KAYGORODOVA, R.Ye.; BEREZOVSKAYA, Ye.K. (Moskva V-334, Vorob'yevskoye shosse, d.2, kv.1)

Endothelioma of the thoracic aorta. Grudn. khir. 5 no.4:88-90 Jl-Ag'63 (MIRA 17:1)

BEREZOVSKAYA, Z.A.

ROMANKOV, P.G.; NOZDROVSKIY, A.S.; SIL'MAN, A.I.; RASHKOVSKAYA, N.B.; BEREZOVSKAYA, Z.A.

Separation of finely dispersed, difficultly filterable suspensions in centrifuges of the sedimentation type. Khim. prom. no.8:480-486 D '57. (MIRA 11:2)

(Colloids) (Centrifuges)

Berezovskaya, Z.A.

AUTHORS: Romankov, P. G., Nozdrovskiy, A. S., Sil'man, A. I., Rashkovskaya, N. B., Berezovskaya, Z, A.

64-8-8/19

TITLE: **Separation of Finely-dispersed, Hard-to-separate Suspensions in Precipitating-type Centrifuges** (Razdeleniye tonkodispersnykh plokho fil'truyushchikhsya suspensiy na tsentrifugakh osaditel'nogo tipa).

PERIODICAL: Khimicheskaya Promyshlennost', 1957, Nr 8, pp. 32-38 (USSR)

ABSTRACT: Here the results are given of the proving of some types of separation centrifuges in operation with suspensions of the azodyes, i. e. of the direct black 3 and of the acid blue black, as well as with suspensions of the iron- and cobalt hydroxides. Investigated were:
1) yeast separators. The experiments showed that these cannot be used for a continuous separation of the suspensions from azodyes in order to obtain a paste-like sediment.
2) Centrifuge with removal of the precipitation by means of a knife. The experiments showed that this can be of certain interest since inspite of a semicontinuity of the process a

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high mechanization degree of the same is obtained and an automatation of the discharge of the liquid and solid phase is possible during the operation. This centrifuge can be used only for a rough separation of the azodye suspensions.
3) The "OCH"-separator with a precipitation discharge by centrifugal force. The experiments showed that this separator is apt for the production of a dye of normal strength. The output of the same from the suspension was satisfactory. The disadvantage of the separator: it is not quite apt for the working of suspensions with high mineral salt content (more than 20%). The experiments carried out for the separation of not salted-out suspensions showed that such one can be carried out with this separator. The dyes of some types (e. g. the direct brown KX) can be separated more easily from the not salted-out suspensions than from the salted-out ones. As a rule, the concentration of the dye from the not salted-out suspensions is higher than from normal suspensions, even if the humidity content of the paste is higher before drying in the first case.
4) Separation centrifuge with a spiral discharge of the precipitation. The experiments showed that inspite of a

velocity up to 6300 U/min (separation factor 2900) no discharge of the precipitation took place. According to the reconstruction of the sample the centrifuge worked normally and the discharge took place continuously. The output amounted to from 20 up to 70 liters/min. The value of the separation factor amounted in the case of the 4 types given here to: 4600, 2100, 7200 and 4000, 1150. It was shown that in the separation of fine-disperse systems, as it is the case with the azodye suspensions the existence of separating plates is indispensable. These plates exist in the separation centrifuge with spiral discharge. This type is interesting for the industry. The construction was made by A. S. Nozdrovskiy. The present paper was carried out with the aid of following persons, or works resp.: B. A. Ikonnikov and I. T. Shkuta of the chemical works of Derbenev; testing industry enrichment factory Zhilevsk; NIIprodmash; M. V. Sizov from the chemical works of Derbenev.
There are 6 figures, 5 tables.

Separation of Finely-dispersed, Hard-to-separate Suspensions in Precipitating-type Centrifuges 64-8-8/19

AVAILABLE: Library of Congress

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APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000204910003-2"

ROMANKOV, P.G.; RASHKOVSKAYA, N.B.; BEREZOVSKAYA, Z.A.

New method of drying paste-like pigments. Lakokras.mat.i ikh prim. no.3:71-74 '60. (MIRA 14:4)

1. Leningradskiy tekhnologiceskiy institut imeni Lensoveta.
(Pigments--Drying)

ROMANKOV, P.G.; RASHKOVSKAYA, N.B.; BEREZOVSKAYA, Z.A.; YABLONSKIY, P.A.

Drying some pastelike pigments in a fluidized bed. Lakokras. mat. i ikh prim. no.6:61-64 '61. (MIRA 15:3)

1. Leningradskiy tekhnologicheskiy institut imeni Leningradskogo Soveta.

(Pigments) (Drying apparatus)

ROMANKOV, P.G., doktor tekhn.nauk; RASHKOVSKAYA, N.B., kand.tekhn.nauk; YABLONSKIY, P.A., kand.tekhn.nauk; BEREZOVSKAYA, Z.A., kand. tekhn.nauk

Drying of a pastelike copper-nickel catalyst in a fluidized bed. Masl.-zhir.prom. 28 no.7:10-13 Jl '62. (MIRA 15:11)

1. Leningradskiy tekhnologicheskiy institut imeni Lensoveta.

(Nickel catalysts--Drying)
(Fluidization)

BEREZOVSKIY, A. A.

PA 33/49T76

USSR/Medicine - Plants
Medicine - Sugars

Oct 48

"Improving Silo Property of Plants With Uncertain Sugar Minimum," A. A. Berezovskiy, Cand Agr Sci, M. F. Yegorova, All-Union Sci Res Inst of Fodder, 4 pp

"Dok v-s Ak Selkhoz Nauk" No 10

Addition of dry fodder to plants, whose humidity has been decreased without maintaining minimum sugar content, increases sugar content in the green fodder due to hydrolysis of polysaccharides. Intensive saccharification of the starch with

[redacted] 33/49T76

USSR/Medicine - Plants (Contd) Oct 48

decrease in humidity is due to increased hydrolytic activity. Method may be used for processing many field products with low sugar content. Good results with potatoes. Submitted 30 Apr 48.

[redacted] 33/49T76

BERESZOVSKIY, A.A.

25125. BEREZOVSKIY, A. A. Silosovaniye Trudnosilosuyushikhsya I Nesnlosuyushikhsya Rasteniy V Smesi S Gumennymi Kormami. V SB: Voirosy Kormodobyvaniga. Uyp. 2. M., 1949. S. 189-91

SO: Letopis' No. 33, 1949

BEREZOVSKIY, A.A. I ORLOV, I. P.

25147. BEREZOVSKIY, A. A. I ORLOV, I. P. Sushica Travy Na Veshalkakh. V. SB: Voprosy Kormoobyvaniya, Vyp. 2. M., 1949, S. 204-08-Bibliogr: 5 Nazv.

SO:Letopis' No. 33, 1949

1. BEREZOVSKIY, A. A.

2. USSR (600)

7. "Procedures for Preparing Special Silos", Sov. Zootekhniya, No 6, 1951, pp 62-67.

9. Mikrobiologiya, Vol XXI, Issur 1, Moscow, Jan-Feb 1952, pp 121-132. Unclassified.

1. BEREZOVSKIY, A. A.

2. USSR (600)

7. "Autumn Ensilage", Kormovaya Baza, No 8, 1951, pp 44-47.

9. Mikrobiologiya, Vol XXI, Issue 1, Moscow, Jan-Feb 1952, pp 121-132. Unclassified.

BEREZOVKSIY, A.A.

Means of raising the quality of ensilage
Sov. zootekh. 7 no. 8, 1952

TOMME, J. F.; SIMON, E.I.; KONDYREV, V.; KABOZOV, S.; BEREZOVSKIY, A.

Feeding and Feeding Stuffs

Feeding chaff to horses. ("Preparation of feed stuffs for feeding." Prof. M. F. Tomme, E. I. Simon; "Organize the preparation of feed stuffs on every farm." V. Kondyrev, S. Kabozov, A. Berezovskiy. Reviewed by N. A. Leyzerson). Konevodstvo 22 no. 8, 1952.

Monthly List of Russian Accessions, Library of Congress, November 1952. UNCLASSIFIED.

BEREZOVSKIY, A.A., kand. sel'skokhozyaystvennykh nauk.

Finishing up the drying of hay with cold and warm air. Zhivotnovodstvo 20 no.5:44-45 My '58. (MIRA 11:5)
(Hay--Harvesting) (Ensilage)

BEREZOVSKIY, Aleksey Aleksandrovich

[Ensilage] Silosovanie kormov. Moskva, Gos.izd-vo sel'khoz. lit-ry, 1959. 105 p. (MIRA 13:8)
(Ensilage)

BEREZOVSKIY, A.A., kand.sel'skokhozyaystvennykh nauk

Mixed silage for swine. Zhivotnovodstvo 22 no.7:17-21 '60.
(MIRA 16:5)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut zhivotnovodstva.
(Swine--Feeding and feeds) (Ensilage)

BEREZOVSKIY, A.A., kand. sel'skokhoz. nauk

Some problems in the preparation of mixed silage. Zhivotnovodstvo 24 no.6:39-41 Je '62. (MIRA 17:3)

BEREZOVSKIY, Aleksey Aleksandrovich, kand. sel'khoz. nauk; LEONOVA, T.S., red.; RAKITIN, I.T., tekhn. red.

["Dietetic" feeds] "Dieticheskii" korm. Moskva, Izd-vo "Znanie," 1963. 29 p. (Novoe v zhizni, nauke, tekhnike. V Seriia: Sel'skoe khoziaistvo, no.2) (MIRA 16:1)
(Ensilage)

BEREZOVSKIY, Aleksey Aleksandrovich, kand. sel'khoz. nauk; GROMOVA, A.V., red.; OKOLELOVA, Z.P., tekhn. red.

[Preparing and using combined silage] Prigotovlenie i ispol'zovanie kombinirovannogo silosa. Moskva, Sel'khozizdat, 1963. 77 p. (MIRA 16:11)

(Ensilage)

BEREZOVSKIY, A.A., kand.sel'skokhoz.nauk

Sugar beet ensilage. Zhivotnovodstvo 24 no.9:39-41 S '62.
(MIRA 15:12)

1. Vsesoyuznyy institut zhivotnovodstva.
(Sugar beets) (Ensilage)

BEREZOVSKIY, A.A., starshiy nauchnyy sotrudnik

Chemical preservation of green feeds. Inform.biul.VDNKH no.5:22-23 My '64. (MIRA 18:5)

1. Vsesoyuznyy institut zhivotnovodstva.

ACC NR: AR6025703 SOURCE CODE: UR/0196/66/000/004/A007/A007

AUTHOR: Berezovskiy, A. A.; Nizhnik, L. P.

TITLE: Surface loss in a nonlinear ferromagnetic semispace

SOURCE: Ref. zh. Elektrotekhnika i energetika, Abs. 4A54

REF SOURCE: Elektromashinostr. i elektrooborudovaniye. Resp. mezhved. nauchno-tekhn. sb. vyp. 1, 1965, 5-8

TOPIC TAGS: electric machine, electromagnetic field, electric equipment, transformer

ABSTRACT: One of fundamental simulation problems in the calculation of additional losses in electrical machinery and transformers is considered, viz., the determination of electromagnetic field and losses in a nonlinear ferromagnetic semispace. A tangential component of the magnetic field strength vector H_{τ} periodically varying with time is specified at the surface of the semispace. An equivalent magnetic permeability $\bar{\mu}$ and a characteristic resistance $\bar{r}$ of the nonlinear semispace are introduced, which permits expressing the surface-loss formula in terms of $\bar{r}$ and $H_{\tau}(0)$ at the surface. Approximate formulas are offered for $\bar{\mu}$ and $\bar{r}$ that permit determining them from an experimental $\mu(H)$-curve which characterizes the semispace. It is shown how $H_{\tau}(0)$ can be determined if the a-c density in air over the metal is known. Bibliography of 2 titles.Yu. Chalisov [Translation of abstract]

SUB CODE: 09

Card 1/1 UDC: 538.311

POSTNIKOV, I.M., doktor tekhn.nauk, prof. (Kiyev); NIZHNIK, L.P., kand.fiz.-matem.nauk (Kiyev); BEREZOVSKIY, A.A., kand.fiz.-matem.nauk (Kiyev); KRAVCHENKO, A.N., inzh. (Kiyev)

Calculation of a traveling electromagnetic field in a lamellar conductive medium. Elektrichestvo no.9:1-7 S '65.

(MIRA 18:10)

L 19412-63 EWP(r)/EWT(d)/EWT(m)/FCC(w)/BDS AFFTC/IJP(C)
ACCESSION NR: AR3005377 S/0044/63/000/006/B063/B064

SOURCE: RZh. Matematika, Abs. 6B284

AUTHOR: Berezovs'kyy, A. A.

TITLE: Integro-differential equations of hollow shell statics

CITED SOURCE: Visnyk Kyyivs'k. un-tu, no. 1, 1958, ser. astron., matem. ta mekhan., vyp. 2, 125-137

TOPIC TAGS: integro-differential equation, hollow shell statics, shell theory, Fredholm integral equation

TRANSLATION: The author reduces the problem of shell theory to a system of integral equations. He introduces an assumption which makes it possible to pass from a system to a single second-order Fredholm integral equation. E. Khasabov.

DATE ACQ: 24Jul63 SUB CODE: MM ENCL: 00

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BEREZOVSKIY, A.A. (Kiyev)

Integrodifferential equations of the theory of thin shallow shells. Ukr.mat.zhur. 11 no.2:146-154 '59. (MIRA 12:11)
(Integral equations) (Elastic plates and shells)

16(1),16(2) 05783

AUTHORS: Berezovskiy, A. A., and Shestopal, A. F. (Kiyev) SOV/41-11-4-9/15

TITLE: Integro-Differential Equations for the Local Stability of Flat Shells

PERIODICAL: Ukrainskiy matematicheskiy zhurnal, 1959, Vol 11, Nr 4, pp 434-438 (USSR)

ABSTRACT: According to [Ref 3] the examination of stability of flat thin shells leads to a certain system of differential equations. Starting from this system, the authors consider two states of equilibrium (an undisturbed and a disturbed state) and formulate a theorem on the duality of the work with respect to the disturbandes (compare [Ref 2]). The theorem is used in order to describe the local stability by a system of integro-differential equations. An approximate equation for the local stability of the bending is obtained. An example is given. There are 4 Soviet references.

SUBMITTED: November 25, 1958

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AUTHOR: Berezovskiy, A.A.

TITLE: On the Motion of a Load on a Flat Shell

PERIODICAL: Ukrainskiy matematicheskiy zhurnal, 1960, Vol. 12, No. 1, pp. 79 - 87

TEXT: On a flat shell being rectangular in plan form and pin-jointed along its boundary, there moves a load P the coordinates of which are described by continuous two times differentiable functions $\xi(t)$ and $\eta(t)$. Under neglection of the forces of inertia the influence of the load onto the shell is interpreted as a normal load

$$(1.1) \qquad q(x,y,t) = \begin{cases} 0 & \text{for } x,y \not\subset \varepsilon\,[\xi(t),\eta(t)] \\ \frac{P}{4\varepsilon^2} & \text{for } x,y \subset \varepsilon\,[\xi(t),\eta(t)] \end{cases} .$$

The problem of the forced transverse vibrations leads to the system

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On the Motion of a Load on a Flat Shell

(1.15)

$$\varphi = \int_0^a \int_0^b w \nabla_k^2 \varphi_1 \, dx_1 dy_1 \,,$$

$$w = w_0 + \int_0^a \int_0^b \varphi \nabla_k^2 w_2 dx_1 dy_1 - \varrho h \int_0^a \int_0^b \frac{\partial^2 w}{\partial t^2} w_2 dx_1 dy_1 \,,$$

where φ, w are the tension and bending ; φ_1, w_2 are the solutions of the equations

(1.8) $$-\frac{1}{Eh} \nabla^4 \varphi_1 = \delta, \; D \nabla^4 w_2 = \delta$$

for boundary conditions not contradicting those for φ, w ; δ is the Delta function ; a and b are the length and the width of the ground plan of the shell ; ϱh is the mass per unit area of the middle surface ; E, ν are the modulus of elasticity and the Poisson coefficient,

(1.9) $$D = \frac{Eh^3}{12(1 - \nu^2)}$$

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On the Motion of a Load on a Flat Shell

(1.10) $$\nabla_k^2 = k_1 \frac{\partial^2}{\partial y^2} + k_2 \frac{\partial^2}{\partial x^2} ,$$

k_1 and k_2 are the radii of the principal curvatures of the middle surface.

Furthermore $w_0 = \int_0^a \int_0^b q(x,y,t) w_2 dx\, dy$.

The solution of (1.15) is sought with the arrangement

(1.16) $$\varphi = \sum_{i,j=1}^{\infty} A_{ij}(t) \sin \alpha_i x \sin \beta_j y$$

(1.17) $$w = \sum_{i,j=1}^{\infty} B_{ij}(t) \sin \alpha_i x \sin \beta_j y$$

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On the Motion of a Load on a Flat Shell

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where $\alpha_k = \frac{k\pi}{a}$, $\beta_l = \frac{l\pi}{b}$.

For the determination of the $A_{ij}(t)$, $B_{ij}(t)$ one obtains the system

(1.20) $$A_{ij}(t) = (k_1\beta_j^2 + k_2\alpha_i^2)\frac{EhB_{ij}(t)}{(\alpha_i^2 + \beta_j^2)^2} ,$$

$$B_{ij}(t) = \frac{4P\sin\alpha_i\xi(t)\sin\beta_j\eta(t)}{abD(\alpha_i^2 + \beta_j^2)^2} - \frac{(k_1\beta_j^2 + k_2\alpha_i^2)}{D(\alpha_i^2 + \beta_j^2)^2}A_{ij}(t) - \frac{\rho h}{D(\alpha_i^2 + \beta_j^2)^2}\frac{d^2B_{ij}(t)}{dt^2} ,$$

wherefrom it follows

(1.23)

$$B_{ij}(t) = C_{ij}\sin\omega_{ij}t + D_{ij}\cos\omega_{ij}t + \frac{1}{\omega_{ij}}\int_0^t \frac{4P}{ab\rho h}\sin\alpha_i\xi(t)\sin\beta_i\eta(t)\sin\omega_{ij}(t-\tau)d\tau ,$$

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On the Motion of a Load on a Flat Shell

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where ω_{ij} is given by

$$\omega_{ij}^2 = \frac{D(\alpha_i^2 + \beta_j^2)^2}{\varrho h} + \frac{E(k_1\beta_j^2 + k_2\alpha_i^2)^2}{\varrho(\alpha_i^2 + \beta_j^2)^2} \quad (1.22)$$

Then the author investigates special cases:

1). P moves with a constant velocity. It is stated that a resonance can be reached by a change of the velocity components.

2). $\eta = \frac{b}{2}$ = const, the velocity u is constant. It is shown that the forced part of the general solution for ω equals the static bending of a shell onto which in the point u t, $\frac{b}{2}$ there acts the load P and besides the compriming compressive force

$$T_1 = u^2 \varrho h \quad (3.6)$$

3). Pulsating load : $P = P_0 \sin kt$, ξ = const, η = const. There are 4 Soviet references.

SUBMITTED: January 5, 1959

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S/041/60/012/004/002/011
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AUTHOR: Berezovskiy, A.A.

TITLE: Integro Differential Equations of the Nonlinear Theory of Flat Thin Shells

PERIODICAL: Ukrainskiy matematicheskiy zhurnal, 1960, Vol. 12, No. 4, pp. 373 - 380

TEXT: Let φ be the tension function, w be the bending of the shell, Z be the normal load ; k_1, k_2 be the curvatures of the middle surface ; E, h, D be the modulus of elasticity, thickness and rigidity of the shell. Let

(1.2) $$\nabla^2 = \frac{\partial^2}{\partial \alpha^2} + \frac{\partial^2}{\partial \beta^2}, \quad \nabla_k^2 = \frac{\partial}{\partial \alpha} k_2 \frac{\partial}{\partial \alpha} + \frac{\partial}{\partial \beta} k_1 \frac{\partial}{\partial \beta}$$

(1.3) $$A = \begin{pmatrix} -\frac{1}{Eh}\nabla^4 & -\nabla_k^2 \\ -\nabla_k^2 & D\nabla^4 \end{pmatrix}$$

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Integro Differential Equations of the Nonlinear Theory of Flat Thin Shells

$$\vec{B}\{\varphi, w\}$$

(1.4) $$\vec{C}\left\{\frac{\partial^2 w}{\partial \alpha^2}\cdot\frac{\partial^2 w}{\partial \beta^2}-\left(\frac{\partial^2 w}{\partial \alpha\,\partial \beta}\right)^2,\quad z+\frac{\partial^2 \varphi}{\partial \beta^2}\cdot\frac{\partial^2 w}{\partial \alpha^2}-2\frac{\partial^2 \varphi}{\partial \alpha\,\partial \beta}\cdot\frac{\partial^2 w}{\partial \alpha\,\partial \beta}+\frac{\partial^2 w}{\partial \beta^2}\cdot\frac{\partial^2 \varphi}{\partial \alpha^2}\right\}.$$

With the aid of these notations the differential equations of the theory of shells of V.Z. Vlasov (Ref. 1) can be written in the form

(1.5) $$A\vec{B}=\vec{C}.$$

Let s be the region of definition of $\vec{B}$ and $\vec{C}$; l be the boundary of s . For arbitrary $\vec{B}^1$ and $\vec{B}^2$ at first it is proved

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Integro Differential Equations of the Nonlinear Theory of Flat Thin Shells

(1.8) $$\iint_s (\vec{B}^1 \cdot A\vec{B}^2)ds = \iint_s (\vec{B}^2 \cdot A^* \vec{B}^1)ds + \oint_l L(\vec{B}^1 \vec{B}^2)dl ,$$

where $A = A^*$ and $L(\vec{B}^1, \vec{B}^2)$ is a differential form consisting of bilinear forms of the components of $\vec{B}^1$, $\vec{B}^2$ and their derivatives up to the third order. Now the solution of the system (1.5) for given boundary conditions is chosen as $\vec{B}^1$, while the solution of

(1.9) $$A_0\vec{B}^{\alpha} = \delta_{1\alpha}\vec{\delta\alpha}(\alpha - \xi, \beta - \eta)$$

for in general other boundary conditions is taken as $\vec{B}^2$. Here $\delta_{1\alpha}$ is the Kronecker symbol, $\vec{\delta\alpha}(\alpha - \xi, \beta - \eta)$ is the Delta-vector function and A_0 is determined by

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(1.6) $$A = A_0 + A_1,\ A_0 = \begin{pmatrix} -\frac{1}{Eh}\nabla^4 & 0 \\ 0 & D\nabla^4 \end{pmatrix},\ A_1 = \begin{pmatrix} 0 & -\nabla_k^2 \\ -\nabla_k^2 & 0 \end{pmatrix}.$$

Then (1.8) changes to a system of nonlinear integro differential equations being equivalent to (1.5). The system reads:

(1.11)
$$\varphi = \iint_s (\vec{F}^1 \cdot \vec{C})ds - \iint_s (\vec{B} \cdot A_1 \vec{B}^1)ds + \oint_l L_1(\vec{B}, \vec{B}^1)dl$$
$$w = \iint_s (\vec{B}^2 \cdot \vec{C})ds - \iint_s (\vec{B} \cdot A_1 \vec{B}^2)ds + \oint_l L_2(\vec{B}, \vec{B}^2)\,dl .$$

By some examples it is shown that the solution of (1.11) leads to the same

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Integro Differential Equations of the Nonlinear Theory of Flat Thin Shells

results as the solution of (1.5). The author considers : a shell rectangular in plan form with k_1 = const , k_2 = const ; a spherical shell with an arbitrary load and great bendings.
There are 8 references : 6 Soviet, 1 German and 1 American.

SUBMITTED: February 5, 1959

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BEREZOVSKIY, A. A., Cand. Phys-Math. Sci. (diss) "Integral Equations of the Theory of Sloping Fine Films." Kiev, 1961, 6 pp. (Combined Scientific Council of Institutes of Math., Physics and Metallic Physics, Acad. of Sci. UkSSR) 170 copies (KL Supp, 12-61, 249).

BEREZOVSKIY, A.A. (Kiyev)

Nonlinear integral equations of shallow shells of revolution. Inzh.zhur. 1 no.4:107-114 '61. (MIRA 15:4)
(Elastic plates and shells)

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AUTHOR: Berezovskiy, A. A.

TITLE: Non-linear integral equations of shallow shells of revolution

PERIODICAL: Inzhenerno-fizicheskiy zhurnal, v. 4, no. 5, 1961, 44-53

TEXT: The problem of bending of a shallow shell of revolution subjected to a perpendicular stress P(r) leads to the solution of the system

$$\theta(x) + \int_a^1 \rho f_1(\rho, \theta, s) k_1(\rho, x) d\rho = 0,$$

$$s(x) + \int_a^1 \rho f_2(\rho, \theta) k_2(\rho, x) d\rho = 0, \tag{1.1}$$

where

$$\rho f_1(\rho, \theta, s) = f(\rho) - k^2(\rho) s + \theta s,$$

$$\rho f_2(\rho, \theta) = k^2(\rho)\theta - \frac{\theta^2}{2}, \quad f(\rho) = \lambda \int_a^\rho p(\rho)\rho d\rho, \tag{1.2}$$

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Non-linear integral equations of...

$$\rho = \frac{r}{a}, \quad \alpha = \frac{b}{a}, \quad \theta = -\frac{1}{h}\sqrt{12(1-\mu^2)}\,\frac{dw}{d\rho},$$

$$s = \frac{12(1-\mu^2)a^2}{Eh^3}\rho N_r,$$

$$k^2(\rho) = \frac{1}{h}\sqrt{12(1-\mu^2)}\,\frac{dz(\rho)}{d\rho}, \quad \lambda = \frac{a^4[12(1-\mu^2)]^{3/2}}{Eh^4}, \qquad (1.3)$$

in the case of strong bending. r is the distance of any point from the axis of revolution; b and a are the inner and the outer radius, respectively, of the shell base; $z(\rho)$ describes the central area; h, w, and N_r indicate the thickness, bending, and radial force in the diaphragm, respectively. E and μ are the modulus of elasticity and Poisson's ratio of the shell material; $k_1(\rho, x)$ and $k_2(\rho, x)$ are Green functions; k_1 and k_2 are the kernels of (1.1). These are positive definite, symmetric, continuous functions for which

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$$k_1(\rho, x) = \sum_{l=1}^{\infty} \frac{Z_1(\lambda_l \rho) Z_1(\lambda_l x)}{\lambda_l^2 \int_a^1 \rho Z_1^2(\lambda_l \rho)\, d\rho},$$

$$k_2(\rho, x) = \sum_{l=1}^{\infty} \frac{Z_1(\gamma_l \rho) Z_1(\gamma_l x)}{\gamma_l^2 \int_a^1 \rho Z_1^2(\gamma_l \rho)\, d\rho}, \qquad (1.4)$$

where

$$Z_1(\lambda_l \rho) = c_1 I_1(\lambda_l \rho) + c_2 N_1(\lambda_l \rho),$$
$$Z_1(\gamma_l \rho) = c_1' I_1(\gamma_l \rho) + c_2' N_1(\gamma_l \rho);$$

can be written. I_1 and N_1 are Bessel functions of first order. By substituting (1.4) in (1.1) one obtains expressions for Θ and s(x), which indicate that the solution of (1.1) is equivalent to that of an infinite system of equations with an infinite number of unknowns. The "approximate solutions"

$$\Theta_n(x) = \sum_{l=1}^{n} \alpha_{ln} Z_1(\lambda_l x), \quad S_n(x) = \sum_{l=1}^{n} \beta_{ln} Z_1(\gamma_l x), \qquad (2.4)$$

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where

$$a_{in} + \frac{\int_0^1 \rho f_1 \left[\rho, \sum_{j=1}^{n} a_{jn} Z_1(\lambda_j \rho), \sum_{j=1}^{n} \beta_{jn} Z_1(\gamma_j \rho) \right] Z_1(\lambda_i \rho)\, d\rho}{\lambda_i^2 \int_0^1 \rho Z_1^2(\lambda_i \rho)\, d\rho} = 0, \qquad (2.5)$$

$$\beta_{in} + \frac{\int_0^1 \rho f_2 \left[\rho, \sum_{j=1}^{n} a_{jn} Z_1(\lambda_j \rho) \right] Z_1(\gamma_i \rho)\, d\rho}{\gamma_i^2 \int_0^1 \rho Z_1^2(\gamma_i \rho)\, d\rho} = 0.$$

are analyzed. It is shown that (2.4) are solutions to (1.1); next the author looks for classes, for which such solutions can be found. In a very detailed investigation of the first approximation for different boundary conditions and different kinds of stress, the author compares the results obtained here with those of perturbation theory and the method of Bubnov-Galerkin. This procedure facilitates calculation considerably and

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is based chiefly on integral tables of Bessel functions. There are 1 figure, 1 table, and 11 references: 9 Soviet-bloc and 2 non-Soviet-bloc.

ASSOCIATION: Institut matematiki AN USSR, g. Kiyev (Institute of Mathematics, AS UkrSSR, Kiyev)

SUBMITTED: October 10, 1960

Card 5/5

BEREZOVSKIY, A.A.

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S/021/61/000/006/004/009
D247/D301

AUTHOR: Berezovs'kyy, A.A.

TITLE: On large sags of a shallow shell

PERIODICAL: Akademiya nauk Ukrayins'koyi RSR, Dopovidi, no. 6, 1961, 722 - 726

TEXT: The author considers deflection of a shallow shell with a given rectangular projection freely supported and uniformly loaded on its contour by moments M_1 and M_2 (Fig. 1). The problem is formulated by a system of non-linear integral equations

$$\varphi = \int_0^a \int_0^b w \nabla_h^2 \varphi_1 dx_1 dy_1 + \int_0^a \int_0^b \varphi_1 \left[\frac{\partial^2 w}{\partial x_1^2} \cdot \frac{\partial^2 w}{\partial y_1^2} - \left(\frac{\partial^2 w}{\partial x_1 \partial y_1} \right)^2 \right] dx_1 dy_1 , \tag{1}$$

$$w = \int_0^a \int_0^b \varphi \nabla_k^2 w_2 dx_1 dy_1 + \int_0^a \int_0^b w_2 \left[\frac{\partial^2 \varphi}{\partial y_1^2} \cdot \frac{\partial^2 w}{\partial x_1^2} - 2 \frac{\partial^2 \varphi}{\partial x_1 \partial y_1} \cdot \frac{\partial^2 \varphi}{\partial x_1 \partial y_1} + \right.$$

Card 1/6

$$+\frac{\partial^2 w}{\partial y_1^2}\cdot\frac{\partial^2 \varphi}{\partial x_1^2}\Bigg|dx_1dy_1+M_1\int_0^a\Bigg[\frac{\partial w_2}{\partial y_1}\Bigg|_0^b\Bigg]dx_1+M_2\int_0^b\Bigg[\frac{\partial w_2}{\partial x_1}\Bigg|_0^a\Bigg]dy_1; \quad (1)$$

where w, φ - sag and stress functions of the shell; φ_1, w_2 - corresponding Green's functions for the biharmonic equation:

$$\varphi_1 = -\sum_{k,l=1}^{\infty}\frac{4Eh\sin\alpha_k x\sin\beta_l y}{ab(\alpha_k^2+\beta_l^2)^2}\sin\alpha_k x_1\sin\beta_l y_1,$$

$$w_2 = \sum_{k,l=1}^{\infty}\frac{4\sin\alpha_k x\sin\beta_l y}{abD(\alpha_k^2+\beta_l^2)^2}\sin\alpha_k x_1\sin\beta_l y_1. \quad (2)$$

X

Substituting this in (1) and changing the order of integration, equations are obtained which, upon further substitution, lead to two infinite systems of non-linear algebraic equations for finding the unknowns φ_{kl} and W_{kl}. Taking only one term of the series there is:

$$\Phi_{kl} = \frac{Eh(k_1\beta_\ell^2 + k_2\alpha_k^2)}{(\alpha_k^2 + \beta_\ell^2)} W_{kl} - \frac{16Eh\alpha_k\beta_\ell}{3ab(\alpha_k^2 + \beta_\ell^2)^2} W_{kl}^2$$

$$W_{kl} = \frac{32\alpha_k\beta_\ell\Phi_{kl}W_{kl}}{3abD(\alpha_k^2 + \beta_\ell^2)^2} - \frac{(k_1\beta_\ell^2 + k_2\alpha_k^2)}{D(\alpha_k^2 + \beta_\ell^2)^2}\Phi_{kl} + \frac{16(\ell^2a^2M_1 + k^2b^2M_2)}{a^2b^2D(\alpha_k^2 + \beta_\ell^2)^2} \quad (3)$$

and eliminating φ_{kl},

$$\frac{512}{9}\frac{Eh}{a^2b^2}\frac{\alpha_k^2\beta_l^2}{(\alpha_k^2+\beta_l^2)^2}W_{kl}^3 - 16\frac{Eh}{ab}\frac{\alpha_k\beta_l(k_1\beta_l^2 + k_2\alpha_k^2)}{(\alpha_k^2+\beta_l^2)^2}W_{kl}^2 +$$

$$+\left[Eh\frac{(k_1\beta_l^2+k_2\alpha_k^2)^2}{(\alpha_k^2+\beta_l^2)^2} + D(\alpha_k^2+\beta_l^2)^2\right]W_{kl} = \frac{16(k^2b^2M_2 + l^2a^2M_1)}{a^2b^2kl}. \quad (6)$$

Thus the relationship between deflection and moments M_1, M_2 is obtained. Equations are given also for a shallow spherical shell with a square projection. For a freely supported cylindrical shell compressed by forces T along the edges X = 0 and x = a (Fig. 4) the formula is:

$$\frac{512}{9}\frac{Eh}{a^2b^2}\frac{\alpha_k^2\beta_l^2}{(\alpha_k^2+\beta_l^2)^2}W_{kl}^3 - 16\frac{Eh}{ab}\frac{k_1\alpha_k^2\beta_l}{(\alpha_k^2+\beta_l^2)^2}W_{kl}^2 + \left[Eh\frac{k_2^2\alpha_k^4}{(\alpha_k^2+\beta_l^2)^2} + D(\alpha_k^2+\beta_l^2)^2\right]W_{kl} = \alpha_k^2 T W_{kl}. \quad (11)$$

When the shell has a square projection then

$$k=e=1, \quad \xi_{11} = \frac{W_{11}}{h}, \quad K = \frac{8f}{h}, \quad p^* = \frac{a^2T}{Eh^3}. \quad (13)$$

applies. There are 4 figures and 5 Soviet-bloc references.

ASSOCIATION: Instytut matematyky AN URSR (Institute of Mathematics, AS UkrRSR)

SUBMITTED: October 1, 1960

BEREZOVSKIY, A.A. [Berezovs'kyi, A.A.]

Nonlinear integral equations in steady-state boundary value problems of heat radiation. Dop. AN URSR no.3:295-299 '63. (MIRA 17:10)

1. Institut matematiki AN UkrSSR. Predstavleno akademikom AN UkrSSR Yu.A. Mitropol'skiy [Mytropol's'kyi, IU.O.].

S/879/62/000/000/013/088

SOURCE: Teoriya plastin i obolochek; trudy II Vsesoyuznoy konferentsii, L'vov, 15-21 sentyabrya 1961 g. [illegible]

TEXT: In the case of bending of a shallow spher[illegible] ments distributed uniformly along the [illegible]

$$\theta(x) + \int_0^1 K_0(\rho, x)(\theta s - k^2 \rho s)d\rho - \frac{m}{[illegible]} x = 0;$$

$$s(x) + \int_0^1 K_1(\rho, x) k^2 \rho\theta - [illegible]$$

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Nonlinear integral equations ...

[illegible]

[illegible]

$s(\rho) = 0,$ $\Theta(\rho) = 2k^2\rho,$ $m = $ [illegible] k^2

Assuming

[illegible]

[illegible]

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...ovs'kyy, A. A.

...ntegral ...

Akademiya nauk UkrRSR ...

part of which ... is kept at a temperature ...
the other part S_2 radiates heat in accordance ...
Boltzmann law. The body G does not ...
... the stationary temperature ...

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Nonlinear integral equations ...

S/021/63/000/003/001/022

BEREZOVSKIY, A.A., (Kiyev)

Approximate solution of nonliner boundary value problems.
Inzh. zhur. 3 no.3:568-572 '63. (MIRA 16:10)

(Integral equations)

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000204910003-2"

BEREZOVSKIY, A.A. (Kiyev)

Nonlinear boundary value problem for a heat-radiating body.
Zhur. vych. mat. i mat. fiz. 4 no.4(suppl.):296-303 '64.
(MIRA 18:2)

BEREZOVSKIY, A.A. [Berezovs'kyi, A.A.]; SHULEZHKO, L.F.

Parametric resonance of a plate under conditions of nonlinearity.
Dop. AN URSR no.8:989-993 '63. (MIRA 16:10)

1. Institut matematiki AN UkrSSR. Predstavleno akademikom
AN UkrSSR Yu.A. Mitropol'skim [Mytropol's'kyi, IU.O.].
(Electrodynamics)
(Integrodifferential equations)

BEREZOVSKIY, A.A.

Nonlinear boundary problems for a heat-radiating cylinder.
Inzh.-fiz.zhur. 6 no.10:121-128 O '63. (MIRA 16:11)

1. Institut matematiki AN UkrSSr, Kiyev.

BEREZOVSKIY, Arnol'd Anatol'yevich; KRAVCHENKO, Adol'f Nikitovich

[Nonlinear boundary problems of an electromagnetic field]
O nelineinykh kraevykh zadachakh elektromagnitnogo polia.
Kiev, Izd-vo AN USSR, 1963. 73 p. (MIRA 17:9)

BEREZOVSKIY, A.A., inzh; FOKIN, V.G., inzh.

New factory techniques. Stroi. i dor. mash. 6 no.5:36 My '61. (MIRA 14:6)

(Karkov--Road machinery industry--Technological innovations)

BEREZOVSKIY, A. D., Engineer

"The Role of Russian Scholars of the 18th and 19th Centuries in the Foundation and Development of the Theory of Calculating Architectural-Engineering Structures." Cand Tech Sci, Moscow Architectural Inst, 10 Feb 55. (VM, 26 Jan 55)

Survey of Scientific and Technical Dissertations Defended at USSR Higher Educational Instiutions (12)
SO: Sum. No. 24 Jun 55

BEREZOVSKIY, A.F.

"Circuit for Imitation of (2-)Phase Short Circuits in the Testing of High-Frequency Filter Protection"

Elek Sta no. 2, 60-61, Feb 53

Gives description of and circuit diagrams for imitation of 2-phase short circuits, used by power systems in the lab testing of protective panels PZ-161, PZ-162. A power system, conducting series of tests by imitation method, uncovered individual defects in protection equipment not observable by other types of tests.

255T57

BEREZOVSKIY, A.F., inzhener.

Unbalances in a voltage filter with negative sequence. Elek.sta. 24 no.8: 57-58 Ag '53. (MLRA 6:8)
(Electric filters)

BEREZOVSKIY, A.F., inzhener.

Faulty connections in secondary circuits. Elek.sta. 25 no.2:
54-55 F '54. (MIRA 7:2)
(Electric circuits)

BEREZOVSKIY, A.F., inzhener.

Circuit of a double automatic reclosing device. Elek.sta. 25 no.3: 56-57 Mr '54. (MLRA 7:6)

(Electric circuit breakers)

BEREZOVSKIY, A.F.

Publication of a reference book for mechnaics. Sakh.prom. 30 no.12:66 D '56. (MLRA 10:1)

1. 2 Ol'khovatskiy sakharnyy zavod.
(Sugar industry--Equipment and supplies.

BEREZOVSKIY, A.F., inzhener (Yaroslavl').

Distance-type induction-dynamic relays with natural biasing. Elektrichestvo no.10:54-56 O '57. (MLRA 10:9)
(Electric relays)

BEREZOVSKII, A.F.

BERBZOVSKIY, A.F., inzh.; NOVIKOV, G.Ye., inzh.

Findings on the operation of relay protection and secondary circuits. Elek.sta. 29 no.1:87-89 Ja '58. (MIRA 11:2)
(Electric relays)

BEREZOVSKIY, A.F.

Asbestos cement shoes for friction clutches. Sakh. prom. 32 no.5: 50-51 My '58. (MIRA 11:6)

1. Novo-Kubanskiy zakharnyy zavod.
(Clutches (Machinery))

BEREZOVSKIY, A.F., inzh.

Checking the differential protection of parallel connected electric transformers. Elek. sta. 31 no.8:81-83 Ag '60. (MIRA 14:9)

(Electric protection) (Electric transformers)

BEREZOVSKIY, A.F., inzh (Yaroslval')

Impedance relay with a magnetized choke. Elektrichestvo no. 11:28-33 N '60. (MIRA 13:12)

(Electric relays)

BEREZOVSKIY, A.F., inzh.

Semigraphical calculation of short circuit currents and selection of settings for simple relay protection. Elek.sta. 31 no.1: 68-73 Ja '60. (MIRA 13:5)
(Short circuits)

BEREZOVSKIY, A.F., inzh. (Yaroslavl')

Calculation of transient processes in complex networks with some nonlinear elements. Elektrichestvo no.1:73-75 Ja '62. (MIRA 14:12)

(Electric networks)
(Transients(Electricity))

BEREZOVSKII, A.I.

L 18804-63 EWT(d)/FCC(w)/BDS AFFTC/IJP(C)

ACCESSION NR: AP3000281 S/0021/63/000/005/0580/0583

54

53

AUTHOR: Berezovs'ky*y, A. I., Ivanov, V. V.

TITLE: Some algorithms of optimal quick response controls (Presented by Yu. O. My*tropol's'ky*y, member, AN URSR)

SOURCE: AN UkrSSR Dopovidi, no. 5, 1963, 580-583

TOPIC TAGS: variable coefficient, constant coefficient, algorithm, quadratic programming, variable imput, variable output, constant imput, constant output

ABSTRACT: The authors analyze their problem for two cases. For the first case they take a linear system with variable parameters, with n number of inputs and m number of outputs. An approach different from the Pontryagin and Boltyanskiy method is proposed in the solution of optimum quick response control. By means of a number of mathematical algorithms the problem was reduced to quadratic programming. In the second case analyzed, the linear system has constant coefficients, with one input and one output. Again the problem is reduced to quadratic programming, but in a simpler fashion.

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L 18804-63

ACCESSION NR: AP3000281

A problem with n number of inputs and only one output can be solved in a similar manner. Orig. art. has: 11 equations.

ASSOCIATION: Insty*tut kibernety*ky* AN UkrSSR (Cybernetics Institute of AN UkrSSR)

SUBMITTED: 29Jun62 DATE ACQ: 17Jun63 ENCL: 00

SUB CODE: MM NO REF SOV: 004 OTHER: 000

Card 2/2

SHIPOV, V.P.; SHITSER, S.S., retsenzent; BEREZOVSKIY, A.I., retsenzent; VASIL'YEVA, G.N., redaktor; KISINA, Ye.I., tekhnicheskiy redaktor.

[Planning work in enterprises of the meat industry; methods and techniques in working out a plan] Planirovanie truda na predpriiatiiakh miasnoi promyshlenosti; metodika i tekhnika raschetov plana. Moskva, Pishchepromizdat, 1956. 73 p. (MIRA 9:5)

(Meat industry)

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ALEKSEYEV, F.K.; ANDRIYUTS, G.L.; ARSENT'YEV, A.I.; ASTAF'YEV, Yu.P.; BEVZ, N.D.; BEREZOVSKIY, A.I.; GENERALOV, G.S.; DOROSHENKO, V.I.; YESHCHENKO, A.A.; ZAPARA, S.A.; KALINICHENKO, V.F.; KARNAUSHENKO, I.K.; KIKOVKA, Ye.I.; KOBOZEV, V.N.; KUPIN, V.Ye.; LOTOUS, V.K.; LYAKHOV, N.I.; MALYUTA, D.I.; METS, Yu.S.; OVODENKO, B.K.; OKSANICH, I.F.; PANOV, V.A.; POVZNER, Z.B.; PODORVANOV, A.Z.; POLISHCHUK, A.K.; POLYAKOV, V.G.; POTAPOV, A.I.; SAVITSKIY, I.I.; SERBIN, V.I.; SERGEYEV, N.N.; SOVETOV, G.A.; STATKEVICH, A.A.; TERESHCHENKO, A.A.; TITOV, O.S.; FEDIN, A.F.; KHOMYAKOV, N.P.; SHEYKO, V.G.; SHEKUN, O.G.; SESTAKOV, M.M.; SHTAN'KO, V.I.

Practice of construction and exploitation of open pits of Krivoy Rog Basin mining and ore dressing combines. Gor. zhur. no.6: 8-56 Je '63. (MIRA 16:7)

(Krivoy Rog Basin--Strip mining)

BEREZOVSKIY, A.M., inzhener; NEDOKUCHAYEV, B.N., inzhener.

[redacted]

Plant for the combined grinding and drying of clay in making bricks by the dry press method. Mekh.stroi.12 no.3:18-20 Mr '55.
(Brickmaking machinery) (MIRA 8:4)

SAVOS'KIN, A.N., kand. tekhn. nauk; BEREZOVSKIY, A.M., inzh.; MUSHKIN, M.L.

Studying the fatigue endurance of the truck frames of ER2 electric trains. Trudy MIIT no.207:162-171 '65.

(MIRA 19:1)

BEREZOVSKIY, A.P.

Lumpiness of ore mined with roof caving at the Tekeli mine. Izv. AN Kazakh. SSR. Ser. gor dela no.2:36-42 '58. (MIRA 12:10)
(Kazakhstan--Mining engineering)

BEREZOVSKIY, A.P.

Evaluation of ore lumpiness in the forced roof caving system. Izv. AN Kazakh. SSR. Ser. gor dela no.1:11-16 '60. (MIRA 13:10)
(Mining engineering)

BEREZOVSKIY, A.P.

Drawing support pillars as previously worked areas in the Dzhezkazganskiy Mine. Trudy Inst. gor. dela AN Kazakh.SSR 12: 13-21 '63. (MIRA 17:8)

TIKHENKO, L.G., gornyy inzh.; STEL'MAKH, N.N., gornyy tekhnik; GUMENOK, G. Ye., gornyy tekhnik; VOLOSHIN, A.M., gornyy inzh.; BEREZOVSKIY, A.P., gornyy inzh.; LYUTYY A.L., gornyy inzh.; BUGAY, V.A., gornyy tekhnik-marksheyder

"Improving underground work" by IA. D. Grossman and E. M. Kozakov. Reviewed by L. G. Tikhenko and others. Gor. zhur. no.3:3-7 Mr '61. (MIRA 14:3)

1. Rudoupravleniye im. Rozy Lyuksemburg, Krivoy Rog (for Tikhenko, Stel'makh, Gumenok). 2. Shakhta "Kommunar-Probeda', Krivoy Rog (for Voloshin, Berezovskiy, Lyutyy). 3. Shakhta "Novaya" rudoupravleniya im. Rozy Lyuksemburg (for Bugay).

(Mining industry and finance)
(Grossman, IA. D.) (Kozakov, E. M.)

BEREZOVSKIY, A.P.; VELICHKIN, A.N.; SILKINA, N.I.

Practice of using continuous-action loading and hauling machines in the Dzhezkazgan Mine. Trudy Inst. gor. dela An Kazakh. SSSR 10:64-66 '63. (MIRA 16:8)

(Dzhezkazgan District—Mining machinery)

SHATS, A.S.; BEREZOVSKIY, A.S.

Semiautomatic machine for centerless burnishing of parts for nickel plating. Mashinostroitel' no.1:7 Ja '60.
(MIRA 13:4)

(Grinding machines)

SHATS, A.S., inzh.; BEREZOVSKIY, A.S.

Eccentric tail-stock clamp. Mashinostroitel' no.3:17 Mr '60. (MIRA 13:6)

(Lathes)

BEREZOVSKIY, A.Ya., red.

[Abstracts of papers of the Republic Scientific Research Institute of Local Building Materials (RSFSR) for 1958 - 1960] Sbornik annotatsii nauchno-issledovatel'skikh rabot instituta "Rosniims" za 1958-1960 gg. Moskva, 95 p. (MIRA 15:4)

1. Moscow. Respublikanskiy nauchno-issledovatel'skiy institut mestnykh stroitel'nykh materialov "ROSNIIMS."
(Building materials)

BEREZOVSKIY, A.Z.; FOKIN, V.G.

The D443 loader-bulldozer. Biul.tekh.-ekon.inform. no.8: 39-41 '59. (MIRA 13:1)
(Road machinery)

BEREZOVSKIY, A.Z.; FOKIN, V.G.

The BU-55 all-purpose bulldozer. Biul.tekh.-ekon.inform. no.1:50-51 '60. (MIRA 13:5)
(Crawler tractors)

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BEREZOVSKIY, A.Z.; FOKIN, V.G.

The D-459 tractor bulldozer. Biul.tekh.-ekon.inform. no.3:39-40 '60. (MIRA 13:6)
(Bulldozers)

BEREZOVSKIY, A.Z., inzh.; FOKIN, V.G., inzh.

Testing the strength of the D-401A trailer. Stroi. i dor. mashinostr. 5 no.4:20 Ap '60. (MIRA 13:9)
(Truck trailers)

BEREZOVSKIY, A.Z.; GORVITS, A.A.

The D-535 bulldozer mounted on the T-75 tractor. Biul.-tekh.-ekon. inform. no.7:52-54 '61. (MIRA 14:8)
(Bulldozers)

BEREZOVSKIY, A.Z., inzh.; GORVITS, A.A.

D-535 bulldozer based on the T-75 tractor. Stroi.i dor.mash. 6 no.8:8-9 Ag '61. (MIRA 14:8)
(Bulldozers)

BEREZOVSKIY, B., inzh.

Using coarse porous concrete in the Chukchi National Area. Stroitel' no.1:3,13 Ja '58. (MIRA 11:2)
(Chikchi National Area--Precast concrete construction)

BEREZOVSKIY, B., inzh.

Building practices on Chukchi Peninsula. Zhil. stroi. no.1:18-20 '59. (MIRA 12:10)
(Chukchi Peninsula--Building--Cold weather conditions)

BEREZOVSKIY, B. I

Nekotoryye Osobennosti Stroitel'stva v Usloviyakh Kraynego Severa. Moskva, Gosstroyizdat, 1960.
126 p. Illus., diagrs., graphs, tables.
Bibliography: P. 122-123.