\nu_c. \quad (59)$$

It is not intended to imply that the equivalence of the eddy coefficients for momentum and heat has been universally accepted in the past. Swinbank<sup>6</sup> from experiments conducted in Australia says "... there is a certain notable consistency about the manner in which  $K_H$  exceeds  $K_m$  ... Not only is this order of the coefficients maintained from one occasion to another, but also, broadly, the proportionality among them." From five measurements of  $K_m$  and  $K_H$ , his average ratio is

$$K_H/K_m = 1.8, \quad (60)$$

which is certainly of the magnitude of the ratio of  $\nu_c$  to  $\nu$ .

Data obtained by Rider<sup>4</sup> at Cardington, England, also supports this value of the ratio of  $K_m$  and  $K_H$ , although Rider did not interpret the results as support for the non-equivalence of the two coefficients. From averaging of nine evaluations of  $K_H$  and  $K_m$  (at 75 centimeters) from observed energy balance computations, Rider finds as an average ratio

$$K_m/K_H = .70.$$

While this value is indeed near unity, it is remarkably near the Prandtl number (.711) for air.

While detailed profiles of wind, temperature, and humidity have been utilized in verifying the turbulent transfer equations, the equations themselves require measurements at only two levels. Since measurement of a detailed profile requires a large number of highly accurate instruments and a comparable amount of technical time and attention, it would seem important to determine the degree of accuracy with which the various terms in the energy budget would have balanced had only two levels been available. Further, the data available should be sufficient to determine the optimum levels at which measurements could have been made.

The matter of optimum levels must require a compromise which will minimize three possible sources of error. First, the lowest level needs to be far enough above the surface that irregularities in that surface do not cause an appreciable uncertainty in determining the height of that level. Second, the difference in height between the two levels needs to be sufficiently great (in terms of doubled levels) so that errors caused by instrument inaccuracies and sampling errors are not too great. Third, the top level needs to be as low as possible so as to avoid the effect of buoyancy.

To study the combined effect of these three error sources, the data of the previous section have been treated in the following way. Values of  $\Delta u$ ,  $\Delta \theta$ , and  $\Delta e$  have been obtained from the 21 pairs of levels; 25 to 50 cm, 25 to 100 cm, 25 to 200 cm, 25 to 400 cm, 25 to 800 cm, 25 to 1600 cm, 50 to 100 cm, 50 to 200 cm, 50 to 400 cm, 50 to 800 cm, 50 to 1600 cm, 100 to 200 cm, 100 to 400 cm, 100 to 800 cm, 100 to 1600 cm, 200 to 400 cm, 200 to 800 cm, 200 to 1600 cm, 400 to 800 cm, 400 to 1600 cm, and 800 to 1600 cm. The number of  $\Delta u$ 's,  $\Delta \theta$ 's and  $\Delta e$ 's, obtained in this manner (per pair of levels) that fall within 10 percent of the corresponding profile determinations are shown in Table 9.3.

As can be seen from this table, the levels at 25 and 100 cm appear to give the most satisfactory representation of the entire profiles. This is further substantiated by Table 9.4 which lists the best fit equations and average error for the four best level pairs, as well as that obtained from use of the profiles to determine  $\Delta u$ ,  $\Delta \theta$ , and  $\Delta e$ .

#### 9.7 Conclusion

The method developed in this paper appears to be satisfactory for calculating the turbulent transport of sensible and latent heat over the range of conditions represented by the data available.

However, since it differs from earlier methods by approximately 50 percent and since the test data are restricted to a summer season with exclusively southerly winds, it would appear desirable that it be tested further, preferably by other workers in the field.

Table 9.3. Percentage of double-level values within 10 percent of profile values

Level Pair (cm)	$\Delta u$ cm/sec	$\Delta \theta$ °C	$\Delta e$ mb	%	Level Pair (cm)	$\Delta u$ cm/sec	$\Delta \theta$ °C	$\Delta e$ mb	%
25-50	17	19	19	38	100-200	15	12	10	26
25-100	25	25	18	47	100-400	15	14	8	26
25-200	28	20	17	45	100-800	8	8	15	22
25-400	24	18	11	37	100-1600	7	8	12	19
25-800	12	17	11	28	200-400	12	9	9	21
25-1600	12	15	15	29	200-800	6	10	12	19
50-100	18	13	8	27	200-1600	3	6	14	16
50-200	17	13	13	30	400-800	4	5	6	10
50-400	19	17	11	33	400-1600	4	4	6	10
50-800	10	11	12	23	800-1600	4	3	6	9
50-1600	9	8	8	17					

Table 9.4. Statistical analysis of heat budget balance

Method	Line of Best Fit*	Average Error (cal/cm <sup>2</sup> sec)	Levels Employed
CLASSICAL	y = 1.37X	$1.60 \times 10^{-3}$	Profiles
DISTORTED AREA	y = .92X	$1.14 \times 10^{-3}$	25-50 cm
DISTORTED AREA	y = 1.0 X	$1.06 \times 10^{-3}$	25-100 cm
DISTORTED AREA	y = 1.0 X	$1.25 \times 10^{-3}$	25-200 cm
DISTORTED AREA	y = 1.0 X	$1.40 \times 10^{-3}$	25-400 cm
DISTORTED AREA	y = .99X	$.43 \times 10^{-3}$	Profiles

\*Line of regression

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CHAPTER 10  
HEAT BUDGET DETERMINATIONS MADE BY THE  
UNIVERSITY OF WISCONSIN GROUP

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#### 10.1 Instrumentation

The instrumentation used in heat budget determinations during Project Prairie Grass was, with two exceptions, the same as that used by the University of Wisconsin during the Great Plains Turbulence Field Program in 1953.<sup>1</sup> The exceptions are as follows:

a. In 1953 the thermocouples in the psychrometers were wired to give the dry bulb temperature difference and the difference in the wet bulb depressions. During these experiments the thermocouples were wired to give the dry bulb temperature difference and the wet bulb temperature difference so that the vapor pressure difference is given by the relation

$$\Delta e = (K + k) \Delta T_w - k \Delta T_d \quad (1)$$

where  $k$  is the psychrometric constant and  $K$  is the slope of the vapor pressure vs. temperature curve at the mean wet bulb temperature.

Every 10 minutes the positions of the two psychrometers were reversed but the connection to the recorder was not. This has the effect of doubling the sensitivity and yet eliminating dead zone and zero errors. Therefore, the vapor pressure and temperature gradients obtained during the Prairie Grass experiments are more accurate than those obtained in 1953. This is especially true during those times that the gradient is small.

b. Soil heat flow was obtained by measuring the change in the heat content of the layer 0-5 cm and the heat flux through the -5 cm

level. The change in mean temperature of the 0-5 cm layer was measured using 12 space-integrating thermometers similar to those used in 1953. Instead of a manual balancing of a Wheatstone bridge, the out-of-balance current was recorded on the 12-point Brown recorder. The out-of-balance current depends on battery voltage as well as resistance; however, the former was held constant by employing mercury alkaline batteries. The heat flow through the -5 cm layer was measured using 5 heat flux plates connected in series. The soil term  $G$  listed in the tables in Section 10.2 is the sum of the change in the heat content of the layer 0 to -5 cm and the heat flux through the -5 cm level.

#### 10.2 Heat Budget Data

The heat budget values listed in Table 10.1 are 20-minute averages centered, in each case, on the period of gas release. Estimated values are shown in parentheses. Missing values, due to instrument failure, are denoted by dashes. Positive signs indicate fluxes toward the air-earth interface; negative signs indicate fluxes away from the interface.

Table 10.1 Heat budget data\* collected by the University of Wisconsin

Gas Release Number	Date	Time (CST)	I	R <sub>N</sub>	L	E	G
3	7/5	2200		-10			
4	7/6	0100		-10			
5	7/6	1400	1.30	1.08			
6	7/6	1700	.73	.50			
7	7/10	1400	1.35	.82	-.39	-.26	-.12
8	7/10	1700	.75	.36	-.23	-.12	.01
9	7/11	1000	1.06	.61	-.30	-.18	-.13
10	7/11	1200	1.23	.76	-.38	-.24	-.14
11	7/14	0800	.72	.39	-.21	-.12	-.05
12	7/14	1000	1.15	.73	-.38	-.21	-.14
13	7/22	2000	.03	-.08	.01	0	.06
14	7/22	2200	0	-.07	.01	.01	.05
15	7/23	0800	.70	.38	-.19	-.08	-.10
16	7/23	1000	1.15	.70	-.36	-.18	-.16
17	7/23	2000	.05	-.06	0	.01	.05
18	7/23	2200	0	-.09	--	--	.04
19	7/25	1100	1.10	.69	-.40	-.16	-.14
20	7/25	1300	1.30	.85	-.52	-.26	-.06
21	7/25	2200	0	-.05	.02	.01	.02
22	7/26	0000	0	-.07	.02	.01	.05
23	7/29	2100	0	-.09	.04	.02	.02
24	7/29	2300	0	-.08	.03	.02	.02
25	8/1	1300	.72	.46	-.19	-.23	-.04
26	8/2	1200	.86	.61	-.20	-.33	-.08
27	8/2	1400	.97	.64	-.19	-.37	-.08
28	8/3	0000	0	-.09	--	--	--
29	8/3	0200	0	-.06	--	--	.01
30	8/3	1300	1.22	.84	-.34	-.39	-.10
31	8/3	1500	.89	.58	-.25	-.31	-.03
32	8/6	2000	.02	(-.09)	--	--	.04
33	8/7	1300	1.09	.83	-.39	-.35	-.08
34	8/7	1500	1.10	.84	-.44	-.36	-.05
35	8/11	2130	0	-.06	.02	.01	.03
36	8/11	2330	0	-.07	.01	0	.05
37	8/12	0300	0	-.05	--	--	.02
38	8/12	0500	.01	-.07	--	--	.02
39	8/13	2230	0	0	-.01	-.02	.03
40	8/14	0030	0	-.01	-.01	-.02	.04
41	8/14	0300	0	-.01	-.01	-.01	.02
42	8/14	0500	0	0	-.01	-.01	.02

Table 10.1 Heat budget data\* collected by the University of Wisconsin (cont)

Gas Release Number	Date	Time (CST)	I	R <sub>N</sub>	L	E	G
43	8/15	1200	1.11	.93	--	--	--
44	8/15	1400	1.13	.93	--	--	--
45	8/15	1200	.41	.25	--	--	--
46	8/15	1845	.05	-.03	--	--	.04
47	8/20	1000	.85	.45	-.21	-.14	-.11
48	8/21	0900	.39	.21	-.11	-.05	-.04

\* All heat budget entries are in langley's per minute.  
 I represents insolation  
 R<sub>N</sub> represents net radiation  
 L represents convective heat transfer  
 E represents evaporation  
 G represents soil heat transfer

( ) denotes estimated value  
 -- denotes missing data due to instrument failure

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CHAPTER 11  
OPTICAL MEASUREMENTS OF LAPSE RATE

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11.1 Introduction

Detailed and very accurate observations of temperature structure in the lowest 50 cm of the atmosphere have been made above a cold water surface by an optical method.<sup>1</sup> These observations reveal a minor anomaly in the temperature profile at a height of about 10 cm of air (equivalent to an optical path length of  $10^{-4}$  gm cm<sup>-2</sup> of water vapor) which is consistent with simple numerical calculations based on extrapolated radiative absorption coefficients for water vapor. At this height above a cold surface, the air cools by radiation at several degrees Centigrade per hour; and, this cooling is reflected in the observed anomaly in the temperature profile.

Optical observations were incorporated in Project Prairie Grass to determine the detailed temperature structure above a warm land surface. The method used was essentially that described in reference 1, but certain modifications in detailed technique were necessary. The instrument used was a field artillery range finder operated in the vertical position. In lapse conditions the two light paths from instrument to target diverge from their respective straight-line directions as shown in Figure 11.1, whereas in inversions the light paths converge from their respective straight-line directions. The instrument is mechanically

\* Personnel of the Texas A&M Research Foundation, under the direction of Professor Maurice Halstead, constructed the optical targets and made the time series observations. Max Scoggins, General Electric Company, Richland, Washington, helped in installation of the equipment and in making the profile observations.

limited to measuring converging angles; consequently, in lapse conditions it was necessary to use targets separated by a vertical distance less than the separation of the lenses. The separation used in lapse conditions was 90 or 95 cm, whereas the separation of lenses is 100 cm. For this reason, in lapse conditions the upper path sloped slightly with respect to the lower path, but not enough to affect the measurements appreciably. From Figure 11.1 and Eq. (1) of reference 1, it follows that

$$h_1' = \frac{h_1 x'}{x} = \frac{xx'(n-1)}{2nT} \left[ \frac{g}{R} + \left( \frac{\partial T}{\partial z} \right)_1 \right] \quad (1)$$

$$h_2' = \frac{h_2 x'}{x} = \frac{xx'(n-1)}{2nT} \left[ \frac{g}{R} + \left( \frac{\partial T}{\partial z} \right)_2 \right] \quad (2)$$

where  $n$  represents index of refraction for air;  $T$ , absolute temperature;  $z$ , height coordinate;  $x$ , horizontal distance between instrument and target; and  $x'$ , apparent distance to point of convergence of tangent lines (instrumental reading). Also, Figure 11.1 shows that

$$h_2' - h_1' = (Z-L) \frac{x'}{x} - Z \quad (3)$$

where  $L$  represents the vertical separation at the target lines and  $Z$  the vertical separation of the lenses. Substitution of Eqs. (1) and (2) in Eq. (3) gives

$$\left( \frac{\partial T}{\partial z} \right)_2 - \left( \frac{\partial T}{\partial z} \right)_1 = \frac{2nT}{x(n-1)} \left[ \frac{Z-L}{x} - \frac{Z}{x'} \right] \quad (4)$$

For  $L = Z$ , Eq. (4) reduces to Eq. (5) of reference 1. Nine targets, each consisting of two (or more) horizontal black lines on white backgrounds were mounted at varying distances from the instrument. The black lines are indicated as target lines in Figure 11.1. Flashlight bulbs were installed at a vertical separation of 100 cm for night observations. Heights of the lower black line, equal to height of the lower lens, were chosen as

indicated in the accompanying data. In order to minimize effects of inhomogeneities in terrain, targets were placed as close as was feasible to a radial line running outward from the instrument. For the first 50 yards the land was extremely flat, the main obstructions to vision being small tufts of grass. On July 11, the grass was cut to lawn height along the light path out to about 100 yards permitting observations at a mean height of about 6 cm above the soil. Between 50 and 300 yards the land was flat except for a few areas of small scale roughness. Between 300 and 500 yards a ridge in the terrain may have influenced the 500 yard (50 cm) readings. However, the portion of the light path near the target is less important than the portion near the lenses, so that the effect of inhomogeneous terrain probably was small compared with the effect of variations in time.

#### 11.2 Observations

The differences in lapse rates at the heights of the upper and lower lenses computed from Eq. (1) are tabulated in Tables 11.1, 11.2, and 11.3. Five of the nine profiles are shown in Figure 11.2. On July 10 at 1715 CST, prior to grass cutting, the anomaly was unmistakable at about 16 cm. On July 11 and 12, after the grass was cut, the anomaly was present at a height of about 12 cm; but the height of the anomaly above the effective radiating surface was comparable to the earlier observations.

In order to develop the temperature profile from the differences in lapse rate, the lapse rate at one height must be known. The lapse rate at 150 cm was approximated by extrapolating the curves of the type shown in Figure 11.2 linearly to 150 cm and assuming that this value represents the lapse rate at this height. Although this assumption may be grossly in error, the lapse rate is in any case small enough in magnitude at this height that subsequent calculations are not significantly affected. Numerical integration then gives the temperature profiles shown in Figure 11.3. The anomaly is evident on all but the inversion profile, and in this case the data reveal a slight anomaly at about 25 cm height.

A time series of observations at 12 cm (50 yard range) was made on 25 July, 26 July, and 2 August. On 2 August four observations were taken during each 5 minutes for 25 minutes out of each hour between 1155 and 1620 CST. These data are tabulated and are shown in Figure 11.4. They show that the variations encountered in 25 minutes are as large as one-fourth to one-half of the difference on lapse rate, itself. It must be concluded that the profiles shown in Figures 11.2 and 11.3 are subject to error from time variation in lapse rate. However, the reality of the anomaly is not in doubt because the anomaly appeared consistently and because the anomaly in lapse rate exceeds the variation in time by roughly an order of magnitude.

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Table 11.1 Values of  $\Delta(\theta T/\theta z)$  Found by Optical Method\*

Lower Lens Height (cm)	Distance (yd)	$\Delta(\theta T/\theta z)$						
		("C/cm)						
		1715 10 July	1110 11 July	1845 11 July	2155 11 July	1130 12 July	1550 12 July	2135 12 July
100	500	+.006						
50	500							
50	300	.015	-.021 to .024	+.005	-.008	.00	+.011	-.110
30	200	.025	.040 to .049	.011	.00	+.050	.017	-.600 to +.004
20	125	.041	.059 to .069	.024	.00	.074 to .090	.029	+.007
.18	75	.060						
17	50	.076						
15	75		.073 to .082	.042	-.025	.110	.040	+.018
14	50	.013						
12	50		.120 to .159	.050	-.048	.170	.045	-.380
12	20	.462						
10	30		.121	.00	-.066	.105	.016	.00
8	25			.027	-.080	.399	.096	-1.20
6	20		1.29	.096	-.092	.438	.204	-.48 to -2.1

Table 11.2 Values of  $\Delta(\theta T/\theta z)$  Found by Optical Method\*

Date	Time (CST)	Lower Lens Height (cm)	Distance (yd)	$\Delta(\theta T/\theta z)$ ("C/cm)
21 July	1300	6	20	+.280
	1309	12	50	.100
	1425	12	50	.255
23 July	0800	12	50	.073
	0803	6	20	.261
	0905	8	25	.140
	0808	10	30	.098
	0810	12	50	.110
	0811	15	75	.064
	0815	20	125	.050
	0819	30	200	.034
	0822	50	300	.020
	0905	8	25	.200
	0909	10	30	.160
	0913	12	50	.127
	0917	15	75	.098
	0921	20	125	.064
	0925	30	200	.047
	0955	12	50	.145
	1007	12	50	.138
1015	12	50	.174	
1200	12	50	.150	
1210	12	50	.188	
1355-1400	1355	12	50	.158, .171, .171, .176, .200
	1510	12	50	.160, .160, .135
	1555	12	50	.130, .138, .128
	1655	12	50	.105, .097, .103
	1755	12	50	.063, .065, .058
31 July	1130	6	20	.200

Table 11.3 Time Series of  $\Delta(\theta T/\theta z)$  at Height of 12 cm

Date	Time (CST)	$\Delta(\theta T/\theta z)$ (C/cm)	Date	Time (CST)	$\Delta(\theta T/\theta z)$ (C/cm)	Date	Time (CST)	$\Delta(\theta T/\theta z)$ (C/cm)
24 July	0655	.005, .002, .002	24 July	0215	.097, .104, .120	25 July	1315	.135, .143, .140
0655	.015, .022, .015	2358	.133, .146, .150	1415	.120, .117, .115	1415	.120, .117, .115	
0715	.095, .095, .098	0100	.107, .126, .088	1515	.123, .117, .115	1515	.123, .117, .115	
0915	.073, .071, .071	0115	.127, .137, .140	1615	.094, .102, .095	1615	.094, .102, .095	
0915	.073, .071, .071	0215	.197, .193, .222, .257	1655	.088, .080, .086	1655	.088, .080, .086	
0955	.107, .112, .109	0255	.140, .136, .142, .126	1755	.046, .048, .039	1755	.046, .048, .039	
1015	.097, .097, .104	0315	.164, .164, .168	1815	.053, .055, .058	1815	.053, .055, .058	
1055	.106, .106, .104	0335	.172, .171, .175, .032	1855	.035, .037, .038	1855	.035, .037, .038	
1115	.118, .119, .120	0455*	.165, .097, .089, .094	1917	.017, .021, .021	1917	.017, .021, .021	
1215	.132, .132, .134	0515	.094, .014, .002	1955*	.079, .076, .069, .072	1955*	.079, .076, .069, .072	
1315	.144, .140, .156	0555	.000, .004, .006	2054	.007, .002, .001, .009	2054	.007, .002, .001, .009	
1415	.144, .142, .142	0655	.063, .062, .061	2155	.080, .105, .081, .066	2155	.080, .105, .081, .066	
1455	.164, .146, .130	0715	.079, .074, .063	2255	.113, .093, .097, .111	2255	.113, .093, .097, .111	
1515	.125, .168, .148	0755	.066, .065, .067	2315	.112, .143, .083, .083	2315	.112, .143, .083, .083	
1555	.119, .117, .121	0815	.074, .069, .069	0215	.038, .031, .037, .047	0215	.038, .031, .037, .047	
1615	.097, .092, .102	0915	.057, .051, .055	0456	.053, .056, .057, .059	0456	.053, .056, .057, .059	
1655	.043, .060, .064	0955	.096, .082, .088	0515	.034, .032, .052, .053	0515	.034, .032, .052, .053	
1855	.011, .016, .009	1055	.124, .129, .134	0555	.047, .039, .049, .047	0555	.047, .039, .049, .047	
2055	.030, .030, .034	1155	.134, .137, .140	0655	.072, .066, .068, .069	0655	.072, .066, .068, .069	
2115	.120, .117, .120	1215	.128, .134, .134	0815	.100, .080, .102, .107	0815	.100, .080, .102, .107	
2155	.094, .102, .130	1255	.126, .123, .128	0915	.071, .071, .071	0915	.071, .071, .071	
0355	.000, .009, .000							
0555	.037, .034, .046							
0715	.060, .071, .063							
0815	.041, .045, .045							
0855	.073, .075, .068							
0915	.137, .125, .133							
0955	.100, .087, .093							

\*Observations were made at 0455 and 1955 on 25 July 1954 using both lights mounted 100 cm apart and black lines 90 cm apart. The members of each pair of lights were separated by 10 cm. The error in the measurements of the target lines was  $\pm 0.1$  cm. The error in the positioning of one of the target lights of two millimeters would result in an error of 0.1C cm<sup>-1</sup> in the lapse rate measurements. An error in positioning of this magnitude easily may have occurred, so that all nighttime observations may be in error by roughly -0.1C cm<sup>-1</sup>.

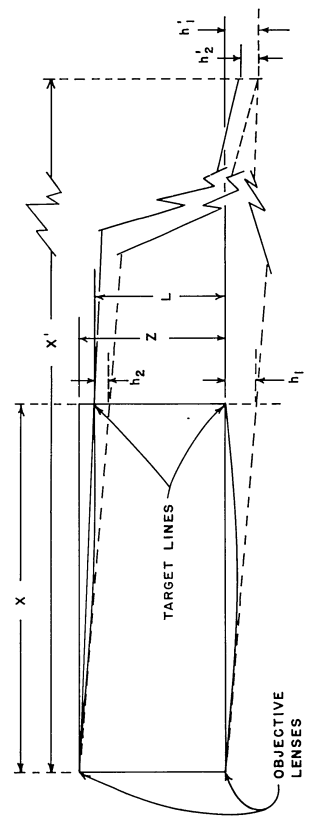


Figure 11.1 Light paths and related geometry.

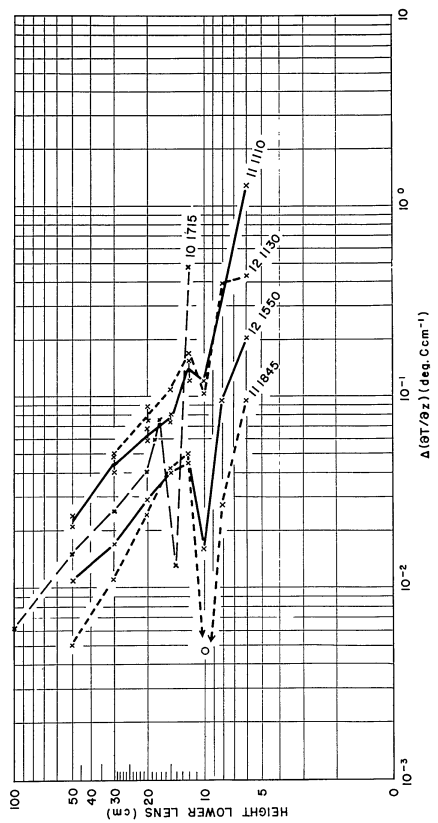


Figure 11.2 Optical observation of  $\Delta(\delta T/\delta z)$  (deg. C cm<sup>-1</sup>), O'Neill, Nebraska, 10-12 July 1956.

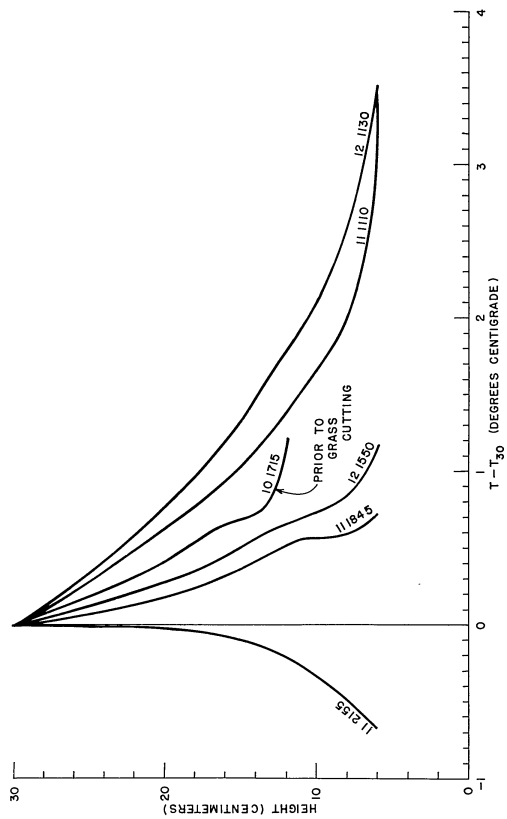


Figure 11.3 Optical temperature profiles, O'Neill, Nebraska, 10-12 July 1956.

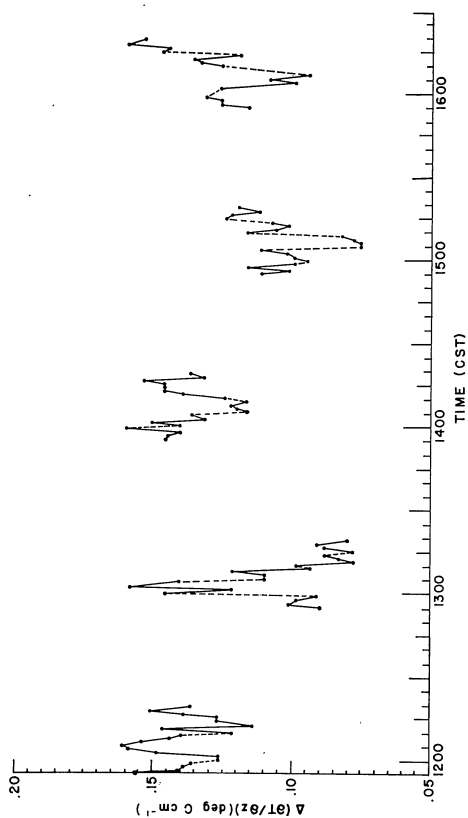


Figure 11.4 Time series of  $\Delta(\partial T/\partial z)$  at a height of 12 cm, O'Neill, Nebraska, 2 August 1956.

## CHAPTER 12 RAWINSONDE DATA

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The table in this chapter contains rawinsonde measurements made by the 6th Weather Squadron (Mobile), Tinker AFB, Oklahoma. A rawinsonde ascent was made at the test site for all gas releases except those numbered 35s and 48s. For each ascent, GMD-1A equipment was used and tabular data computed according to the instructions contained in the USWB Circular P and Air Weather Service Addenda. The computations were reviewed by an independent group using the same techniques.

Values of pressure, height, temperature and relative humidity are given for the significant and mandatory levels. The pressure is given in whole millibars, the height in meters above the ground (elevation of site above mean sea level is 603 meters), the temperature in tenths of degrees centigrade and the relative humidity in percent.

Values of the wind are given for standard heights. The height is given in meters above the ground, the direction in degrees (360 degree compass) to the nearest ten degrees, and the speed to the nearest tenth of a meter per second.

Table 12.1

Gas Release No. 1  
3 July 1956 1050C

Gas Release No. 2  
3 July 1956 1450C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
945	0	22.5	65	945	0	24.0	66
954		20.0	67	933		21.8	61
900	420	17.6	78	900	423	19.0	72
860		14.4	91	850	912	14.7	86
850	906	13.8	91	844		14.3	88
800	1416	11.1	93	800	1423	11.5	93
744		7.9	94	771		9.4	96
730		5.5	81	729		7.5	100
706		3.8	45	700	2530	5.4	100
700	2522	4.7	52	679		3.9	100
694		5.5	58	655		3.5	100
638		1.6	61	620		- 1.5	97
600	3767	1.1	70	609		- 0.0	89
				604		- 0.1	82
				600	3778		
Winds				Winds			
Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)	
SFC	02	120	1.	SFC	02	140	1.6
	350	140	2.7		370	120	2.0
	630	160	2.2		690	140	2.6
	920	180	3.0		960	170	3.1
	1200	190	3.9		1250	160	2.6
	1470	200	4.1		1550	160	2.1
	1770	190	3.5		1820	170	2.3
	2050	220	2.6		2120	190	2.2
	2320	250	3.2		2410	230	2.7
	2630	250	3.4		2710	250	3.3
	2920	230	3.2		3030	270	8.8
	3190	210	3.0		3320	280	10.6
	3470	190	2.9		3620	350	9.0
	3750	190	2.1		3900	270	10.3
	4020	190	3.2				

Table 12.1 (Continued)

Gas Release No. 3  
5 July 1956 2150C

Gas Release No. 4  
6 July 1956 0050C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
948		19.8	85	947		19.1	94
940		24.8	61	926		25.8	74
900	454	21.9	62	900	446	23.4	61
882		20.5	63	880		21.6	52
850	948	18.1	54	851	941	19.0	63
837		17.1	50	850		19.0	63
805		14.5	58	800	1459	15.6	56
800	1464	14.1	56	731		10.6	45
762		11.9	45	700	2578	8.2	44
755		9.0	60	661		4.1	42
700	2578	6.5	62	626		0.9	57
695		5.9	62	611		0.9	35
672		4.0	64	600	3831	- 0.1	36
636		0.8	54				
600	3823	- 3.1	55				
Winds				Winds			
Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)	
SFC	02	140	1	SFC	02	180	2
	250	140	3.2		360	190	5.4
	520	160	3.0		690	180	4.3
	810	180	1.9		910	170	3.8
	1080	140	1.8		1170	160	3.2
	1360	130	2.2		No Data		
	1630	190	0.6		2990	290	9.9
	1920	270	0.6		3280	290	8.1
	2220	300	4.5		3600	310	9.5
	2460	290	5.0		3850	300	10.8
	2710	280	5.2				
	2980	290	5.0				
	3230	300	5.2				
	3490	300	6.0				
	3730	280	8.2				

Table 12.1 (Continued)

Gas Release No. 5  
6 July 1956 1350C

Gas Release No. 6  
6 July 1956 1650C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
946	0	31.1	34	944	0	31.5	34
932		27.5	38	900	425	26.8	42
900	440	24.1	43	866		23.1	50
885		22.6	44	850	926		
856		22.0	33	822		20.8	39
850	938	21.5	34	800	1449	20.2	45
800	1462	17.8	47	794		15.1	38
750		11.5	67	700	2579	10.0	42
700	2591	8.4	71	660		6.0	50
660		4.9	76	600	3843	2.5	34
632		2.8	47				
600	3849	0.0	40				
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	160	4	SFC	02	170	5
	280	170	7.4		300	180	11.8
	550	170	5.8		700	180	13.4
	850	190	6.2				
	1130	200	6.2				
	1470	210	5.8				
	1800	210	5.9				
	2100	220	7.7				
	2440	220	11.0				
	2750	230	10.6				
	3050	240	9.8				
	3380	230	13.9				
	3700	230	16.0				
	4020	220	15.6				

Table 12.1 (Continued)

Gas Release No. 7  
10 July 1956 1350C

Gas Release No. 8  
10 July 1956 1650C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
946	0	31.0	30	945	0	31.6	30
938		26.8	28	930		28.9	30
904		24.5	35	900	433	25.9	35
900	439	24.1	37	850	931	20.9	42
850	935	19.5	49	837		19.4	45
800	1433	14.6	59	821		18.6	52
732		7.4	76	800	1451	16.7	55
702		5.5	61	705		8.0	66
700	2564	5.4	60	700	2571	7.3	65
666		4.1	23	674		4.5	59
655		5.1	mb	655		3.5	32
633		3.8	mb	644		4.5	21
600	3817	1.0	mb	600	3824	1.1	mb
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	190	4.1	SFC	02	190	4.1
	310	210	6.1		330	170	4.7
	670	210	5.1		690	190	5.8
	1050	210	4.7		1050	200	7.2
	1430	220	4.8		1410	220	6.4
	1780	260	3.4		1710	230	6.8
	2130	300	5.6		2100	250	8.3
	2460	310	8.5		2400	290	9.4
	2800	310	9.4		2660	310	7.8
	3130	310	9.5		2940	330	6.7
	3450	310	9.6		3200	330	8.4
	3780	300	9.5		3460	320	7.8
	4120	300	10.1		3720	320	7.1
					4000	330	7.4



Table 12.1 (Continued)

Gas Release No. 9  
11 July 1956 0950C

Gas Release No. 10  
11 July 1956 1150C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
941		27.2	52	941	0	30.8	44
930		24.9	48	925		26.5	47
900	390	22.2	52	900	394	24.4	52
890		21.4	54	850	892	19.9	63
874		23.4	57	846		19.4	64
850	888	22.4	53	832		20.5	57
803		20.5	48	800	1415	18.6	50
800	1414	20.2	47	768		16.5	43
716		12.5	35	714		10.9	56
700	2548	10.9	40	700	2545	9.7	52
635		4.4	64	663		6.1	46
600	3812	0.7	66	600	3804	0.2	65
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	180	4.6	SFC	02	220	3.6
	350	210	10.0		200	230	6.0
	680	220	8.2		580	230	5.9
	960	220	7.5		900	220	6.0
	1220	210	8.5		1220	210	8.0
	1520	210	8.8		1600	210	7.8
	1830	220	7.0		1950	220	6.8
	2120	230	7.2		2300	240	6.7
	2410	250	8.0		2570	250	7.5
	2720	260	6.0		3000	260	9.5
	3000	290	6.3		3330	270	11.2
	3240	290	8.5		3690	280	11.2
	3510	290	11.0		4070	290	13.2
	3750	290	12.1				
	4000	290	14.2				

Table 12.1 (Continued)

Gas Release No. 11  
14 July 1956 0750C

Gas Release No. 12  
14 July 1956 0950C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
944		24.5	66	944	0	30.0	48
933	0	22.4	55	936		25.0	56
902		22.8	68	900	421	22.9	67
800	417	22.9	68	896		22.5	68
850	916	21.7	48	890		23.5	64
816		20.8	34	850	920	23.1	35
800	1442	19.4	36	843		23.1	30
727		12.2	42	800	1446	19.9	30
700	2570	9.4	52	752		15.8	32
664		5.3	63	700	2577	10.3	49
624		3.4	34	648		4.4	66
600	3829	1.2	48	624		3.2	42
				604		1.4	60
				600	3836	1.1	59
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	180	4.6	SFC	02	180	3.6
	300	190	11.8		300	200	11.0
	630	210	14.7		680	200	12.8
	940	210	12.8		1030	200	12.5
	1280	210	10.0		1400	200	10.3
	1650	210	6.8		1780	210	6.5
	1960	210	4.7		2130	210	5.0
	2250	210	4.6		2470	220	4.4
	2600	230	3.5		2850	250	4.4
	2880	230	3.5		3270	280	5.2
	3350	280	6.5		3530	310	9.4
	3730	290	8.5		3850	290	9.8
	4080	300	10.6				

Table 12.1 (Continued)

Gas Release No. 13  
22 July 1956 1950C

Gas Release No. 14  
22 July 1956 2150C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
949	0	21.9	69	950	0	16.4	89
940		22.8	59	940		22.2	64
900	459	19.0	65	900	467	19.8	58
850	950	15.9	73	898		19.7	57
800	1462	11.8	82	890	957	15.7	70
747		7.1	92	882		11.5	86
700	2566	4.4	80	800	1468	11.4	85
685		3.4	76	700	2569	4.0	77
645		- 0.4	80	654		0.2	72
634		- 0.1	34	631		0.5	49
622		- 0.6	22	620		- 0.6	21
601		- 0.6	mb	600	3807	- 0.8	mb
600	3807						
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	170	1.0	SFC	02	160	1.0
	350	180	4.6		290	170	4.8
	700	180	4.6		610	180	4.5
	1020	180	5.0		960	190	3.0
	1340	180	4.0		1210	230	3.2
	1660	180	3.0		1500	260	2.9
	1960	190	1.8		1800	270	1.3
	2270	260	1.1		2100	300	2.1
	2570	310	2.9		2390	310	5.0
	2880	320	4.7		2660	310	7.5
	3200	320	6.0		2930	310	8.2
	3520	340	7.6		3210	310	7.8
	3840	340	9.3		3500	310	7.9
					3800	330	8.3

Table 12.1 (Continued)

Gas Release No. 15  
23 July 1956 0750C

Gas Release No. 16  
23 July 1956 0950C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
949		21.0	64	948	0	26.5	48
940		19.4	66	935			
924		21.1	67	900	454	20.8	60
900	458	20.8	59	850	945	16.7	69
897		20.7	58	841		15.9	70
853		17.0	66	810		14.4	33
850	948	16.8	65	800	1458	13.6	34
800	1462	13.0	48	709		10.9	38
728		7.2	19	728		7.1	59
700	2569	6.8	mb	715		6.7	50
688		6.7	mb	708		6.4	27
644		4.0	mb	700	2564	6.4	26
600	3820	0.0	mb	681		6.4	22
				658		3.9	46
				600	3812	- 0.5	37
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	230	2.1	SFC	02	180	2.1
	300	230	4.4		300	200	2.6
	600	240	2.8		610	190	2.6
	910	230	1.6		950	190	2.0
	1210	230	1.0		1300	180	1.1
	1500	260	0.9		1650	360	4.2
	1800	330	2.0		1980	010	7.3
	2090	360	4.7		2290	010	10.6
	2380	360	7.8		2600	010	12.5
	2680	350	9.5		2910	010	13.5
	2980	350	10.7		3230	010	13.2
	3290	340	10.9		3570	010	12.4
	3580	350	10.0		3880	350	10.2
	3850	350	8.9				

Table 12.1 (Continued)

Gas Release No. 17  
23 July 1956 1950C

Gas Release No. 18  
23 July 1956 2150C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
943	0	28.0	39	943	0	23.6	54
828		29.0	32	928		27.6	35
900	414	27.0	35	900	411	26.0	33
850	916	23.1	40	898		25.9	33
804		19.5	43	850	911	23.1	39
800	1441	19.1	45	841		22.8	39
700		9.8	64	800	1435	18.9	47
600	3829	- 0.7	85	700	2564	9.0	64
				684	2755	7.2	67
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	170	2.1	SFC	02	180	2.1
	310	190	9.8		300	200	13.1
	620	200	1.5		650	220	15.2
	930	220	12.5		1000	240	13.2
	1280	230	13.6		1310	260	13.6
	1620	250	12.0		1670	280	15.0
	2000	270	10.4		2000	290	14.5
	2330	310	10.8		2310	300	14.5
	2670	320	13.9				
	3010	320	15.8				
	3350	320	16.8				
	3700	320	18.1				
	4060	230	18.9				

Table 12.1 (Continued)

Gas Release No. 19  
25 July 1956 1050C

Gas Release No. 20  
25 July 1956 1250C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
945	0	28.8	38	942	0	31.0	30
932		25.8	41	917		36.6	33
900	429	22.8	47	900	406	25.1	35
878		20.5	51	870		22.0	38
850	923	20.5	26	850	904	22.3	27
823		20.8	21	838		22.5	18
800	1447	19.1	24	804		21.2	23
711		11.9	38	800	1430	20.9	24
700	2577	11.1	36	700	2565	11.5	38
678		9.5	28	687		10.6	24
600	3844	2.4	30	610		2.6	31
				600	3827	1.8	34
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	160	3.6	SFC	02	160	6.7
	320	170	6.3		360	180	12.8
	620	180	7.6		700	180	11.2
	900	180	8.8		1020	190	8.6
	1130	190	9.0		1370	200	6.8
	1380	190	6.6		1700	240	5.5
	1620	210	2.8		2050	230	5.1
	1820	220	2.0		2420	260	4.8
	2060	250	1.4		2770	270	5.7
	2230	300	2.0		3140	270	7.0
	2480	310	2.3		3380	270	7.4
	2700	300	2.4		3630	270	7.8
	2880	300	3.0		3900	290	10.0
	3000	290	4.5				
	3260	280	5.0				
	3430	250	4.0				

Table 12.1 (Continued)

Gas Release No. 21  
25 July 1956 2150C

Gas Release No. 22  
25 July 1956 2350C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
938	0	29.0	41	937	0	26.5	45
911		27.1	39	910		25.5	45
900	367	26.3	34	900	355	26.3	43
889		29.6	30	896		26.8	42
861		28.1	27	850	859	25.2	36
850	875	26.5	27	800	1990	23.4	27
844		25.5	27	749		19.0	29
806		24.8	25	700	2532	13.4	38
800	1408	24.2	26	636		5.7	50
728		16.8	35	600	3800	2.0	55
700	2557	14.0	41				
678		11.6	44				
632		4.7	59				
620	3563	3.0	70				
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	180	4.1	SFC	02	170	4.6
	150	200	8.0		300	180	20.0
	370	220	11.3		660	200	25.0
	540	220	12.3		930	210	24.6
	780	230	12.3		1220	220	25.3
	1030	250	14.4		1500	240	22.0
	1300	260	17.0		1800	260	16.0
	1630	260	14.0		2050	250	16.0
	2020	260	15.0		2360	250	18.8
	2380	265	20.8		2630	250	21.0
	2680	260	17.5		2930	250	19.5
	2950	270	9.0		3180	250	17.0
	3150	270	12.0		3450	250	17.0
	3340	260	19.5		3750	250	13.0
	3550	260	19.5		4080	270	11.4

Table 12.1 (Continued)

Gas Release No. 23  
29 July 1956 2050C

Gas Release No. 24  
29 July 1956 2250C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
944	0	23.9	70	945	0	22.2	80
900	417	21.7	78	936		22.4	80
860		19.4	84	900	424	19.9	85
850		19.5	82	897		19.7	85
838	911	19.1	90	854		20.9	75
804		17.5	76	850	919	20.9	75
800	1432	17.6	70	815		19.5	65
776		18.6	47	800	1443	18.5	69
700	2567	11.9	45	774		16.3	72
696		11.4	44	750		15.9	64
685		10.1	54	700	2576	11.1	66
614		3.9	63	684		9.6	67
600	3837	2.2	65	659		7.0	57
				600	3842	1.0	72
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	120	4.6	SFC	02	130	3.8
	290	130	13.1		290	150	13.3
	600	120	15.0		600	160	14.4
	890	090	11.5		930	190	13.7
	1190	070	11.5		1270	210	14.2
	1480	050	11.1		1620	230	12.4
	1730	020	7.8		1920	250	10.2
	2020	030	5.6		2270	260	8.1
	2290	030	4.1		2600	260	6.1
	2520	020	3.7		2910	260	5.3
	2820	010	5.3		3230	260	5.3
	3100	010	6.4		3590	270	5.7
	3360	360	6.6		3880	270	6.0
	3630	360	6.5				
	3920	360	6.0				

Table 12.1 (Continued)

Gas Release No. 25 1 Aug 1956 1257C				Gas Release No. 26 2 Aug 1956 1150C			
P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
946	0	24.7	66	942	0	30.3	56
934		22.4	70	922		25.4	64
900	436	15.7	78	900	404	22.6	70
878		18.0	84	883		22.1	73
850	927	16.6	84	850	901	20.7	70
800	1443	13.9	84	800	1424	18.4	64
700	2559	8.2	83	790		18.0	62
694		7.8	83	795		10.6	78
636		3.6	83	700	2555	10.1	79
620		3.4	79	648		5.9	85
600	3819	1.8	78	600	3822	2.4	83
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	180	2.1	SFC	02	170	3.6
	350	190	4.5		230	180	9.7
	680	200	6.1		500	190	11.2
	960	200	6.5		770	200	11.0
	1200	210	5.8		1030	200	11.5
	1450	210	5.9		1300	210	12.5
	1750	220	6.9		1590	210	13.8
	2120	220	7.3		1910	210	13.5
	2420	220	7.1		2210	210	13.5
	2720	220	9.0		2520	210	14.7
	3080	230	11.1		2820	230	16.0
	3460	220	9.3		3130	230	17.0
	3870	220	5.7		3420	230	17.0
	3990	220	5.5		3730	230	18.0
					4030	230	19.0

Table 12.1 (Continued)

Gas Release No. 27 2 Aug 1956 1350C				Gas Release No. 28 3 Aug 1956 0035C			
P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
941	0	32.2	48	940	0	25.9	66
934		29.6	52	925		28.0	59
900	398	25.5	56	900	385	26.6	55
850	898	22.0	60	892		26.1	54
813		18.5	65	878		26.6	51
800	1421	18.5	56	850	889	24.2	51
700	2551	10.5	69	810		21.0	51
668		7.7	73	800	1416	20.0	54
600	3817	2.6	72	721	2551	13.1	74
				700		11.1	78
				630		4.1	90
				600	3818	1.9	89
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	170	5.1	SFC	02	170	3.1
	280	190	9.2		300	200	13.2
	580	180	7.0		590	210	18.4
	880	180	6.5		830	210	22.2
	1200	190	12.0		1090	210	21.3
	1500	200	13.9		1320	210	20.5
	1800	210	14.0		1580	210	20.1
	2100	210	15.6		1870	220	21.5
	2420	210	17.0		2200	220	24.0
	2720	210	18.5		2490	220	20.0
	3020	220	18.5		2770	210	18.5
	3320	220	19.8		3020	210	18.5
	3820	210	19.8		3300	210	18.7
	3920	210	19.3		3550	210	18.7
					3820	210	17.0

Table 12.1 (Continued)

Gas Release No. 29  
3 Aug 1956 0150C

Gas Release No. 30  
3 Aug 1956 1250C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
941	0	25.5	61	941	0	34.6	36
928		26.6	56	932		31.6	42
900	393	25.4	54	900	401	28.7	49
893		25.1	53	850	906	23.9	56
870		25.1	48	846		23.5	57
850	895	23.8	50	800	1432	19.1	63
800	1422	20.4	54	757		14.8	70
787		19.4	55	732		14.3	60
700	2557	10.9	72	700	2564	11.5	62
668		7.5	80	630		4.8	66
601		1.9	79	607		3.7	66
600	3824	1.8	80	600	3834	3.0	66
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	180	4.3	SFC	02	180	5.1
	300	200	16.0		200	190	9.5
	620	210	20.0		580	190	11.7
	950	210	23.0		880	190	11.6
	1270	210	23.8		1190	190	8.4
	1600	220	21.0		1450	200	8.6
	1900	220	19.0		1800	200	13.4
	2210	220	19.0		2150	210	18.5
	2530	230	18.0		2480	210	18.5
	2850	220	15.5		2780	210	18.5
	3150	210	16.2		3040	210	19.0
	3470	210	17.0		3300	210	21.0
	3780	200	19.0		3560	220	20.0
	4100	200	19.0		3810	220	20.5
					4100	220	20.8

Table 12.1 (Continued)

Gas Release No. 31  
3 Aug 1956 1450C

Gas Release No. 32  
6 Aug 1956 1950C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
941	0	34.0	37	945	0	24.3	36
932		31.5	40	933		27.0	35
900	400	28.8	46	900	430	24.7	38
850	906	24.2	56	850	929	21.0	43
800	1433	19.7	66	800	1450	17.3	48
738		13.6	80	783		16.0	49
700	2565	10.5	76	770		15.0	41
617		3.5	68	758		14.4	51
600	3833	2.7	72	700	2576	9.2	60
				647		4.1	57
				600	3834	0.3	53
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	200	5.1	SFC	02	130	2.1
	320	200	9.7		300	170	11.0
	690	210	9.0		630	160	14.5
	1010	210	10.1		980	160	17.0
	1360	210	12.0		1300	150	16.0
	1690	210	12.0		1680	140	16.2
	2000	210	11.8		2030	130	16.2
	2300	210	12.9		2400	130	13.1
	2620	220	13.6		2720	140	8.8
	2930	220	15.9		3080	160	8.8
	3390	220	15.5		3470	220	9.6
	3620	220	13.5		3840	260	12.2
	3940	230	15.0				

Table 12.1 (Continued)

Gas Release No. 33  
7 Aug 1956 1258C

Gas Release No. 34  
7 Aug 1956 1456C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
944	0	28.8	48	944	0	30.5	38
900	422	24.2	49	928		26.0	46
894		23.6	49	900	422	23.6	53
864		23.3	38	868		20.7	58
850	921	22.2	40	850	918	20.3	55
800	1444	15.0	48	800	1440	18.7	42
700	2570	9.0	66	798		18.6	41
677		6.9	70	2569		10.3	48
640		5.5	51	620		3.3	55
600	3832	1.8	43	600	3833	1.0	57
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	170	4.6	SFC	02	170	4.6
	300	170	13.3		340	150	13.0
	600	170	15.2		620	150	15.4
	960	170	14.5		960	170	15.5
	1320	180	14.0		1290	180	13.8
	1700	180	8.4		1690	180	11.9
	2080	180	5.3		1930	200	11.0
	2450	150	7.2		2210	210	12.1
	2830	150	8.0		2500	220	14.1
	3170	170	7.8		2800	230	13.7
	3470	200	7.3		3050	240	12.0
	3800	230	7.3		3330	240	9.5
					3620	240	6.8
					3900	240	6.1

Table 12.1 (Continued)

Gas Release No. 35  
11 Aug 1956 2122C

Gas Release No. 36  
11 Aug 1956 2328C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
945	0	20.0	62	943	0	18.8	85
938		24.8	59	930		23.5	79
900	426			900	406	21.8	74
850	920			860		19.5	66
806		15.0	67	850	900	19.0	68
800	1436			800	1418	15.7	74
700	2549	5.4	90	738		11.3	83
682		4.9	77	700	2537	7.6	70
656		4.0	24	683		6.8	68
600	3799	1.3	mb	677		6.3	24
				650		6.0	mb
				618		3.4	24
				600	3794	1.3	30
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	170	1.6	SFC	02	180	1.6
	300	160	6.1		350	180	11.3
	630	180	7.0		600	190	10.0
	940	200	7.0		880	200	8.0
	1240	220	8.6		1170	220	7.0
	1580	240	9.8		1420	240	9.0
	1850	250	10.8		1700	250	13.0
	2250	260	11.9		2000	260	15.7
	2510	260	11.5		2300	260	15.0
	2760	260	11.4		2600	260	13.3
	3000	270	11.2		2930	270	12.0
	3260	280	13.1		3270	280	12.0
	3480	290	16.2		3580	300	13.8
	3710	300	17.8		3900	300	16.2

Table 12.1 (Continued)

Gas Release No. 37  
12 Aug 1956 0250C

Gas Release No. 38  
12 Aug 1956 0450C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
942	0	20.0	75	942	0	20.0	81
912		22.8	77	905		22.5	55
900	398	22.2	71	900	395	22.5	51
883		21.3	61	886		22.5	45
850	894	19.3	61	852		20.5	45
823		17.6	62	850		20.3	45
800	1413	16.0	66	800	1411	16.9	59
726		11.0	81	735		12.1	78
702		9.3	69	712		10.5	54
700	2538	9.0	64	700	2534	9.1	59
677		7.6	23	673		6.0	66
622		2.0	30	656		5.0	34
600	3794	- 0.1	41	633		3.5	24
				600	3787	0.2	33
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	180	3.1	SFC	02	180	3.6
	300	190	14.0		330	180	14.0
	630	190	16.8		680	190	18.3
	950	200	12.3		1020	200	12.7
	1240	220	13.4		1370	210	17.5
	1520	230	15.4		1870	230	12.5
	1830	250	14.8		1950	240	10.0
	2140	270	12.5		2300	250	8.8
	2410	270	11.2		2600	260	8.5
	2700	260	10.5		2900	240	10.0
	3000	260	8.0		3220	240	9.0
	3300	260	7.8		3480	240	10.0
	3640	260	7.4		3760	230	13.0
	3960	260	6.6		4000	230	14.6

Table 12.1 (Continued)

Gas Release No. 39  
13 Aug 1956 2220C

Gas Release No. 40  
14 Aug 1956 0020C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
948	0	20.5	41	948	0	20.6	62
937		25.4	38	940		25.5	49
930		27.4	35	932		27.6	40
900	457	25.4	30	900	457	25.1	42
886		24.6	28	850	955	21.0	48
850	955	21.9	36	805		17.0	49
800	1477	17.9	48	800	1476	16.9	50
761		14.5	56	763		15.0	56
700	2599	8.6	69	700	2598	8.4	49
680		6.4	71	676		5.8	46
637		2.5	26	628		0.1	53
600	3849	- 0.2	24	609		0.0	24
				600	3849	- 0.6	mb
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	160	2.6	SFC	02	200	2.0
	420	150	10.3		300	200	12.6
	850	170	9.0		600	210	14.2
	1200	200	9.0		900	210	13.8
	1580	230	10.3		1230	210	12.3
	2030	250	12.0		1570	230	10.2
	2460	280	13.0		1870	270	9.5
	2780	290	13.0		2160	300	9.3
	3170	300	14.0		2470	310	11.4
	3560	300	14.6		2760	320	14.0
	4000	310	16.0		3080	320	15.5
					3400	320	16.5
					3700	320	15.5
					3990	320	12.5



Table 12.1 (Continued)

Gas Release No. 41  
14 Aug 1956 0250C

Gas Release No. 42  
14 Aug 1956 0450C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
947	0	20.0	66	947	0	21.7	55
933		24.2	60	920		26.6	31
915		26.0	40	900	448	26.0	30
900	446	25.3	40	869		24.9	30
850	946	22.8	36	850	948	22.9	41
840		22.2	36	841		22.0	46
800	1470	18.9	52	800	1473	20.0	53
793		18.2	55	792		19.5	54
700	2597	9.3	59	733		12.7	67
696		8.9	59	711		11.1	53
600	3850	- 2.3	65	700	2603	10.0	52
				674		7.1	51
				614		- 0.8	73
				600	3858	- 2.0	69
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	180	3.1	SFC	02	210	4.6
	260	210	13.2		340	230	20.9
	530	220	14.2		690	230	20.6
	830	220	14.0		1020	240	16.3
	1130	240	12.2		1330	260	17.1
	1450	260	11.0		1680	260	16.5
	1780	270	10.8		2000	270	14.0
	2100	280	12.0		2330	270	12.4
	2430	290	12.8		2630	270	11.0
	2730	290	14.0		2940	280	12.0
	3050	300	14.2		3270	290	12.0
	3400	310	15.0		3590	290	14.0
	3680	310	15.0		3910	300	15.5
	4000	310	16.5				

Table 12.1 (Continued)

Gas Release No. 43  
15 Aug 1956 1150C

Gas Release No. 44  
15 Aug 1956 1350C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
945	0	34.5	24	943	0	36.8	19
931		30.4	26	930		31.9	22
900	436	27.6	30	900	418	29.1	25
850	937	22.9	35	874		26.8	27
846		22.4	36	850	922	24.5	30
832		23.3	18	806		20.6	35
800	1462	20.1	24	800	1448	20.1	37
762		17.2	49	746		16.5	52
746		16.1	41	718		13.3	54
705		12.0	56	700	2585	11.8	43
700	2598	11.8	53	695		11.6	40
685		10.7	47	658		8.5	37
630		4.2	53	600	3853	1.2	64
600	3863	0.0	69				
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	160	1.5	SFC	02	150	4.1
	280	160	5.0		260	150	6.0
	570	150	4.2		570	150	8.5
	750	140	5.0		880	160	9.2
	1130	150	5.8		1210	170	8.3
	1430	200	4.4		1550	200	7.7
	1720	220	5.7		1920	230	8.4
	2050	250	7.0		2300	250	10.2
	2390	260	8.7		2650	250	11.9
	2700	260	9.8		3000	240	11.5
	3000	260	10.7		3380	240	10.2
	3300	260	11.2		3720	250	9.2
	3600	260	11.2		4080	250	10.1
	3910	260	11.2				

Table 12.1 (Continued)

Gas Release No. 45  
15 Aug 1956 1658C

Gas Release No. 46  
15 Aug 1956 1835C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
940	0	36.5	21	939	0	33.5	24
930		33.6	22	919		33.2	22
900	392	31.0	26	900	379	31.6	26
862		27.8	30	850	898	26.9	34
850	899	26.6	31	842		26.0	37
800	1429	22.0	40	800	1420	22.3	41
700	2569	12.0	59	778		20.4	44
600	3839	2.6	77	700	2564	12.9	62
				687		11.6	65
				656		7.6	63
				600	3834	1.9	71
Winds				Winds			
	Z (m)	ddd (deg)	fff (m/sec)		Z (m)	ddd (deg)	fff (m/sec)
SFC	02	160	4.1	SFC	02	140	4.6
	310	160	7.4		300	140	11.2
	620	160	9.0		600	140	12.7
	960	160	9.2		900	150	12.3
	1300	170	9.5		1210	180	13.5
	1610	190	9.6		1570	190	12.9
	1970	210	8.5		1890	210	14.0
	2180	230	9.5		2210	220	14.0
	2470	230	12.0		2500	230	14.6
	2760	240	12.0		2910	240	14.0
	3020	240	11.3		3240	240	13.6
	3290	240	11.2		3570	250	13.6
	3550	240	13.5		3880	260	13.0
	3800	250	13.5				
	4000	260	13.0				

Table 12.1 (Continued)

Gas Release No. 47  
20 Aug 1956 1005C

Gas Release No. 48  
21 Aug 1956 0850C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
955	0	19.0	50	947	0	18.8	59
945		16.5	40	930		15.8	63
900	502	13.1	51	900	433	13.5	69
850	979	9.1	63	868		14.5	62
842		8.4	65	850	915	12.3	48
800	1477	4.9	60	849		12.3	48
754		0.9	56	824		10.5	51
729		- 0.4	75	812		10.9	22
706		- 1.8	43	800	1420	11.8	mb
700		- 1.1	39	792		12.3	mb
694	2550	- 0.5	34	756		11.6	mb
686		- 3.1	24	716		8.5	mb
645		- 3.3	mb	700	2532	8.0	mb
600	3768	- 6.5	mb	686		7.7	mb
				610		1.6	mb
				600	3787	0.5	mb
Winds				Winds			
	Z (m)	ddd (deg)	fff (m/sec)		Z (m)	ddd (deg)	fff (m/sec)
SFC	02	250	3.1	SFC	02	180	5.7
	320	230	3.7		330	210	9.0
	690	250	2.5		680	230	10.8
	1050	260	0.8		1030	240	12.3
	1420	010	2.7		1400	250	11.0
	1800	350	2.8		1730	260	9.7
	2150	320	3.9		2050	260	9.0
	2530	320	6.5		2360	290	11.2
	2900	340	8.9		2700	290	14.0
	3270	340	9.5		3050	290	16.0
	3620	340	10.0		3400	290	16.5
	3990	340	11.4		3710	300	16.8
					4030	300	16.0

Table 12.1 (Continued)

Gas Release No. 49  
21 Aug 1956 1050C

Gas Release No. 50  
21 Aug 1956 1350C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
946	0	23.8	44	943	0	29.0	38
912		17.1	44	937		25.7	40
900	430	16.5	48	900	408	22.3	48
874		14.8	54	895		21.9	49
860		15.3	54	850	901	19.0	40
850	914	14.8	56	820		17.4	35
800	1424	11.2	65	800	1417	13.3	37
796		11.0	66	793		11.9	20
782		9.6	20	764		8.8	mb
767		11.8	mb	742	2533	8.8	mb
723		8.8	mb	700	3790	0.9	mb
715		9.8	mb	600			
700	2533	8.6	mb				
608		1.4	mb				
600	3788	0.5	mb				
Winds				Winds			
Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)	
SFC	02	180	5.7	SFC	02	200	5.1
	330	210	7.8		230	200	8.0
	700	230	10.3		480	220	8.0
	1050	250	12.2		700	240	7.6
	1400	260	13.8		850	250	9.7
	1750	260	13.3		1200	270	11.0
	2120	270	13.2		1480	280	11.0
	2480	280	13.2		1750	290	12.0
	2800	290	14.5		2010	300	13.5
	3130	290	15.3		2290	300	15.0
	3480	290	16.5		2590	300	14.8
	3800	290	17.5		2870	300	13.5
					3110	300	16.0
					3320	300	17.5
					3520	300	18.5
					3910	300	17.0

Table 12.1 (Continued)

Gas Release No. 51  
21 Aug 1956 1520C

Gas Release No. 52  
24 Aug 1956 1105C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
942	0	31.0	33	952	0	25.0	22
932		26.7	36	932		20.7	29
900	403	23.9	41	900	485	18.2	38
850	899	18.4	50	850	971	14.1	39
818		16.4	57	848		13.9	39
800	1417	14.6	60	800	1482	13.3	49
770		11.6	66	793		13.1	50
733		8.3	54	740		8.5	60
722		8.3	22	713		8.9	25
700	2530	7.6	mb	700	2593	7.4	42
695		7.5	mb	688		6.5	30
600	3784	0.8	mb	676		5.5	41
				600	3842	-2.7	56
Winds				Winds			
Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)	
SFC	02	240	4.6	SFC	02	140	3.1
	320	240	9.5		400	110	6.1
	680	250	13.0		760	110	5.0
	1010	250	13.5		1100	080	2.8
	1370	260	12.4		1460	340	3.8
	1710	270	10.4		1810	320	5.9
	2050	280	9.5		2190	310	7.2
	2400	290	11.8		2600	310	8.5
	2780	300	12.0		3020	330	8.4
	3080	300	13.2		3400	330	8.1
	3400	300	14.5		3760	330	9.2
	3720	310	15.6				
	4030	310	17.0				

Table 12.1 (Continued)

Gas Release No. 53  
24 Aug 1956 1950C

Gas Release No. 54  
24 Aug 1956 2150C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
948	0	18.0	44	949	0	20.0	51
940		22.7	41	918		20.8	42
900	450	21.0	35	904		20.0	35
850	941	17.2	42	900	459	19.8	35
825		15.1	45	850	950	17.3	43
800	1455	14.4	42	800	1466	14.6	50
774		13.8	38	772		13.6	32
700	2572	8.0	41	700	2583	8.7	42
686		7.0	42	600	3533	- 2.0	67
600	3822	- 1.4	63				
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
Equipment Failure No Sounding				SFC	02	150	3.1
					380	160	12.5
					720	180	13.2
					1080	190	9.2
					1450	210	4.9
					1760	240	2.0
					2100	270	3.0
					2460	280	5.9
					2800	300	7.3
					3160	310	8.9
					3520	320	10.2
					3900	320	11.6

Table 12.1 (Continued)

Gas Release No. 55  
25 Aug 1956 0055C

Gas Release No. 56  
25 Aug 1956 0250C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
948	0	17.0	60	948	0	15.0	66
904		20.0	43	900	444	20.0	47
900	446	19.9	43	850	936	19.4	49
882		19.0	48	815		18.8	50
850	938	18.4	49	800	1457	17.2	51
800	1456	15.0	52	761		13.3	56
756		11.9	56	726		10.7	44
710		9.2	41	700	2579	8.2	50
700	2576	8.2	50	600	3829	- 2.1	74
694		7.3	54				
615		- 0.5	70				
600	3825	- 2.1	70				
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	150	8.2	SFC	02	160	6.9
	360	160	14.3		260	170	11.8
	700	190	12.0		560	190	14.6
	1030	200	10.2		1040	200	12.9
	1350	210	9.2		1500	220	8.1
	1680	220	6.0		1900	230	7.5
	1980	230	4.0		2370	240	8.6
	2280	240	4.6		2760	240	8.5
	2600	250	5.8		3190	250	7.9
	2900	260	5.7		3550	270	6.0
	3230	270	7.0		3900	290	6.5
	3600	290	7.7				
	3920	300	7.4				

Table 12.1 (Continued)

Gas Release No. 57  
25 Aug 1956 1720C

Gas Release No. 58  
25 Aug 1956 1920C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
940	0	34.5	18	939	0	29.2	25
900	390	30.5	22	932		31.5	25
850	897	25.2	30	900	379	29.0	27
800	1425	19.9	39	850	884	25.0	30
784		18.0	42	800	1410	20.6	33
738		15.0	23	762		17.1	36
700	2557	11.1	31	744		15.5	23
600	3819	0.4	50	700	2546	11.3	33
				610		20.0	52
				600	3812	1.0	55
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	200	9.8	SFC	02	180	2.1
	450	200	13.0		360	200	12.8
	870	200	15.0		730	200	14.5
	1250	210	14.0		1110	210	14.6
	1640	210	17.8		1500	220	15.0
	2200	220	17.5		1900	220	15.0
	2650	230	15.8		2280	240	11.9
	3000	240	14.0		2630	240	11.1
	3300	250	10.2		3020	250	10.4
	3620	200	9.0		3350	250	8.5
	3950	270	8.0		3750	260	8.9
					4030	260	9.5

Table 12.1 (Continued)

Gas Release No. 59  
25 Aug 1956 2220C

Gas Release No. 60  
26 Aug 1956 0020C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
939	0	25.5	38	938	0	25.5	35
913		31.0	23	907		29.1	26
900	378	30.2	24	900	375	29.0	35
855		27.4	24	860		27.4	25
850	886	26.0	25	850	882	26.5	35
800	1417	21.9	32	800	1413	22.0	28
716		12.9	45	754		20.5	29
700	2554	11.3	43	720		14.0	42
648		6.1	37	700	2552	11.8	47
600	3816	0.3	57	602	3818	0.4	72
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	190	2.6	SFC	02	210	6.2
	400	200	15.8		440	220	22.5
	780	210	16.5		850	220	24.1
	1170	210	15.3		1200	220	19.2
	1570	220	15.0		1520	220	21.8
	1960	230	14.0		1850	220	14.2
	2350	240	11.3		2270	220	15.3
	2730	240	11.0		2750	220	11.2
	3160	240	10.8		3150	210	7.9
	3600	250	8.0		3490	210	8.1
	4000	260	6.6		3850	200	9.0

Table 12.1 (Continued)

Gas Release No. 61  
27 Aug 1956 1050C

Gas Release No. 62  
27 Aug 1956 1350C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
934	0	31.8	26	934	0	29.0	37
916		28.0	30	924		28.0	30
900	330	26.0	30	900	329	26.9	30
888		24.5	30	869		25.4	-30
874		23.2	27	850	831	23.5	32
850	832	24.3	29	800	1357	19.6	38
800	1358	20.2	32	744		14.5	43
735		14.4	39	700	2488	10.3	54
700	2492	10.9	47	635		3.8	71
634		3.8	62	600	3749	0.2	75
600	3754	- 0.1	62				
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	180	5.7	SFC	02	180	1.6
	317	200	9.7		280	210	6.5
	560	210	11.8		550	200	4.2
	990	220	8.0		800	200	3.0
	1290	220	7.0		1050	210	4.4
	1600	210	8.7		1250	220	5.6
	1900	210	8.4		1500	230	5.6
	2180	210	9.0		1750	220	5.9
	2490	220	9.2		1950	220	8.0
	2800	220	7.3		2200	220	9.5
	3070	230	7.5		2500	220	10.5
	3370	230	8.6		2800	230	12.0
	3650	230	9.7		3090	230	11.2
	3950	240	10.5		3350	230	11.7
					3700	230	12.0
					4000	220	10.5

Table 12.1 (Continued)

Gas Release No. 63  
27 Aug 1956 1950C

Gas Release No. 64  
27 Aug 1956 2220C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
931	0	24.5	47	932	0	19.6	67
923		30.7	34	921		29.1	40
900	302	29.0	34	900	309	29.6	30
853		25.4	34	894		29.7	28
850	807	25.1	34	858		27.3	28
800	1335	21.3	32	850	816	25.6	28
773		19.1	31	800	1346	22.0	29
700	2473	11.8	34	742		16.5	29
654		6.9	36	700	2484	11.9	35
600	3739	1.1	45	600	3747	6.0	41
Winds				Winds			
	Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)
SFC	02	240	1.0	SFC	02	230	3.0
	230	230	3.4		350	230	4.6
	480	220	5.0		720	230	6.6
	720	210	6.1		1080	230	8.0
	980	210	7.7		1460	230	8.0
	1290	210	6.0		1790	230	7.7
	1520	210	3.7		2110	240	5.8
	1810	210	3.5		2450	240	5.3
	2100	210	3.2		2790	240	4.4
	2370	220	3.5		3100	240	3.3
	2660	220	3.5		3490	240	4.6
	2940	230	2.4		3880	230	5.8
	3200	240	1.8				
	3450	260	2.5				
	3680	280	3.8				
	3970	280	4.0				

Table 12.1 (Continued)

Gas Release No. 65  
29 Aug 1956 1920C

Gas Release No. 66  
29 Aug 1956 2120C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
933	0	26.5	28	933	0	21.0	42
900	315	24.9	32	916		25.6	37
850	812	19.9	40	900	316	24.9	33
800	1331	15.8	50	850	814	22.1	23
766		14.4	52	818		22.0	23
700	2447	7.1	42	800	1336	18.0	28
658		3.4	39	750		13.4	34
600	3696	- 1.2	24	700	2460	8.4	46
				650		3.0	58
				600	3711	- 2.0	56
Winds				Winds			
Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)	
SFC	02	180	3.1	SFC	02	180	3.6
	360	180	11.8		380	180	15.3
	700	180	13.6		750	190	17.4
	1080	190	13.0		1100	200	14.5
	1440	200	11.0		1420	220	14.1
	1830	220	10.6		1800	220	13.9
	2200	240	11.0		2150	230	10.2
	2530	250	11.5		2460	250	9.1
	2900	260	11.2		2750	250	9.6
	3220	260	12.2		3130	260	12.0
	3580	270	12.2		3520	260	14.1
	3900	270	10.0		3920	270	15.0

Table 12.1 (Continued)

Gas Release No. 67  
30 Aug 1956 0020C

Gas Release No. 68  
30 Aug 1956 0220C

P (mb)	Z (m)	T (°C)	R.H. (%)	P (mb)	Z (m)	T (°C)	R.H. (%)
932	0	21.0	47	931	0	21.0	45
911		24.6	37	916		24.2	40
900	304	23.8	40	900	295	23.6	37
876		21.9	45	850	791	21.3	30
850	801	21.1	34	830		20.4	27
830		20.5	24	800	1312	17.7	30
800	1323	17.8	30	700	2434	8.0	43
700	2444	7.9	46	672		5.2	47
686		6.4	49	635		2.2	43
600	3687	- 2.4	59	600	3685	- 1.8	50
Winds				Winds			
Z (m)	ddd (deg)	ff (m/sec)		Z (m)	ddd (deg)	ff (m/sec)	
SFC	02	180	3.1	SFC	02	180	4.6
	380	190	16.0		400	210	14.6
	720	200	16.5		800	220	15.3
	1030	210	16.8		1160	220	13.8
	1320	220	17.3		1530	210	13.8
	1680	220	16.4		1920	210	12.7
	2000	220	13.6		2290	200	10.2
	2300	210	13.0		2640	200	9.7
	2620	210	11.0		3020	210	7.7
	2950	230	7.0		3380	240	6.4
	3230	260	5.0		3770	260	8.3
	3530	250	6.0				
	3900	260	7.3				

CHAPTER 13  
AIRPLANE OBSERVATION DATA

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13.1 Introduction

The aircraft soundings taken at O'Neill, Nebraska at the times of the diffusion experiments are tabulated on the following pages. The data were recorded on an AFCRC Aerograph (Kollsman KS-4). In addition, altitude was read from a calibrated sensitive altimeter by an observer who also noted air conditions.

The pattern for the sounding which was regularly followed consisted of horizontal passes at constant airspeed and altitude along the north mile of the site section for altitudes up to 1000 ft. Then a box climb was made with observations on each side in level flight for 30 seconds. Unless clouds intervened, this was continued to 7000 ft above the site itself (9000 ft mean sea level indicated altitude). A spiral descent followed with one observation at either 1000 ft or 300 ft and a final traverse at an altitude similar to the initial run.

13.2 Tabulated Data

The first column,  $Z_p$ , gives the pressure altitude obtained from altimeter readings. The height of the lowest level was adjusted to match the pilot's intention to fly by his own calibrated altimeter and by visual reference to 50-foot instrument towers nearby. The other levels were corrected for scale and installation errors but can be as much as 25 feet too high due to a lack of up-to-date information on these errors and on the airport elevation.

The  $P_{mb}$  column is the pressure in millibars obtained by converting altimeter readings through use of a standard altitude table.

The T column is the temperature in °C read from a thermistor bead in a stagnation type probe on a boom on the wing. The value represents an average for the traverse when the trace was changeable and a value at the end of the traverse when a drift of temperature was noted. The value represents a free air temperature because it has been corrected for dynamic heating using a recovery factor of 0.85, found to be typical for the equipment used. The accuracy was of the order  $\pm 0.2^\circ\text{C}$ . Part of this spread was due to a modification to make the recorder more sensitive, which allowed the indicator to hunt through this range during the time of high ambient temperatures.

A column marked # refers to the behavior of the temperature trace. The code used is similar to the one used for pressure tendency reports. The first figure indicates the trend shown by the trace during the traverse, which lasted about 30 seconds. (The time taken to cover the one mile at 100 knots indicated air speed.) The second figure is the amount of change (plus or minus) indicated by an oscillating trace or the amount of temperature shift as indicated by the drifting of the trace. The significant values are given in the legend prefacing the table.

The RH column lists the estimated relative humidity obtained from a carbon-element electric hygrometer. The calibration curve used was that for a batch of pre-production elements. This was checked against apron values of a sling psychrometer before and after the flights. Comparison was made with the daily radiosonde upper air observations (lithium chloride elements) and the calibration curve was shifted to match the deviation of the overall average. As is customary, allowance was made for a small temperature shift; also in this RH column an allowance was made for the increase in probe pressure of 15 mb. The same element was used throughout because no deterioration nor regular shift could be proven in the field. The accuracy is of the order of 5 percent.

The VP column for vapor pressure in millibars and the DP column for dew point in °C are slide rule values. They are computed without allowance for the above mentioned probe-pressure effect. The gradient



values are considered good due to the fast response of the humidity element at these high temperatures. The accuracy of the absolute values is limited as noted above.

The TIME shown for each sounding is generally that of the time of gas release for convenient reference. The sounding actually started with the first pass; this first pass almost always corresponded with the start of the ground meteorological observations which was 5 minutes before gas release time. The first traverse followed the radiosonde balloon release by 5 minutes. The top level of a complete sounding was reached about 30 minutes and the final run about 45 minutes after the first traverse.

13.3 Remarks

Aircraft observations were not made for tests 23, 24, 31, 32, 33, and 34. At these times the aircraft was at Omaha for engine change and installation of additional instruments. An extra run of note was made and this is included as Field Test No. 48S.

The aircraft used was a standard USAF L-20, instrumented by the Research Airborne Engineering Branch of the Hanscom Air Force Base, Bedford, Mass. The crew consisted of Lt. George A. Sexton, Lt. E. E. Clark, pilots, and A/1c John I. Knutla, A/1c Joseph H. Driever, crew chiefs.

The thermistor used was modified for a response time of about three seconds and calibrated by James H. Meyer of the Lincoln Laboratory. The calibration used with the carbon element was provided by Alfred Spatola of the Cloud Physics Section of GRD.

Table 13.1 Aircraft Observations

LEGEND

Code for the # symbol

<u>First Figure</u>	<u>Temperature Behavior</u>
2	Unsteady or oscillating trace, may include a jump or a hump.
3	Drift to warmer temperature which is maintained.
8	Drift to colder temperature which is maintained.
dash	Smooth trace, no temperature change.

<u>Second Figure</u>	<u>Temperature Oscillation</u>	<u>Temperature Drift</u>
none	± 0.2°C	less than 0.5°C
2	± 0.3	0.5
4	± 0.5	1.0
5	± 0.6	1.2
6	± 0.8	1.5

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Abbreviations used are those of the airways teletype code and contractions whose meaning is evident.

The observer's initials are listed because non-meteorological aides made frequent flights on which their observations are sparse. The pilots alternated in flying and no difference in techniques was noted.

Table 13.1 (Continued)

FIELD TEST NO. 1				3 JULY 1956			1100 CST	Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
50	943.5	21.0		97	24.4	20.7		
100	941.5	21.3		95	24.4	20.6		
180	939.0	21.1	22	91	23.0	19.7		
390	932.0	20.4	--	91	22.0	19.0		
610	924.0	19.2		94	21.2	18.4		
830	917.0	18.1		98	21.0	19.0		
1000	911.0	18.6		>100	21.4	18.6	Ocnl bump lower levels	
1520	893.5	17.3		>100	19.7	17.3	In clear	
2015	876.0	16.3		>100	18.5	16.3	Base of clouds-in wisps	
2400	865.0	15.1		>100	17.2	15.1		
990	911.5	17.5		>100	20.0	17.5		
130	940.5	20.6		>100	24.3	20.6		
50	943.5	21.1		96	24.4	20.7		
50	943.5	21.2		95	24.4	20.7	Second pass Obsr P.H.	

FIELD TEST NO. 2				3 JULY 1956			1500 CST	Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
50	943.0	23.5		82	24.0	20.4		
85	941.5	23.4		83	24.1	20.5		
160	939.0	23.4		83	24.1	20.5	Bump	
430	931.0	22.6		85	23.2	19.9		
630	923.0	21.9		86	22.8	19.6		
840	916.0	21.1		85	21.6	18.8		
1025	909.5	20.7		89	22.0	19.0		
1515	893.5	19.6		92	21.2	18.5		
2025	876.5	18.2	82	96	20.4	17.3	Steady	
2535	860.0	17.0		99	19.4	17.0	Ocnl bump	
3020	844.5	15.7	--	100	17.8	15.7	In clds	
3545	828.0	14.4		>100	16.4	14.4	Thru hole in clds	
4065	812.0	13.6	82	>100	15.6	13.0	Thru thin clds	
5040	782.5	11.7		>100	13.7	11.7	Between clds	
1000	910.5	18.8	32	>100	21.7	18.8	First bump about 1200'	
60	943.0	21.4	22	100	25.4	21.4	Descending 500'/minute	
60	943.0	22.3		94	25.4	21.4	Abrupt descent to here	
							Traverse after 30 seconds	

# See Legend

No. 1 & 2

Table 13.1 (Continued)

FIELD TEST NO. 3				5 JULY 1956			1100 CST	Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
		22.4		95	25.7	21.5		
220	940.0	26.0		58	19.7	17.3		
160	942.0	25.8		60	20.2	17.7		
390	934.5	25.2	21	60	19.6	17.2		
600	927.0	24.5		63	19.7	17.2		
840	919.0	24.0	62	65	19.7	17.2		
1010	913.0	24.3		66	20.0	17.6		
1520	896.5	23.0	82	67	19.1	16.8		
2010	880.0	21.9	82	67	17.9	15.7		
2505	864.0	20.6		72	17.6	15.5		
3025	847.5	19.1		67	15.0	13.0		
3505	832.5	18.0		65	13.8	11.7		
4045	815.5	16.5		60	11.5	9.0		
5025	786.0	14.7		64	11.0	8.4		
220	940.0	23.9	32	73	21.8	18.9	Obsr P.H.	

FIELD TEST NO. 4				6 JULY 1956			0100 CST	Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
		20.6		92	21.8	18.9		
180	941.0	25.9	--	60	20.2	17.7	Equip Osc ±0.2°C per 10 sec-taxing	
405	933.5	26.1	--	60	20.4	17.8	Tmp max on Sdg	
615	926.0	25.4	--	60	19.6	17.2		
820	919.5	24.8	21	60	19.0	16.7		
1010	913.0	24.4		59	18.5	17.3		
1500	896.5	23.4	22	60	17.4	15.3		
1995	880.0	22.0		59	15.8	13.8		
2495	860.5	20.6		69	10.9	14.9		
3000	848.0	19.2		75	16.8	14.8	Pireps slight turbc	
3505	832.0	17.8		74	15.2	13.3	above 3000'	
3990	817.0	16.6		71	13.6	11.5		
5025	785.5	14.4		58	9.8	6.7		
190	941.0	23.6	44	82	23.8	20.3	Pireps slight turbc Sharp 2" inversion	

# See Legend

No. 3 & 4

Table 13.1 (Continued)

FIELD TEST NO. 5							6 JULY 1956		1400 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)					
60	944.0	29.4		47	19.2	16.9				Ocnl gust all levels	
75	943.5	29.4		47	19.3	17.0					
170	940.0	29.3		47	19.2	16.9				Bumpy below	
375	933.0	28.5	22	48	18.8	16.5					
630	924.5	27.8		49	18.6	16.3					
820	918.0	27.2	22	50	18.2	16.1					
990	912.0	26.2	22	53	18.3	16.1					
1500	895.0	25.3	82	52	17.0	1.50				One gust	
2000	878.5	23.8	82	54	16.3	14.3					
2505	862.5	22.3	22	56	15.5	13.6					
3005	846.5	21.2	22	49	12.6	10.4					
3495	831.0	20.1	22	49	11.5	9.1					
4030	814.5	18.2		49	10.9	8.2					
5045	784.0	17.4		52	10.4	7.6					
300	935.5	26.5	32	63	22.1	19.1				Obsr J.D.	
35	945.0	28.5	32	52	20.0	17.5					

FIELD TEST NO. 6							6 JULY 1956		1700 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)					
50	942	30.3	22	43	18.5	17.3					
75	941	30.7	--	46	20.3	17.8					
165	938	30.2		46	19.8	17.3					
375	930.5	29.0		46	18.4	16.2					
635	922	28.0	82	46	18.6	16.4					
805	916	28.3		46	17.8	15.7					
1005	909.5	27.8		48	18.1	15.9					
1515	892.5	26.7		46	16.3	14.3					
1995	876.5	25.3	82	50	16.4	14.4					
2500	860.5	23.3	82	54	16.6	13.6					
3020	843.5	22.8		50	14.2	12.2					
3560	827.0	21.2		46	11.5	9.1					
4000	813.0	20.5		42	10.3	7.4					
5010	783.0	18.3		49	10.4	7.4					
275	934.0	27.7	33	54	20.3	17.7				Obsr J.D.	
65	941.0	30.0		47	20.0	17.5					

# See Legend

No. 5 & 6

Table 13.1 (Continued)

FIELD TEST NO. 7							10 JULY 1956		1400 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)					
50	944.5	30.1	22	38	16.3	14.3				Obrep sounding	
90	943.0	29.6		39	16.3	14.3					
180	940.0	29.2	22	40	16.0	14.1				Rough aloft	
390	933.0	28.6		39	15.3	13.4					
590	926.0	27.8		41	15.5	13.5					
820	916.0	27.2	22	42	15.4	13.4					
1000	912.0	26.9		42	14.8	12.8					
1520	894.5	25.3		45	14.4	12.4					
2015	878.5	23.8	22	47	13.8	11.8					
2505	862.5	21.8		50	13.0	10.9					
3005	846.5	20.5	82	52	12.6	10.4					
3515	830.5	18.9	82	56	12.4	10.2					
4035	814.5	17.3		59	11.9	9.6					
5045	784.0	14.6	82	62	10.4	7.6					
6085	753.5	12.3	82	66	9.6	6.4				Turbulence noted	
7090	725.0	9.8		68	8.4	4.5					
290	938.0	26.4	32	45	15.6	13.6				Obsr J.D.	
90	943.0	29.1	32	41	17.0	15.0					

FIELD TEST NO. 8							10 JULY 1956		1400 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)					
50	943.0	30.5	22	39	17.1	15.0				Ocnl bumps and drafts Drafts	
90	941.5	30.1	23	39	16.7	14.7					
180	938.5	29.8	22	41	17.4	15.2				Ocnl bumps	
395	931.0	29.3	22	42	17.3	15.2					
640	922.5	28.2	23	43	16.4	14.4					
830	916.0	27.8		42	15.8	13.8					
1000	910.5	27.0		44	15.5	13.6					
1500	894.0	25.7		45	14.7	12.7				Ocnl yaw	
2015	877.0	23.8		48	14.2	12.1					
2525	860.5	22.1	22	50	13.4	11.3					
3035	844.0	20.5		54	13.4	11.3					
3545	828.0	19.0		59	13.2	11.0					
4045	813.0	17.6		59	13.0	10.8					
5065	782.0	14.6		68	11.6	9.1					
6075	752.5	11.9		73	10.3	7.4				Cloud bases these altitudes Wallowy	
7090	723.5	9.3		79	9.5	6.2					
320	937.0	29.1	32	39	15.8	13.8				Obsr P.H.	
95	941.5	30.7	22	39	17.3	15.2					

# See Legend

No. 7 & 8

Table 13.1 (Continued)

FIELD TEST NO. 9				11 JULY 1956				1000 CST	
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)	Remarks		
50	939.0	25.9	23	62	21.2	18.4	Bumpy		
100	937.5	25.6	23	62	20.8	18.2			
165	935.0	25.3	22	65	21.2	18.4			
335	927.5	24.7	22	67	21.0	18.3	Drafts		
610	920.0	23.9	22	70	21.1	18.4			
825	912.5	23.1	22	72	20.4	17.8			
990	907.0	23.2	72	72	19.3	16.9	Bumps lift		
1490	890.5	21.1	23	73	18.4	16.2			
2025	875.0	21.4	16	73	18.8	16.5	Slow osc		
2515	857.0	22.4	23	66	18.3	16.1	Steady		
3015	841.5	21.5	22	68	17.6	15.5	Hzzy vsb 8 to 10		
3495	826.5	20.9	65	65	16.4	14.4			
4035	809.5	20.6	54	54	13.2	11.1			
5025	780.0	18.6	50	50	11.0	8.4			
6035	750.5	16.1	47	47	8.7	5.0	Ac clids 5000' above		
7060	721.5	13.1	49	49	7.4	2.6	Hazy		
280	931.5	25.2	34	70	22.7	19.5			
55	939.0	26.6	23	60	21.3	18.5	Obsr P.H.		

FIELD TEST NO. 10				11 JULY 1956				1200 CST	
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)	Remarks		
45	939.0	28.4	22	55	21.5	18.7			
90	937.5	28.2	23	56	21.8	18.8			
185	934.0	27.8	22	56	21.2	18.5			
405	926.5	26.9	22	60	21.7	18.8			
635	919.0	26.3	23	63	21.8	18.8			
820	912.5	25.4	66	66	21.7	18.8			
990	907.0	25.5	22	66	21.8	18.9			
1490	890.5	23.6	22	70	20.8	18.2			
2005	873.5	21.9	22	72	19.3	17.0	Direps rough below		
2505	857.5	20.4	22	74	18.0	15.8	Relatively smooth above		
3015	841.5	19.7	14	70	16.3	14.3			
3515	825.5	20.3	32	62	15.0	13.0			
4015	810.0	19.7	22	54	12.5	10.3			
5015	780.0	18.1	54	54	11.4	8.8			
6025	750.5	15.5	22	53	9.5	6.3			
7040	722.0	12.9	22	60	9.1	5.6			
290	930.5	27.7	22	58	21.9	19.0			
60	938.5	29.0	32	55	22.3	19.2	Obsr J.D.		

# See Legend

No. 9 & 10

Table 13.1 (Continued)

FIELD TEST NO. 11				14 JULY 1956				0800 CST	
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)	Remarks		
40	942.5	23.5	23	83	24.2	20.6	Bump		
90	941.0	32.4	23	88	24.2	20.5			
190	937.5	23.1	22	83	23.7	20.2	Drafts		
380	931.0	22.4	22	83	22.7	19.5			
640	922.0	21.5	22	85	22.4	19.3	Bumps		
840	915.5	22.4	23	84	23.0	19.8			
1040	908.5	23.1	23	76	21.8	18.8	Steadier		
1520	892.5	22.5	32	82	22.8	19.6			
2010	876.5	23.5	50	50	14.8	12.3	Smooth		
2495	861.0	22.6	22	55	15.2	13.2			
3025	844.0	22.4	42	42	11.5	9.0			
3495	829.0	22.2	42	42	11.4	8.8			
4035	812.5	20.8	39	39	9.7	6.5	Oscillation		
5035	782.5	17.7	46	46	9.4	6.2	Smooth		
6035	753.0	15.5	46	46	8.1	4.0			
7080	723.5	12.5	43	43	6.3	0.4	Oscillation bumps at 1300'		
290	934.0	23.8	32	85	25.2	21.3			
50	942.5	23.9	63	80	23.8	20.3	Obsr P.H.		

FIELD TEST NO. 12				14 JULY 1956				1000 CST	
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)	Remarks		
75	941.0	27.8	22	66	24.8	21.0	Bumpy		
160	939.5	27.2	22	66	24.3	20.5	Lifts begin		
300	931.5	26.7	22	70	24.8	21.0			
620	922.5	25.9	22	73	24.7	20.9			
800	916.5	25.4	22	77	25.4	21.4	Gusts at end		
1000	909.5	24.9	22	78	24.8	21.0			
1510	892.5	24.4	24	72	22.2	19.1	Occasional bumps		
2005	876.5	24.6	23	52	16.4	14.4	Smooth		
2485	861.0	23.9	22	50	14.6	12.9			
3015	844.0	23.1	22	39	11.1	8.5	Steady		
3495	829.0	21.9	--	38	10.0	7.0			
4030	812.5	21.1	35	35	8.6	5.0			
5035	782.5	18.4	39	39	8.4	4.4	Yaw		
6035	753.0	16.1	40	40	7.3	2.4			
7040	724.5	13.0	48	48	7.1	2.1	Steady		
280	934.0	27.6	34	44	16.4	14.4	Bumps at 1900		
70	941.5	29.2	24	50	20.8	18.2	Bump		
							Obsr P.H.		

# See Legend

No. 11 & 12

Table 13.1 (Continued)

FIELD TEST NO. 13		22 JULY 1956					2000 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
45	947.0	23.3	82	62	18.1	16.0		SC vesperalis 9000' Sun low at the horizon	
80	945.5	22.8		65	18.2	16.0			
180	942.5	23.1	--	59	17.0	15.0		Smooth	
400	935.0	23.0		59	16.9	14.9		Very smooth One lift; sunset	
620	927.0	21.8	32	62	16.6	14.6			
830	920.0	21.2		65	16.5	14.5			
1000	914.5	20.9		67	16.9	14.9		Very light turb Smooth	
1505	897.5	19.6	82	71	16.5	14.5			
2000	881.0	18.0		72	15.0	13.1			
2500	865.0	16.6		72	13.8	11.8			
3020	848.0	15.1		73	12.8	10.6		R H Osc Smooth	
3505	833.0	13.7		77	12.2	10.0			
4045	818.5	12.5		90	13.3	11.2		Cloud base 5800 Top about 6500 vrbl	
5030	786.5	10.4		97	12.4	10.1			
6070	756.0	8.1	100	11.3	8.1	6.0			
7080	727.0	6.3		96	9.4	6.0			
285	938.5	22.3		62	17.0	15.0		Obsr P.H.	
180	942.5	22.6	22	60	16.8	14.8			

FIELD TEST NO. 14		22 JULY 1956					2200 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
170	943.5	21.7	22	57	15.0	13.0		Light turb Light turb	
355	937.0	22.4		54	14.8	12.9			
600	928.5	21.5		60	15.8	13.8			
820	921.0	21.4	22	59	15.2	13.2			
985	915.5	21.0		56	14.3	12.3			
1500	898.5	19.6		62	14.4	12.4			
1985	882.5	18.1		73	15.4	13.4		Ocnl bump above	
2485	866.0	16.7	22	81	15.6	13.6			
2955	850.0	15.0		83	14.4	12.4			
3495	834.0	14.4		90	15.0	13.0			
4005	818.0	13.1		99	15.0	13.1		Obsr J.D.	
4990	788.0	11.3		82	11.2	8.7			
6025	758.0	9.4		75	9.0	5.4			
7020	729.5	6.9		87	8.8	5.1			
260	940.0	22.3		54	14.8	12.8		Obsr J.D.	
170	943.5	22.3	22	53	14.5	12.5			

# See Legend

No. 13 &amp; 14

Table 13.1 (Continued)

FIELD TEST NO. 15		23 JULY 1956					0800 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
50	947.0	19.4	22	84	19.2	16.8		Occasional H turb	
75	942.5	19.2		83	18.8	16.5			
185	942.0	19.0		84	18.8	16.5			
395	935.0	18.9		84	18.6	16.4			
635	926.5	20.1	22	80	19.1	16.8		Hazy level not sharp	
845	919.5	20.3		81	19.6	17.2			
1005	914.0	20.1		82	19.6	17.2			
1525	897.0	20.0		65	15.8	13.6		Above smoky layer	
2020	880.5	18.8		69	15.2	13.2			
2500	865.0	17.1	--	78	15.5	13.5			
3030	848.0	15.9		84	15.3	13.3			
3520	832.5	15.2		59	10.4	7.5		Few Ac on horizon	
4050	818.0	13.9	--	47	7.5	2.8			
5040	786.0	11.7		42	5.9	-0.4			
6060	756.0	9.4		36	4.3	-4.1			
7085	727.0	7.8		32	3.5	-6.5		A few little bumps Obsr P.H.	
285	938.5	20.4	32	84	20.3	17.8			
60	946.5	21.3		75	19.3	14.9			

FIELD TEST NO. 16		23 JULY 1956					1000 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
50	946.5	24.4	24	62	19.4	17.0		Obreps bumpy to here	
100	944.5	24.4	24	62	19.2	16.9			
190	938.0	24.1	22	62	18.8	16.6			
400	934.0	23.3	22	65	18.8	16.6			
610	927.0	22.6	82	64	17.8	15.7			
830	919.5	21.9	22	72	18.3	17.0			
1010	913.5	21.5	22	76	19.7	17.3			
1500	897.0	20.3	22	73	17.6	15.5			
2005	880.5	18.8	22	74	16.2	14.2			
2495	864.5	17.9	--	78	15.5	13.5			
3015	848.0	16.0		78	14.5	12.5			
3495	833.0	14.8	22	71	12.2	9.9		A light layer of scattered clouds	
4035	816.0	14.7		42	7.3	2.2			
5025	786.0	12.4		38	5.5	1.2			
6045	756.0	10.3		54	6.9	1.8			
7050	727.0	8.0		74	8.1	3.9		Obsr J.D.	
300	937.5	24.4	32	58	18.1	16.9			
50	946.0	25.8	32	50	16.7	14.7			

# See Legend

No. 15 &amp; 16

Table 13.1 (Continued)

FIELD TEST NO. 17				23 JULY 1956				2000 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)				
50	941.0	29.0	--	37	14.6	12.6				
80	940.0	28.8		37	14.4	12.4				
180	936.5	29.3	--	35	14.4	12.4				
390	929.0	29.5	22	33	13.7	11.6				
620	921.5	29.4	29	29	12.0	9.6				
820	914.5	28.6	22	31	12.2	10.0				
990	909.5	28.2		33	10.7	10.5				
1480	892.5	26.9	22	32	11.9	9.5				
2005	875.5	25.5		34	11.3	8.8				
2505	859.0	24.8	12	36	11.2	8.7				
2955	844.0	23.2		38	10.8	8.2				
3505	827.5	21.7		39	10.2	7.3				
3995	812.5	20.3		44	10.4	7.6				
5015	781.5	17.5		49	9.9	6.8				
6005	752.5	14.9		52	8.9	5.4				
7040	723.5	11.8		60	8.4	4.5				
280	933.0	28.4	--	35	13.7	11.6				
180	936.5	28.4	22	36	14.1	12.1				

Obsr J.D.

FIELD TEST NO. 18				23 JULY 1956				2200 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)				
160	939.0	27.6	32	39	14.3	12.2			(St. Cu drifted out, wind varied with cloud cover)	
345	932.5	27.9	22	35	13.3	11.2				
605	925.5	27.9	32	36	13.4	11.2				
815	916.5	27.7	82	33	12.4	10.2				
985	911.0	27.2	22	33	12.1	9.8				
1475	894.5	26.4		32	11.1	8.6				
1980	878.0	25.6	--	36	11.7	9.3				
2490	861.5	24.4		39	11.8	9.4				
2970	846.0	23.4	22	39	11.3	8.8				
3510	829.0	21.8	62	42	11.1	8.6				
4010	813.5	20.3	22	46	10.9	8.2				
5010	783.5	17.4	22	54	10.8	8.2				
6010	754.0	14.6		61	10.3	7.4				
7030	725.5	11.5		65	9.0	5.5				
255	935.5	26.4	62	42	14.4	12.4				
155	939.0	26.7		43	15.0	13.1				

Obsr P.H.

# See Legend

No. 17 & 18

Table 13.1 (Continued)

FIELD TEST NO. 19				25 JULY 1956				1100 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)				
50	943.0	27.0	23	40	14.2	12.1			Cirrus clouds sun out Bouncy	
75	942.0	26.7	22	40	14.0	11.9				
175	939.0	26.4	22	41	14.0	12.0			Bumps	
390	931.5	25.7	22	42	13.9	11.9				
620	923.5	25.2		43	13.8	11.8			Drafts	
850	916.0	24.5	22	45	14.0	12.0				
1000	908.5	24.0	22	45	13.5	11.4			Bouncing	
1500	894.0	22.4	23	50	13.5	11.4				
2015	877.0	21.0	22	53	13.4	11.4			Less drafty RH data doubtful this test, response sluggish	
2505	861.0	20.5	24	35	8.4	4.5				
3025	844.5	20.3	22	25	6.0	-0.3				
3515	829.5	20.0	22	25	5.9	-0.5				
4035	813.5	20.0	22	25	5.9	-0.5			Smooth	
5035	783.0	18.2	12	28	6.0	-0.3				
6045	753.5	16.2		31	5.7	-0.4			Slow osc Bumps at 2500' Lift at 800 Big bump	
7080	724.0	13.5		36	5.7	-0.9				
300	934.5	26.8	22	43	15.1	13.1			Obsr P.H.	
100	941.5	28.4	22	40	15.4	13.4				

FIELD TEST NO. 20				25 JULY 1956				1300 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)				
75	939.5	32.8	23	31	12.7	10.6			Humidity element inspected	
		29.4								
175	936.0	29.3	23	29	11.8	9.4				
375	929.0	28.6	22	31	12.1	9.8				
595	921.5	27.7	22	33	12.4	10.1				
805	914.5	27.0	22	36	12.8	10.6				
1015	907.5	26.2	22	36	12.4	10.2				
1505	891.0	25.1	22	35	11.3	8.3				
2000	875.0	23.2		35	10.2	7.2				
2490	859.5	21.8	22	43	11.1	8.5				
3020	842.5	21.8	26	28	7.4	2.5				
3490	827.5	22.0	24	25	6.6	1.0				
4010	811.5	21.4	23	25	6.8	0.6				
5020	781.0	19.4	22	28	6.4	0.6				
6030	751.5	17.0		28	5.6	-1.1				
7045	723.0	13.8		36	5.8	-0.6				
275	932.5	30.0	33	25	16.5	7.7			Turbe below 3000 ft	
85	939.0	30.5	82	24	10.8	8.0				

# See Legend

No. 19 & 20

Table 13.1 (Continued)

FIELD TEST NO. 21		26 JULY 1956				2100 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
175	932.0						Rough Ling to N	
390	924.5							
600	917.5							
850	908.0	28.6	32	34	13.3	11.2		
1020	903.5	29.5	22	32	13.2	11.1	Smooth suddenly	
1490	898.0	28.8	32	29	11.5	9.0		
2015	870.5	27.7		28	10.4	7.6		
2495	855.0	27.6		24	8.9	5.3	Steady	
2995	839.5	26.9		25	8.0	5.3		
3495	824.0	25.4		26	8.5	4.6	Temp min sharp about 3800'	
3895	808.0	24.4		20	8.8	5.2	Smooth	
5020	778.5	21.2	24	31	7.8	3.4	Bumpy then steady	
6045	749.0	18.1		35	7.3	2.4	Hvy ling to N Smooth	
7070	719.5	16.5	32	27	5.1	-2.2	-1.5° C temp dip on climb	
							Equipment looks OK	
295	928.0	28.7		31	12.2	10.0	Bumps at 800'	
180	932.0	28.7		30	11.8	9.4		

Obsr P.H.

FIELD TEST NO. 22		26 JULY 1956				0000 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
180	931.0	27.6		37	13.7	11.6	Ptrops strong winds aloft	
400	923.5	27.1	22	37	13.3	11.1	Bumpy	
640	915.5	26.6	35	37	12.9	10.8		
850	908.0	26.4	24	38	13.0	10.9		
1030	902.0	26.2	25	38	12.9	10.8		
1500	886.5	27.5	84	34	12.5	10.2		
2025	830.5	27.4		29	10.3	7.8		
2515	853.5	27.5	22	25	9.2	5.8		
3035	837.5	27.0	22	24	8.6	4.8		
3515	822.5	25.9	23	23	7.7	3.2	Very lgt turbe	
4035	806.5	24.9		23	7.3	2.4	Lgt turbe at 4500'	
5025	776.5	21.6		23	5.9	-0.4	Smooth at 5500'	
6045	747.0	19.5		23	5.2	-1.9		
7080	710.0	16.6	22	23	4.4	-4.0	Lt turbe at 5600' descent into haze at 4400'	
280	927.5	26.6	--	36	12.6	10.4	Out haze at 1400'	
200	930.0	26.9		36	12.8	10.6	Bumps at 300'	

No. 21 & 22

# See Legend

Table 13.1 (Continued)

FIELD TEST NO. 25		1 AUGUST 1956				1300 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
50	944.0	22.6	22	96	26.5	22.0	Douney	
100	942.5	22.6	22	94	25.8	21.6		
190	930.5	22.0	22	96	25.5	21.4		
410	932.0	21.4	22	94	24.3	20.0	Drafts and acceleration	
630	924.5	20.7		>100	24.7	20.7	R H sluggish	
845	917.0	20.0		>100	24.4	20.0	Bumpy	
1035	910.5	19.5		>100	23.7	19.5	R H sluggish	
1510	895.0	18.2		>100	22.2	18.2	Bumpy at base about 1600' In clouds at 1750' and drafts	
1000	912.0	19.4		>100	23.2	19.4	Bumpy	
50	944.0	22.9	32	96	27.0	22.4	Est 60 ft by the tower 40 ft indicated	

Obsr P.H.

FIELD TEST NO. 26		2 AUGUST 1956				1200 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
50	940.0	27.3	24	66	24.2	20.5		
80	939.0	26.9	23	68	24.4	20.6		
190	935.5	26.9	23	67	24.0	20.4	Drafts	
395	920.0	26.3	23	72	24.8	21.0	Bumpy	
630	920.0	25.6	22	75	24.0	21.0		
830	913.5	25.6	22	71	23.7	20.2	Bumpy	
1010	907.5	24.4	22	78	23.9	20.4		
1490	891.5	23.0	82	82	23.2	19.9		
2005	874.5	21.2		92	23.4	20.0	Turbe	
2460	860.0	20.4	14	91	22.0	19.1	Wobbles no drafts	
2985	843.0	18.6	66	88	19.0	16.7		
3495	827.0	18.6	24	81	17.6	15.4	Seld cld bases below	
4035	810.5	18.4	63	83	13.6	11.5	Passing cld bases at 3700'	
5025	781.0	16.2	83	82	15.3	13.3	Climb in clear	
6045	751.0	14.0	--	78	13.7	10.6		
7050	722.5	11.8		95	12.9	9.6	In clds 4500 to 4800 ft on descent	
1020	907.0	24.8	34	73	23.1	19.8	Bases est 3500 ft Bumps	
295	931.5	27.6	33	57	21.4	18.6	Bumps	
50	940.0	28.4	22	54	21.2	18.4	Low 50' pass	

No. 25 & 26

# See Legend

Table 13.1 (Continued)

FIELD TEST NO. 27		2 AUGUST 1956					1400 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
50	939.5	29.9	24	50	21.2	18.5		Bumpy	
80	938.5	30.1	23	49	21.0	18.3		Drafts already	
175	935.5	29.6	23	50	20.8	18.2			
390	927.5	29.2	63	50	20.5	17.8		Drafts	
615	920.0	27.9	23	52	20.0	17.5		Occasional gusts	
830	913.0	27.5	22	54	20.2	17.6		Ups & Downs	
1020	906.5	26.9	22	56	20.4	17.8		Negative G acceleration	
1500	890.5	25.4		67	22.0	19.0		Bumpy	
2015	873.5	23.6		79	23.2	19.0			
2495	858.0	22.1		80	21.4	18.6		Now under clouds, bumpy	
3025	841.5	20.6		84	20.6	18.0			
3515	826.0	19.0	22	93	20.7	18.0		Wobbly	
4025	810.5	17.6		98	19.9	17.4		Base of clouds just above	
5035	780.0	16.4	22	72	13.7	11.6		Cloud haze at 4800 ft	
6045	750.5	14.6		75	12.6	10.4		Cl'd tops 5000-5500 ft	
7065	721.5	11.7		81	11.3	8.7		Deck Ac est 1000' above	
								Lgt moisture content in cl'ds	
290	931.0	30.1	22	50	21.6	18.7		Bumps at 300'	
70	938.5	31.0	23	49	22.0	19.0		Bumpy	

Obsr P.H.

FIELD TEST NO. 28		3 AUGUST 1956					0000 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
165	934.5	28.2	22	72	25.0	21.1		Bumpy	
385	927.0	26.5	22	70	24.6	20.8		Lgt rain bumps	
605	919.5	26.4	22	70	24.6	20.8		Humidity sluggish	
835	911.5	26.5	22	65	22.8	19.6			
1005	906.0	26.9		61	20.3	17.7			
1605	889.5	26.4	22	52	18.2	16.0			
1980	873.5	25.2		51	16.7	14.7		Ling to N	
2490	857.5	23.8		52	15.5	13.6		Occ'l bump	
2980	841.5	23.8	22	51	15.4	13.4		Smooth	
3510	825.0	23.0		49	13.7	11.6			
4030	809.0	21.4		50	12.8	10.6			
5040	779.0	19.1		54	12.1	9.8		Smooth	
6050	749.5	15.6		76	13.5	11.6		Strong S Wind	
7025	722.0	12.8		82	12.3	10.0		Freq ling N	
								-3°C at about 700' due R	
1475	890.5	26.4		50	17.2	15.1		High pass account wca	
175	934.0	27.4	22	55	20.4	17.8			

# See Legend

No. 27 &amp; 28

Table 13.1 (Continued)

FIELD TEST NO. 29		3 AUGUST 1956					0200 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
165	935.0	27.4	22	50	18.4	16.2			
365	928.0	26.8	22	50	17.7	15.6			
595	920.0	26.5	12	50	17.6	15.5		Gusts	
795	913.5	25.9	49	49	16.5	14.5		Accelerations felt	
995	906.5	26.0	22	50	16.7	14.7			
1475	890.5	26.2		45	15.3	13.4		Smoother ling E & SW	
2000	873.5	25.8	32	45	15.0	13.0		Smooth	
2470	858.0	24.2		45	13.8	11.9			
3010	841.0	22.7		46	12.6	10.4			
3490	826.0	21.3	22	47	12.1	9.8			
4000	810.5	19.8		49	11.3	8.8		Rain encountered	
965	907.5	26.2	32	48	16.3	14.3		approaching strm Bumps at 700' No low pass	

Obsr P.H.

FIELD TEST NO. 30		3 AUGUST 1956					1300 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
75	938.0	31.8	23	42	18.8	17.3		Rough	
175	935.0	31.4	23	43	19.7	17.2		Bumpy	
375	928.0	30.6	23	45	20.2	17.7		Drafts	
625	919.5	30.0	23	46	19.5	17.1		Drafts	
850	912.0	29.4	--	50	20.7	18.0		Drafts	
995	907.0	28.6	63	47	18.5	16.2			
1465	891.5	27.4	12	50	18.4	16.2		Occasional light bumps	
2030	873.0	25.7	22	54	18.2	16.0		Drafts	
2505	857.5	23.9	22	61	18.3	16.1			
3020	841.0	22.5	12	64	17.8	16.7			
3525	825.5	20.7		72	17.8	15.7		Wallowy	
4010	810.5	19.0	22	76	17.0	15.0			
5060	779.0	16.4	--	83	15.7	13.7		Occasional bump	
6050	750.0	14.8		64	11.0	8.4		Approaching base level at	
7105	720.0	11.9	32	76	10.8	8.1		5800' Edge of FrCu	
								Base cl'ds 6000' tops 7000'	
985	907.5	28.6	62	47	18.2	16.0		No level pass account of boom oscillation	

# See Legend

No. 29 &amp; 30



Table 13.1 (Continued)

FIELD TEST NO. 35		11 AUGUST 1956					2100 CST	
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)	Remarks	
180	939.0	22.6		55	18.3	16.1	Smooth Ocnl draft	
360	932.0	25.5		53	17.4	15.3	Tiny bumps	
590	924.5	25.4	22	51	16.7	14.7		
810	917.0	24.5	22	54	16.7	14.7	Occasional bump	
980	911.0	23.7		54	16.1	14.1		
1490	894.0	22.5	22	58	16.2	14.2		
1995	877.5	20.8		08	16.8	14.8	Blue sky above	
2465	862.5	19.5		70	16.1	14.1		
3000	845.5	18.3		74	15.7	13.7		
3470	830.5	17.4		72	14.5	12.5		
4030	813.0	16.4		68	13.0	10.8	Altostratus deck	
5015	783.5	13.7		78	12.3	10.0		
6015	754.0	11.3	--	84	11.3	8.8	Hazy	
7030	725.5	8.9		89	10.3	7.4	Possible draft	
980	911.0	23.7		51	15.2	13.3	Smooth	
140	940.0	24.0		63	19.0	16.7	Obsr P.H.	

FIELD TEST NO. 36		11 AUGUST 1956					2300 CST	
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)	Remarks	
165	939.0	22.9		66	18.7	16.4		
365	932.0	23.7		60	18.0	15.8		
595	924.0	24.8		54	17.2	15.2		
815	916.5	24.4	--	54	16.8	14.8		
995	910.5	24.0		52	15.6	13.6		
1495	894.0	22.5		53	14.6	12.6		
1990	877.0	21.1		59	15.1	13.1		
2480	861.5	19.9		68	16.1	14.1		
2970	846.0	18.5		72	15.5	13.5		
3480	830.0	17.5		74	15.1	13.1		
3990	814.5	16.5		77	14.6	12.6		
5010	783.5	13.4		84	13.2	11.1		
6010	754.0	11.7		90	12.5	10.3		
7035	725.0	9.6		96	11.6	9.2		
985	911.0	23.5		54	15.8	13.8		
165	938.5	22.9		66	19.9	16.8	Obsr J.D.	

# See Legend

No. 35 & 36

Table 13.1 (Continued)

FIELD TEST NO. 37		12 AUGUST 1956					0300 CST	
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)	Remarks	
		19.1						
165	936.5	21.1	32	84	21.3	18.5	Bumps ltng N & NE	
385	929.0	22.4		78	21.6	18.7		
605	921.5	22.9		74	20.8	18.1		
810	914.5	22.9		72	20.4	17.0		
975	909.0	23.0		58	16.7	14.7		
1475	892.5	22.6	--	54	15.0	13.0		
2000	875.0	21.5	--	53	13.8	11.8	Lgt trube prep	
2510	858.5	20.6		53	13.1	11.0		
2995	843.0	19.8		53	13.5	10.2		
3470	828.5	18.4		52	11.2	8.7		
4000	812.0	17.2		53	10.7	8.0	Very light turbc	
5010	781.5	16.2		76	10.2	7.3		
6020	765.0	14.2		74	12.1	9.8		
7040	723.0	11.3		83	11.2	8.7	Ltng E	
							Light turbc at 3500	
975	909.0	22.1	--	77	20.9	18.2		
155	937.0	21.2	12	84	21.5	18.6	Bumpy	
							Obsr P.H.	

FIELD TEST NO. 38		12 AUGUST 1956					0500 CST	
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)	Remarks	
		21.2						
170	936.0	21.1		85	21.5	18.6	Pireps sfc the same	
380	929.0	22.6	33	78	21.5	18.6		
630	920.5	23.2	22	70	20.2	17.6		
830	914.0	23.3		61	17.6	15.5		
1010	907.5	23.6		49	14.3	12.3		
1510	891.0	24.0		42	12.6	10.4		
2015	874.5	22.4		48	13.2	11.1		
2495	859.0	21.7		44	11.8	9.4		
3005	843.0	20.0	--	47	10.9	8.2		
3515	827.0	18.6		50	10.7	8.0		
4015	811.5	17.8		59	12.3	10.0	Light turbc	
5025	781.0	16.5		51	9.7	6.5		
6035	761.5	13.9		87	14.0	12.0	R H jump about 5200'	
7040	723.5	11.2		89	12.0	9.7	Pireps lgt turbc	
							R H drop about 5600'	
990	908.5	22.5		63	17.4	15.3		
30	941.0	20.5	82	89	21.8	18.9		
							Obsr J.D.	

# See Legend

No. 37 & 38

Table 13.1 (Continued)

FIELD TEST NO. 39							13 AUGUST 1956		2200 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)					
190	941.5	26.2	12	44	15.3	13.4				Ocnl bump at 300'	
420	933.5	27.1	63	43	15.8	13.8				Smooth	
620	927.0	27.3	42	42	15.3	13.3				One bump, ocnl draft	
850	919.0	27.3	22	40	14.4	12.4					
1000	912.0	26.4	22	40	13.8	11.8					
1525	895.5	25.7	--	39	12.8	10.6				Smooth	
2045	879.0	24.3		39	11.8	9.4					
2515	864.0	23.0	22	39	11.0	8.4					
3035	847.5	21.8		42	11.0	8.3					
3525	832.0	20.0		47	11.0	8.3				Pireps added power needed	
4040	816.0	18.3		50	10.6	7.9				Several bumps, lgt turbc	
5040	785.5	16.3	62	55	10.3	7.4				Some bases at 5500, turbc	
6070	755.5	14.3		67	11.1	8.5				Clds above, turbc, drafts	
7090	726.5	11.3		72	9.8	6.7					
1000	914.0	26.4	--	40	13.7	11.6				Bumps at 500	
205	941.0	25.0		32	14.2	12.2				Turbc noted thruout	

Obsr P.H.

FIELD TEST NO. 40							14 AUGUST 1956		0030 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)					
150	942.5	26.4	82	44	15.1	13.1				No turbc noted	
385	934.5	27.2	22	44	15.8	13.8					
610	926.5	27.9	22	43	16.2	14.2				Pireps strong wind	
810	919.5	27.3	22	43	15.6	13.7					
1000	913.5	27.3	22	43	15.6	13.7					
1510	898.5	25.5		45	14.8	12.3				Pireps less power reqrd	
2010	880.0	24.3		45	13.8	11.7					
2500	864.0	22.7		47	13.2	11.1				Pireps ditto	
3000	848.0	21.2		47	11.8	9.4					
3480	832.5	20.0		48	11.2	8.7					
4000	817.0	18.4		48	10.2	7.2				Ocnl drafts	
5030	785.5	16.3		63	11.8	9.4				Lgt turbc 5600 ft	
6040	755.0	14.1		66	10.6	8.1				Bumps, wallow	
7070	726.5	11.3		71	9.6	6.4					
980	914.0	26.4	32	47	16.4	14.4				Turbc at 300'	
150	942.5	24.4		47	14.4	12.4					

No. 39 &amp; 40

# See Legend

Table 13.1 (Continued)

FIELD TEST NO. 41							14 AUGUST 1956		0300 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)					
160	941.5	24.4		49	15.0	13.0					
395	934.0	26.2		45	15.3	13.3				Gusts	
615	926.0	27.0	32	43	15.4	13.4				Ocnl gust	
825	919.0	26.7		43	15.1	13.1				Ling N	
985	913.5	26.7		42	14.7	12.7					
1485	897.0	25.5	22	41	13.4	11.3					
2005	879.5	24.9		41	12.9	10.7				3 Hng cells N & NE	
2500	863.5	23.6		42	12.4	10.2					
3030	846.5	22.7	22	42	11.7	9.3					
3520	831.5	21.8		46	11.9	9.6					
4025	815.5	20.3		50	11.9	9.6					
4500	801.0	19.1		53	11.8	9.4					
5025	785.5	17.8		55	11.3	8.6					
6060	755.0	15.2	--	67	11.8	9.4				Ocnl draft	
7065	726.5	12.3		65	9.5	6.2				Bumps	
1005	913.0	26.4	40	40	13.7	11.7				Lgt turbc around 2000'	
175	941.0	23.8	22	50	14.8	12.8				Sfc turbc	

Obsr P.H.

FIELD TEST NO. 42							14 AUGUST 1956		0500 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)					
180	940.5	22.8		52	14.4	12.4					
410	932.5	23.2	23	49	14.0	12.0					
650	924.5	26.1	22	42	14.2	12.2					
840	918.0	27.0		37	13.1	11.0					
1040	911.0	26.7		39	13.6	11.6					
1540	894.5	25.8	22	39	12.9	10.8					
2025	878.5	24.3		42	12.8	10.6					
2525	862.5	24.0		39	11.6	9.2					
3025	846.5	23.4	22	41	11.8	9.5					
3535	830.5	21.6		43	11.0	8.4					
4045	814.5	20.3		46	10.9	8.2				Lgt turbc	
5065	784.0	17.2	32	64	12.7	10.5					
6055	754.5	15.6	--	69	12.3	10.1				Turbc	
7010	727.5	12.7		60	9.0	5.4				Turbc	
1000	912.5	25.9		42	14.0	12.0					
60	944.5	22.3		46	12.4	10.2					

No. 41 &amp; 42

# See Legend

Table 13.1 (Continued)

FIELD TEST NO. 43		15 AUGUST 1956					1200 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
50	943.5	31.7	22	33	15.4	13.4		(Temp adjustment too sluggish, accuracy ± 0.3 this run only)	
80	942.5	31.7	23	31	15.4	13.3			
190	938.5	31.2	22	33	15.1	13.2		Bumpy	
380	932.0	30.4	22	35	15.4	13.4		Drafts oncl	
600	924.5	29.7	22	33	14.0	12.0		Bump	
820	917.0	29.0	12	36	14.6	12.6		Draft	
1010	910.5	28.4	82	36	14.0	12.0		Smooth over cldy grd	
1510	894.0	27.4	32	37	13.3	11.2		Draft	
2005	878.0	25.8	22	35	11.8	9.5		Wallowy	
2515	861.5	25.0	23	30	9.6	6.4		Gusty	
3015	845.5	23.7	22	25	7.3	2.5		Small oncl gusts	
3525	829.5	23.2	13	25	7.1	2.1			
4015	814.0	21.6	--	28	7.4	2.6			
5030	783.5	18.7	41	3.9	5.3			Relatively smooth	
6035	754.0	17.2	50	9.9	6.8				
7065	725.0	14.6	50	8.5	4.7				
990	911.5	29.1	12	35	14.3	12.3		Drafts noted at 1500'	
75	942.5	33.6	22	33	17.3	15.2		Bouncy	

FIELD TEST NO. 44		15 AUGUST 1956					1400 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
50	942.5	34.3	22	29	15.6	13.6		(Temp amp closely adjusted, esp osc = 0.3°C per 15 sec at this temp)	
95	941.0	34.2	29	29	15.5	13.5			
180	938.0	33.8	24	29	15.1	13.1		(Jitters at high temp.)	
380	931.0	32.8	22	29	14.3	12.3			
640	922.0	32.1	13	29	13.9	11.9			
850	915.0	31.6	22	29	13.6	11.5			
1000	910.0	30.6	22	29	12.7	10.5			
1540	892.0	29.3	33	13.6	11.6				
2015	876.0	27.6	33	12.4	10.2				
2515	860.5	26.2	22	36	12.2	9.9			
3025	844.0	24.4	82	-36	11.0	8.4			
3515	829.0	22.8	22	39	10.8	8.1			
4055	812.0	21.2	39	9.9	6.8				
5065	781.5	19.1	32	47	10.4	7.5			
6065	752.5	17.0	50	10.0	7.0				
7070	724.0	14.0	63	10.2	7.3			(Jitter ± 0.1°C at this temp)	
995	910.5	30.9	29	29	13.0	10.8			
70	942.0	34.3	33	26	13.8	11.8		Height estimated Obsr P.H.	

# See Legend

No. 43 &amp; 44

Table 13.1 (Continued)

FIELD TEST NO. 45		15 AUGUST 1956					1700 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
75	938.0	35.3	22	29	16.4	14.4		Fgt bumps Obsr P.H.	
190	934.0	34.6	23	29	15.9	13.9		Oncl drafts	
380	927.5	33.9	22	29	15.1	13.1		Drafts	
620	919.5	33.3	22	29	14.8	12.8		Drafts	
835	912.0	32.4	22	29	14.1	12.1			
1020	908.0	32.0	22	31	14.8	12.8		Wallow	
1525	888.0	30.1	31	13.3	11.2			Lgt gusts	
2035	872.5	28.7	62	33	13.1	11.0			
2490	857.5	27.1	36	36	12.8	10.6			
3025	840.5	25.6	22	35	11.7	9.3			
3525	825.0	24.0	38	11.4	8.9			Draft	
4025	809.5	22.5	39	10.7	8.0				
5045	779.5	19.7	46	10.5	7.7				
6055	749.5	17.0	52	10.2	7.3				
7065	721.0	14.2	61	10.1	7.1			Brkn clds 2000' above	
1005	906.5	31.6	33	28	13.3	11.2		Bumpy about 1200	
100	937.0	35.0	63	25	14.4	12.4		Steady run Gain 30' on traverse; gusty	

FIELD TEST NO. 46		15 AUGUST 1956					1840 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
45	937.5	34.5	22	29	15.7	13.7		Bumpy flight	
90	936.0	34.0	22	25	13.6	11.6			
180	933.0	34.0	22	25	13.7	11.6			
400	925.5	33.4	63	25	13.2	11.1			
620	918.0	32.6	22	29	14.3	12.3			
840	910.5	31.6	62	29	13.4	11.3			
1020	904.5	31.2	--	29	13.1	11.0			
1500	888.5	29.8	33	13.9	11.9				
2035	871.0	28.1	35	13.4	10.4				
2515	855.5	26.8	39	13.8	11.7				
3025	839.5	25.9	12	39	13.1	11.0			
3535	823.5	24.4	41	12.6	10.4				
4035	808.0	22.8	41	11.4	8.9				
5065	777.5	20.1	46	10.8	8.1				
6075	748.0	17.0	55	10.9	8.2				
7080	719.5	14.4	61	10.2	7.3			(Cld to cld lng, strong lng W & N, crew felt static shock on final approach)	
1010	905.0	30.8	32	29	12.8	10.6			
60	937.0	32.8	23	25	12.8	10.6		Sprinkling Obsr J.D.	

# See Legend

No. 45 &amp; 46

Table 13.1 (Continued)

FIELD TEST NO. 47				20 AUGUST 1956			1000 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
50	953.5	15.5	23	55	9.9	6.8			
80	952.5	15.5		54	9.7	6.6			
180	949.0	15.2		55	9.7	6.6		Bumps	
400	941.0	14.7		55	9.4	6.1			
640	933.0	13.3		60	9.7	6.5		Bumps	
870	925.0	13.3		63	9.8	6.7			
1010	920.5	12.7		65	9.7	6.5			
1520	903.0	11.5		58	8.1	3.9			
2025	886.5	10.5		62	8.1	3.9			
2535	869.5	9.1		66	7.8	3.4			
3025	854.0	8.4		76	8.5	4.7			
3525	841.5	7.0		80	8.2	4.1			
4025	822.5	5.9		70	6.7	1.2			
5055	791.5	3.5	82	71	5.7	-0.8		Lgt scld cld at 4500	
6055	762.0	1.7		71	5.0	-2.4			
7080	732.5	0.2		90	5.7	-0.9			
1000	921.0	12.8		32	64	9.7	6.5		Lgt turbc at 2400
40	953.5	15.5	32	52	10.0	7.0		Turbc Obsr J.D.	

FIELD TEST NO. 48S				20 AUGUST 1956			1200 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
50	951.5	18.0	32	49	10.3	7.4			
85		17.4	22	46	9.2	5.7			
175	948.5	17.5		49	9.8	6.8			
385	941.5	16.9	22	49	9.6	6.3			
625	933.0	16.2		51	9.5	6.3			
835	926.0	15.5		51	9.2	5.8			
1015	920.0	15.0		53	9.2	5.8		Turbc	
1525	902.5	13.6		82	9.8	6.7		Hvy turbc	
2520	870.0	10.8		66	8.7	5.0			
3020	854.0	9.3		77	9.2	5.8			
3510	838.5	8.0		80	8.8	5.1			
4030	822.0	6.5		83	8.3	4.0			
5040	791.5	4.3	32	88	7.5	2.8			
6040	762.0	2.2		90	6.6	1.0		Cloud layer 4600-5460'	
7075	732.5	-0.2	--	95	6.3	-0.5			
995	920.5	15.1	36	56	9.7	6.6		Turbc	
65	952.5	18.6	22	49	10.6	7.9		Obsr J.D.	

# See Legend

No. 47 & 48S

Table 13.1 (Continued)

FIELD TEST NO. 48R				21 AUGUST 1956			0900 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
75	944.5	16.2		74	13.9	11.9		(T eq response rate checked) Bouncy - sudden drafts	
185	940.5	15.8		72	13.2	11.0		Bouncy	
405	933.0	15.2		75	13.2	11.1		Continual turbc	
645	925.0	14.5		79	13.3	11.2			
830	918.5	13.8	22	81	13.1	11.0			
1015	912.5	13.4		82	12.9	10.7		Less turbc	
1595	895.5	13.3	28	80	12.4	10.2		Inversion osc = 0.6°C in half mile	
2040	878.5	14.2		65	10.8	8.1		Smooth onl bump	
2520	863.0	13.0		69	10.5	7.7			
3050	846.0	11.7		65	9.2	5.8		Smooth	
3540	830.5	11.3		60	8.4	4.1		(Vaby exceptional haze)	
4050	815.0	10.8		47	6.7	1.0		(Dark to S)	
5050	784.5	11.7		39	5.4	-1.5		(White streak E horizon)	
6060	755.0	10.9		36	5.1	-2.2			
7095	725.5	9.1		40	4.6	-3.4			
995	913.0	14.2	34	81	13.3	11.2		Bumps at 1500', temp drops	
95	944.0	17.4	32	66	13.3	11.2		Gusts Obsr P.H.	

FIELD TEST NO. 49				21 AUGUST 1956			1100 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
75	943.0	20.5	23	49	11.9	9.5		(T eq response = 0.1°C/10 sec) Side gust felt	
165	940.0	19.9	22	50	11.7	9.3			
375	933.0	19.6		50	11.5	9.0		Up & downs	
615	924.5	18.5		52	11.3	8.8			
835	917.0	18.1		55	11.7	9.2		Bumpy	
995	912.0	17.5		58	11.8	9.4		Drafts	
1505	895.0	16.3	22	64	12.1	9.8		Sharp gusts, wallow	
2000	878.5	15.6	22	64	11.6	9.1			
2510	862.0	14.5		62	10.4	7.6			
3040	845.0	14.2	32	70	11.3	9.0		Lgt drafts felt to 3500'	
3520	830.0	14.0		60	9.8	6.7			
4030	814.0	13.0		62	9.5	6.3		R II dip around 3800'	
5030	784.0	11.7		33	4.5	-3.5		R II drop about 4800'	
6060	754.0	11.1		35	4.7	-3.2			
7075	725.0	9.0		35	4.1	-4.8			
995	912.0	18.4	34	60	12.8	10.7		Neg 1/2 G at about 1800'	
85	943.0	21.9		49	12.8	10.6		Rough Obsr P.H.	

# See Legend

No. 48R & 49

Table 13.1 (Continued)

FIELD TEST NO. 50		21 AUGUST 1956					1400 CST	Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
110	939.0	26.3	23	43	14.7	12.7		
185	936.5	25.6	23	43	14.1	12.1		
390	929.5	25.2	23	43	13.8	11.8		
650	921.5	24.3	23	45	13.8	11.7		
850	914.0	23.7	22	45	13.3	11.2		
1020	908.0	22.9	22	46	13.0	10.8		
1530	891.0	21.3		52	12.6	10.4		
2045	873.5	19.6	22	54	12.8	10.6		
2535	856.5	18.6		52	11.4	9.9		
3055	842.0	17.8	82	36	7.4	2.6	Sharp temp drop	
3555	826.0	16.8	32	36	6.9	1.7		
4045	811.0	15.4		38	6.7	1.4		
5055	780.5	12.7		38	5.6	-1.0		
6085	750.5	10.8	82	35	4.6	-3.4		
7040	723.5	10.1		29	3.6	-6.3		
1010	908.5	23.7		45	13.4	11.2	at 3400 turbc	
100	939.5	27.8	23	36	13.3	11.2	Obsr J.K.	

FIELD TEST NO. 51		21 AUGUST 1956					1530 CST	Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
75	939.0	30.5 27.4		39	14.1	12.1	Yawing in cross wind	
175	935.5	27.4	22	39	14.2	12.1	Drafts, Pireps	
365	925.0	26.8	22	40	14.0	12.0	Hard to hold EI at 600	
615	920.5	26.4	23	42	14.4	12.5	Wallows, bumps, drafts	
805	914.0	25.7	62	41	13.6	11.5	Drafts	
1015	907.0	25.0	--	42	13.3	11.2		
1525	890.0	23.5	22	43	12.5	10.2		
1890	875.0	21.6		45	11.7	9.4		
2520	858.0	20.4	22	46	11.2	8.6	Hard to hold wings level	
3015	842.0	18.8		47	10.2	7.3		
3500	827.0	17.0		50	9.9	6.8	Bumpy	
4015	811.0	15.4		68	12.0	9.8	Rocky like boat	
5030	780.5	12.9		71	10.8	8.1		
6035	751.9	9.9		80	10.0	7.0	Rocky	
6975	724.5	8.0	22	50	5.5	-1.3	R H Response marked	
6500	737.8	8.4		82	9.3	5.9	In clear (base at 6800')	
1015	907.0	25.3		39	12.6	10.4	In cloud tmp drops 2°C	
85	939.5	28.6		37	14.4	12.4	Obsr P.H.	

# See Legend

No. 50 & 51

Table 13.1 (Continued)

FIELD TEST NO. 52		24 AUGUST 1956					1115 CST	Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
50	950.5	22.9	23	38	10.5	7.7		
115	948.0	22.3	23	38	10.3	7.4		
175	946.0	22.0	22	38	10.1	7.1		
385	938.5	21.4	22	39	10.0	6.9		
630	930.0	20.8	22	39	9.6	6.4		
825	923.5	19.8		44	9.6	6.3	Bumpy	
1015	917.0	18.3		42	9.5	6.2		
1515	900.5	17.8	82	47	9.6	6.4	Drafts	
2010	884.0	16.6		45	8.5	4.6	Drafts	
2535	867.0	15.2		47	8.2	4.0		
3030	851.0	13.6		50	7.9	4.5		
3535	835.0	13.2	23	47	7.1	2.1	Undulations on traverse	
4030	819.5	12.8	33	50	7.4	2.7	Smooth RH change 4500'	
5060	798.5	12.5		70	10.3	7.4	Shallow Ac to S at	
6060	788.0	10.3		75	9.6	6.4	Top haze layer	
7085	730.0	8.5		60	6.8	1.4	Cold noted on descent.	
1005	917.5	19.5	32	42	9.6	7.4	Bumpy around 4000'	
60	950.0	23.1	23	35	10.1	7.1	Pireps updraft, also recorded	

Obsr P.H.

FIELD TEST NO. 53		24 AUGUST 1956					2000 CST	Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
165	942.5	22.7	--	39	10.7	8.0	One bump	
395	934.5	22.5		39	10.6	7.8	Very smooth	
635	926.0	21.6	--	39	10.1	7.2		
835	919.5	21.1		41	11.3	7.4		
1015	913.5	20.7		41	10.1	7.1	Smooth	
1520	896.5	20.1		38	8.9	5.4		
2020	880.0	18.6		39	8.4	4.4		
2520	863.5	17.1		41	8.1	4.0	Minor bump	
3030	847.5	16.0		43	7.8	3.4		
3530	831.5	15.0	32	47	8.0	3.8	Tiny bump	
4035	816.0	15.2	22	48	8.3	4.3		
5045	785.5	13.9		50	8.0	3.8		
6065	755.5	12.3		43	6.2	0.2		
7070	727.0	10.1		48	5.9	-0.4	Above haze	
995	914.0	20.8		39	9.6	6.4		
185	941.5	21.4		42	10.7	8.0	Obsr P.H.	

# See Legend

No. 52 & 53

Table 13.1 (Continued)

FIELD TEST NO. 54		24 AUGUST 1956				2200 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
6	948.5	18.1		53	11.2	8.6	Take off	
160	943	19.9		47	11.2	8.6	Slight turb	
370	936	20.2		46	11.3	8.8		
610	929	21.0		41	10.5	7.7		
820	920.5	20.4		42	10.2	7.4	Smooth	
990	915	20.5		42	10.4	7.5	Bump	
1505	897.5	19.6		40	9.5	6.2		
2195	875.0	18.8		43	9.6	6.4		
2495	865.5	18.0		45	9.5	6.2		
3000	849.0	17.4		45	9.1	5.6		
3495	833.5	17.0		46	9.1	5.6		
4005	817.5	16.3		45	8.4	4.4		
5005	787.5	14.4		47	8.0	3.7		
6030	757	12.6	--	36	5.7	-1.6		
7050	728	10.3		64	8.2	4.1		
970	916	20.2		42	10.1	7.1	(Pireps higher engine output reqrd all traverses)	
160	943	19.5		47	10.9	8.2		
6	948.5	19.1	--	50	10.8	8.2	Landing Obsr P.H.	

FIELD TEST NO. 55		25 AUGUST 1956				0100 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
6		16.4		67	12.7	10.6	Take off	
155	942.5	17.1		58	11.8	9.4		
405	934.0	17.4		54	11.2	8.6		
615	927.0	18.7	32	50	11.2	8.6		
845	919.0	19.6		46	10.8	8.2	Pireps turbc noted below	
1015	913.5	19.6		46	10.6	7.8		
1525	896.0	20.0		43	10.1	7.2		
2000	880.0	19.8		45	10.4	7.6		
2490	864.5	19.1		48	10.8	8.1		
3020	847.5	19.2		49	11.2	8.6		
3515	832	18.1		49	10.2	7.2		
4025	816.5	17.1		52	10.2	7.6	Steady going	
5020	786	15.0		52	9.2	5.7		
6040	756.5	13.2		48	7.4	2.6		
7035	728	11.2		41	5.5	-1.2		
985	914.5	19.3		45	10.2	7.2		
195	941	18.4		62	12.0	9.7		
6	948	16.5		60	11.6	9.1	Landing Obsr J.K.	

# See Legend

No. 54 &amp; 55

Table 13.1 (Continued)

FIELD TEST NO. 56		25 AUGUST 1956				0300 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
6	948	16.4		70	13.2	11.2	Take off	
155	942.5	16.0		68	12.8	10.6	Lgt turbc	
385	934.5	17.2		63	12.8	10.6	Lgt turbc	
625	926.5	17.9		57	12.0	9.7		
855	918.5	19.3		49	11.1	8.5		
1015	913.5	19.6		47	10.9	8.2	Possible Neg G	
1515	896.5	20.3	32	46	11.0	8.4		
2020	880.0	19.9		48	11.3	8.8		
2510	864.0	19.6		49	11.2	8.6		
3020	847.5	19.7		48	11.0	8.4	Possible Neg G	
3510	832.5	18.9		49	10.8	8.1		
4030	816	18.4	32	48	10.3	7.4		
5040	785.5	16.3		46	8.7	4.9	Some lgt turbc	
6340	756.5	13.2		53	18.8	4.4	Draft	
7055	727.5	10.2		66	8.5	4.6	Down Draft. Undulations Ac E1500MSL	
985	914.5	19.7	62	46	10.5	7.7	Rough now	
165	942.5	19.2		68	12.8	10.6	Landing	
6	948.0	16.5		66	12.6	10.4	Obsr P.H.	

FIELD TEST NO. 57		25 AUGUST 1956				1730 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)		
50	938.5	33.7		25	13.4	11.3		
95	936.5	33.7		26	13.4	11.4	Turbc	
195	933.5	33.1	22	29	14.6	12.6		
395	926.5	32.7	82	29	14.4	12.4		
615	919.0	32.1	22	29	13.9	11.9		
845	911.0	31.1		29	13.2	11.1	Turbc	
1015	905.5	30.5	22	29	12.6	10.4		
1545	888.0	22.8		30	8.4	4.5		
2035	872.0	27.6	22	54	9.2	5.8		
2535	856.0	25.7		34	10.8	9.4		
3030	841.0	23.9		36	10.7	8.0		
3550	824.0	22.2		39	10.5	7.7		
4040	809.0	21.4		38	9.7	6.5		
5070	778.0	18.2		41	8.7	5.0		
6070	749.0	16.2		40	7.3	2.5		
7075	720.5	13.4		31	4.8	-3.0		
1015	905.5	30.4		29	12.7	10.4		
60	938.0	33.4		29	14.9	12.9	Obsr J.D.	

# See Legend

No. 56 &amp; 57

Table 13.1 (Continued)

FIELD TEST NO. 58							25 AUGUST 1956			1930 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)	Temp eq damping checked OK					
190	932.0	31.1	--	31	14.0	12.0	Smooth					Anvil cld West Floccus overhead
410	924.0	32.2	--	26	12.4	10.1						
660	916.0	32.1	62	26	12.4	10.1						
870	909.0	31.2	22	26	11.7	9.3						
1080	902.5	30.5	62	29	12.6	10.4	Bluish haze noted					
1560	886.0	29.2	29	11.8	11.8	9.4						
2055	870.0	27.6	22	29	10.8	8.0						
2545	854.5	26.2	29	10.0	10.0	7.0	Ocni very lgt updraft					
3070	837.5	24.9	--	33	10.3	7.4						
3565	822.0	22.7	35	9.6	6.4		Clear overhead					
4075	806.5	21.2	22	35	8.8	5.1						
5080	776.5	18.4	22	35	7.4	2.6						
6075	747.5	16.3	--	25	4.7	-3.2						
7100	718.5	13.3	29	4.4	-3.9		Floccus overhead					
1010	904.5	30.3	62	28	12.1	9.8	Ocni bump					
215	931.0	30.1	13	30	13.8	10.6	Obsr P.H.					

FIELD TEST NO. 59							25 AUGUST 1956			2230 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)						
190	935.0	26.0		44	13.0	10.8						
490	928.0	29.8		35	13.4	11.2						
630	920.0	31.2		31	13.0	10.8						
850	912.5	30.8		26	11.7	9.2						
1050	906.0	30.9		26	11.5	9.0						
1530	890.0	29.7	--	26	10.8	8.1						
2030	873.5	28.5	--	26	10.1	7.1						
2525	857.5	26.8	--	29	10.3	7.4						
3035	841.5	25.4		28	9.2	5.7						
3525	826.0	23.9		30	9.0	5.5						
4025	811.0	22.3	22	30	8.2	4.1						
5035	780.5	19.1	22	36	8.0	3.8						
6075	750.0	15.9	40	7.2	2.2							
7060	722.0	13.1	--	46	7.0	1.9	T lag test 63% in few sec					
1020	907.0	30.5	26	11.4	8.8							
170	936.0	27.8	35	13.2	11.1		Obsr J.D.					

# See Legend

No. 58 &amp; 59

Table 13.1 (Continued)

FIELD TEST NO. 60							27 AUGUST 1956			0030 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)						
6	938.0	24.2		40	12.1	9.8	Take off					
185	932.0	26.8		34	12.0	9.7	Turbc below 600 ft					
385	925.0	28.1	23	31	11.8	9.4						
625	917.0	28.8		28	11.1	8.5						
825	910.0	29.0		28	11.6	9.2						
1015	903.5	28.3		29	11.2	8.6						
1515	887.0	29.0		26	10.3	7.4						
2005	871.0	27.9		29	10.9	6.3						
2490	855.5	26.6		28	9.8	6.7						
3025	838.5	25.3		28	9.1	5.6						
3510	823.5	23.8		30	9.0	5.4						
4030	807.5	22.2	--	33	8.8	5.2						
5020	777.5	19.1		33	7.2	2.4						
6030	748.5	16.1		36	6.8	1.2						
7085	718.5	13.1		42	6.5	0.8						
1025	903.5	29.9		25	10.4	7.5						
195	931.5	26.6	--	34	11.8	9.5						
9	938.0	25.7		36	11.9	9.5	Landing					

Obsr J.D.

FIELD TEST NO. 61							27 AUGUST 1956			1100 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)						
6	934.0	32.5	23	39	19.1	16.8	Take off					
90	931.0	28.7	23	33	13.2	11.0	Bouncy					
190	927.5	28.6	23	33	13.0	10.0						
380	921.0	28.0	22	33	12.6	10.4	Lift					
645	912.0	27.3	23	33	11.1	9.8	Bouncy					
845	905.5	26.5	32	11.2	8.7		G felt in drafts					
1015	900.0	26.2	22	34	11.8	9.4	Drafts					
1525	883.0	24.9	24	35	11.0	9.4						
2030	866.5	24.9	62	32	10.2	7.3	Small bumps					
2525	850.5	24.4	64	32	10.0	7.0						
3040	834.0	22.5	--	32	8.8	5.1						
3540	819.0	21.0		35	8.7	4.9	Bumps with drafts					
4040	803.5	20.3	22	32	7.8	3.4	Wallowy					
5045	773.5	17.4		38	7.6	3.1						
6050	744.5	14.7	22	47	7.9	3.6						
7065	716.0	11.8	--	50	7.0	1.9	Not smooth					
995	900.5	26.4	33	34	11.8	9.4	Bouncy & drafts					
90	931.0	29.6	14	31	12.8	10.7						
6	934.0	30.2		32	13.6	11.6	Landing					

# See Legend

No. 60 &amp; 61

Table 13.1 (Continued)

FIELD TEST NO. 62		27 AUGUST 1956					1400 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
6	934.0	28.9		43	17.0	15.0	Take off Turbc		
90	931.0	28.3		39	15.2	13.2			
180	928.0	28.3	22	36	14.0	12.0			
380	921.5	27.8		36	13.6	11.6			
620	913.0	27.8		36	13.2	11.1			
810	907.0	28.0		31	11.8	9.4			
1010	900.0	27.7		31	11.6	9.1			
1505	883.5	26.4	32	32	11.0	8.4			
2015	867.0	25.5		30	9.9	6.8			
2505	851.5	24.3	22	30	9.2	5.8			
3015	835.5	22.6	62	32	8.9	5.2	Bumps		
3515	820.0	20.9		36	9.0	5.4	Bumps		
4025	804.0	19.4	22	39	8.8	5.1			
5035	774.0	16.6	43	43	8.1	4.0			
6045	744.5	13.6		49	7.7	3.2			
7050	716.5	12.6		51	7.4	2.8			
900	901.0	28.2	--	30	11.4	9.0			
80	931.5	31.6	62	26	12.0	9.6	Landing		
6	934.0	31.4		32	14.6	12.7			

Obsr J.D.

FIELD TEST NO. 63		27 AUGUST 1956					2000 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
6	931.0	28.3		31	11.9	9.6	Take off		
195	925.0	31.4	--	33	15.2	13.2	Smooth		
385	918.5	31.2		33	15.1	13.2	Smooth		
630	910.0	30.6		31	13.8	11.7			
835	903.0	30.0		33	14.2	12.2			
1015	897.0	29.7	--	33	13.8	11.8	Smooth		
1525	880.5	28.2		33	12.8	10.6			
2020	864.5	26.8		36	12.6	10.4			
2520	845.5	25.4		36	11.6	9.2			
3050	831.5	23.7		36	10.6	7.8			
3540	816.5	22.5		35	9.6	6.4		Smooth	
4055	801.0	21.6		30	8.2	4.0	Smooth		
5050	771.0	18.5		33	6.9	1.6			
6070	741.5	16.0		32	5.9	-0.4			
7075	713.5	13.1	--	33	5.0	-2.4			
1005	897.5	29.1	32	33	13.4	11.4			
180	925.5	31.2		33	15.0	13.0		Landing	
6	931.0	28.7		38	15.0	13.0			

No. 62 &amp; 63

# See Legend

Table 13.1 (Continued)

FIELD TEST NO. 64		27 AUGUST 1956					2200 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
6	931.0	20.5		69	16.6	14.6	Take off		
205	924.0	30.0		33	14.0	12.0	Very steady going		
435	916.0	30.4	22	33	14.4	12.4			
670	908.5	30.0		22	13.2	11.2			
890	901.0	30.0	22	29	12.4	10.1			
1055	895.0	29.7		29	12.1	9.8			
1560	879.0	28.6		29	11.6	8.1			
2080	862.0	27.5		29	10.7	8.0			
2575	846.0	26.1	22	30	10.2	7.3			
3070	830.5	24.8		32	10.0	7.0			
3565	815.5	23.0		32	9.2	5.8			
4070	800.0	21.8		28	7.4	2.7			
5080	769.5	18.7		33	7.2	2.0			
6080	741.0	15.6		33	5.9	-0.5			
7105	712.5	12.6		40	5.8	-0.6			
1045	896.0	28.9		31	12.5	10.3	Landing		
195	924.5	27.7	24	42	15.6	13.6			
6	931.0	25.9		43	14.4	12.4			

Obsr J.K.

FIELD TEST NO. 65		29 AUGUST 1956					1900 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
6	932.0	24.5		33	10.3	7.4	Take off		
190	925.5	26.4	22	30	10.2	7.4	Smooth oncl bump		
395	919.0	26.3		28	9.6	6.4			
645	910.0	25.8		28	9.3	6.0			
875	902.5	25.2		30	9.7	6.5			
1045	897.0	24.7		32	10.0	7.0	Slight draft Occasional light turbc		
1530	881.0	22.6		32	9.0	5.4			
2020	865.0	21.7		36	9.3	6.0			
2510	849.0	20.0		38	9.0	5.6			
3040	832.5	18.6	22	43	9.2	5.8			
3540	817.0	17.5	--	46	9.2	5.8			
4050	801.5	15.8		49	8.7	5.0			
5050	771.5	13.3		50	7.6	3.0			
6080	741.5	11.8		43	6.0	-0.2			
7105	713.0	9.4		36	4.3	-4.2			
1005	898.0	24.9		32	10.2	7.4	Slt turbc Landing		
195	925.5	25.7	33	32	10.6	7.8			
6	932.0	24.7		33	10.4	7.4			

No. 64 &amp; 65

# See Legend



Table 13.1 (Continued)

FIELD TEST NO. 66		29 AUGUST 1956					2133 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
6	932.0	20.7	82	46	11.2	8.8		Take off delay - flat tire	
190	925.5	23.6		36	10.5	7.6		Gust or bump Draft or bump	
400	918.5	25.8	65	32	10.5	7.8			
640	910.5	25.7		30	10.0	7.0			
885	902.0	25.2	--	32	10.4	7.5			
1060	896.5	24.4	82	33	10.0	7.0		Smooth	
1560	880.0	23.1	13	30	8.6	4.8			
2085	863.0	22.8	13	25	7.0	1.8			
2555	848.0	22.1	12	25	6.8	1.2			
3085	831.0	20.6	22	25	6.1	0.0			
3580	818.0	19.4	32	31	6.9	1.8		Slt turbc Slt turbc	
4090	800.0	18.0	32	32	6.8	1.5			
5080	770.5	15.2	22	36	6.3	0.2			
6095	741.5	12.6	32	39	5.7	-0.8			
7120	712.5	9.9		40	4.9	-2.8			
1030	897.5	24.5		32	10.0	7.0		Slight turbc Landing	
205	925.0	22.3	--	41	11.1	8.5			
6	932.0			38	10.2	7.2			

Obsr P.H.

FIELD TEST NO. 67		30 AUGUST 1956					0020 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
6	932.0	19.7	--	48	10.5	8.2		Take off	
220	924.5	21.7		41	10.7	8.0		Bumpy below 300 ft	
430	917.5	24.6	25	36	11.0	8.4		Slight turbc	
670	909.5	24.6	82	35	10.9	8.2		Smooth	
880	902.5	23.7	62	37	10.2	7.2			
1080	896.0	23.2	82	36	10.4	7.4		Lting SW Pireps slt turbc Slt turbc	
1570	879.5	21.6		46	12.0	9.6			
2075	863.5	21.0		42	10.5	7.8			
2545	848.5	20.5		33	7.9	3.5			
3065	832.0	20.0	22	29	6.8	1.4			
3565	816.5	19.6	32	25	5.7	-1.0		Turbc wallowy	
4085	800.5	18.4	32	28	6.1	-0.2			
5085	771.0	15.2		35	6.2	0.0			
6090	741.5	12.6		36	5.4	-1.6			
7110	713.0	9.7		40	4.8	-2.8			
1040	897.0	23.2		41	11.7	9.3		Rough at 200' Bumps Landing	
225	924.5	22.1	62	39	10.4	7.5			
6	932.0	22.1		37	9.9	6.8			

# See Legend

No. 66 &amp; 67

Table 13.1 (Continued)

FIELD TEST NO. 68		30 AUGUST 1956					0230 CST		Remarks
Z <sub>p</sub> (ft)	P (mb)	T (°C)	#	RH (%)	e (mb)	T <sub>d</sub> (°C)			
6	931.0	21.6	22	43	11.2	8.6		Take off	
200	924.5	22.8	64	39	10.8	8.1		Bump not turbc	
420	917.0	23.4	14	36	10.3	7.4		Turbc	
675	908.0	23.8	24	35	10.5	7.6			
880	902.0	23.6	12	32	9.3	6.0		Turbc draft Lgt bump Wallowy	
1050	896.0	23.2		32	9.1	5.6			
1540	879.5	22.2	22	32	8.7	5.0			
2040	863.5	22.2	12	28	7.7	3.2			
2525	848.0	22.8	32	25	6.9	1.8			
3045	831.5	21.4	62	25	6.4	0.7			
3565	815.5	20.2	--	25	5.9	-0.4		Pireps rocky Down draft at 4500	
4055	800.5	18.9	12	28	6.3	0.4			
5065	770.5	16.0	22	28	5.2	-2.0		Turbc Gusts in descent Bouncy Down draft at 250'	
6075	741.0	13.2		33	5.0	-2.3			
7100	712.5	10.1		36	4.5	-3.8			
1010	897.0	25.0	23	27	8.8	5.0		Mild wind shift encountered. in about 2 miles 2 cycles ± 1°C tmp change at 725', updraft with ΔT 2.1°C in about 1/2 mile	
200	924.0	23.6	82	38	11.0	8.4			
6	931.0	24.1		35	10.6	7.8			

# See Legend

No. 68

GEOPHYSICAL RESEARCH PAPERS

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- No. 3. Diffraction Effects in the Propagation of Compressional Waves in the Atmosphere, Norman A. Haskell, Geophysics Research Directorate, March 1950.
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- No. 5. Investigation of Stratosphere Winds and Temperatures From Acoustical Propagation Studies, Albert P. Crary, Geophysics Research Directorate, June 1950.
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- No. 7. Proceedings of the Conference on Ionospheric Research (June 1949), edited by Bradford B. Underhill and Ralph J. Donaldson, Jr., Geophysics Research Directorate, December 1950.
- No. 8. Proceedings of the Colloquium on Mesospheric Physics, edited by N. C. Gerson, Geophysics Research Directorate, July 1951.
- No. 9. The Dispersion of Surface Waves on Multi-Layered Media, Norman A. Haskell, Geophysics Research Directorate, August 1951.
- No. 10. The Measurement of Stratospheric Density Distribution with the Searchlight Technique, L. Elterman, Geophysics Research Directorate, December 1951.
- No. 11. Proceedings of the Conference on Ionospheric Physics (July 1950) Part A, edited by N. C. Gerson and Ralph J. Donaldson, Jr., Geophysics Research Directorate, April 1952.
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