

EWP(q)/EWT(m)/BDS--AFFTC/ASD--JD/JG L 11203-63

ACCESSION NR: AP3000490

\$/0129/63/000/005/0049/0054

AUTHOR: Bernshteyn, M. L.; Demina, E. L.; Liberman, Ye. E.; Chernukha, L. G.

TITLE: Polygonization in molybdemum and its alloys.

SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 5, 1963 49-54

TOPIC TAGS: polygonization in molybdenum, zirconium, titanium

ABSTRACT: Authors made tests on molybdenum which was obtained by powder metallurg method, on cast molybdemum, on cast molybdenum alloys with admixtures of zirconium titanium as well as cast melybdemum alloys with simultaneous admixtures of zirconium and titanium. For selection of recrystallization conditions, the samples were heated to 1250, 1300, 1400, 1500 and 1600 degrees with holding at 5, 10, 15, 20 and 30 minutes. The microstructures were studied and optimum annealing conditions were established. In addition, treatment conditions were established which produced the most developed polygonized structure in the molybdenum and its alloys. Microstructure testing was done by subjecting the samples to deformation. deformation and annealing at 1000-1600 degrees, and, finally, after deformation and double annealing at polygonization and higher temperatures. The changes in the structure of molybdenum and its alloys were also studied in relation to

Card 1/2

L 11203-63

ACCESSION NR: AP3000490

holding period at optimum treatment conditions. Authors conclude that polygonization raises the temperature of subsequent recrystallization which is important for employing molybdenum and its alloys at elevated temperatures. As a result of development of polygonization in the tested materials, an increase of resistance to small plastic deformations occurs. Orig. art. has: 6 figures.

ASSOCIATION: Moskovskiy institut stali i splavov (Moscow Institute for Steels and Alloys)

SUBMITTED: 00

DATE ACQD: 03Jun63

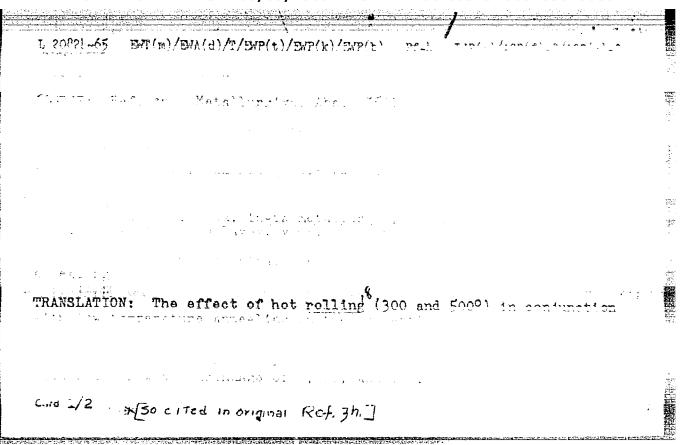
ENCL: 00

SUB CODE: 00

NO REF SOV: 000

OTHER: 000

Card 2/2



	하고 있다. 아프리아 아이들 등에 가는 100 이 등을 교육하고 최고하고 있으로 하고 하고 하는 100 등을 하는 100 등을 보는 100 등을 하는 100 등을 보는 100 등을 하는 100 등을	
į. Įs	0821,-65 ESSION NR: AR4048249	
t)	e annealed for 1 hr at 250, 350, and 500°. As a result of rmomechanical treatment the strength properties of Ti increasion to its increasion after not relieve. We	
·	ling at Koop with shrinkage of 28% with subsequent these	* · · · · · · · · · · · · · · · · · · ·
S	CODE: MM ENCL: 00	
-(d 2/2 ——————————————————————————————————	

BORZDYKA, A.M., doktor tekhn. nauk; TSEYTLIN, V.Z., kand. tekhn. nauk; BERNSHTEYN, M.L., doktor tekhn. nauk, prof., retsenzent

[Heat treatment of heat-resistant steels and alloys] Termicheskaia obrabotka zharoprochnykh stalei i splavov. Moskva, Mashinostroenie, 1964. 246 p. (MIRA 17:9)

ACCESSION NR: AP4010067

\$/0129/64/000/001/0012/0013

AUTHORS: Bernshteyn, M.L.; Birman, S.R.; Demina, E.L.

TITLE: Investigation of polygonization in nichrome

SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 1, 1964, 12-13

TOPIC TAGS: nichrome, Kh20N8O alloy, plastic deformation, elastic limit, polygonization, annealing

ABSTRACT: The conditions for treating Kh20N80 alloy causing polygonization were established. As a result of polygonization the resistance to small plastic deformation is increased 1.5-2 times. Annealing for 1 hour at 850C increases resistance to 1% deformation at 450C by 1.5 times; this value is increased somewhat more by annealing for 100 hours, then it decreases. For 4% deformation at 450C, optimum annealing is for 1 hour at 750C (increasing resistance 2 times); further annealing up to 40 hours reduces the elastic limit and with longer annealing the elastic limit remains

Card 1/2

ACCESSION NR: AP4010067

constant. Orig. art. has: 2 figures.

ASSOCIATION: Moskovskiy institut stali i splavov (Moscow Steel

and Alloy Institute)

SUBMITTED: 00 DATE ACQ: 07Feb64 ENCL: 00

SUB CODE: ML NO REF SOV: 000 OTHER: 000

Card 2/2

ACCESSION NR: APho19482

S/0133/64/000/003/0269/0270

AUTHORS: Kal'ner, V. D.; Kossovskiy, L. D.; Bernshteyn, M. L.

TITLE: Thermomechanical treatment of 55khCR steel springs

SOURCE: Stal', no. 3, 1964, 269-270

TOPIC TAGS: steel, 55KhGR steel, spring band, thermal treatment of steel, mechanical treatment of steel, rolling 55KhGR steel, hardening, compressed air hardening, water hardening, tempering, 300-2 rolling mill

ABSTRACT: A series of experiments was performed in Chelyabinskiy metallurgicheskiy zavod (Chelyabinsk Metallurgical Plant) on the different thermal and mechanical treatments of steel spring bands. The samples were made of 55KhCR steel, were 7.5 x 63 mm in size, and their chemical composition (%) was:

C Mn SI S P Cr Ni Cu B

0.58 1.06 0.27 0.014 0.021 1.13 0.16 0.15 0.0023

After hot rolling at 930-9500 in the 300-2 mill, the samples were hardened in a jet of compressed air or in water. Their hardness was 57-58 and 60-61 $R_{\rm C}$. They showed no usual cracking after water hardening (due to an increase of their

Card 1/2

ACCESSION NR: AP4019482

residual plasticity). They were tempered at 240-265C. It was established that a combined thermal and mechanical processing resulted in a good combination of high strength and the desired plasticity. The assemblies for thermomechanical treatment of steel spring bands are not complicated, can be installed in any plant, and may be used in mass production operations. The strength and plasticity values of the 55KhGR spring bands obtained in a continuous rolling mill were much higher than those obtained in the laboratory. The hardening effect of the thermomechanical treatment produced lasting results. Orig. art. has: 3 tables and 2 figures.

ASSOCIATION: none

SUBMITTED: 00

DATE ACQ: 27Mar64

ENCL: 00

SUB CODE: ML

NO REF SOV: 002

OTHER: 000

Card 2/2

ACCESSION NR: AP4037064

8/0129/64/000/005/0010/0013

AUTHOR: Chudnovskaya, L. A.; Bernshteyn, M. L.; Granik, G. I.; Gladshteyn, V. A.

TITIE: Thermomagnetic Tempering of "R-18" Steel

BOURCE: Metallovedeniye 1 termicheskaya obrabotka metallov, no. 5, 1964, 10-13

TOPIC TAGS: austenite transformation, variable magnetic field, tempering, bend test, automated heat treatment, high speed steel

ABSTRACT: The authors consider the possibility of accelerating the austenite transformation during magnetic tempering of high-speed steel in: (1) 75 mm-long , specimens prepared from a ground rod with an 8 mm diam used for the determination of the amount of residual austenite and Hc; (2) 30 mm-long dilatometric specimens prepared from a ground rod with a 3 mm diam; and (3) $4.5 \times 4.5 \times 50$ mm specimens prepared from 25 x 15 mm hot-rolled strip for bending tests. Tempering with the application of a 600 and 1200 e variable magnetic field greatly accelerates the transformation of residual austenite at 550-560 C; 30 min. holding results in complete transformation. The magnetic field has the same effect when applied during holding and quenching. Bending strength is enhanced at all temperatures.

Cord 1/2

ACCESSION NR: AP4037064

The application of a magnetic field enhances austenite decomposition time by one and a half after a 500 C temper, 60 min holding period and quenching from 1300 C. Residual austenite content was 3% as against 10% without a magnetic field. The expedience of replacing the current technique of prolonged triple tempering by single tempering and the employment of a magnetic field was tested by the authors in 6 mm-diam. drills hardened by heating to 1280 C in a salt bath for 1.5 minutes and cooling in saltpeter to 400-500 C. After pickling the specimens were subjected to various tempering conditions with and without a magnetic field. The authors found that accelerated magnetic field tempering would make automation possible in the heat treatment of high-speed steel tools. Orig. art. has: 6 figures.

ASSOCIATION: Moskovskiy institut stali i splavov (Moscow Institute of Steel and Alloys), VNII (All Union Scientific Research Institute)

SUBMITTED: 00

DATE ACQ: 05Jun64 .

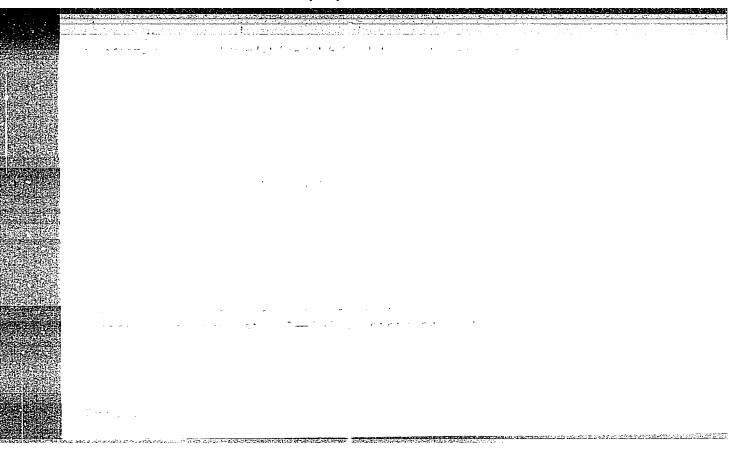
encl: 00

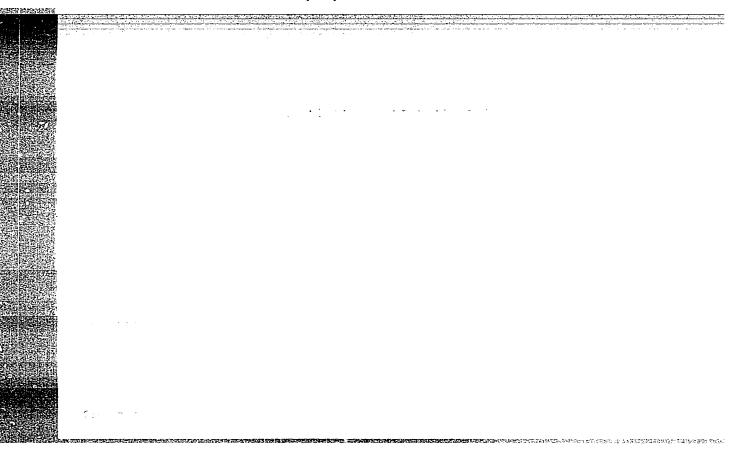
SUB-CODE: MM

NO REF. SOV: COL

OTHER: OOO

Cord 2/2





BRON, D.I.; BERNSHTEYN, M.L., doktor tekhn.nauk; RAKHSHTADT, A.G., kand. tekhn.nauk; LEVITES, I.I.

Hardening 55KhGR spring steel by the method of high-temperature thermomechanical treatment. Avt.prom. 30 no.1:35-38 Ja '64. (MIRA 17:3)

l. Nauchno-issledovatel'skiy tekhnologicheskiy institut avtomobil'noy promyshlennosti, Moskovskiy institut stali i splavov i Moskovskoye vyssheye tekhnicheskoye uchilishche imeni Baumana.

BERNSHTEYN, M.L.; YELAGINA, L.A.; FATKULLINA, L.P.; Prinimali uchastiyas KHROMEYEV, Yu.V.; SEMENOVA, N.M.

Thermomechanical treatment of VTZ1 VT8 and VT14 titanium alleys. TSvet. met. 37 no.12:80-83 D 164 (MIRA 18:2)

POGODIN-ALEKSEYEV, G.I., doktor tekhn. nauk, prof., otv. red.;

RAKHSHTADT, A.G., kand. tekhn. nauk, dots., nauchn. red.;

SHREYBER, G.K., kand. tekhn. nauk, dots., nauchn. red.;

HERNSHTEYN, M.L., doktor tekhn. nauk, red.; LAKHTIN, Yu.M.,

doktor tekhn. nauk, prof., red.; RUSTEM, S.L., kand. tekhn.

nauk, dots., red.; FEDOTENKO, N.S., inzh., red.

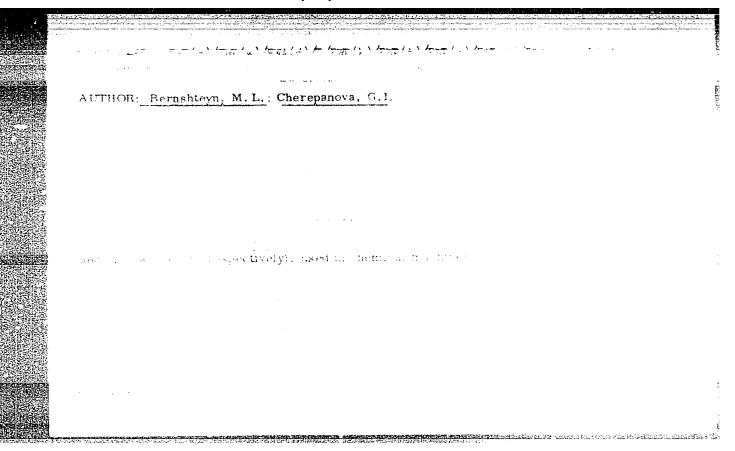
[Study of metals and their heat treatment] Metallovedenie i termicheskaia obrabotka. Moskva, Mashinostroenie, 1964.
195 p. (MIRA 18:7)

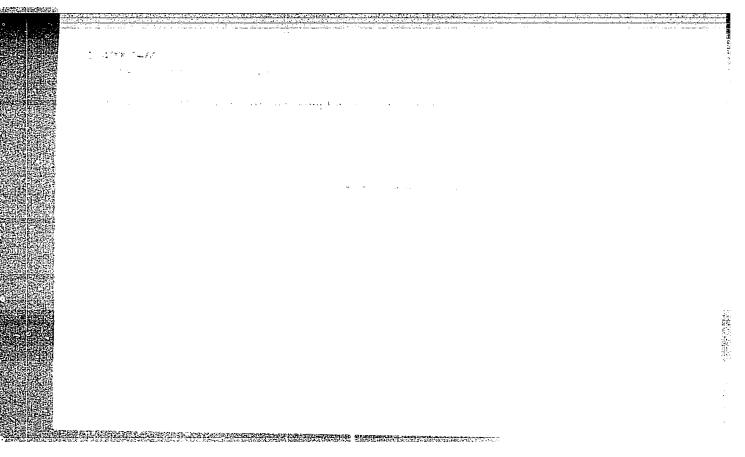
1. Nauchno-tekhnicheskoye obshchestvo mashinostroitelinoy promyshlennosti. Sektsiya metallovedeniya i termicheskoy obrabotki.

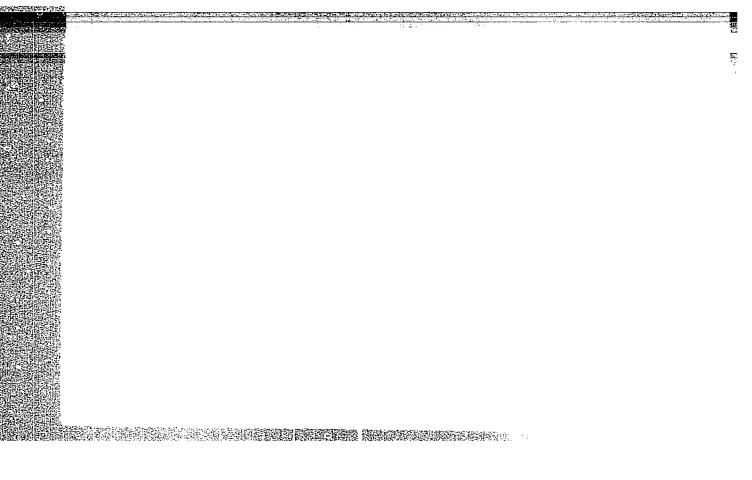
BERNSTEIN, M.L. [Bernshteyn, M.L.]

Thermomechanical treatment of steels. Koh lap 98 no.1:1-6 Ja 165.

1. Moscow Steel Institute.









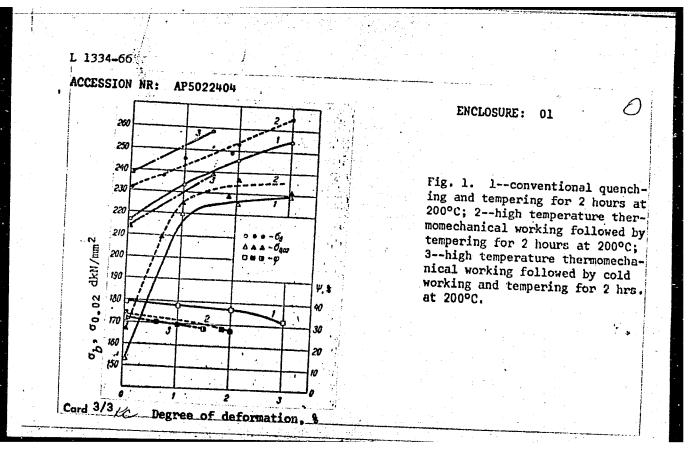
BERNSHTEYN, M.L.

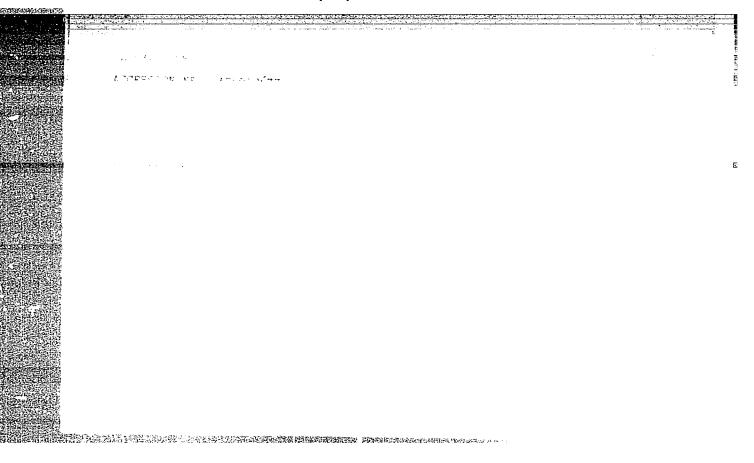
Reviews. Zashch.met. 1 no.4:456-457 J1-Ag 165.

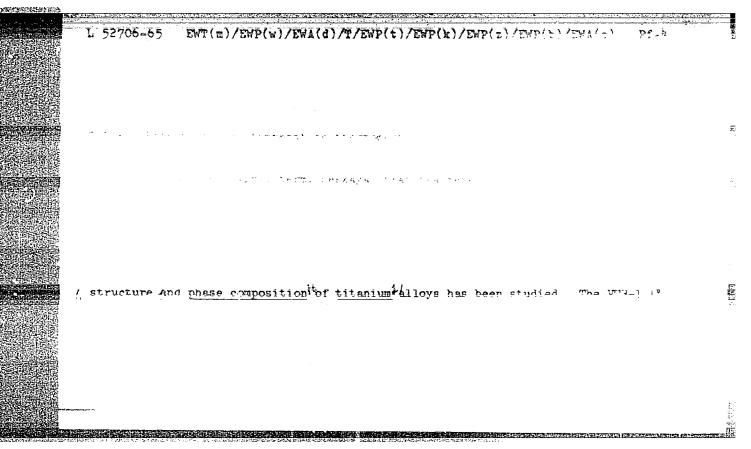
(MIRA 18:8)

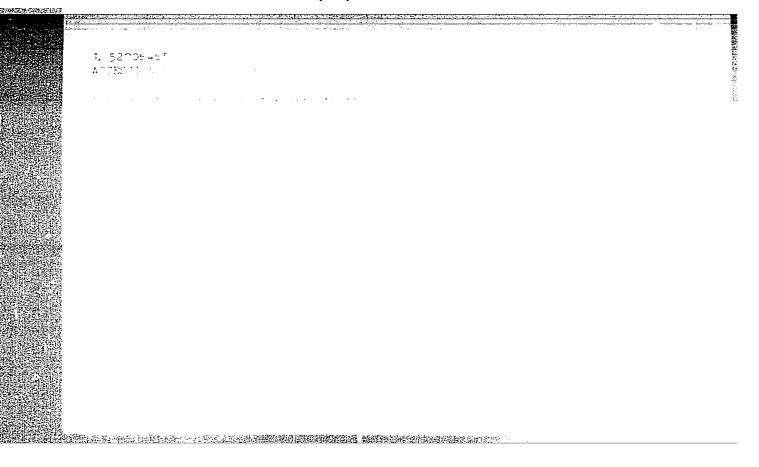
hFA steel by means of cold 4, 1965, 473-476 echanical property, steel/ on mechanical properties of
hFA steel by means of cold 4, 1965, 473-476 echanical property, steel/
echanical property, steel/
echanical property, steel/
on mechanical amazani
on mechanical properties of teel samples. The 55KhFA of Cr, (.17% V, 0.02% P, and 2 hours and cut. The hardnching in oil, and tempering king was conducted as follow quenching in oil, forging at 200°C, and grinding to mm in length were deformed

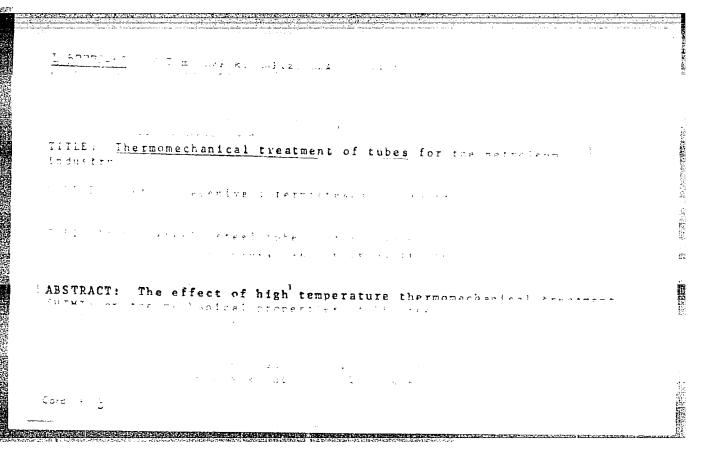
ACCESSION 1	YR: AP50	22404		and the same of th	range of the second		7** ·*· .	
by stretchi tensite def either temp properties, y, of quence site deform observed to orig, art.	endurance hed and detailed	2 hours a ce limit of leeply tem	at 200°C b, propo pered 55 fig. 1 effect tables.	or not ter priionality okhFA steel of the End on the med	mpered. / limit of samples closure. chanical	The depen 0.02. and upon the In gener propertie	on, samples dence of braking degree (al, cold s of 55K	s were mechanical elongation of marten- working wan FA steel.
ASSOCIATION Alloys)		skiy inst	itut sta	li i splav	ov (Mosco	w Institu	ute of St	hee lee
SUBMITTED:	: Hoskov	skiy inst	itut ata	li i splav		ow Institu		
SUBMITTED:	: Hoskov	skiy inst	itut sta	v	1	ow Instit	SUB CODE	
SUBMITTED:	: Hoskov	skiy inst	itut sta	ENCL: 0	1	ow Instit		
SUBMITTED:	: Hoskov	skiy inst	itut sta	ENCL: 0	1	ow Institu		
ASSOCIATION Alloys) SUBMITTED: NO REF SOV:	: Hoskov	skiy inst	itut sta	ENCL: 0	1	ow Institu		

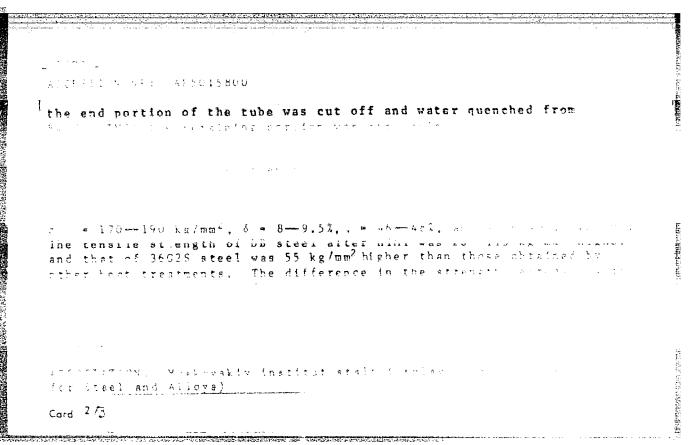


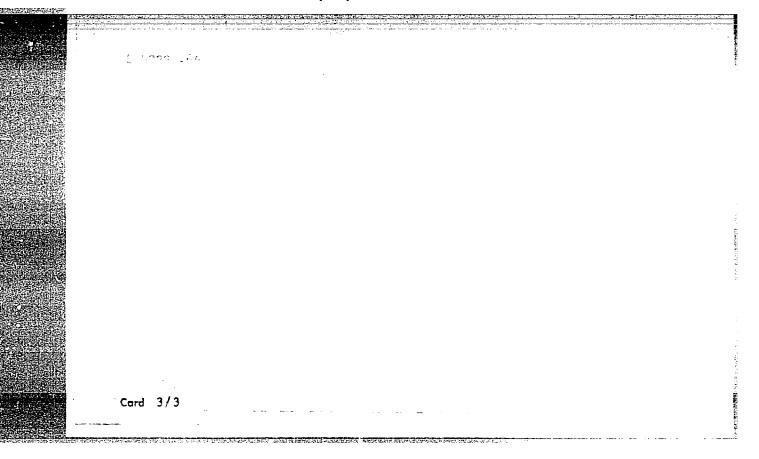








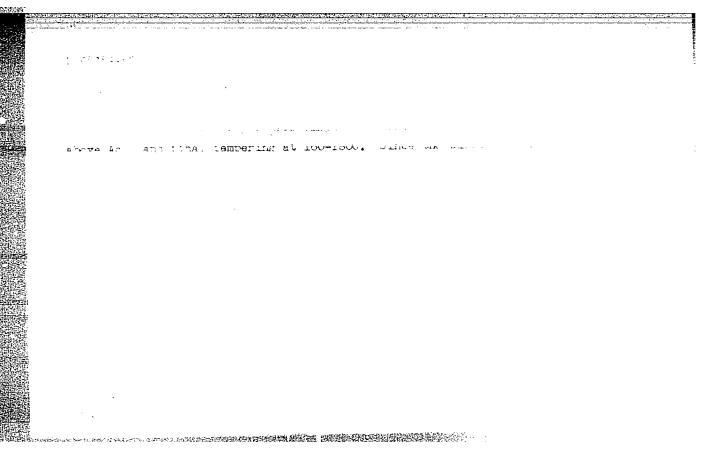




BERNSHTEYN, M.L.; YELAGINA, L.A.; FATKULLINA, L.P.; SEMENOVA, N.M.

Effect of high temperature thermomechanical treatment on the fine structure of titanium alloys. Metalloved. i term. obr. met. no.5:35-38 My '65. (MIRA 18:7)

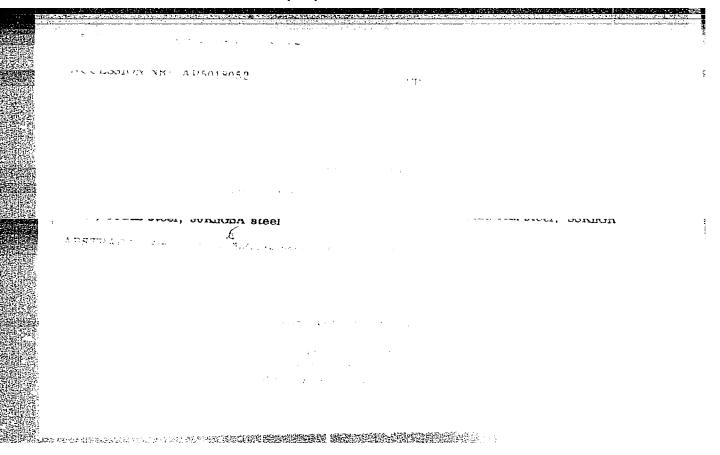
	The second second of the second of the second of the second of the second second of the second of th	
		4
social Land	The state of the s	
	9Ch steel	1
	at a rate of deformation of 180 mm/min. After surface treatment, we specimens	
	at a rate of deformation of too many mine the surface endurance formles to	
		landerial

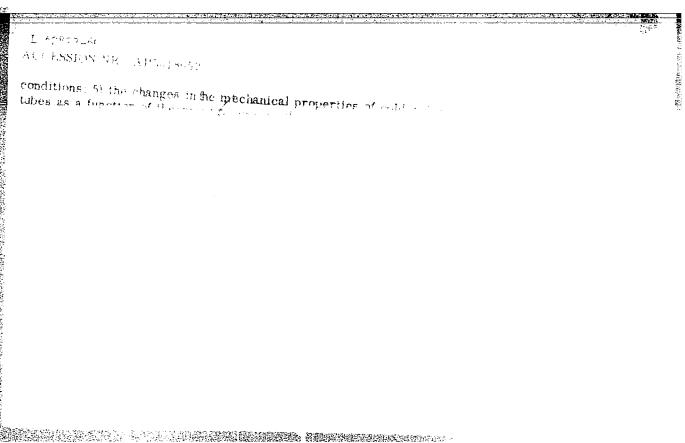


BERNSHTEYN, M.L.; GRANIK, G.I.; DOLZHANSKIY, P.R.

Effect of magnetic fields on phase transformations in nickel steel. Fiz. met. i metalloved, 19 no.6:882-890 Je '65. (MIRA 18:7)

1. Moskovskiy institut stali i splavov.





L 14420_66 EWT(m)/EWA(d)/T/EWP(t)/EWP(k)/EWP(z)/EWP(b) IJP(c) NJW/JD/HW/JG
ACC NR: AP6002120 SOURCE CODE: UR/0369/65/001/006/0701/0706

AUTHOR: Bernshteyn, M. L.; Kalyagina, G. P.; Venzhega, A. S.; Belkin, M. Ya.; Ryabova, E. A.

ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov)

TITLE: High-temperature thermomechanical surface treatment (with 9 Kh steel as example)

SOURCE: Fiziko-khimicheskaya mekhanika materialov, v. 1, no. 6, 1965, 701-706

TOPIC TAGS: steel, surface hardening, metal heat treatment, mechanical heat treatment

ABSTRACT: The paper gives the results of a study and adoption in industry of a new method of hardening the surface layers of cold rolls, the high-temperature thermomechanical surface treatment (HTMST). In experiments with rolls of 9Kh steel, the greatest increase in the contact strength of 9Kh steel rolls as compared to ordinary hardening treatment with high-frequency currents and low tempering is provided by HTMST involving an austenizing temperature of 900-950C, a draft pressure of 64 dkN, a longitudinal feed of 180 mm/min, and a rotation velocity of 720 rpm. After this treatment, the contact strength in the zone of Card 1/2

I 14420-66

ACC NR: AP6002120

2

limited life increased from 4.1—5.4 to 13.0—14.8 million cycles (in some samples, up to 50—55 million cycles). The life of the working rolls of a twelve-roll mill increased by a factor of over 2. Metallographic studies and microhardness measurements following the HTMST showed the presence of a markedly hardened surface layer characterized by a high etchability. HTMST results in a refinement of carbide particles, an increased alloying with chromium, and causes a certain orientation to appear in the separation of these particles. Orig. art. has: 3 figures and 2 tables.

SUB CODE: 11 / SUBM DATE: 11Mar65 / ORIG REF: 001

Card 2/2

EWT(m)/EWA(d)/EWP(t)/EWP(k)/EWP(z)/EWP(b)/EWA(c) MJW/JD/HW L 12144-66 ACC NR: AP6000595 SOURCE CODE: UR/0133/65/000/012/1108/1110 1/1/10 41.1 AUTHOR: Bernshteyn, M. L.; Dregan, N.; Korobochkin, I. Yu.; Vil'yams, O. S.; Kurilenko, V. Kh.; Koval chuk, T. M. dis ORG: TITLE: Possibilities and prospects for the combined hot and cold working of drilling rig pipe SOURCE: Stal', no. 12, 1965, 1108-1110 TOPIC TAGS: pipe, hear treatment, cold working, work hardening, carbon steel low alloy steel/ D steel, 36G2S steel 844.55 ABSTRACT: It is shown that the high-temperature thermomechanical treatment (combined cold and hot working) of pips manufactured from D and 36G2S steels (0.44% C, 1.10% Mn, 0.32% Si and 0.38% C, 1.65% Mn, 0.58% Si, respectively), as based on water quenching from 840-850°C immediately after rolling, followed by tempering for 1 hr at temperatures of from 100 to 600°C, markedly increases the mechanical properties of the pipe (following low-temperature tempering, $\sigma_{\rm B}=220\text{-}240~{\rm kg/mm^2}$ at $\delta=7\text{-}87$, and following high-temperature tempering $\sigma_{\rm B}=95\text{-}115~{\rm kg/mm^2}$ at $\delta=11\text{-}147$) This effect is still further enhanced when the treatment is followed by tempering at 500°C for 1 hr, highspeed heating to 850°C for 3 min, water quenching, and final low-temperature temper-

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205020008-4"

Card 1/2

L 12144-66

ACC NR: AP6000595

(

ing, which results in the work-hardening of the metal. Experiments with accelerated compressed-air cooling of the pipe immediately after rolling show that this magnifies even further the effect of preceding work hardening as compared with ordinary normalization, as was found by subjecting pipe rolled from D and 36G2S steels to cooling with high-pressure compressed air immediately after rolling, with subsequent tempering at from 400 to 600°C for 1.5 hr. This opens broad vistas for replacing alloy steels with carbon and low-alloy steels. Orig. art. has:5 tables, 1 figure.

SUB CODE: 11, 13/ SUEM DATE: none/ ORIG REF: 004/ OTH REF: 000

Cord 2/2

BERNSHTEYN, M.L.; CHEREPANOVA, G.I.

Feasibility of increasing the strength and heat resistance of Kh 8-type steels by thermomechanical treatment. Fiz.-khim. mekh. mat. 1 no.1:60-66 '65. (MIRA 19:1)

1. Institut stali i splavov, Moskva. Submitted September 28, 1964.

"APPROVED FOR RELEASE: 06/08/2000

0

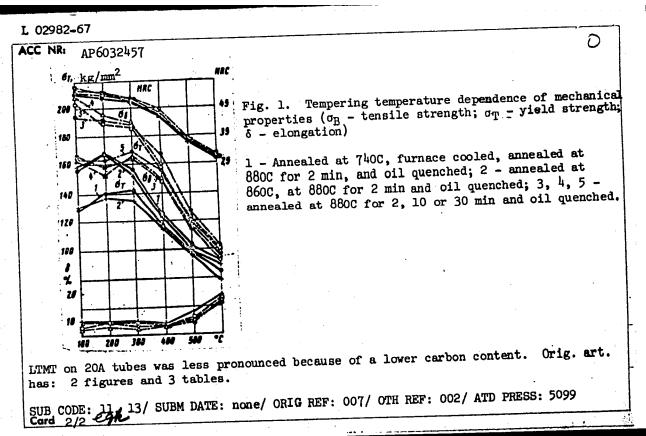
CIA-RDP86-00513R000205020008-4 L 15/11-06 EWT(m)/EWA(d)/T/EWP(t)/EWP(k)/EWP(z)/EWP(b) MJW/JD/EW ACC NR: AP6003297 (N) SOURCE CODE: UR/0129/66/000 SOURCE CODE: UR/0129/66/000/001/0002/0005 AUTHOR: Kagan, D. Ya; Bernshteyn, M. ORG: none TITLE: Hardening treatment for high-temperature alloys SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 1, 1966, 2-5 TOPIC TAGS: heat resistant alloy, metal hardening, crystal structure, metal heat treatment, metal aging, plastic deformation / KhN77TYuR alloy, KhN70MVTYuB alloy ABSTRACT: The strength of metals can be effectively increased by inducing a pile-up of defects and creating a definite fine crystalline structure by means of heat treatment combined with plastic deformation. On applying various combinations of this kind in order to harden KhN77TYuR and KhN70MVTYuB heat-resistant the authors found the optimal combination to be as follows: for KhN77TYuR alloy -- heating to 1120°C for 30 min + 25-30% deformation (with ending of deformation at 1050-1030°C) + air cooling; for KhN70MVTYuB alloy -- heating to 1150°C for 60 min + 25-30% deformation (with ending of deformation at 1050-1070°C) + sir cooling. Both alloys were aged for 16 hr (at 700 and 800°C, respectively). This treatment increases the plasticity and reduces the notch sensitivity of metal, and it is simpler, faster and more effective than the conventional thermomechanical treatment consisting in quenching, aging and prolonged Card 1/2

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205020008-4"

ODC: 539.374;621-785;669.14.018.45

work harden has: 4 figu	ome embrittl	e embrittlement of the ma			terial. Orig. art.		
SUB CODE:	11, 13, 20/	SUBM DATE: none	/ ORIG REF:	000/ o	TH REF: (000	
				:		_	
	•	•				•	
l ,				•			
		•• •		•			
		•					
1							

02982-67 EWT(m)/T/EWP(t)/ETI/EWP(k) IJP(c) JD/HW
02982-67 EWI(m)/1/EWF(C)/C11/EWICE CODE: UR/0129/66/000/009/0039/0042 CC NRi AP6032457 SOURCE CODE: UR/0129/66/000/009/0039/0042
UTHOR: Dregan, N.; Bernshteyn, M. L.
RG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov)
ITLE: Preliminary thermomechanical treatment of tubes
OURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 9, 1966, 39-42
COPIC TAGS: alloy steel, steel tube, tube thermomechanical treatment, low temperature thermomechanical property /30KhGSA steel, 20A steel ABSTRACT: Hot-rolled 30KhGSA and 20A steel tubes, 57 mm in diameter with a wall thickness of 3.5—3.75 mm, were subjected to low temperature thermomechanical treatment (LTMT), i.e., cold rolled to 45 mm diameter and 1.6 mm wall thickness (30KhGSA), for 30 mm diameter and 2 mm wall thickness (20A), annealed in salt bath at 880C for 22—30 min, oil or water quenched and then tempered at 100—600C. The LTMT significantly increased the tensile and yield strength of the 30KhGSA tubes without a significant reduction of ductility (see Fig. 1). Additional tests revealed that the austenite grain size or shape has little or no effect on strengthening in LTMT. The effect of
Card 1/2 UDC: 539.374.621.785.622.245



/ETI/EWP(k) JD/HW/JG_ IJP(c) EWT (m)/EWP(t) 47302-66 SOURCE CODE: UR/0148/66/000/009/0153/0157 ACC NR: AP6032054 AUTHOR: Bernshteyn, M. L.; Shtoydten, V. ORG: Institute of Steels and Alloys, Moscow (Moskovskiy institut stali i splavov) TITIE: Thermomechanical treatment of EI-612 type heat-resistant steel SOURCE: IVUZ. Chernaya metallurgiya, no. 9, 1966, 153-157 TOPIC TAGS: nickel chromium alloy, manganese containing alloy, tungsten containing alloy, molybdenum containing alloy, titanium containing alloy, heat resistant alloy, alloy thermomechanical treatment, low temperature thermomechanical treatment, alloy property/EI-612 alloy ABSTRACT: Experiments have been made to increase the strength of Khl5N35VT (EI-612) type alloy by increasing the chromium content up to 20%, additional alloying with molybdenum in amounts of 2, 4 or 6%, and thermomechanical treatment. Steel specimens annealed at 1180C for 2 hr and water quenched were subjected to low-temperature thermomechanical treatment (LTMT), i.e., either cold drawn with 5, 50 or 75% reduction or rolled at 600C with 50% reduction, in both cases followed by aging at 760C for 25 hr or at 600C for 100 hr. LTMT increased significantly the strength of alloys. The alloy with 2% molybdenum, drawn with 50% reduction, had a room-temperature tensile strength of 105 kg/mm² and a yield strength of 81.6 kg/mm² compared to 84.5 and 49 kg/mm², respectively, for conventionally heat-treated specimens. LTMT, however, UDC: 669.14.018.45:621.785.53

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205020008-4"

Card 1/2

L 47302-66

ACC NR: AP6032054

reduced the elongation and reduction of area to 14 and 28% compared to 30 and 42% for conventionally treated specimens. In tests at 700C, the difference became insignificant. The reduction of area of specimens rolled at 600C and aged at 600C for 100 hr was 55.6%; much higher in comparation to other heat treatment processes. Both types of LTMT lowered impact strength to 5.7 kg/cm² at 20 or 700C compared to 23.3 kgm/cm² in conventionally heat-treated specimens. LTMT greatly improved the heat resistance. Alloy containing 6% molybdenum, rolled at 600C and aged at 760C for 25 hr, had at 700C under a stress of 25 kg/mm² a rupture life of 1200 hr compared to 179 hr for conventionally treated alloy. Alloy with 4% molybdenum, cold-drawn with 50% reduction and tested at 700C under a stress of 20 kg/mm², failed after 5000 hr, compared to 1700 hr for conventionally treated alloy. Orig. art. [AZ]

SUB CODE: 11, 13/ SUBM DATE: 07Aug65/ ORIG REF: 002/ ATD PRESS: 5094

Card 2/2 afs

ķ

EWT(m)/EWP(w)/EWP(k)/EWP(t)/ETI IJ'(c) SOURCE CODE: UR/0370/66/000/004/0064/0067 AP6027741 AUTHOR: Kal'ner, V. D. (Moscow); Kidin, I. N. (Moscow); Bernshteyn, M. L. (Moscow) 40 ORG: None 37 B TITLE: Electrical ausforming of spring steel SOURCE: AN SSSR. Izvestiya. Metally, no. 4, 1966, 64-67 TOPIC TAGS: metal ausforming, spring steel, mechanical heat treatment, metal deformation, ductility ABSTRACT: The authors study the possibility of using high-speed electrical heating in ausforming of 55KhGR spring steel. The contact method was used for heating to 950°C before deformation at rates of 15, 30, 45 and 120°/sec. The back-up roll on the mill was used as one of the contacts so that deformation was done practically at the neating temperature. The blanks subjected to reduction measured 120×15 mm with thicknesses from 3 to 5 mm depending on the degree of deformation (15-38%). Immediately after rolling, the workpiece went into a quenching vat with oil or onto a cold metal plate (for air-quenching) and was then tempered at 250°C for one hour. The mechanical properties were studied on flat tensile specimens with working dimensions of 30×2×4 mm and compared with similar data for ausforming in a conventional electric furnace (heating temperature 950°C with holding for 5 minutes). An increase in the heating rate UDC: 539,4,015/019 Card 1/2

L 07389-67 ACC NR: AP6027741 3 results in additional improvement in mechanical properties with reductions of 15-30%. For small deformation or none at all, high-speed electric heating produced a slight increase in tensile strength although brittle fracture was observed with an elongation of less than 2%. No further increase in tensile strength was observed with deformation of more than 25% and there was even a slight reduction in tensile strength at a heating rate of 120 deg/sec while specimens subjected to conventional ausforming showed a continuous increase in strength at deformations of 37-40%. Strength characteristics are practically identical for both types of ausforming at these deformations. Electrical ausforming improves ductility with elongation reaching 9% as against 6.5% for conventional ausforming with corresponding figures of 35-40% against 18-20% for constriction. Improvement in the properties of 55KhGR spring steel with conventional susforming is reached at a reduction of 25-30%, while this "threshold" deformation is much more pronounced in electrical ausforming and is reached at a reduction of approximately 15-20%. The maximum difference between strength and ductility produced by electrical and conventional ausforming is also observed at reductions of 15-20%. Orig. art. has: 4 figures, 1 table.

EUB CODE: 11/ SUBM DATE: 27Nov64/ ORIG REF: 004

Card 2/2 LS

ACC NRI AP6036393

(A)

SOURCE CODE: UR/0032/66/032/011/1405/1406

AUTHOR: Bernshteyn, M. L.; Marko, I.

ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov)

TITLE: Characteristics of stress-strain diagrams of superstrength steel with strain-hardened martensite

SOURCE: Zavodskaya laboratoriya, v. 32, no. 11, 1966, 1405-1406

TOPIC TAGS: superstrength steel, steel thermomechanical treatment, stress strain diagram, strain hardening/50KhFA steel

ABSTRACT: Specimens of 50KhFA steel were subjected to a combined thermomechanical treatment (CTMT) which consisted of high-temperature thermomechanical treatment followed by quenching to obtain a martensitic structure and tempering at 200C for 2 hr, and low temperature thermomechanical treatment (LTMT) which consisted of cold deformation with 1—3% reduction followed by aging at 100C for 40 hr. The diagrams of the conventionally treated specimens did not show a distinct yield point. The thermomechanically treated specimens, however, show very distinct upper and lower yield points (see Fig. 1). The difference between these two points increased with increasing reductions in LTMT, and in specimens deformed with 3% reduction, amounted to 55 kg/mm², It is assumed that aging of martensite whose matrix

Cord 1 /2

UDC: 620.172.2

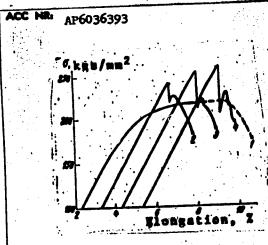


Fig. 1. The effect of reduction in martensite deformation on the shape of the stress-strain curve of 50KhFA steel

1 - Conventionally hardened and tempered at 200C; 2 - same with 1% reduction aged at 100C for 40 hr; 3 - same with 2% reduction; 4 - 4 - same with 3% reduction.

was distorted by cold deformation plays a significant part in strengthening. The second maximum on the stress-strain curve corresponds to the intensive reduction of area and is brought about by the strain aging occurring during the test. Orig. art. has: 3 figures.

SUB CODE: 11, 13/ SUBM DATE: none/ ORIG REF: 002/ OTH REF: 002/

the second of the second second

ATD PRESS: 5107

Card 2/2

L 08687-67 EWP(k)/EWT(m)/EWP(t)/ETI IJP(c) JD/HW ACC NR: AP6031718 (A) SOURCE CODE: UR/0370/66/000/005/0091/0097 AUTHOR: Bernshteyn, H. L. (Moscow); Zlochevskaya, I. I. (Moscow)
ORG: none TITLE: Dislocation structure of Nimonic-type alloy after thermo- mechanical treatment performed under different conditions
SOURCE: AN SSSR. Izvestiya. Metally, no. 5, 1966, 91-97 CRYSTAL DISLOCATION, ANNEALING, METAL ROLLING, CRYSTAL DISLOCATION, ANNEALING, METAL ROLLING, TOPIC TAGS: Anickel chromium alloy, alloy thermomechanical treatment, nickel chromium alloy structure, dislocation structure/KhN77TYUR alloy ABSTRACT: A series of specimens of KhN77TYUR Nimonic-type alloy were subjected to two variants of thermomechanic treatment: (1) annealing subjected to two variants of thermomechanic treatment: (1) annealing at 1080C for 8 hr, water quenching, cold rolling, and aging at 700C at 1080C for 8 hr, water quenching, water quenching, and aging.
for 16 hr or (2) annealing, hot rolling, water quantoms of about 50%, a increased with increased reduction. At reductions of about 50%, a increased with increased reductions took place, with a random accumulation redistribution of dislocations took place, with a random accumulation of dislocations within cells 0.1—0.2 micron in diameter. No selective of dislocations within cells 0.1—0.2 micron in diameter. No selective precipitation of y'-phase on the dislocations during aging was observed. In spacimens cold rolled with reductions up to 20%, the aging promotes a polygonization accompanied by considerable annihilation of dislocations. Cord 1/2 UDC: 669.245

L 08687-67 ACC NR: AP6031718 0 However, the cellular structure, formed in cold rolling with 50% reduction, remains stable during aging. Also, in hot rolling simultaneously with an increase in dislocations density, a redistribution of dislocation and the formation of a structure with stable subboundaries occurred. Within polygon and recrystallized grains, the dislocation structure remains unchanged. The structure, formed by high-temperature deformation, is not affected by subsequent aging at 700C. Orig. art. has: 4 figures. SUB CODE: 13, 11/ SUBH DATE: 05Ju165/ ORIG REF: 003/ OTH REF: 002 Card 2/2 ml

L 08426-67 EWT(m)/EWP(w)/EWP(k)/EWP(t)/ETI IJP(a) ID/HW/JG/GD SOURCE CODE: UR/0000/66/000/	·
ACC NR. AT6034438 (W) SOURCE CODE: UR/0000/66/000/	/000/0084/0086
AUTHOR: Demina, E. L.; Bernshteyn, M. L.	36.
ORG: none	(84)
TITLE: Effect of polygonization on the heat resistance char of molybdenum	acteristics
SOURCE: AN SSSR. Institut metallurgii. Svoystva i primeneni zharoprochnykh splavov (Properties and application of heat ralloys). Moscow, Izd-vo Nauka, 1966, 84-86	ye 'esistant
TOPIC TAGS: molybdenum, molybdenum-mechanothermal treatment polygonization, po	· nolybdenum
ABSTRACT: Specimens of sintered-molybdenum wire, 1.00 mm in	diameter
were drawn at 300 or 1150C with 5, 9 or 13% reduction, vacuu at 1150C for 1 hr, and subjected to stress-rupture tests at	900C under
a stress of 20 kg/mm. The rupture life was found to increa	se with in-
creasing reductions. For instance, specimens drawn at 1150C reduction and then annealed at this temperature for 1 hr wi	with 5%
95 min, while specimens reduced by 9 or 13% and annealed wit or 585 min respectively. The annealing of deformed molybden	hatood 240
the formation of a polygonized structure which has a high cr	um stimulates
Cord 1/2	18

L 08426-67

ACC NR: AT6034438

ance. However, with drawing at low temperature or with lower reduction, the polygonization is not completed after 1 hr at 1150C. Only drawing with 13% reduction at 1150C, followed ay annealing at the same temperature produces a complete polygonization and the highest increase of rupture life. This mechanothermal treatment, which creates a polygonized structure, also substantially improves the ductility. For instance, the maximum elongation of molybdenum deformed at 1150C with 9% reduction and annealed at 1150C is 24% compared with 6% for molybdenum deformed at 300C and tested without being annealed. Specimens deformed at 300C with 5 and even 13% reduction also have a lower ductility. Orig. art. has: 2 figures.

0

SUB CODE: 13, 11/ SUBM DATE: 10Jun66/ ATD PRESS: 5103

Cord 2/2 LS

ACC NR. AP6032199 SOURCE CODE: UR/0133/66/000/010/0944/0946 AUTHOR: Dregan, N.; Bernshteyn, M. L. ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov) TITIE: High temperature thermomechanical treatment of 38KhNM alloy steel drill pipes SOURCE: Stal', no. 10, 1966, 944-946 PIPE, HOT ROLLING, alloy steel, high temperature thermomechanical treatment, drill pipe, TOPIC TACS: metal property /38KhNM alloy steel ABSTRACT: Hot-rolled 38KhNM drill pipes were subjected to high temperature thermomechanical treatment (HTMT) and water quenched immediately after rolling. Pipes which were tempered at 500-600C or at 200C after HTMT had a tensile strength 125-132 and 220-235 kg/mm², a yield strength of 118-123 and 185-200 kg/mm², an elongation of 10% (in both cases), a reduction of area of 52-55% and 40-50%, and a notch toughness of 9.5-11.5 and 7.5-10 kgm/cm2, respectively. Corresponding figures for conventionally treated (annealed at 860-9000 and air cooled) pipes were 85 kg/mm², 62 kg/mm² 17%, 53%, and 7.5 mkg/cm². Pipes which were tempered at 500C after HTMT then reheated in a molten salt bath to 850C quenched, and tempered at 600C, still had a tensile strength of 100 kg/mm², a yield strength of 82 kg/mm², and elongation of 13.5%, a reduction of area of 58%, and a notch toughness of 10.4 kg/cm². Orig. art. has: 2 figures. SUB CODE: 11/ SUBM DATE: none/ ORIG REF: 002 Card 1/1 <u> UDC: 621.785:621.774.3</u>

ACC NR. AP6035960 SOURCE CODE: UR/0129/66/000/010/0069/0070 AUTHOR: Bernshteyn, M. L.; Zuyeva, O. M. ORG: Moscow Institute of Steel and Alloys (Non'tovskiy institut stali i splavov) TITLE: Recrystallization of manganese and nickel steels in hightemperature thermomechanical treatment SOURCE: Hetallovedeniye i termicheskaya obrabotka metallov, no. 10, 1966, 69-70 TOPIC TAGS: metal recrystallization, meetal recrystallization temperature, steel thermomechanical treatment, high temperature thermomechanical treatment, manganese steel, nickel steel, MFCHANICAL HEAT THEATMENT ABSTRACT: The effect of manganese (2, 4, 6 and 8%) and nickel (4, 8, 12 and 16%) on the recrystallization of steels containing 0.01-0.8% carbon during high temperature thermomechanical treatment (HTMT) has been investigated. Prior to HTMT, manganese steel specimens were fully annealed at 800-850C for 1.5-2 hr, and nickel steel specimens were tempered at 500-550C for 7-10 hr. HTMT consisted of heating to a temperature 70-90C above the Ac, point, holding for 20 min, rolling with a reduction of 50% and subsequent water quenching. It was found that Card 1/2 UDC: 669.24 74:621.977:620.186.5

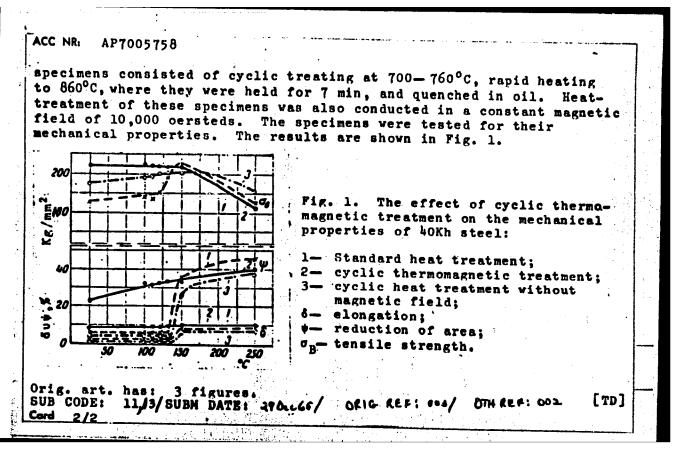
manganese and nickel delay the recrystallization, particularly in steels with a very low carbon content. Increased carbon content contributes to the development of recrystallization. Hanganese steels containing 0.01% and 6—8% Mn may be subjected to HTMT, since these steel exhibit a considerable delay of at least 10 sec in recrystallization with 50% deformation. Orig. art. has: 2 figures.

SUB CODE: 13, 11/ SUBM DATE: none/ ORIG REF: 002

SOURCE CODE: UR/0129/66/000/010/0069/0070 ACC NR: AP6035960 AUTHOR: Bernshteyn, M. L.; Zuyeva, O. M. ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov) TITLE: Recrystallization of manganese and nickel steels in hightemperature thermomechanical treatment SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 10, 1966, 69-70 TOPIC TAGS: metal recrystallization, metal recrystallization temperature, steel thermomechanical treatment, high temperature thermomechanical treatment, manganese steel, nickel steel, MFCHANICAL HEAT THEEATMENT ARSTRACT: The effect of manganese (2, 4, 6 and 8%) and nickel (4, 8, 12 and 167) on the recrystallization of steels containing 0.01-0.87 carbon during high temperature thermomechanical treatment (HTMT) has been investigated. Prior to HTMT, manganese steel/specimens were fully annealed at 800-850C for 1.5-2 hr, and nickel steel specimens were tempered at 500-550C for 7-10 hr. HTMT consisted of heating to a tenperature 70-90C above the Ac, point, holding for 20 min, rolling with a reduction of 50% and subsequent water quenching. It was found that UDC: 669.24'74:621.977:620.186.5 Card 1/2

	manganese and nickel delay the recrystallization, particularly in with a very low carbon content. Increased carbon content contrib to the development of recrystallization. Manganese steels contain 0.01% and 6—8% Mn may be subjected to HTMT, since these steel a considerable delay of at least 10 sec in recrystallization with deformation. Orig. art. has: 2 figures.						
1	SUB CODE	13, 11/	SUBM DATE	: none/	ORIG REF:	002	
	Card 2/						

ACC NRI AP7005758 SOURCE CODE: UR/0126/67/023/001/0158/0161 AUTHOR: Bernshteyn, M. L.; Granik, G. I.; Zaymovskiy, V. A. ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali The effect of cyclic thermomagnetic treatment near the Curie point on the ductility of iron SOURCE: Fizika metallov i metallovedeniye, v. 23, no. 1, 1967, 158-161 alloy fiet fustment, iron, allow steel, but lity, thermomagnetic effect, Curic point, iron property, steel TOPIC TAGS: property/Armco iron, 40Kh steel ABSTRACT: Armco iron specimens were heated for five cycles, each at 750 for 10 min and 790°C for 10 min; after which the temperature was rapidly raised to 920°C where the specimens were held for 3 minutes and then quenched in water. The thermal treatment was conducted in a constant magnetic field of 10,000 oersteds. It was found that magnetic treatment lowered the nil-ductility temperature of the Armco iron specimens. For instance, at - 96°C the notch toughness was increased from 3.5 kgm/cm² (cyclic heat treatment without magnetic field) to 11 kgm/cm2 (cyclic thermomagnetic treatment), and at -75°C it was increased from 6.5 to 19 kgm/cm2, respectively. Thermal treatment of 40Kh steel Card 1/2 UDC: 539.4.016



ACC NR: AP7005762

(A, N)

SOURCE CODE: UR/0126/67/023/001/0176/0179

AUTHOR: Bernshteyn, M. L.; Goller, R.

ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov)

TITLE: Effect of high-temperature thermomechanical treatment combined with cold deformation of martensite on the properties of machine steel

SOURCE: Fizika metallov i metallovedeniye, v. 23, no. 1, 1967, 176-179

TOPIC TAGS: machine steel, metal heat treatment, tempering, cold rolling / 40KhN4 type steel

ABSTRACT: This is a continuation of previous investigations of the Czechoslovak ChSN 16440 machine steel (0.44% C, 3.7% Ni, 0.84% Cr) of the 40KhN4 type (Bernshteyn, M. L., Dregan, N. Metallovedeniye i term. obrabotka metallov, 1965, no. 6, 3; Goller, R. Materialovy Sbornik, SVUMT, 1965) with the difference that it deals with combining the high-temperature thermomechanical treatment (HTTMT) of this steel (deformation at 920-950°C, followed by low-temperature tempering at 100, 150 and 200°C for 2 hr) with subsequent deformation of its martensitic structure by cold rolling. HTTMT enhances the plasticity of steel and hence prevents

Card 1/2

UDC: 669.14.018.295

ACC NR: AP7005762

to some extent premature brittle fracture compared with control (quenched) specimens. Findings: tempering at 100°C is ineffective; it is only following tempering at 150-200°C that the positive effect (increase in strength without detriment to the plasticity induced by HTTMT) of subsequent (following HTTMT) deformation of martensite manifests itself and the ultimate strength of 40KhN4 type steels rises to as much as 300 kg/mm². This favorable change in properties following HTTMT + cold deformation of martensite is due to the processes of dispersion hardening in the partially recrystallized structure of the material. Orig. art. has: 4 figures.

SUB CODE: 13, 20, 11/ SUBM DATE: 14Feb66/ ORG REF: 005/ OTH REF: 002

 C_{ard} 2/2

SOV/137-58-11-22504D

Translation from: Referativnyy zhurnal. Metallurgiya, 1958, Nr 11, p 95 (USSR)

AUTHOR: Bernshteyn, M. M.

An Investigation of the Process of Cold Drawing of Small and Extra-TITLE:

small Precision Tubing of Stainless and Carbon Steel and of Alloys (Issledovaniye protsessa kholodnogo volocheniya pretsizionnykh trub malykh i sverkhmalykh razmerov iz nerzhaveyushchey i uglerodistoy

stali i splavov)

PERIODICAL: Author's dissertation for the degree of Candidate of Technical

Sciences, presented to the Vses. n. -i. trubn. in-t (All-Union

Scientific Research Institute for Piping), Dnepropetrovsk, 1958

An equation is derived for determining change in wall thickness ABSTRACT:

per pass in drawing (D) tubes (T) without mandrel. This formula shows that: 1) Change in wall thickness depends primarily upon the ratio of the initial thickness So to the initial outside T diameter Do, upon the reduction ratio E, and upon the coefficient of tension B; when the S₀:D₀ ratio is very small, the thickening of the wall is at a maximum; 3) when Δ S₀:S₀ is zero, it is possible to find a

So:Do critical ratio at which the wall thickness does not change. Card 1/3

SOV/137~58~11-22504D

An Investigation of the Process of Cold Drawing (cont.)

Ittis:experimentally established that the conditions of strength of the T cross section and the strength of the head in D without mandrel permit partial reductions of as much as 42-47%. In mandrel-less D of thin-walled and extra-thin-walled T, the degree of deformation of the T is limited by the stability of its profile. A formula is derived for determination of the maximum deformation, & %, under these conditions, when S:D<0.04. Diameter shrinkage rises with increase in the S:D ratio; the reduction ratio , μ , and the angle of inclination of the bell generatrix are determined by the formula derived. It is found that on multiple D of T without heat treatment, the value of σ_V rises in proportion to ε up to a given limit. A formula is derived for total reduction ratio, μ , which makes it possible to discover the required strength properties of T of Nr 1Kh18N9T steel in accordance with the terminal values of Sk and Dk. When T are drawn on a long mandrel (M), the forces of friction in the die and the M are different in direction. The forces of friction on the M facilitate D. It is experimentally established that when T is drawn on a long M, the maximum draft per pass with a copper-plated M surface is $\mu = 2.6$. When the M surface has been polished with emery cloth, $\mu = 2.75 - 2.8$; when the M surface has been worked with rough emery wheel, μ =3.05. Subsequent D of T without mandrel and with no prior heat treatment showed that they could be D to 4.1x0.45 mm. Card 2/3

SOV/137-58-11-22504D

An Investigation of the Process of Cold Drawing (cont.)

ASSOCIATION: Vses. n. -i. trubn. in-t (All-Union Scientific Research Institute for Piping), Dnapropetrovsk

P. G.

Card 3/3

SOV /137-58-12-25246

Translation from: Referativnyy zhurnal. Metallurgiya, 1958, Nr 12, p 172 (USSR)

AUTHORS: Borisov, S. I., Bernshteyn, M. M.

TITLE: Changes in the Mechanical Properties of IKh18N9T Stainless Steel in Relation to the Degree of Deformation During Cold Drawing (Izmeneniye mekhanicheskikh svoystv nerzhaveyushchey stali marki 1Kh18N9T ot

stepeni deformatsii pri kholodnom volochenii)

PERIODICAL: Byul. nauchno-tekhn. inform. Vses. n.-i. trubnyy in-t, 1958, Nr 4,

pp 62-70

ABSTRACT: An investigation was made of the effect of different procedures of cold

drawing and intermediate heat treatment on the mechanical properties of 1Kh18N9T steel in the manufacture of capillary, thin-walled, and precision tubes. A batch of 10 x 1 mm hollow ingots was divided into six groups. Each group was drawn under different conditions with a view of determining the reduction operation after which heat treatment of the tubes should be terminated. Specimens were taken from each group after each reduction in order to determine their mechanical and

technological characteristics, namely: σ_b, δ, the bending stress

Card 1/2 corresponding to the beginning of residual deformation, the bending

SOV /137-58-12-25246

Changes in the Mechanical Properties of 1Kh18N9T Stainless Steel (cont.)

moment, and the number of bendings. It was established that upon the cessation of heat treatment σ_b increases and attains its maximum after 7-10 reductions. At that point δ has a value of 2-2.5%, and further drawing of the tubes is feasible. With a lower value of δ the number of ruptures increases appreciably. Therefore, in the examined case of drawing of tubes with 0.6-1.5 mm outer diameter and walls 0.15 mm thick, the number of reductions without heat treatment should be limited to 7-10. On the basis of the findings of the work a diagram was constructed correlating that value of the draft μ which ensures the maximum strengthening of steel with the ratio of the wall thickness to the tube diameter, μ =2.2 S/D. The formula affords a means for tentative calculation of pass sizing during the drawing of thinwall tubes with cold-hardened surface without preliminary experiments.

M.Sh.

Card 2/2

SOV/137-59-3-6962

Translation from: Referativnyy zhurnal. Metallurgiya, 1959, Nr 3, p 290 (USSR)

Borisov, S. I., Bernshteyn, M. M. AUTHORS:

4-5, pp 71-76

Permissible Reductions During Drawing of Small Pipes Without a Mandrel Based on Considerations of Their Stability With Regard to TITLE: Buckling in the Area of Contact (Depustimyye velichiny obzhatiy pri bezopravochnom volochenii trub malykh razmerov s uchetom ustoychivosti formy truby v ochage deformatsii)

PERIODICAL: Byul. nauchno-tekhn. inform. Vses. n-i. trubnyy in-t, 1958, Nr

ABSTRACT: In order to determine the effect of the strength of the exit cross section on the magnitude of maximum deformation (D) of small pipes (P), the process of drawing of P's with a wall thickness-diameter ratio (S/D·100%) of 4-30% was investigated at D's amounting to 47% per pass and at a velocity of drawing of 12 m/min. Graphs are presented showing the maximum D as a function of the ratio of wall thickness to the diameter (S/D ratio) of the P for various angles of cone-shaped entrance openings of the drawing dies. These graphs

indicate that P's with ratios $S/D \cdot 100\% = 4 - 10\%$ and $S/D \cdot 100\% = 10 - 18\%$ Card 1/2

SOV/137-59-3-6962

Permissible Reductions During Drawing of Small Pipes (cont.)

may be drawn at D's of 35-40% and up to 25%, respectively. Correspondingly, at S/D = 100% = 20-25% and S/D = 100% > 25%, the D must not exceed 18 and 10%, respectively. The optimal angle a of the inclination of the fibers amounts to 120. The results of experiments dealing with resistance to buckling of P's within the draw plate during drawing without a mandrel demonstrated that in the case of drawing of thin-walled P's the degree of D is limited by the specific value of the S/D ratio rather than by the absolute values of the wall thickness and the diameter of the P. Graphs showing the D as a function of the ratio of the wall thickness to the diameter of the P demonstrate that at ratios S/D 100%=2%, S/D 100%=3%, and $S/D \cdot 100\% = 3.5\%$ the D must not exceed 10, 25, and 35%, respectively. At $S/D \cdot 100\% = 4\%$ the maximum **D** is already governed by the strength characteristics of the gripped end or of the final cross section of the P. A reduction in the resistance to buckling of the P in the draw plate is significantly affected by the shape of the pointed end and by the extent of variations in wall thickness of the P. Experimental results demonstrated that, compared with the D of P's with standard ends, the critical D of P's having cupped ends was 1.3 - 1.5 times greater.

M.K.

Card 2/2

BERNSHTEYN, M.M., inch.

Changes in wall thickness in drawing small-diameter tubes without mandrels. Obr. met. davl. no.5:179-197 '59. (MIRA 13:3)

1. Vsesoyusnyy nauchno-issledovatel'skiy trubnyy institut.
(Deep drawing (Metalwork))

8/137/61/000/005/023/060 A006/A106

AUTHOR:

Bernshteyn, M.M.

TITLE:

Changes in the wall thickness during mandrelles drawing of small-

size pipes

PERIODICAL:

Referativnyy zhurnal. Metallurgiya, no. 5, 1961, 27, abstract 5D256

("Tr. Ukr. n.-i. trubn. in-ta", 1959, no. 1 , 125 - 145)

To check the derived theoretical dependences of metal deformation and the distribution of stresses in the draw plate, affecting changes in the wall thickness of pipes, tests were performed on a 15-ton mill at a drawing rate as high as 12 m/min. Cold-stretched seamless pipes of 1 X 18H 9T (1Kh18N9T), 30 XTC A (30KhGSA), Fe-Ni steel, Armco-Fe and Cu were subjected to drawing. Graphite mixed with automobile lubricating oil was used as a grease. Broaching of the pipes was performed at 10, 20 and 30% degrees of deformation. The draw plates were made of $\coprod X$ 15 (ShKh15) steel with $R_c = 52 - 56$. The theoretical and experimental results were used for the plotting of curves which show the changes in the thickness of pipe walls and whose results are in a satisfactory agreement. The magnitude of reduction is an important factor, affecting the

Card 1/2

Changes in the wall thickness ...

S/137/61/000/005/023/060 A001/A101

wall thickness of the pipes and the shifting of the critical correlation S/D where S is the wall thickness of the pipes and D is the external diameter of the pipe. Graphs are plotted showing the changes in the thickness of pipe walls and a formula is derived to determine the initial thickness of pipe walls at a 12° inclination angle of the generatrix of the draw plate aperture.

A.B.

[Abstracter's note: Complete translation]

Card 2/2

S/137/61/000/006/049/092

AUTHOR:

Bernshteyn, M.M.

TITLE:

Determining the drawing force and the mean value of deformation

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no. 6, 1961, 36, abstract 6D295

("Tr. Ukr. n.-1. trubn. in-ta", 1959, no. 1, 145 - 156)

TEXT: The author studied changes in the strength properties of metal along the deformation seat during mandrelless drawing of pipes and derived a formula for determining the mean value of deformation resistance. An empiric formula is suggested for calculating the magnitude of axial stress and pull force during the drawing of stainless and carbon steel pipes of 2.0 - 16 mm in diameter on a long mandrel and without a mandrel. Calculations made by the formulae suggested, yield values the most approaching actual data. For stainless seel the following formula was obtained: $f_h \approx 0.82 \text{ R}^B$.

V. Pospekhov

[Abstracter's note: Complete translation]

Card 1/1

8/123/61/000/011/015/034 A004/A101

AUTHORS:

Pishik, N. S.; Vdovin, F. V.; Chukmasov, A. S.; Bernshteyn, M. M.

TITLE:

Investigating centrifugal castings from 1X13H18B25 (1Kh13N18V2B)

steel for the production of particularly thin-walled tubes

PERIODICAL: Referativnyy zhurnal, Mashinostroyeniye, no. 11, 1961, 66, abstract

11B511 (V sb. "Proiz-vo trub" no. 3, Khar'kov, 1960, 123-130)

TEXT: The authors investigated the microstructure of 1Kh13N18V1B steel specimens in the cast and heat-treated state. To check the quality of hot-rolled 89 x 6.5 mm tubes from this steel after heat treatment, their mechanical properties were determined, the macro- and microstructure analyzed and the intercrystalline corrosion tested. The obtained results confirm the possibility of producing especially thin-walled tubes (25 x 1 and 19.5 x 0.2 mm) from 1Kh13N18V1B steel blanks cast by the centrifugal method. There are 3 figures and 3 references.



[Abstracter's note: Complete translation]

Card 1/1

ACC NR: AR6035104 SOURCE CODE: UR/0137/66/000/008/D034/D034

AUTHOR: Alferova, N. S.; Bernshteyn, M. M.; Kurdyumova, G. G.

TITLE: Mastering of technology for making pipe from N36KhT steel

SOURCE: Ref. zh. Metallurgiya, Abs. 8D233

REF SOURCE: Sb. Proiz-vo trub. Vyp. 16. M., Metallurgiya, 1965, 41-45

TOPIC TAGS: pipe, pipe manufacture/N36KhT steel

ABSTRACT: A detailed analysis was made of the manufacturing technology of pipe from austenitic precipitation hardenable N36KhT steel. With this technology, more than 8000 m of various gages of pipe were produced from centrifugal hollow billets by cold rolling and drawing. The results of technological tests (flattening and expanding) indicated that the finished pipes meet all requirements. Comparison of their qualities with the qualities of cold-formed pipe produced from rolled drilled billets, indicated that the two types of pipe did not differ one from another in mechanical properties and impurity contentration of nonmetallic inclusions. Orig. art. has: 3 figures. L. Kochenova. [Translation of abstract] [NT] SUB CODE: 11/

Card 1/1

UDC: 621, 774, 35

BERNSHTEYN, M.M.

New method of gluing soles without damaging the footwear Leg. prom., no. 2, 1952

BERNSHTEYN, M.M.

Classification of hard leather Leg. prom., no. 3, 1952

BERNSHTKYN, M. L.

Leather Industry and Trade

Measuring stiff leather by its weight and area, Leg. prom. 12 No. 4, 1952

Monthly List of Russian Accessions, Library of Congress, July 1952. Unclassified.

BERNSHTEYN, M.M.

Effect of hydrothermal actions on the firmness of glue strength Leg. prom., 12, no. 6, 1952

BERNSHTEYN, M.M., kandidat tekhnicheskikh nauk; RAUZER, E.K., inzhener.

Introducing a new method of testing the durability of gluing soles and of statistical quality control. Leg. prom. 14 no.4:16-19 Ap '54. (MLRA 7:6) (Boots and shoes) (Quality control)

BERESHTEIN, M.M., kandidat tekhnicheskikh nauk.

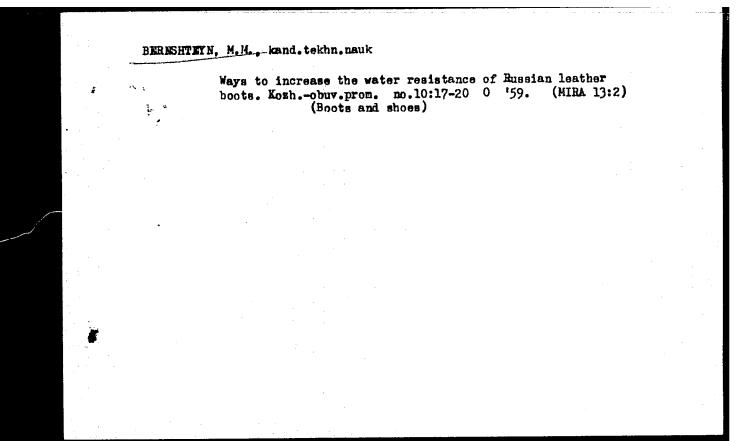
Bificient method of cutting out stiff leather. [MLRA 8:2]

ne.12:39-42 D 154.

(Shee industry)

BERNSHTEYN, M.M., kandidat tekhnicheskikh nauk

Wear resistance of children's "parko" footwear. Leg.prom. 15 no.5: 29-32 My '55. (MIRA 8:7) (Shoe industry)



BERNSHTEYN, M.M., kand.tekhn.nauk

New technology for assembling and fastening two-layer counters as a factor for increasing the water resistance of Russian leather boots. Kosh.-obuv.prom. 2 no.5:19-23 My 160.

(MIRA 13:9)

(Boots and shoes)

HERNSHTEYN, M.M.

Improving the waterproofing of boots made with Russian leather.

Manch.-issl.trudy TSNIKP no.32:103-122 '60. (MIRA 15:12)

(Boots and shoes) (Waterproofing)

GAMOVA-KAYUKOVA, N.I., kand.biol.nauk; SAMYSHKINA, M.A., starshiy nauchnyy sotrudnik; BERNSHTEYN, M.M., kand.tekhn.nauk; MUSATOVA, M.D., mladshiy nauchnyy sotrudnik; ABOLTINA, E.M., mladshiy nauchnyy sotrudnik; CHERKESOVA, E.I., mladshiy nauchnyy sotrudnik; IVANOVA, R.A., laborant.

Resistance to moulds of artificial leather, cardboard and 'entduck samples. Nauch.-issl. trudy VNIIPIK no.13:65-83 '62. (MIRA 18:1)

BERNSHTEYN, M.M.

Methods for the classification and determination of the basic parameters of stiff leather according to the established regularities of thickness distribution. Nauch.-issl. trudy TSNIKP no.33: 116-136 *63 (MIRA 18:1)

BERNSHTEYN, Maks Mikhaylovich; ZAYONCHKOVSKIY, A.D., prof., red.; KALASHNIKOVA, L.V., red.

[Manufacture of artificial leather in rclls on continuous production lines; a textbook] Proizvodstvo rulonnoi iskusstvennoi kozhi na potochnykh liniiakh; uchebnoe posobie. Moskva, Legkaia industriia, 1964. 42 p. (MIRA 18:5)

L 23826-66 ENT(m)/ENP(w)/EWA(d)/T/EWP(t)/EWP(k) IJP(c) JD/HW ACC NR. AP6013358 UR/0370/66/000/002/0061/0068 SOURCE CODE: AUTHOR: Zaymovskiy, V. A. (Moscow); Bernshteyn, M. L. (Moscow) 16 ORG: none 13 TITLE: High-temperature thermomechanical treatment of carbon steels SOURCE: AN SSSR. Izvestiya. Metally, no. 2, 1966, 61-68 TOPIC TAGS: thermomechanical treatment, high temperature treatment, carbon steel treatment ABSTRACT: Carbon steels St40 (0.447C) and U9 (0.867C) have been tested for the effect of high-temperature thermomechanical treatment (HTMT). Steel specimens 2-3 mm thick were austenitized, rolled with 15,25, and 50% reduction with rolling ending at 790-800C for U9 steel and 830-840C for St40, immediately water quenched, and then tempered at 100-500c. HTMT improved considerably the strength and ductility of both steels. St40 rolled with 50% reduction and tempered at 1500 had a tensile strength of 190 kg/mm², an elongation of about 2%, and a reduction of area of 11%. The strength of U9 steel rolled with a reduction of 25% and tempered at 300C reached a maximum of 210 kg/mm² at an elongation of 5% and a reduction of area of 12%. Conventional hardening produced a measurable ductility (elongation of 1-5%) in U9 and St40 tempered at 350C or 300C, respectively, after which the steels have a respective tensile strength of 160 and 145 kg/mm². The results of these UDC: 669.14-157.9 Card 1/2

19 mm in d is 2.5—3	iameter. times his	ed as a basis for d The unit has alrea ther than those product				
SUB CODE:	11, 13/	SUBM DATE: none/	ATD PRESS:	4247	,	
				•	•	
		마이 회사 회사 (1922년 - 1922년 - 1922 1922년 - 1922년	e e	٠.,	•	
	Y ₁				•	
·						
	•			•		

BERNSHTEYN, M. S.

Bernshteyn, M. S. "The form of flow and the pressure of grain in silos", in the collection: Issled. raboty po inzh. konstruktsiyam, Issue 2, Moscow, 1948, p. 139-68, - Bibliog: 12 items.

SO: U-3261, 10 April 53, (Letopis 'Zhurnal 'nykh Statey, No. 11, 1949).

BERESHTEYN, M.S., kandidat tekhnicheskikh nauk.

Approximate calculation of stability of elastic systems subjected to the joint action of several loads. Stroi.prom.34 no.12:31-33 D 156.

(Elasticity)

BERNSHTEYN, N.S., dots., kand. tekhn. nauk

Effect of initial stresses on the stability of plates. Nauch. trudy MLTI no.8:36-49 58. (MIRA 13:3)
(Elastic plates and shells)

ZHEMOCHKIN, B.N., prof.; PASHCHEVSKIY, D.P., dotsent; BERNSHTEYN, M.S., dotsent; NIKIFOROV, S.N., prof.; TOCHISKIY, V.F., dotsent [deceased]; VILKOV, G.N., red.izd-va; RUDAKOVA, N.I., tekhn.red.

[Course in structural mechanics] Kurs stroitel noi mekhaniki. Pod obshchei red. B.N. Zhemochkina. Izd. 2. Moskva, Gos.izd-vo lit-ry po stroit., arkhit. i stroit.materialam. Pt. 3. [Statics of structures] Statika soorushenii. 1959. 333 p. (MIRA 12:12) (Structures, Theory of)