



CIA-RDP86-00513R000412610004-3



APPROVED FOR RELEASE: 03/20/2001

CIA-RDP86-00513R000412610004-3

307/51-6-5-26/34 24(4) AUTHORS : Zakharyevskiy, A.N. and Fedin, L.A. TITLE : Measurement of Double Refraction of Fibres (Izmereniye dvoynogo lucheprelomleniya volokon) PERIODICAL : Optika i Spektroskopiya, 1959, Vol 6, Nr 5, pp 701-703 (USSR) ABS TRACT: A polarization microscope suitable for measurement of double refraction in fibres is shown in Fig 1. A fibre F is placed in a suitable immersion medium between an objective Ob and a condenser K. The other parts of the microscope are: a polarizer P, an analyser A, an ocular Oc and a Wollaston prism W (placed in the image plane). For 0.01-0.02 mm thick fibres the magnification is 500 X. The system produces linear interference bands at right-angles to the fibre. A fibre displaces the bands by an amount $\Delta \mathbb{N}$ which is related to double refraction, defined as the difference between the refractive indices of polarized rays $(n_{H} - n_{1})$, by the following expression $\Delta^{\mathrm{N}} \stackrel{\mathrm{a}(\mathrm{n}_{\mathrm{I}} - \mathrm{n}_{\mathrm{I}})}{}$ (1)where a is the thickness of the fibre and λ is the wavelength of the light used. Fig 2 shows a microphotograph taken in green light Card 1/3

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SOV/51-6-5-26/34 Measurement of Double Refraction of Fibres (546 mµ). The five fibres shown in Fig 2 are: (1) caprone, (2) "lavsan", (3) nitron, (4) cuprammonium rayon, (5) viscose rayon. The strongest double refraction occurs in "lavsan" (fibre 2) and the weakest (it is also of the opposite sign) in cuprammonium rayon (fibre 4). In order to measure ΔN precisely it is convenient to use a screw micrometer with its hair-line in the image plane. For this purpose the scheme of Fig 1 is replaced by one of the two variants shown in Fig 3: two Wollaston prisms W_1 and W_2 are used and the micrometer hair-line is placed in the image plane Q. This idea is due to L.A. Fedin (author's certificate No. 604720/26 dated July 25, 1958). Double refraction $(n_{||} - n_{\perp})$ of a uniform fibre is now calculated from $(n_{\parallel} - n_{\perp}) = \frac{R\lambda}{RMS}$ (7) where R is the area (measured microphotometrically) bounded by the curved interference band in the fibre and the original rectilinear band Card 2/3

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Monsurement of Double Refraction of Fibros 507/51-6-5-28/34
(c.f. Fig 4, part A), S is the separation between undisplaced bands, M is the magnification of the microscope and S is the cross-sectional area of the fibre. There are 4 figures and 2 references, 1 of which is German and 1 English.
SUBMITTED: December 4, 1958
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AUTHOR:	Radin T 4
TITLE:	Fedin, L. A. On the application of a thin Luman of
	On the application of a thin Lummer-Ghercke plate. (O primenenii tonkoy plastinki Lyummera - Gerke):
PERIODICAL:	Astronomicheskii Zhurnal, 1957, Vol.34, No.1, pp. 135-138 (Magn)
ABSTRACT:	that the resolving power of a thin (0.2 mm) Lummer-Ghercke plate as calculated by H. V. Merkvlov (1) is incorrect. The figure given by him is
	whereas the correct value is
	This is, of course, of the order of the resolving power of a prism spectrograph. The same applies to the dispersion of the plate.
	The spectral range of the plate is only 10 - 15 Å and there are considerable constructional difficulties. On balance, the thin Lummer-Ghercke plate is of doubtful value. 1 Figure and 1 Table. 5 references, all of which are Russian.
	Recd. Oct. 15, 1955.
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ALEKSANDROV, V.Ya., prof.; HRODSKTY, V.Ya.; HRONSHTEYH, A.A.; HRUMHERG, Ye.M.; VAKHTIN, Yu.B.; VINNIKOV, Ya.A.; CAYTSKHOXI, V.S.; GOROSHCHENKO, Yu.L.; CULYAYEV, V.A.; ZHINKIN, L.N.; ZAVARZIN, A.A.; ZALXIND, S.Ya.; ZBANSKIY, I.B.; KATSNEL'SON, Z.S.; KONISSARCHIK, Ya.Yu.; LEVIN, S.V.; MARAKHOVA, I.I.; MASHANSKIY, V.F.; MOSEVICH, T.N.; NIKOI'SKIY, N.N.; PESHKOV, M.A.; POLENOV, A.A.; POLYANSKIY, Yu.I.; ROZENTAL', D.L.; RUMYANTSEV, P.P.; TITOVA, L.K.; <u>FEDIN, L.A.;</u> KHENSIN, Ye.M.; CHERNORGRYADSKAYA, N.A.; TROSHIM, A.S., otv. red.; MEYSEL', M,N., red.; MIKHAYLOV, V.P., rod.; NEIFAKH, S.A., red.; PARIBOK, V.P., red.; PULYANSKIY, Yu.I.; red.; RAYKOV, I.B., red.
[Manual on cytology in two volumes] Rukovodstvo po tsitologii v dvukh tomakh. Moskva, Nauka. Vol.1. 1965. 571 p. (MIRA 18:2)
1. Akademiya nauk SSSR. Institut tsitologii.

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 *FEDIN, Leonid Andreysvich; PAPIYANTS, K.A., kand. fiziko-matem. nsuk, retsenzent; KOROLEV, N.V., inzh., retsenzent; IOFFE, G.A., red.; fOKAR', V.M., red. izd-va; ORESHRINA, V.I., tekhn. red.
 [Mammal on microscopes, their accessories, and 'Demes] Mikroskoy; primadlezhnosti k nim i Jupy spravochnátě Imiga. Pod red. G.A.Ioffe. Moskva, Gos. naushno-tekhn. izd-vo Oborongiz, 1961. 251 p. (Microscope)

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IEV, V.A.; DUBOVA, L.S.; PRYANIKOV		
Inhomogeneity of oriented fibers 1307 Jl '64	• Vysokom. soed. 6 no.781302 (MIRA 1882)	
1. Nauchno-issledovatel'skiy ins	titut shinnoy promyslennosti.	•

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 PEDIN, N. Creative 23 Åg 15	work on building	; projects. Proj	tekh, obr. 11; (MLRA	no.5:22- 7:9)	
(91	tor stroitel'noy osnyBuilding transformed and teaching-	ades-~Stndv end	o-savodskogo obuc teaching)(Buildi	bheni ya. ing trades	
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FEDIN, N. Without departmental partitions. Sov. profsoluzy 6 no.1:36-38 Ja '58. (MIRA 11:1) 1.Predsedatel' Gor'kovskogo oblastnogo soveta profsoyusov. (Trade unions)

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1.	FEDIN, N.F.	
2.	¥SSR, (600)	
4.	Technology	
7.	Kzyl-Ordin massif of irrigation of the left shore of the lower reaches of the Syr-Dar'ia riger, Alma-Ata Izd. AN Kazakhskoi SSR, 1952.	
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9• _	Monthly List of Russian Accessions, Library of Congress, March, 1953. Unclassified.	
1.37K4 F 1531515		ji P

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USSR/Geolog	y - Mineralogy		• • • • •
Card	: 1/1 Pub. 1.23 - 11/19		
Authors	: Fedin, N. F., Cand. of Geological-Mineralogical Sciences		
Title	: Determination of water output coefficient of rocks		
Periodical	Vest. AN Kaz. SSR 12, 78 - 83, December 1953		
Abstract	An experimental method for the determination of the coeff extraction from rocks, is described. Three USSR reference Graphs, diagram.	icient of w ss (1934-19	rate: 950).
Institution	. Acad. of Sc. Kaz. SSR, Alma-Ata	· · · · · · · · · · · · · · · · · · ·	··· ··· ··· ··· ··· ··· ··· ··· ··· ··
Presented by	Academician K. I. Satpaev		
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FEDIN, N. F.

"Problems of Studying the Mineralization of Ground Waters of Irrigated Regions," Izv. AN KazakhSSR. Ser. geol., No 16, 76-84, 1953

TATISTIC CONTRACTOR OF THE STREET S

The authors considers the laws governing the transposition and accumulation of salts in the ground waters of irrigated regions and of neighboring territories on the example of the left-bank portion of the Kzyl-Orda land mass being irrigated. On the basis of a processing of the data of more than 250 chemical analyses of water by methods of variational statistics, the author obtains typical analyses for each degree of mineralization of the ground waters and obtains curves showing the dependence of this degree on depth of the water and remoteness from irrigated land.

RZhGeol, No 1, 1955

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USSR/Miscel	lane	aus - Archaeology	، مرتبع		
Card 1/1		Pub. 123 - 10/13			1
Authors	1	Fedin, N. F., and Vladimirov, N. M.			
Title		Archaeological finds in the region between the Volga	and the	Ural	
Periodical	\$	Vest. AN Kaz. SSR, 11/2, 75-81, Feb 1954	• •		
		springtime, there is a slightly higher and drier area of an ancient civilization were found. A study of the to determining their origin and date, led to the conci region was inhabited from the Neolithic era up to the first millenium A. D. Illustrations; map.	ese, wit Lucion t	h a v hut t	iaw he
Institution	t				
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<u></u>	organizatsi	n organization and t ia i tekhnicheskii j 1961. 77 p.	technological progres progress, Moskva, Iz	ss] Profsoiuznaia zd-vo VTs SPS (MIRA 14:11)	
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	din).	(Trade unions)	(Technology)	••••	•••
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SIDORENKO, G.I.; FEDIN, P.G.

Vicarious menstruations in the form f pulmonary hemorrhages. Probl. endok. i gorm. 10 no.6:53-55 N-D '64. (MIRA 18:7)

1. Kafedra fakul'tetskoy terapii Minskogo meditsinakogo instituta i 4-ya klinicheskaya bol'nitsa (glavnyy vrach Ye.M.Sel'dimirova), Minsk.

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EDN,T COUNTRY : Rumania E2 CATLGORY :	
ABS. JOUR. : RZKhim., No. 1959, No. 86180	
 AUTHOR :Banateanu, Ch.; Serbanescu, A.; * INST. : Bucharest Institute of Fetroleum and Gas TITLE : Hapid Determination of Fhosphoric Acid in Kola Apatite and Bone Meal by the Method of Copaux. ORIG. PUB. : Lucrarile Inst. petrol si gaze Bucuresti, 1957, 3, 345-352 ABSTRACT : For determination of P205 in apatite and bone meal, use is made of the method of Copaux (Copaux H., C. R. das Seances de 1 Macad. des sciences, 1921, 173, p. 656), based on formation of ether-phosphonolybdic acid complex in an acidic medium (pH 0.45-0.65). The latter, after centrifugation, is separated from excess ether and water, as a yellow, oily liquid, the volume of which depends on P205, content of the sample. To the sample being analyzed (5 g) are added 10 ml concentrated ENO3 and 50 ml concen- trated H2S04, the mixture is evaporated until S03-fumes are evolved, cooled, 200 ml water are added, heated to a boil, cooled, diluted with water to 500 ml, and filtered. CARD: 1/3 *Vrabiescu, E.; Fidin, T. 	
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COUNTRY CATEGORY	: Rumania :	£-2		-
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ABSTRACT	: Bone meal is f	irst calcined. P20), is de-	1. 1.
termined in	n a snecial test t	the into which are	I fm C handford	
of the above	re-stated filtrate	, 3 ml water, 5 ml	15% HC1 (or	
$20\% H_2 SO_{1_4}$)	, 4 ml ether (free	, 3 ml water, 5 ml from C_2H_5OH , and mixture is thoro	15 ml 142	
and centri	. Na-molypdate, the	e mixture is thoro s. The ether-phosp	bughly stirred	
complex col	lects in the lowe	r, narrower, gradu	momory ourc	
of the tes	st tube. where its	volume can be rea	d off (with	
an error of	up to 0.01 ml).	It was ascertained	that there	
is exact pr	coportionality bet	ween volume of the	liquid and	
content of	P_2O_5 ; therefore t	he latter is deter	mined by the	
	nterpolation, usi	ng for this purpos	e the data	
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	CATEGORY	Rumania :	E-2	
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• • • •	ABS. JCUR.	: RZKhim., No.	1959, No. 86180	
	AUTHOR INST. TITLE	:		
	ORIG. PUB.	:		
	ABSTRACT ($\simeq \epsilon$ g/lit the gravime	: obtained with er). In accuracy, tric; duration of	a standard solution of 1 the method is not infer determination is of 15 m B. Manole.	KH ₂ PO ₄ ior to minutes.
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1 39301 64 T DY/MD	
ACC NR. AT6029143 DJ/WE SOURCE CODE: 111/0007/66/017/002/0084/0094	
AUTHOR: Serbanescu, Ana (Engineer); Fedin, Tarara (Engineer); Popovici, Tatiana (Engineer)	
ORG: none	
TIFLE: Determination of the total sulphur content of some Rumanian crude oils from different geological formations	
SOURCE: Petrol si gaze, v. 17, no. 2, 1966, 0/1-9/1	
TOPIC TAGS: chemical composition, crude petroleum, petrology	•
ABSTRACT: A report on the dotormination of the total sulphur contents of 19 crude oils from well-known geologic formations in six different Rumanian petroliferous structures. The importance of sulphur contents analysis is discussed, and an attempt is made to correlate the sulphur contents with the age of the geological formations. Orig. art. has: 2 figures, 2 formulas and 5 tables. [JPRS: 36,556]	
SUB CODE: 11, 07 / SUBM DATE: none / ORIG REF: 017 / SOV REF: 005 OTH REF: 051	
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	R/007/61/012/001/003/003 A231/A126	
AUTHORS:	Constantinescu, M., Constantinescu, T. and Fedin, Tamara	
TITLE:	Contributions to the study of the catalytic condensing of ethylene with hydrogen sulfide	
PERIODICAL:	Petrol și Gaze, v. 12, no. 1, 1961, 33 - 43	
T.: "Petrol tans can be monoester (R pressure, and with reactan mercaptan. synthesis of will be made	The article presents a solution regarding the production of ethyl- om ethylene and H_2S with the aid of palladious and nickel sulfide ca- a previous work: [Ref. 1: Constantinescu, M., and Constantinescu, si Gaze", no. 7, 1959, 298-304], the authors have shown that mercap- produced by three method groups: i.e. by treating a neutral alkylic - SO4Na) with Na SH; from alkylic halogens (R - Cl) with NaS under d by catalytic methods. The catalysts allow a synthesis starting ts such as ethyl alcohol or ethylene, which directly lead to ethyl- In the above mentioned work (Ref. 1), the authors have studied the mercaptans from lower alcohols. Since in the near future ethylene from cracking gases or chemical reactions of methane, the study has a also on the synthesis of ethylene and hydrogen sulfide: $C_2H_4 + H_2S$	
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Contributions to the study ...

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 \rightleftharpoons C₂H₅SH. According to the technical literature the photosynthesis with ultra violet rays has also been studied before beside the above mentioned three methods. The majority of the publications refer to higher olefines, but not to ethylene. On the basis of the foreign literature, the authors have established that only the photochemical method supplied a higher efficiency (80%) for propylmercaptan at a temperature of 0° C. For ethylmercaptan the temperature is lower and the efficiency is negligible. The photochemical method, however, is very difficult to be applied in engineering, and needs an additionally catalyst. The only practical method is the catalytic method after having found a catalyst which supplies corresponding results at a temperature as low as possible and at usual pressure. The oldest examinations were carried out by H.R. Duffey in 1934, who used different catalysts and obtained a maximum ethylene transformation of 23.3% on a nickel catalyst. The task of this work is to find a highly efficient catalyst for the conversion of ethylene into ethylmercaptan. On the basis of the studied literature, the authors could establish that generally the catalysts, which supply a rather weak efficiency for the desired reaction, are the catalysts used also in hydrogenation and dehydrogenation reactions. For this purpose, this field has also been studied and proved to be the right way. A.W. Schultzeps publication [Ref. 4: A.W. Schultze, J.P. Lyon, and G.H. Schort: "Ind. Eng. Chemis-

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Contribution to the study ...

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try", Ibid: US 2,392.555; 40, 12, 1948] clearly shows that no higher mercaptan efficiency (66%) was obtained even in the presence of a catalyst, except in two recirculating stages with different catalysts for every stage and different pressures, i.e. 33 and 100 atm, when the reactants were partially in liquid phase. The authors' study was conducted to find a solution usable at ordinary pressure, to avoid technical complications, physical condensations, etc. This paper establishes the conditions and main parameters necessary for the transposition to the pilot or industrial scale. There are 5 tables, 1 figure and 9 references: 7 Soviet-bloc and 2 non-Soviet-bloc. The references to the English-language publications read as follows: Ref. 2: W.F. Vaughan, F.F. Rust, J. Evans: Org.Chem. 7,466,1942. Ref. 4: A.W. Schultze, J.P. Lyon, G.H. Schort: Ind. Eng. Chemistry Ibid.: U.S. 2.392.555; 40, 12, 1948.

SUBMITTED: August 29, 1960

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and a second the second second the second second ing the second alc L 18316-65 EWU(1)/EWI(1)/EWP(e)/EWG(k)/EWI(n)/EPF(c)/EFF(n)-2/EPR/EEC(b)-2/EWP(b) Ps-6/Pr-4//Ps-4/Pu-4 IJP(e)/AFWL/SSD WW/AI/WH ACCESSION NR: AP4049532 L 18316-65 Millionshchikov, M. D.; Gverdtsiteli, I. G.; Abramov, AUTHOR: Millionshchikov, M. D.; Gverdtsiteli, I. G.; Abramov, A. S.; Gorlov, L. V.; Gubanov, Yu. D.; Yefremov, A. A.; Zhukov, V. F. Ivanov, V. Ye.; Kovy*rzin, V. K.; Koptelov, Ye. A.; Kosovskiy, V. G.; Kukharkin, N. Ye.; Kucherov, R. Ya.; Laly*kin, S. P.; Markin, V. I.; Nechayev, Yu. A.; Pozdnyakov, B. S.; Ponomarav-Stepnoy, N. N.; Samarin, Ye. N.; Serov, V. Ya.; Usov, V. A.; Fedin, V. G.; Yakovlev, V. V.; Yakutovich, M. V.; Khodakov, V. A.; Kompaniyets, G. V. TITLE: The "Romashka" high-temperature reactor-converter /9 SOURCE: Atomnaya energiya, v. 17, no. 5, 1964, 329-335 TOPIC TAGS: nuclear power reactor, reactor feasibility study, research reactor, thermoelectric converter/Romashka ABSTRACT: The authors briefly describe the construction, parameters, test results, and operating experience of the "Romashka" reactor-Card 1/17

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converter unit, which has been in operation at the Kurchatov Atomic Energy Institute since August 1964. The fuel used is uranium dicarbide enriched to 90% U^{435} . Graphite and beryllium are used as reflectors. Electricity is generated by silicon-germanium semiconductor thermocouples distributed on the outer surface of the reflector and connected in four groups which can be connected in series or in parallel. The temperatures of the active zone and outer surface are 1770 and 1000C, respectively. The power ratings are 0.50-0.80 kW electric and 40 kW thermal, the maximum current (parallel connection) is 88 A, the neutron flux is 10^{13} neut/cm² sec in the center of the active zone and 7 x 10^{12} on its boundary. The reactor has a negative temperature reactivity coefficient. The equipment has high inherent stability and requires no external regulator, and little change was observed in the thermocouple properties after 2500 hours of operation. Tests on the equipment parameters are continuing, and the results are being analyzed for use in future designs. Orig. art. has: 8 figures and 1 formula.

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alphal-, alpha2-, and serum. These increase protein fractions chan electrophoretic moveme albumin and gamma-glob affect the relative in excluded. The mechanic	protein fractions for vibra same. Protein is found to beta-globulin fractions of v s indicate that during vibra ge their electrical properti nt rate. The possibility th ulin molecules with ultrason crease of alpha- and beta-gl sm of ultrasonic biological Orig. art. has: 2 tables.	increase in the ibrated blood and tion the separate es related to thei at the splitting o ic action may also obulins is not	
masnoyarsk State Medical	rskly gosudarstvenny#y medit Institute); Institut fiziki Sibir ics Institute of the Siberian Div	skoga otdelenive	•
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AUTHORS:	Bayrakov, V. I., Fedin, V. P.	
TITLE:	Investigation of 1,200-mm Reversing Thin-Strip Mill With Coilers Located in Heating Furnace	
PERIODICAL:	Stal', 1960, Nr 2, pp 130-133 (USSR)	
ABSTRACT:	The authors investigated the power parameters of a two-high mill with coilers inside the furnaces at Nove-Lipetskiy Metallurgical Plant in Lipetsk (Nove-Lipetskiy metallurgicheskiy zavod). The following strips from St.2 and St.3-steel (regular C steel) were rolled: $8 - 10 - 12 - 16 - 20 \times 1,000$ mm and 11×750 mm in roughing stand; $1.5 - 1.75 - 2.0$ $- 2.5 - 3.0 \times 710$ mm, $1.5 - 1.75 - 2.5 - 3.0 \times 620$ mm, $2.0 - 2.5 - 3.0 \times 710$ mm, $1.5 - 1.75 - 2.5 - 3.0 \times 620$ mm in finishing stand. The following measurements were made in the course of tests: (1) metal pressure on rolls (by wire pickup) and torsional moments during rolling; (2) current voltage, and number of revolutions	
Card 1/6	Folling, (2) callent	
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Investigation Thin-Strip Mi in Heating Fu	of 1,200-mm Reversing 11 With Coilers Located rnace	17610 SOV/133-60-2-10/25	
-	rolls increased from rough	rometer of strip being As a rule, metal pressure of ing to finishing passes. ns) in rolling 8 × 1,000 mm seventh pass. Figure 1 show	
Card 2/6	M As this ratio increased, t grew due to a stronger eff speed of deformation, and A comparison between theor showed good conformity. T culated according to a met	section of strip being follo be mean specific pressure ect of external friction, lower metal temperature. etical and practical data beoretical data were cal- hod advanced by A. I. (8). In rolling 2.0 × 1,000 al pressure (1,260 tons) was	mm

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Investigation of 1,200-mm Reversing Thin-Strip Mill With Coilers Located in Heating Furnace 77610 SOV/133-60-2-10/25

Figure 3 shows the relation between p_m and $h_1:D$ ratio in finishing stand; as the strip gets thinner, this ratio decreases while p increases. Maximum specific pressure (129 kg/mm^{2"}) was achieved in rolling 1.5 mm thick strip. A comparison of experimental and calculated pressure in finishing stand showed, on the whole, good conformity, although in some cases the difference amounted to 30%. The latter is due to errors in measurements of metal temperatures and reduction per pass. Maximum torsional moments on the main motor shaft of the roughing stand exceed the nominal moment by 1.2-2.5 times and by 1.4-2.0 times in the finishing stand, which is within permissable limits. Maximum specific power consumption in roughing stand did not exceed 24 kw/hr/ton in rolling an 8 × 1,000 mm strip from a 120 mm thick slab. Rolling $12 \times 1,000$ mm strip from the same slab requires a power consumption of 10.5-14.0 kw/hr/ton. This

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Investigation Thin-Strip Mil in Heating Fur	of 1,200-mm Reversing 1 With Coilers Located mace	77610 SOV/133-60-2-10/25
ASSOCIATION:	scattering is primarily due ture conditions in rolling heated in rolling 10-8 × 1, 2.5) in roughing stand. In narrower strip the motor has With a root-mean-square cur equalling $I_{r-m-s} = (0.99-1)$ also overheated during the × 1,000 mm strip in 5 passe normally in rolling thicker There are 6 figures; 2 tabl VNIIMETMASh	Motor was over- ,000 mm (from 2.1 to) rolling thicker or as a 10-30% heating margin. Prent in the finishing .14)I nom, the motor is rolling of 2.5 to 2.0 x May while working
Card 6/6	5. · · ·	

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18.5100	78043 SOV/130-60-3-12/23
AUTHORS :	Fedin, V. P., Prikhod'ko, I. F., Gritsuk, N. F.
TITLE:	Concerning Trends in the Development of Guides and Repeaters
PERIODICAL:	Metallurg, 1960, Nr 3, pp 17-22 (USSR)
ABSTRACT :	Before 1950 rolling mills were equipped with slider- types only. At present roller-type guides are added to the above. Existing guides are classified according to: (1) position in stand; (2) design of grade units; (3) type of friction between strip and guide elements. Roll pass design has a considerable effect on the design of entry guide units. Delivery guides prevent bending of strip ends and secure correct entry into repeater. In rolling shapes and rails, slider-type guides are used. This is justified by the simplicity of
	such guides. In Soviet as well as foreign practice, roller guides with one pair of rollers (such as entry boxes with rollers set on flat springs) are popular.

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Concerning Trends in the Development of Guides and Repeaters

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Similar designs are used at finishing stands of section mills of Magnitogorsk Metallurgical Combine (MMK), Chelyabinsk, Makeyevo, Stalino, Krivoy Rog, and "Serp 1 Molot" Metallurgical Plants (Chelyabinskiy, Makeyevskiy, Stalinskiy, Krivorozhakiy 1 "Serp 1 molot" metallurgicheskiye zavody). Advantages: easy set-up, dependability, low forces in pushing strip through rollers. For simple shapes (rounds and squares) funnel-type guides are recommended, as designed by N. F. Gritsuk (see Fig. 2).

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Concerning Trends in the Development of Guides and Repeaters 78043 sov/130-60-3-12/23

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S. V. Merekin suggested the use of twist rolls which were eventually modernized at Makeyevo Metallurgical Plant upon the proposal of V. F. Laganskiy and K. V. Kuchevskiy. Roller straighteners set behind the finishing stands prevent the strip from twisting before delivery to cooler. The life of roller-type guides and repeaters is prolonged by increasing the durability of main parts, 1.e., rollers. this connection rollers from gray and alloy cast iron with chilled surface as well as from low and medium carbon steel with surface hardfaced by TsI-IM, Ts-1, and Ts-2 hard-alloy electrodes are used. These rollers are reconditioned by repeated hard-facing directly in the shop. Roller-type guides are particularly recommended for intermediate and finishing stands of rolling mills for rolling nonferrous metals and alloys which are very sensitive toward scratching. Roller-type guides used for small-shape and rod mills are of larger size than slider-type guides.

Card 4/5

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Concerning Tre of Guides and	nds in the Development Repeat e rs	78043 sov/130-60-3	-12/23
· · ·	Therefore, slider-type e Their wear resistance is times by chromizing or k this respect, the author experience of such advar States and Sweden. The	a increased by 7.5 to 13 poronating work surfaces rs recommend a study of nced countries as the Un	· 5 . In the
ASSOCIATION:	All-Union Scientific Res Machinery and Magnitoron (VNIIMETMASh)	search Institute of Meta rsk Metallurgical Combir	llurgical e
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TRADERAGE AND DESCRIPTION AND ADDRESS AND ADDRESS AND ADDRESS ADDR ADDRESS ADD i e sasar PRIKHOD'KO, I.F.; JEDIN, V.P.; IVANOV, Yu.G. Wear-resistant materials for the manufacture of roller bearings for the equipment of rolling mill fittings. Metallurg 5 (MIRA 13:7) no.8:27-31 Ag '60. 1. Vsesoyuznyy nauchno-issledovatel'skiy institut metalloobrabotki 1 mashinostroyeniya. (Rolling mills) (Roller bearings)

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EFERING STREET

CIA-RDP86-00513R000412610004-3

s/133/61/000/003/009/014 A051/A033 Shevchenko, A. A., Doctor of Technical Sciences; (hilyayev, G. I. Candidate of Technical Sciences; Anisiforov, V. PL, Candidate AUTHORS: of Technical Sciences; Arutyunov, I. G., Gandidate of Technical Sciences; Yurgelenas, V. A., Engineer, and Fedin, V. P., Engin neer The performance of two-high reducing mills with individual TITLE: drive PERIODICAL: Stal', no. 3, 1961, 251 - 256 When planning three-high reducing mills, the VNEIWEWMASh and UkrNITI made a thorough study of the two-high reduction mills with indivi-TEXT : dual drive, not supplied with rotation-stabilizers. In order to match the operation of these two types of mills the single deformation values were taken a little higher (mi = 3.5 + 4.2 %) than usual in Soviet plants. The tube dimensions varied between 96 x 3.25 - 3.5; 96 x 4 - 4.5 and 96 x 5 mm. The motor speeds for these types of tubes are given in table 2. Before reduction the tubes were heated to 1040 - 1080°C, the number of motor revolutions was recorded on the switchboard by means of an MM type tachovolt-Card 1/6

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The performance of two-high reducing

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meter with a relatively low accuracy (± 10 rpm). The data compiled for the average change indwall-thickness at the end and central parts of the tubes rolled in 21 and 1? stand mills are given in tables 3 and 4. They show that when the tension is increased the wall-thickness in the central part of the tube decreases, while the increase in wall-thickness at the tube ends will reach a maximum only at tensions of 0 - 0.5 %. In all other cases any increase in tension reduces the wall-thickness at the tube ends. Table 4 shows that the deviation in wall-thickness in lateral direction. suddenly increases at the ends, irrespective of the tension, while it decreases in the central parts, when the tension is raised. With templates of 96 x 4 and 96 x 5 mm tubes it was established that the transverse section remains fairly stable even when no tension at all was applied, whereas the 96 x 3.25 mm tubes displayed defects (beads and fractures) when reduced without tension, by 5.1; and 7 %. When applying a tension of 3.5%, no defects were observed in the wills of the 96 x 3.5 fm tubes. The values of kinematic tension of 3.5 % in the 21-stand and of 4% in the 17-stand mills does not represent the limit. Experiments showed that it was possible to increase the kinematic tension and to produce tubes with even thinner walls in the central parts. If the tubes are rolled at the right temperature and

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The performance of two-high reducing

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the roll speed adjusted carefully, the coefficient of tension can be as high as 0.7 - 0.8 (Ref. 7: G.I. Gulyayev; V. A. Yurgelenas: Determination of Some Basic Technological Parameters of Tube Reduction with Tension. Transactions of the UkrNTO ChM, 1958, vol. 13). Tests carried out to establish the maximum values of torgues and those for stabilized operation show that the torque values characterize the non-uniform load of the stands which in the first place depends on the adjustment of the roll-speed. When the tension is increased from 3.5 to 1,%, the torques of the middlestand motors decrease uniformly, once the rolling process has been stabilized. The tests also proved that in the experimental reductions the motors were not always loaded to full capacity, while overloading also occurred due to the inaccurate adjustment of the revolution of rolls, (n). When calculating the reduction of the mills, depending on the tension applied, the wall-thickness of the tube and partial deformation obtained in one stand have to be taken into account. The oscillogram of current intensity shows that, at the rate at which the tube proceeds to the next stand, the current intensity curve declines, under the effect of the frontal tension of the following stand. This step-like character of the de-

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The performance of two-high reducing

crease in current intensity indicates the moment, when the tube enters the next stand. When the tension at the rear (viewed from the preceding stand) is taken as constant, the maximum stretching force will be proportionate to the difference of the ordinates of the maximum and stabilized values of the current. The decrease in the general moment from the maximum to stabilized state will be proportionate to the moment acting on the stand investigated from the next following stand:

 $\Delta M_{gen} = TD_r \qquad (1)$

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$$T = k \Delta I \qquad (2)$$

$$\Delta I = I_{max} - I_{stab} \qquad (3)$$

$$k = \frac{v}{\overline{I \cdot 03 n_{1}} \cdot r} \cdot Dr \qquad (4)$$

where M_{gen} = general moment, k = coefficient of proportionality, v = vol-

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The performance of two-high reducing ...

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tage, v, D_r = rolling diameter of the roll, mu, ni.r = velocity of idle run of rolls, rpm, T = stretching force, kg, Imax and Istab = currnet in-tensities for maximum and stabilized moments, a. ABSTRACTR'S NOTE: subscripts gen. (general), r(rolling), i.r. (idle run), stab. (stabilized) are translations of the original co (obshchyy), M (katayushchyy), XX (kholostoy khod) and (ustanovlenyy). Based on these formulas it is possible to calculate the atual stretching forces and longitudinal stresses in the tube on the stand, when being reduced at different tnesions and various initial wall-thicknesses. The distribution of forces and stresses of tension has no regular character; e.g., the maximum value of tension stress is 3.6 kg/sq mm (practically the yield point of the metal processed) while at a tension of 3.5% it amounts to 2.6 kg/sq mm and at 4 % to 1.8 kg/sq mm. The maximum stretching force attains 2100 kg. The difference in stretching forces for the various stands of the mill are, to a certain extend, caused by the inaccurate adjustment of the rolls. The investigation of roil-speed shows that there is a deviation between the actual and the rated speed of the rolls, both in idle run and in operation. In some cases the speed increases for the subsequent rolls, sometimes, however, a

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decelaration is observed. The velocity drops on successive rolls affects the reduction process in several aspects: energy consumption, torques, forces, tension, etc. Therefore the correct adjustment of the number of roll revolution in stands with individual drive is of great importance, because variations in the roll speed result in an irregular change of energetic parameters, which unfavourably affects the tube quality. The tube walls will not be of uniform thickness and cracks may occur even at relatively low tensions. There are 5 figures, h tables and 8 references: 7 Soviet, 1 non-Soviet.

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FOLUKHIN, P.I., prof., doktor tekhn.nauk; EAYHAKUV, V.I., kand.tekhn.nauk; HEDIN, V.P., inzh.
"Changes in the mechanical properties of metals and alloys under the effect of cold rolling" by V.A. Tret'liakov, K.M. Radohenko. Reviewed by P.I. Eolukhin, V.I. Bainokov, V.P. Fedin. Stal* 21 no.2155 F*61. (MIRA 14:3)
(Rolling (Metalwork))(Tret'liakov, V.A.)(Eadchenko, K.M.)

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CIA-RDP86-00513R000412610004-3

s/133/61/000/012/002/006 A054/A127 Fedin, V.P. Rolling mills with reelers in the furnace (as a matter for discus-AUTHOR: TITLE: sion) Stal', no. 12, 1961, 1,096 - 1,100 Opinions are divided about the efficiency of reversing rolling PERIODICAL: mills with reelers in the furnace. Studies were carried out during a period of 3 years on the "1200" reversing rolling mill (with reelers in the furnace) of the Novolipetskiy metallurgioheskiy zavod (Novolipetsk Metallurgical Plent), which showed that this arrangement has a number of structural and technological drawbacks. Among other things, it was not possible to maintain the temperature of the strip coming from the roughing stand and the heat distribution was not uniform over the strip cross section. The heat distribution could be improved by redesigning the pulling rolls in such a way that the strip end, remaining outside the furnace, could not cool down before the pass. When the design of the heating furnace at the finishing stand was improved, the required temperature in the slab could be ensured. The rolling process on the finishing stand Card 1/2 生活的時代的 Sec. Sec. - - i. 2916 1.1

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SHEVCHENKO, A.A., doktor tekhn.nauk; GULYAYEY, G.I., kand.tekhn.nauk; ANISIFOROV, V.P., kand.tekhn.nauk; ARUTYUNOV, I.G., kand.tekhn.nauk; YURDELENAS, V.A., inzh.; FEDIN, V.P., inzh.
Peformance of a two-high reduction mill with individual drive. Stal' 21 no.3:251-256 Mr '61. (MIRA 14:6)
1. Ukrainskiy nauchno-issledovatel'skiy trubnyy institut i Vsesoyuznyy nauchno-issledovatel'skiy institut metalloobrabotki i mashinostroyeniya. (Rolling mills)

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FEDIN, V.F. Mills with coilers in the furnace. Stal' 21 no.12:1096-(MIRA 14:12) 1100 D '61. 1. Vses yuznyy nauchno-issledovatel'skiy institut metallurgicheskogo (Relling mills---Equipment and supplies) mashinos broyeni.". THE REPORT OF THE PROPERTY OF

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S/659/62/008/000/021/028 1048/1348

The problem of high-temperature diffusion ...

alloy quenched from 450° in water. This indicates that the increase in ρ is not caused by excessiv vacencies in the alloy, and that the P from the P-containing alloys combines with the vacancies reducing their mobility. Both ρ and H_v in the alloys quenched from 700°C are lower than in non-quenched specimens, indicating the existence of a highly ordered structure in the alloys quenched from hightemperatures. During annealing, ρ decreases with time at the annealing temperature, the decrease in the pure alloys being much larger than in the P-containing ones, i.e., the stability of the quenched state is much higher in P-containing alloys. The energy of activation of the diffusion processes increases with the P content of the alloy and reaches 35±3.7 kcal./mole in an alloy containing 0.06% P, which is almost twice the value for the pure Cu-Al alloy; due to the decreased mobility of vacancies in the P-containing alloys. Diagrams show the effect of temperature on the electric resistivity and internal friction in the alloys. In the friction

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5/659/62/008/000/021/028 1048/1248

The problem of high-temperature diffusion ...

diagram for pure alloy maxima at 260°C and 520°C are associated with the motion of the constituent atoms, and with stress relaxation on the grain boundaries respectively. The internal friction in pure alloy specimens quenched from 700-900°C and in the alloys containing P is much lower than in the annealed pure alloy; this proves that the specimens quenched from high temperatures possess an ordered structure, and that the P from the P-containing alloys reduces the mobility of defects within the alloy. There are 3 figures.

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CIA-RDP86-00513R000412610004-3"

FEDIN, V.P.; IVANOV, Yu.G. Guids unit or continuous billet mills. Metallurg 8 no.5:23-27 My '63. (MIRA 16:7) 1. Vessoyusnyy nauchno-issledovatel'skiy i proyektno-konstruktorskiy institut metallurgicheskogo meshinostroyaniya. (Rolling mills-Equipment and supplies)

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9.6150	S/024/62/000/001/012/013 E140/E435	
AUTHOR:	Fedin, V.T. (Noscow)	
TITLE :	On the problem of determining the spectral density at the output of a synchronous detector for a modulation type radiometer	
PERIODICAL:	Akademiya nauk SSSR. Izvestiya. Otdeleniye tekhnicheskikh nauk. Energetika i avtomatika. no.l, 1962, 181–185	
modulation	author claims that the previous literature on the function at the output of a synchronous detector of a ype thermal noise receiver is in error. This error the assumption that the correlation function component	han
τ.	$-x(l)x(l+\tau)\frac{\cos v(2l+\tau)}{2}=0$ (1.2)	6
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	Souther that the second s	1997 655197859159
	S/024/62/000/003/011/011 E140/E463	
AUTHOR:	Fedin, V.T. (Moscow)	
TITLE:	Certain methods of controlling the output characteristics of low-frequency and ultra-low- frequency noise generators	
PERIODICAL:	Akademiya nauk SSSR. Izvestiya. Otdeleniye tekhnicheskikh nauk. Energetika i avtomatika, no.3, 1962, 208-215	
output (fre generators square-low simpler but	author considers the possibilities for modifying the quency) characteristics of low-frequency noise utilizing normal noise generators and synchronous or frequency changers. He shows that the latter are that the former present richer possibilities of characteristics. There are 8 figures.	
SUBMITTED:	January 3, 1961	
Card 1/1		

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STATISTICS SHOW FORES

NIKOLAYEV, Andrey Grigor'yevich; PERTSOV. Sergey Viktorovich; PERESLEGIN, S.V., retsenzent; FEDIN, V.T., retsenzent; KRASOVSKIY, A.A., prof., doktor tekhn.nauk, nauchn. red. MASHAROVA, V.G., red.

> [Radar detection of thermal radiation; passive radar] Radioteplolokatsiia; passivnaia radiolokatsiia. Moskva, Sovetskoe radio, 1964. 334 p. (MIRA 17:12)

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1.	FEDINA, A. YE.	
	USSR (600)	
	Geology and Geography	
7.	Books on Crimea. Reviewed by A. Ye. Fedina,	Sov. Kniga, No. 4, 1952.
9.	Report U-3081, 16 Jan 1953, Unclassifie	a. A state of the second s

KAPTIN M



Dissertation: "Experience Gained in the Physicogeographical Regionalisation of the Caucasus (In Connection With the Creation of Exhibits for the Geography Museum in Moscow State University)." Cand Geog Sci, Moscow State U, Moscow, 1953. (Referativnyy Zhurnal--Geologiya/Geografiya, Moscow, Aug 5h)

SO: SUM 393, 28 Feb 1955

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EDINA, H.,	14-5/-(-14592
Translation i	<pre>rom: Referativnyy zhurnal, Geografiya, 1957, Nr. 7, p 19 (USSR)</pre>
AUTHORS :	Gvozdetskiy, N.A., Fedina, A.Ye.
TITLE:	Physical Geographical Districts in the Caucasus (Fizikc- geograficheskoye rayonirovaniye Kavkaza)
PERIODICAL:	Vopr. geografii, 1956, sb 39, pp 130-150
ABSTRACT :	This new division was accomplished by analyzing the interaction of all physical and geographical factors. The historical, or more accurately, the genetic approaches were used whenever possible. Close at tention was paid to the relief. The authors have tried to find the processes or factors which caused the differentiation among the regions. Changes caused by human activities were studied as far as possible. The authors regard the zones differentiated by the ele- vation on mountain slopes merely as one provincial
Card 1/7	

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Physical Geographical Districts (Cont.)

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or local peculiarity. A map of the physical districts of the Caucasus is included. It shows the region to be divided into 46 districts. 1. The western and central Ciscaucasian district. IA. The western Ciscaucasian subdistrict: 1) the Kuban'-Azov plain; 2) the Kuban' Ciscaucasian subdistrict: 5) the Kuban' Peninsula. 1B. The sloping plain; 3) the Kuban'delta; 4) the Taman' Peninsula. 1B. The central Ciscaucasian subdistrict: 5) the Stavropol' highland; 6) The northeastern Stavropol' region; 7) the Mineral'nyye Vody laccolith region; 8) the Terek-Sunzha highland; 9) the Kabardinskaya, Osetinskaya and Groznenskaya sloping plains. II. The Caspian lowland district. IIA. The Terek-Kuma lowland subdistrict: 10) the Kuma plain; 11) the Terek-Kuma sand mass, which includes the adjacent section of the Terek River valley; 12) the deltas of the Terek and Sulak Rivers. III. The Greater Caucasus district. IIIA. The subdistrict on the northern slope of the Great Caucasus: 13) the Black Sea Caucasus; 14) the Kuban'-Ardon cuesta region; 15) the Ardon-Sulak region; 16) the outer Dagestan region and the intermountain district of northern Azerbaijan; 17) the limestone karst region in southeastern Dagestan;

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Physical Geographical Districts (cont.)

18) the interior limestone part of Dagestan; 19) the Caspian foothill littoral region; 20) the Samur-Akzybir region; 21) the Caspian Caucasus. IIIB. The high mountain Great Caucasus subdistrict: 22) the high mountain region in western and central Caucasus; 23) the high mountain region in the eastern Caucasus. IIIC. The subdistrict on the eastern slope of the Great Caucasus: 24) the northern Black Sea region; 25) the northern Pontic foothills (Sochi) 26) the southern Pontic foothills (Kolkhida); the limestone karst region; 28) the intermountain region of Georgia and Azerbaijan. IV. The Kolkhida lowland district: 29) The eastern Kolkhida region; 30) the maritime Kolkhida.region. V. The Kura valley district: VA. The Apsheron-Kura subdistrict: 31) the Apsheron Kobystan region; 32) the Kura-Araks lowland. VB. The Kura Alazani subdistrict: 33) the Kura region; 34) the Shirakskaya (Steppe)-Adzhinour region; 35) the Alazani-Agrichay region; 36) the Goric the region. VI. The trans-Caucasian highand district. VIA. The Little Caucasus subdistrict: 37) the Adzharo-Trialetskiy region; 38) the Somkhetskiy-Murov Dag region; 39) the Karabakhskiy region. VIB. The Armenian highland subdistrict; 40) the Dzhavakhetskiy region;

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41) the Aragat 43) the centra The Talysh-Len Talysh region;	aphical Districts (C s-Karabakhskiy regio l Araks basin. VII. koran' subdistrict: 46) the region whic Diabarskaya Kotlovir es is included.	ont.) n; 42) the Darala The Girkanskaya 44) the Lenkoran'	lowland; 45)	the
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