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BSKIN, G.I. (Moskva); FRIDLYANDER, I.N. (Moskva); RUBLEVA, M.K. (Moskva)
Formation of structural components in aluminum alloys under the affect of
ultrasonic waves. Izv. AN SSSR. Otd. tekh. nauk. Met. 1 gor. delo no.1:
109-112 Ja-F '63.
(Aluminum alloys-Metallography)
(Ultrasonic waves-Industrial applications)

APPROVED FOR RELEASE: 06/13/2000

CIA-RDP86-00513R000513720001-2

SHAMRAY, V.F.; FRIDLYANDER, I.N.; SOKOLOV, A.N.

Studing transformations during the crystallization of alloys in the system aluminum - copper - lithium. Issl. splav. tsvet. met. no.4:100-107 '63. (MIRA 16:8)

> (Aluminum-copper-lithium alloys---Metallography) (Phase rule and equilibrium)

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ACCESSION NR: AP4005828	8/0129/63/000/012/0026/0028
AUIHOR: Fridlyander, I. N.; Zaytaeva	, N. I.; Artemova, M. S.
TITLE: Effect of multistage aging on nesium system	a properties of alloys of aluminum-zinc-mag-
SOURCE: Metalloved. 1. termich. obra	ib. metallov, no. 12, 1963, 26-28
TOPIC TAGS: manganese alloy, zinc al property, stress corrosion, corrosion multistage aging, alloy aging, alumin	lloy, magnesium alloy, V92 alloy, mechanical n resistance, artificial aging, natural aging, num base alloy
is susceptible to stress corrosion. deficiency by two-stage aging while a Specimens containing 2.5% Zn, 4.4% Mg regimes and then to a 7% solution of for the formation of macroscopic crack (120 hours) was achieved with aging (by has generally high corrosion resistance, it Experiments were conducted to rectify this retaining adequate mechanical properties. 3, and 0.7% Mn were subjected to various aging NaCl. Specimen "life" was the time required cks. The highest stress corrosion resistance at 60 C for 24 hours followed by additional r at 200 C for 1, 3, and 10 hours. By way of
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comparison, tests were	also run on an alloy containing 4 ntents of Zn with respect to Mg.	High mechanical proper-	
ies and satisfactory	stress corrosion resistance were a	chieved by aging at 100 C	
for 5 hours plus 150 C	for 12-10 hours. Data are proven	for corrosion resistance	
under various aging rel	rimes. Orig. art. has: 4 tables.		
ASSOCIATION: none			
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CIA-RDP86-00513R000513720001-2

ACCESSION NR: AP4005830

s/0129/63/000/012/0035/0037

AUTHOR: Sidorin, I. I.; Fridlyander, I. N.; Silayeva, V. I.; Kuznetsova, Ye. A.

TITLE: Investigation of the structure and properties of SAP-1 material

SOURCE: Metalloved. i termich. obrab. metallov, no. 12, 1963, 35-37

TOPIC TAGS: sintered aluminum powder, SAP sheet, SAP sheet structure, SAP sheet strength, SAP sheet ductility, SAP cold colling, SAP hot colling, SAP sintering SAP annealing, SAP structure, SAP property, SAP alloy

ABSTRACT: The authors have investigated the effect of technological conditions, especially the temperature of preliminary sintering and annealing, on the structure and mechanical properties of sintered aluminum powder products at higher temperatures (especially above 500C). The tested material was first sintered at temperatures of 500 and 650C for 2 hours, hot pressed at 500C under a specific pressure of 55 kg/mm², pressed at 500-550C with 89.5% deformation, hot rolled at 500C with 70% deformation, and cold rolled with a deformation of 50%. Preliminary sintering at higher temperatures (650C) decreased the strength and hardness of the semifinished product and increased the percentage of elongation. This effect may be due to recrystallization in microvolumes. The texture formed as a result of pressing and hot and cold rolling of this material was very stable up Card 1/2

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ACCESSION NR: AP4005830

to 650C. The mechanical properties of pressed and rolled SAP-1 material deteriorated after annealing, and microcracks appeared. The temperature of annealing leading to microcracks depends on the temperature of preliminary sintering of the briquets. It was concluded that an increase in the sintering temperature up to 650C markedly increases the degasification coefficient and consequently reduces the tendency to microcrack formation during annealing while widening the temperature interval of the stability of the mechanical properties of the annealed and rolled sheet of SAP-1. Orig. art. has: 1 figure and 1 table.

ASSOCIATION: none

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L 8913-65 AFETR/BED/AFTC	WT(m)/EFR/T/E./(k)/EXP(q)/EXP(1 (p) KJW/JD	b) $Pf-l_1/Pe-l_1 = EAEM(t)/ASIN(m)-3/$	
ACCESSION NR:	AT4012729	S/2981/63/000/002/0169/0174	
AUTHOR: Frid	lyander, I. N.; Agarkov, G. D.;	Klyagina, N. S.; Krivenko, 8. A.	B
TITLE: Prepar	ration of standard <u>aluminum</u> allo	ys by the powder method	
	alnivevv×ve splavv*. Shoenik et	atey, no. 2. Spechenny*ye splavys	
TOPIC TAGS: p property	owdered aluminům, <u>powder metall</u>	urcy, aluminum alloy, mechanical	
mixture, and s	tructural changes on their mach	red by a newly developed powder men atlon, thermal treatment, Al_2O_3 ad anical properties. The 3-stage pow	
ma ² for 1.0-1. 1.5-2.0 hrs.	5 min., hot briquet precompress The effect of thermal freatment	ng at a maximum pressure of 100 kg. Ing and rod compacting at 4000 for	
tent is low.	Homogenization ¹ reduced, to a cer s prepared by atomization water	t of both alloys when the Al_2O_3 contain degree, the strength of V96.	the second s
I FEIEE OF MAAIN	Ч СИС НИЦІЧІЦЦАІ СОБОЛЛАТСТС. ГН	the smaller the powder particles, the smaller the powder particles, thile V96 was not affected. Techno	
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Section 2

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equal to SAR; they resemb content is low but have a	nd D16 with aluminum contents i le in behavior ordinary cast al more homogeneous structure. T s found to be highly dispersed gures, and 5 graphs.	loys when the eluninum he microstructure of both	
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<u>U 2387?-65</u> EWT(m)/EPF(n)-2/EPR/EWP(t)/EWP(b) Ps-4/Pu-4 IJP(c) JD/ JG/MLK \mathcal{O}	
JG/MLK JG/NLK S/0000/64/000/000/0172/0175	
AUTHOR: <u>Nagorskaya, N. D.; Simanov, Yu. P.</u> (Deceased); <u>Nikolayava,</u> <u>V. V.; Novoselova, A. V.; Fridlyander, I. N.; Yatsenko, K. P.;</u> Savostin, A. P.	
TITLE: Investigation of the interaction of beryllium with rhenium $\frac{1}{27}$	
SOURCE: <u>Vsesoyuznoye soveshchaniye po probleme reniya</u> , <u>2d</u> , Moscow, 1962. Reniy (Rhenium); trudy soveshchaniya. Moscow, Izd-vo Naika, 1964, 172-175	
TOPIC TAGS: beryllium, rhenium, beryllium rhenium system, beryllium alloy, rhenium containing alloy, microstructure, hardness	
ABSTRACT: The microstructure and hardaese of cast, annealed, and quenched Be-Re alloys containing up to 45 wt (3.79 at)% Re have been investigated, (The alloys were induction maited from 99.52-pure Be	
and 99,952 pure Re. Microstructure exemination showed that alloys at the investigated portion of the Be-Re system crystallize according to eutectic type diagrams. In hyposytectic alloys the grains of Be-	
base solid solution are contained in a binary autectic. In the eu-	
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tectic which contains 9 8 wet (0 (t -+ W)		
tectic which contains 8.8 wt% (0.45 at%) Re, the γ -Be20Re compound forms a finely branched network.	phase based on	
tions of the Y-phase in hypereutectoid allows are a	cattered within	
the solid solution of Be. In the investigated allo	vs Be is precent	
in the form of the a-modification and in an f.c.c.	y-phase on a Be; oRe	
base which has a theoretical Re content of 50.78 bility of Re in Be is less than 1.0 wtZ at the cute	wt%. The sclu-	
and less than 0.7 wt% at 600C. The cast allove con	taining 2-12% to	
nave a considerably higher hardness than that accor	ding to the addi-	
civity rule, which is ascribed to the presence of m	echanical erracead	
in the finely branched eutectic crystallized under cooling. As the amount of the autectic decreases a	conditions of rapid	
the Y-phase increases, the hardness of the allove d	rone and in allows	
containing more than 12% Re it is equal to the mean	arithmatic value	
of the hardnesses of individual phases. Orig. art. and 1 table.		
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ASSOCIATION: none	•	
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ACCESSION NR: AT4037643	S/2981/64/000/003/0005/0026	
UTHOR: Edel'man, N. M.; Fridlyander, I.	N.; Starostina, Z. I.	
TITLE: A study of the properties of alloys in	the Al-Mg-Si system	
SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1	1964. Deformiruyemy*ye splavy* (Malleable	
alloy AD33, alloy AD35, alloy mechanical provision resistance, alloy weldability, alloy he taining alloy, magnesium containing alloy	agnesium silicon alloy, alloy AV, alloy AD31, operty, alloy chemical composition, alloy cor eat treatment, alloy stampability, silicon con-	1
ABSTRACT: Tests were carried out on shee to determine the effects of alloy composition properties, the effects of composition on cor of Mg varied by 0.2% from 0 to 2.0%, Si by (Mg content. The samples were annealed (1)	et samples (1.5 mm thick) of 87 alloy composi- and heat treatment conditions on mechanical rrosion resistance, and the weldability. Contro 0.2 or 0.4% from 0.0 or 0.2% to 2.0% for eac hr. at 370C, cooled in a furnace to 150C, ther nd tested either prior to aging, after 15 days ging at 160C. Machine welding operations wer ble electrode and welding rods of the basic	ent h of
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ACCESSION NR: AT4037643

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material. Analysis of concentration triangles plotted for the system indicates that peak strength for all hardening procedures used applies to alloys in the triphasic area $G + Mg_2Si$ Si at Mg + Si = 2.5 to 4% total. The alloys exhibited good plasticity after annealing, as well as after hardening with artificial aging or prior to aging. Stamping, cupping, flanging and extrusion are possible at high levels of deformation. Corrosion resistance to immersion in 3% NaCl with 0. 1% H₂O₂ added decreased with an increase in Si and the Mg₂Si phase, was relatively unaffected by an increase in Mg, and deteriorated sharply in the direction from excess Mg to excess Si where Mg₂Si was constant. Weldability was adequate for argon are roll or spot welding, tensile strength of seams was 60-70% of initial material levels and was restored to 90-95% by subsequent heat treatment. Tendency to crystallization cracking was high when using welding rods of original material (cracking coefficient 60-80%), but use of SVAK5 rods (5% Si, balance Al) reduced that value to 0-20%. Use of such rods did not affect strength, plasticity or corrosion resistance. Alloys in this system are recommended for applications requiring high corrosion resistance in riveted or cemented constructions, nalium), good weldability and a decorative appearance in riveted or cemented constructions,

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lloys (AD31, AD33 and nitted for industrial use	ures where lowered stren AD35, composition and m as a result of this study. Arbuzov and R. N. Naum phs.	echanical properties g "Yo. A. Gubarova,	given) were sub- Ye, I. Burova,	. T
ASSOCIATION: none	÷ é			
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S/2981/64/000/003/0051/0065		
ACCESSION NR: AT4037647 S/2981/64/000/000/000/000/ VIL P.		
Toutcava N. L.; Burova, Ye. L.; Arbuzov, Id		
AUTHOR: Fridlyander, L. N.; Zaytsova, In any TITLE: Principles of variation in the weldability and mechanical and corrosion properties of		
the second s		
TITLE: Principles of Variation in the		
Al-Zn-Mg alloys SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1964. Deformiruyemy*ye splavy* (Malleable	E.	
Alexaniniverve splavy*, no. 3, 1964. Deformiruyoniy yo open y		
SOURCE: Alymmingory John C		
alloys), 51-65 TOPIC TAGS: aluminum alloy, aluminum zinc magnesium alloy, alloy heat treatment, alloy topic trades aluminum alloy corrosion resistance, alloy weldability, maganese admixture,	- <u>{</u> } }	
TOPIC TAGS: aluminum alloy, aluminum zinc magnesium alloy, alloy heat troublet, mechanical property, alloy corrosion resistance, alloy weldability, maganese admixture,	i.	
machanical property, alloy corrosion resistance, alloy wordship,	- la	
zinc, magnesium	1	
zinc, magnesium ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mn was tested for 2 hrs. at 400C and 1.5% Mn was tested for 2 hrs. at 400C and 1.5% Mn was tested for 2 hrs. at 400C and 1.5% Mn was tested for 2 hrs. at 400C and 1.5% Mn was tested for 2 hrs. at 400C and 1.5% Mn was tested for 2 hrs. at 400C and 1.5% Mn was test		
ABSTRACT: A group of alloys with 1.5-6% Zn, 1.5-8% Mg and 0.6-1.0% Mill was toologing, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, and mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition, heat mechanical properties, corrosion resistance and weldability in relation to composition.	į.,	
mechanical properties, corrosion resistance interview were annealed for 2 hrs. at 4000 and	Ē	
ABSTRACT: A group of alloys with 1.0 of and weldability in relation to composition, many mechanical properties, corrosion resistance and weldability in relation to composition, and treatment and aging procedure. Sheets (2 mm thick) were annealed for 2 hrs. at 400C and treatment and aging procedure. Sheets (2 mm thick) were annealed for 2 hrs. at 400C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, then in free air, or water quenched from 440-460C and furnace cooled at 30 /hr. to 200C, the furnace cooled at 30 /hr.		
furnace cooled at 00 7 mills an artificially for 96 hrs. at 1000. Collocation of NoCl solution		
treatment and aging procedure. Biccus (in free air, or water quenched from 440-4000 dimensional formation of the second	Ĕ.	
positions with 2.5-6.0% 2n and 1. corrosion in an industrial atmosphere. The tendency	E.	
positions with 2. 3-0. 0.0 En the corrosion in an industrial atmosphere. The thus trated plus 0. 1% H_2O_2 or exposed to corrosion in an industrial atmosphere. The thus trated joints to cracking was studied in relation to composition. The results are illustrated	t i	
joints to cracking was obtained		
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ACCESSION NR: AT4037647]
graphically and led the authors (2.9-3.6% Zn, 3.9-4.6% Mg, Z development. "M. S. Artemov work." Orig. art. has 9 graph	n : Mg \sim 0.8 : 1) and 0.6-1 a and L. I. Agapova took p	.0% Mn for further	r testing and	
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ACCESSION NR: AT4037648	S/2981/64/000/003/0066/C075 , N. I.; Burova, Ye. I.; Arbuzov, Yu. P.
AUTHOR: Fridlyander, I. N.; Zaytseva TITLE: Effect of various additives o	n properties of alloys of the system
Al-Zn-Mg SOURCE: Alyuminiyevy*ye splavy*, no. (Malleable alloys), 66-75	3, 1964. Deformiruyemy*ye splavy*
alloy mechanical property, beryllium additive, zirconium additiv manganese additive, iron additive, s	ve, cerium additive, taleida ditive, copper ilicon additive, titanium additive, copper
ABSTRACT: Admixtures of $0.002 - 0.3$ 0.2 - 0.8% Ca were analyzed for their of the state of the	% Be, 0.05 - 0.3% Zr, 0.1 - 2.0% Ce and r effect on the properties of aluminum 0.8% Mn. Other experiments involved ad- % Fe, 0.1 - 0.3% Si, up to 0.2% Ti and 0.05 - ding 2.7% Zn, 3.7% Mg and 0.002% Be (the

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ACCESSION NR: AT403764	8	
Mechanical tests used 2 cooled to 200C at 30°/h ing from 445 ± 5C) and 100C) aged. Hardened a	ixtures was verified on an alloy wi mm sheet samples, either annealed r. or slower), freshly hardened or naturally (1 week- 3 months) or art nd naturally aged welded sheet samp e month after welding by intermitte	(2 hours at 400C, hardened (water quench- ificially (96 hrs., les were tested for
NaCl solution over a per of the alloys. Results in summary form, that a the content of Cu, Fe a	riod of three months. Other tests are mostly tabulated or plotted or ddition of Zr, Be and Mn to these s nd Si should be severely controlled part in the work." Orig. art, has	concerned weldability a graphs and indicate, systems is useful, while b. "M. S. Artemova and
NaCl solution over a per of the alloys. Results in summary form, that a the content of Cu, Fe a	riod of three months. Other tests are mostly tabulated or plotted or ddition of Zr, Be and Mn to these s nd Si should be severely controlled	concerned weldability a graphs and indicate, systems is useful, while b. "M. S. Artemova and
NaCl solution over a per of the alloys. Results in summary form, that a the content of Cu, Fe a L. I. Agapova also took	riod of three months. Other tests are mostly tabulated or plotted or ddition of Zr, Be and Mn to these s nd Si should be severely controlled	concerned weldability a graphs and indicate, systems is useful, while b. "M. S. Artemova and

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TITLE: The V92 weldable aluminum alloy SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1964, Deformiruyemy*ye. splavy* (Halleable alloys), 76-79 TOPIC TAGS: aluminum alloy, weldable aluminum alloy, heat resistant alloy, V92 alloy, heat treatable alloy, wrought alloy, alloy weldability, alloy corrosion, resistance alloy property ABSTRACT: The V92 aluminum base alloy contains the following principal components: Mg, 3.9-4.6%; Zn, 2.9-3.6%; Mn, 0.6-1.0%; and Be, 0.0001-0.005%. The optimum combination of properties is obtained at a Zn + Mg sum of 7-8% and a Zn:Mg ratio of 0.75.		· · · · · · · · · · · · ·		76 /00 79
Arbuzov, Yu. P. TITLE: The V92 weldable aluminum alloy SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1964, Deformiruyemy*ya splavy* (Halleable alloys), 76-79 TOPIC TAGS: aluminum alloy, weldable aluminum alloy, heat resistant alloy, V92 alloy, heat treatable alloy, wrought alloy, alloy weldability, alloy corrosion, resistance alloy property ABSTRACT: The V92 aluminum base alloy contains the following Market alloy, 20-4 67: 7n, 2,9-3,67; Mn,0.6-1.07; and	ACCESSION NR: AT403764	•		· :
TITLE: The V92 weldable aluminum alloy SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1964, Deformiruyemy*ya- splavy* (Malleable alloys), 76-79 TOPIC TAGS: aluminum alloy, weldable aluminum alloy, heat resistant alloy, V92 alloy, heat treatable alloy, wrought alloy, alloy weldability, alloy corrosion, resistance alloy property ABSTRACT: The V92 aluminum base alloy contains the following principal components: Mg, 3.9-4.67; Zn, 2.9-3.67; Mn, 0.6-1.07; and Be, 0.0001-0.005%. The optimum combination of properties is obtained at a Zn + Mg sum of 7-87 and a Zn:Mg ratio of 0.75. The alloy is heat treatable: it is solution heat treated at 450-470C and artificially aged at 60C for 24 hrs and then at 200C for 12 hr.	AUTHOR: Fridlyander, I Arbuzov, Yu. P.	. N.; Zaytseva, N.	I.; Burova, Ye. I.	• •
SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1964, Deformiruyemy*ye. splavy* (Malleable alloys), 76-79 TOPIC TAGS: aluminum alloy, weldable aluminum alloy, heat resistant alloy, V92 alloy, heat treatable alloy, wrought alloy, alloy weldability, alloy corrosion, resistance alloy property ABSTRACT: The V92 aluminum base alloy contains the following principal components: Mg, 3.9-4.67; Zn, 2.9-3.67; Mn, 0.6-1.07; and Be, 0.0001-0.005%. The optimum combination of properties is obtained at a Zn + Mg sum of 7-87 and a Zn; Mg ratio of 0.75.	TITLE: The V92 weldabl	e aluminum alloy		
TOPIC TAGS: aluminum alloy, weldable aluminum alloy, heat resistant alloy, V92 alloy, heat treatable alloy, wrought alloy, alloy weldability, alloy corrosion, resistance alloy property ABSTRACT: The V92 aluminum base alloy contains the following principal components: Mg, 3.9-4.6%; Zn, 2.9-3.6%; Mn, 0.6-1.0%; and Be, 0.0001-0.005%. The optimum combination of properties is obtained at a Zn + Mg sum of 7-8% and a Zn:Mg ratio of 0.75.	SOURCE: Alyuminiyevy*y splavy* (Halleable allo	ve splavy*, no. 3, 1 bys), 76-79	-	my * y a
ABSTRACT: The V92 aluminum base alloy contains the following principal components: Ng, 3.9-4.6%; Zn, 2.9-3.6%; Mn, 0.6-1.0%; and Be, 0.0001-0.005%. The optimum combination of properties is obtained at 4 Zn + Mg sum of 7-8% and a Zn:Mg ratio of 0.75.	TOPIC TAGS: aluminum	alloy, weldable alum	inum alloy, heat alloy, wrought a ance alloy proper	11 0y, ty
	ABSTRACT: The V92 alu principal components: Be,0.0001-0.005%. Th obtained at a Zn + Mg	minum base alloy cor Mg, 3.9-4.6%; Zn, 2 e optimum combinatio sum of 7-8% and a	tains the followi 9-3.6Z; Mn.0.6- on of properties i Zn:Ng, ratio of 0.	n8 1.0%; and .s 75. 450470C
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The natural aging proceeds rather slowly and is not completed in 30 days. In 3 months of natural aging the tensile strength and yield strength increase by $2-3 \text{ kg/mm}^2$. The alloy is annealed at 320-3500for 2-3 hr with furnace cooling to 200C to room temperature. The annealed alloy has a tensile strength of 27-30 kg/mm², a yield strength annealed alloy has a tensile sciength of $27-30 \text{ kg/mm}^-$, a yield scrength of 13-17 kg/mm², and elongation of 18-22%. The tensile strength of the solution heat treated and artificially aged alloy is $43-48 \text{ kg/mm}^2$, yield strength 29-35 kg/mm², and elongation 18-21% at room temper-ature; 28 kg/mm², 22 kg/mm², and 25-30%, respectively, at 200C; and 9 kg/mm² 6 kg/mm² and 70% respectively at 300C. The tensile and ature; 20 kg/mm², 22 kg/mm², and 23 box, to product they, at 2000, and 9 kg/mm², 6 kg/mm², and 70%, respectively, at 300C. The tensile and yield strengths of naturally aged alloy are somewhat lower, but the difference becomes smaller with increasing temperature. The alloy can be extruded and cold formed. V92 alloy is welded satisfactorily by argon shielded arc welding; filler wire of the same alloy with 0.2-0.5% Zr and increased Mg and Zn content is recommended. No heat treatment is necessary after welding since the "critical cooling rate" of the alloy is rather low. The strength of welded joints is approximately 0.8 of that of the base metal. Corrosion resistance of V92 Qrig. art. has: 5 tables. alloy is satisfactory. Card 2/3

APPROVED FOR RELEASE: 06/13/2000

<u>A CONSTRUCTION CONSTRUCTION OF MODILARY</u>

ARBUZOV, Yu.P.; Prinimali uchastiye: FRIDLY NDER, I.N.; ZAYTSEVA, N.I.; BUROVA Ye.I.; SOLOV'YEVA, V.V.; ARTEM'YEVA, N.F.; ARTEM'YEVA, M.S.

> Properties of welded joints in the B92 aluminum alloy. Alium. splavy no.3:80-91 '64. (MIRA 17:6)

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ACCESSION NR: AT4037655 S/2981/64/000/003/0145/0152 AUTHOR: Fridlyander, L.N.; Khol'nova, V. I.; Yelagina, Z. A. TITLE: Effect of iron and silicon admixtures on the microstructure of alloy V93 SOURCE: Alyuminityevy*ye splavy*, no. 3, 1964. Deformiruyemy* ye splavy* (Malleable alloys), 145-152 TOPIC TAGS: aluminum alloy, alloy V93, alloy microstructure, hot prossed aluminum alloy, heat treated aluminum alloy, alloy grain growth, iron admixture, silicon admixture ABSTRACT: Ingots (diameter 70 mm) were dip-cast, then homogenized (48 hrs., 445- ' ABSTRACT: Ingots (diameter 70 mm) were dip-cast, then homogenized for preheating for 3 hours at 400-415C, to study the effect of Fe and Si concentration on alloy microstructure. 3 hours at 400-415C, to study the effect of Fe and Si concented from 470 ± 5C, aged 3 hours 7.03% Zn, 1.41-1.96% Mg, 0.77-1.68% Cu, traces to 0.31% Si and 0.073-0.5% Fe. Samples were either hot pressed or heat treated (wator quenched from 470 ± 5C, aged 3 hours 120C and 4 hours at 165C). Increase of Fe to levels above 0.10% results in a finer at 120C and 4 hours at 165C). Increase of Fe to levels above 0.10% results in a finer at 20C and more equant structure of hot pressed samples. The heat treated material grained and more equant structure of hot pressed samples. The heat treates in Fe.
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AT402765	5		
ACCESSION NR: AT403765 It is concluded that ferrous inhibit grain growth by form 1 table and 11 photomicrogr	components can act as recrystallization in the solution in the	on nuclei and that Fe can the A1. Orig. art. has:	
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ASSOCIATION: none.	DATE ACQ: 04Jun64	ENCL: 00	
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ACCESSION NR: AT4037658	S/2981/64/000/003/0175/0181	2
AUTHOR: Romanova, O. A.; Fridlyand	er, I. N.	
TITLE: Dovelopment and analysis of the	sheat resistant, ductile aluminum alloy D21	
SOURCE: Alyuminiyevy*ye splavy*, no. alloys), 175-181	3, 1964. Deformiruyemy*ye splavy* (Malleable	
	1, alloy D20, modification, alloy D16, alloy AK4-1, l property, heat resistant alloy, alloy corrosion	×.
D16, AK4-1 and D20 in an attempt to dev 225-250C. D20 was selected as the best modified alloy obtained was designated D 20-100C to 33.74 \cdot 10 ⁻⁶ 1/°C at 300-400 0.24 cal/g \cdot °C at 400C). Creep strength limit $\sigma_{25} = 23$ kg/mm ² at 200C to 12 kg/	elements were added experimentally to base alloys velop a heat resistant and ductile alloy for use at base and modified by adding 0.25-0.45% Mg. The 021 (sp. gr. = 2.84 g/cm ³ , $\alpha = 19.0.10^{-6}$ at C, $\rho = 0.054$ ohm \cdot mm ² /m, C = 0.18 at 50C to n = 20 kg/mm ² (0.2%, 100 hrs, 200C). Fatigue /mm ² at 270C, $\sigma_{100} = 22$ and 11 kg/mm ² , respec- esistance of stressed forgings was high (5 months) in	× × • •
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SUBMITTED: 00 DATE ACQ: 04Jun64 ENCL: 00	press gratitude to V.	L Dobatkin and N. F. Anoshkin for their as	Literal Assess
	ASSOCIATION: none		······
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ACCESSION NR: AT4037659	S/2981/64/000/003/0182/0193	
ACCESSION NR: AIHOUTOT	dreyev, A. D.; Pavlova, I. K.; Romanova, O. A.;	}
AUTHOR: Fridlyander, I. N.; An	dreyev, A. D.; Faviova, I. al,	
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	tion process and a study of the effects of tructure and properties of alloy VAD23	
TITLE: Selection of a labrice	ructure and properties of alloy VAD23	
technological factors on one of	and a permit we were aplayy	× ^
SOURCE: Alyuminiyevy*ye splavy	/*, no. 3, 1964. Deformiruyemy*ye splavy*	
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	lloy VAD23, alloy structure, alloy mechanical oy aging, alloy casting, alloy hot pressing,	•
TOPIC TAGS: aluminum alloy, a	oy aging, alloy casting, alloy hot pressing, not aging, alloy casting, alloy semiproduct aniso-	
property, alloy hardening, alloy cold	oy aging, alloy casting, alloy hot product aniso- rolling, alloy forging, alloy semiproduct aniso- alloy, heat resistant aluminum alloy	1
LIGH CPPANOED ALUMINUM		
	- $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$	×-
ABSTRACT: Ingots (diameter 30	0 mm, length 1000 mm) of alloy VAD23 were factory 0 min. at 745-780C, poured, 1.4% Li and 0.15% Cd 1 LiCl plus 54% KCl, mixed, settled at 750-770C,	
IL AAR (FINY TATINED, NOPO "		1
dip rate 15-16 may many into PR	homogenized for 24 hrs. at 510 ± 100. the standard for 24 hrs. at 510 ± 100. the standard for the standard f	-
60 min. at 525 + 5C, aged 12 h	306-7 sections (deformation 94%, 420 4-15 mm; ars. at 170C), panels (wall thickness 4-15 mm;	
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pr 17 ro me 4 ta tu tha str str str str str cre fro and	CESSION NR: AT4037659 essed at 420C from forgings 550 x 150 x 600 mm; 525 \pm 5C, then aged 16 H OC), 0.8 - 8.0 mm thick sheets (hot rolled at 370-390C to 8 or 4 mm, the asuring 90 or 120 x 200 x 400 mm (forged after 24 hrs. at 400-450C, hard hrs. at 525 \pm 5C, aged 16 hours at 170C). Results of mechanical tests a bulated for all intermediate products and show that pressing or rolling reserver no significant effects on mechanical properties of rods and sh rength or yield of hot pressed rods, but relative elongation increased. mm ² at 12% to 58 at 32%), relative elongation increased from 0.5% at 12% X at 51%. The optimal hardening temperature was found to be 525C, and sile strength sharply when exceeding 30 sec., while relative elongation m 1-3 kg/mm ² for twice pressed samples to 10-13 kg/mm ² for once pressed I. Potapova and Ye. N. Kalinina also took part in the work." Orig. art.	en cold ngs lened ore tempera- eets in sile Tensile % to the reduces in- ged rods.	
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CIA-RDP86-00513R000513720001-2

S/2981/54/000/003/0194/0200 ACCESSION NR: AT4037660 AUTHOR: Fridlyander, I. N.; Romanova, O. A.; Archakova, Z. N.; Gur'yev, I. I.; Dronova, N. P.; Petrova, A. A.; By*chkova, Z. S. TITLE: Preparation and testing of intermediate shapes from high-strength heat resistant aluminum alloy VAD23 SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1964. Deformiruyemy*ye splavy* (Malleable alloys), 194-200 TOPIC TAGS: aluminum alloy, alloy VAD23, heat resistant aluminum alloy, high strength aluminum alloy, alloy mechanical property, hot pressed rod, hot pressed section, hot pressed strip, hot rolled sheet, cold rolled sheet, forged piece, double pressing ABSTRACT: Immersion-cast ingots (diameter 260 mm) of alloy VAD23 (5.1-5.7% Cu, 1.2-1.4% Li, 0.096-0.11% Cd, 0.60-0.7% Mn, 0.15-0.25% Ti) were hot pressed (430-450C) into rods (intermediate diameter 127 mm or final diameter 20 mm), sections PR306-7, strips with 25x210 mm cross section and pressed panels. The pieces were water quenched from 525+5C, then aged 16 hours at 170C. Sheets 1.0, 1.5 and 2.0 mm thick were hot Card 1/2

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annealing and finally heat tr Forgings (90 or 120x200x400 heating 3 hours to 420-440C Pressed shapes exhibited hi 3-4%. It was noted that dou shape) reduced the tensile s sheets and forgings were low	5 mm, then cold rolled to desired th eated (water quenched from $523\pm5C$, 0 mm) were forged on a vertical pres) from rods (diameter 180 mm) and h gh tensile strength (66-70 kg/mm ²) a ble pressing (i.e., into intermediate trength and increased the plasticity. wer than those of the pressed shapes	aged 16 hours at 170±5C). ss (deformation 65%, pre- heat treated as for sheets. at a relative elongation of diameter rods, then final Mechanical properties of . "K. N. Fomin, N. S.	
Lebedeva, P. G. Reznik, N N. N. Tyurin also took part	. Averkina, L. S. Zheltovskaya, Yu in the work." Orig. art. has: 7 tabl	. A. Vorob'yev and les.	
ASSOCIATION: none	X		
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ACCESSION NR: AT4037667	8/2981/64	/000/003/0263/	0270	
UTHOR: Galatskiy, B. D.; Afanas'y	ova, I. S.; Fridly	yander, I. N.	•	
TTLE: A study of the rate of Cu, Mg legree of deformation during extrusio	g and Mn diffusion n	in aluminum in	relation to the.	
OURCE: Alyuminiyevy*ye splavy*, Malleable alloys), 263-270	no. 3, 1964. Defe	ormiruy'emy*ye	splavy*	
TOPIC TAGS: aluminum alloy, dural nanganese diffusion, magnesium diffu related diffusion, temperature diffusion	usion, component	diffusion analys	is, extrusion	•
ABSTRACT: Samples (150 mm long) twinned ingots (see Fig. 1 in the Encl in $\%$: 0.015 - 4.1 Cu, 0.016 - 1.62 M were preheated for 10 ² to 10 ⁵ sec. in analyzed along diagonal sections (1° to of diffusion coefficients on temperatur and 47.0). Results are tabulated (sec	osure) of alloys A g, 0.008 - 0.44 M a niter bath at 47 o 1°30') to determ re and coefficients	1 and D16 (cont In, 0.19 - 0.43 Io, 490 or 510C ine depth of diff s of elongation (aining, respective Fe, 0.18 - 0.36 and spectrally usion and depend $\lambda = 3.7, 10.0, 2$	lence
Card 1/4				

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ACCESSION NR: AT4037667	-	·		
diffusion coefficient D, express of the cast material and n is an of deformation and by the degre tables and 8 graphs.	sed as $D = D_1 \cdot \lambda^n$ (where D_1 a exponent), is governed princes are of deformation as λ increases	is the diffusion coefficient by D_1 at small ases. Orig. art. has:	cient degrees 3	
ASSOCIATION: None		the second second	•	
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va, L. V.; Rayevskaya, M. V.; .; Yatsenko, K. P.; Rogova, L. K system kaya obrabotka metallov, no. 6,
kaya obrabotka metallov, no. 6,
kaya obrabotka metallov, no. 6,
m, beryllium niobium alloy, allo loy phase composition, alloy beryllium solubility
f the Be-Nb system containing up ree phases: the beryllium base e, and the NbBel7 compound 6- to 46% Nb, the a- and y-phases amount of the latter phase. The ed at 850° for 14 days and water niobium to 1108 at 58% niobium.
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ACCESSION NR: AP40406	87		
29 days. The Vickers vater quenched) was for sutectic, 480 for the state solubility of ni amount of NbBe ₁₂ was for the eutectic of the a- comperature is close t	ghly the same hardness as a hardness of individual phase ound to be 110 for the a-pha γ -phase, and 1060 for the δ obium in beryllium is low. Found in an alloy containing and γ -phases contains 2.5% to the melting temperature of and hypoeutectic compositi	es (annealed and se, 160 for the -phase. The solid A considerable as little as 0.72 Nb. The eutectic f pure beryllium.	Nt
structure, but at a centralic compounds, th alloys the structures different due to segre	rtain amount of primary for the fine structure disappears of the upper and lower part gation. Orig. art. has: 3	mations of inter- . In hypereutectic s of ingots are	
structure, but at a centrallic compounds, th alloys the structures	rtain amount of primary for the fine structure disappears of the upper and lower part	mations of inter- . In hypereutectic s of ingots are	
structure, but at a centralic compounds, th alloys the structures different due to segre	rtain amount of primary for the fine structure disappears of the upper and lower part	mations of inter- . In hypereutectic s of ingots are	
tructure, but at a centrallic compounds, the alloys the structures different due to segre ables.	rtain amount of primary for the fine structure disappears of the upper and lower part	mations of inter- . In hypereutectic s of ingots are	an Gran
tructure, but at a centrallic compounds, the structures ifferent due to segre tables.	rtain amount of primary for the fine structure disappears of the upper and lower part gation. Orig. art. has: 3	mations of inter- . In hypereutectic s of ingots are figures and 2	ann da na a ann ann ann ann ann ann an ann an a

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DRITS, M.Ye., doktor tekhn. nauk, otv. red.; EOCHVAR, A.A., akademik, red.; BELOV, A.F., doktor tekhn. nauk, red.; DOBATKIN, V.I., doktor tekhn. nauk, red.; MAL'TSEV, M.V., doktor tekhn. nauk, red.; FRIDLYANDER, I.N., doktor tekhn. nauk, red.; SVIDERSKAYA, Z.A., kand. tekhn. nauk, red.; YELAGIN, V.I., kand. tekhn. nauk, red.; BARBANEL', R.I., kand. tekhn. nauk, red.; SHAHOV, M.V., kand. tekhn. nauk, red.; KADANER, E.S., kand. tekhn.nauk, red.; TROKHOVA, V.F., red.; CHERNOV, A.N., red.

[Metallography of light alloys] Metallovedenie legkikh splavov. Moskva, Nauka, 1965. 226 p. (MIRA 18:10)

1. Moscow. Institut metallurgii.

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L 40715-65 EPF(c)/EPR/EPA(s)-2/EWP(k)/EWP(z)/EWA(c)/EWT(m)/15 EWP(v)/EWP(t) Pf-4/Ps-4 IJP(c) EW/MJW/JD/H4/HW/JG/WP ACCESSION NR: AP5006998 S/0129/65/0 AUTHOR: Fridiandam	01001/002/005	
AUTHOR: Fridlyander, I. N.; Yatsenko, K. P.; Semen	DVA, Z. G.1	
TITLE: <u>Aluminum</u> beryllium-base alloys	49 13	
SOURCE: Hetallovedeniye i termicheskaya obrabotka : 1965, 2-5, and top half of insert facing p. 24	ecallov, no. 3,	
TOPIC TAGS: aluminum alloy, complex aluminum alloy, containing alloy, high elasticity alloy, alloy works	beryllfum bility	
ABSTRACT: Alloying beryllium is the most effective the specific <u>elasticity modulus</u> (the elasticity moduratio) of aluminum alloys. High-modulus aluminum-be have an adequate fabricability and yield better to p than pure beryllium. The heterogeneity of their str impedes the grain growth even with prolonged holding atures. However, binary Alme allo	means of increasing ilus-to-density ryllium alloys ressure working ucture strongly at high tempor-	
have a low tensile and creep strength. Two types of Card 1/43	high-strengtli,	

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ACCESSION NR: AP5006998

high-elasticity AlBe-base alloys have been developed. Alloys of the first type are nonheat treatable, contain 15-60% Be and up to 15% of other alloying elements, and have a tensile strength $\sigma_b = 40-60 \text{ kg/mp}^2$, an elongation $\delta = 8 - 202$, and $E = 10,000 - 18,000 \text{ kg/mm}^2$. Alloys of the second type are heat treatable, contain 15-40% Be and up to 10% of other alloying elements, and have $\sigma_0 = 52-69 \text{ kg/mm}^2$, $\delta = 8-122$, and E = 11,500-14,000 kg/mm². Alloys of the first type have a better formability, sustain prolonged holding at temperatures up to 5000 without impairing the rcom-temperature mechanical properties, and have a higher specific modulus of elasticity than any of the structural materials presently used, including aluminum or titanium base alloys and steels. These alloys can be used at temperatures up to 450C; they have a tensile strength of 30-36, 20-34, 12-16, and 3-8 kg/mm² at 200, 300, 400, and 500C, respectively; the corresponding figures for elongation are 11-35, 9-30, 7-37, and 4-31Z. At 20C, workhardened sheets of the alloys of this type with the highest Be content have $\sigma_b = 70 - 75 \text{ kg/mm}^2$, $\delta = 2 - 5.6 \text{X}$ and $E = 18,000 \text{ kg/mm}^2$. Hot, extruded or rolled, complex-alloyed, Al-Be alloys have a cyclic strength and notch sensitivity comparable to those of D 16 [U.S. 2024] sluminum alloy. Annealing of work-hardened sheets at a temperature above 3500 Card 2/4

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ACCESSION NR: AP5006998

restores the plastic properties of the alloys without increasing the grain size; the cooling rate after annealing has no effect on the mechanical properties of the alloys. The AlBe-base valloys are not susceptible to intercrystalline and stress corrosion, and their general corrosion resistance is higher than that of upclad D16 aluminum alloy. The alloys can be extruded or rolled. Parts of a complex shape can be made from these alloys by die forging or sheat forming. They can be joined by riveting, and spot, seam, and automatic and manual argon shielded-arc welding. The argon shielded-arc welded joints with reinforcement have a tensile strength equal to 90% of the strength of the base metal, with the weld ductility equal to that of the base metal; the weld strength is 5 kg/mm² at 500C. The alloys is particularly effective in structures requiring high rigidity. When the alloys are used in combination with other materials, a saving of 20-50% in the weight of a structure can be achieved. Orig. art. has: 1 figure and 2 tables. [HS]

Card 3/4

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L 00851 66 EMT(m)/EVP(w)/EPF c)/EPF(n)-2/EMA(d)/ENP(v)/T/EMP(t)/EMP(k)/EMP(b)/EMA(c	-)	•
ACCESSION NR: AP502070 669.715'72'5'3:621.785.76		
AUTHOR: Fridlyander, I. Neve, 53/		
TITLE: Investigation of aging in aluminum alloys of the Al-Zn-Mg and Al-Zn-Mg-Cu systems		
SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 8, 1965, 43-48		
TOPIC TAGS: aging stage, zone aging, phase aging, aluminum alloy, ternary alloy, metastable phase, Guinier zone, Preston zone, preliminary aging, additional aging, prolonged aging, alloy weldment, stress corrosion		
ABSTRACT: The strongest aluminum alloys are those containing Zn and Mg or Zn, Mo,		
and <u>Cu</u> 'as alloy elements along with small additions of <u>Mn</u> /[Cr] or Zr] The high strength of these alloys is chiefly due to their aging. There exist two different		
aging stages: zone aging, where hardening is caused by the Guinier-Preston zones (natural aging), and phase aging, where hardening is produced by particles of me- tastable phases (artificial aging). The characteristic features of the zone-		
aging stage are: a relatively low ratio of strength to yield point (0.6-0.7), a high and constant (20%) elongation, and an increasing electrical resistance. At		
80-200°C the strength curves display two maxima. The phase-aging stage is charac-		
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	ACCESSION NR: AP5020708 terized by a higher ratio of strength to yield point (0.8-0.95) and a smaller elongation and electrical resistance; the transition from zone to phase stages occurs in between the first and second maxima. Preliminary aging at 20°C has a definite affect on subsequent aging at higher temperatures. Thus, for example, following its brief aging at 20°C, an alloy immediately begins to harden when heated to 160°C. By contrast, if the aging at 20°C but ultimately its strength turns out to be higher than that of the alloy briefly aged a priori at 20°C and the alloy aged at 160°C without preliminary low-temperature aging. Similarly, an alloy aged at 195°C immediately after quenching gets softened, clearly owing to the segregation of a stable phase. Preliminary prolonged aging of this alloy at 20°C or 60°C, by contrast, assures higher stability of metastable segregations, as well as higher strength, higher yield point, and lower elongation, on subsequent aging at 195°C. Only the concept of the existence of two essentially different metastable particles, forming directly from the matrix as a result of interaction with previously formed zones can account for such a considerable effect of prelim- inary low-temperature aging on the properties of alloys subsequently aged at high- er temperatures. A reversal of the procedure, namely, preliminary high-tempera- ture aging followed by subsequent aging at lower temperatures can also be highly effective and warrants further investigation. It is particularly important to Card 2/3	· · · · · · · · · · · · · · · · · · ·	
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ACCESSION NR: AP5020708			5
corresponds to possible if crack proneness of Al-Zn- aging stages and prolonge ture strength and stress alloys. The aging of Al-	extremely prolonged aging insolation in the summer (for Mg alloy weldments.) Analog ad additional heatings at 70 corrosion of welded specime -Zn-Mg alloys creates an uni- formed earlier, in the pre- iderably the subsequently for , 2 tables.	gously, in metallurgy, di O°C markedly affect the f ens of high-strength Al-Z usual diversity of atruct sence of lower or higher	ffemnt rac- n-Mg ures; temp-
ASSOCIATION: none			
SUBMITTED: 00	ENC: 00	SUB CODE: MM,	SS
NO SOV REF: 004	OTHER: 000		
Card 3/3			

<u>I 10951-66 3WT(m)/3WP(k)/T/EMP(w)/EWP(t)/ETI IJP(c) JH/JD/HW</u> ACC NR: AT6024907 (A) SOURCE CODE: UR/2981/66/000/004/0005/00	14
AUTHOR: Fridlyander, I. N. (Doctor of technical sciences); <u>Pomanova, O. A.:</u> Archakova, Z. N. 49	
ORG: none 4.1	
TITLE: Properties of VAD23 alloy	
SOURCE: Alyuminiyevyye splavy, no. 4, 1966, Zharoprochnyye i vysokoprochnyye splavy (Heat-resistant and high-strength alloys), 5-14	Ÿ
TOPIC TAGS: aluminum alloy, copper containing alloy, lithium containing alloy, cadmium containing alloy, manganese containing alloy, titanium containing alloy, alloy composition, metal property/VAD23 aluminum alloy	
ABSTRACT: The effects of <u>copper</u> , <u>lithium</u> , <u>cadmium</u> , <u>manganese</u> , t <u>itanium</u> , <u>iron</u> , and <u>silicon</u> on the properties of VAD23 aluminum alloy have been studied under laborator Jconditions. Ingots 70 mm in diameter, cast in a water-cooled mold, were extruded in	
round bars 10 mm in diameter, which were machined into the test specimens. In one series of ingots lithium content varied from 0 to 3.0% at copper contents of 4.0%, 5.0%, and 6.0%, and constant cadmium (0.15%), manganese (0.6%), and titanium (0.15%)	
content. In the other series of ingots at a constant lithium (1.3%) and copper (5.2%) content, the manganese content was varied from 0 to 2.0\%, cadmium from 0 to 5.0\%, titanium from 0 to 0.3\%, and iron and silicon from 0 to 0.9\%. It was	
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L 10951-66 ACC NR: AT6024907

found that: lithium intensifies the effects of aging; copper at contents of 4X-5Z. increases strength: manganese at contents up to 1.0% improves strength and ductility, up to 0.2% cadmium increases strength of aged alloys and intensifies the effects of artificial aging; and titanium at contents of up to 0.3% has no effect on tensile strength but improves rupture strength. Iron and silicon were found to be harmful; impurities. On the basis of these results the optimum composition of VAD23 alloy was established as follows: 4.9-5.8% copper: 1.0-1.4% lithium, 0.1-0.25% cadmium: s 0.4-0.8% manganese; a maximum of 0.3% each of iron and silicon: and a maximum of > 0.15% titanium. Artificial aging at 150-160C for 10-12 hr produces the best combination of mechanical properties: tensile strength, 51-54 kg/mm²; yield strength, 36-44 kg/mm² with an elongation 10-15%. Cold rolling prior to heat treatment, with reductions from 4% to 10%, promotes intensive grain growth and lowers strength and ductility. At the present, round and flat ingots are produced by continuous casting and processed by rolling and extrusion. (Orig. art. has: 10 figures. [TD] SUB CODE: 11/ SUBM DATE: none/ ORIG REF: 007/ OTH REF: 006/ ATD PRESS: 50.56 Card 2/2

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ACC NR: AT6024921		2
at 100 (100,hr) or 120 (10 hr	nr) and 175 (1 hr) were very susceptible. The susce	epti-
bility of ATsM was also affe	ected by the filler wire. The specimens welded with	h l
AMgo alloy filler wire were	e less susceptible to delayed failure than those we	lded
alloy and failure was observ	susceptibility of ATsMU alloy was lower than that a wed only on the specimens welded with AMg4 filler w	or Arsm vire and
aged at 120C for 10 hr $+$ at	: 175 for 1 hr. Specimens of ATSM and ATSMU alloys	tested
in argon remained intact for	or 50, 60 days. Even when removed from argon and 1	left -
under stress in air, no crac failure of ATeM and ATeMI	acking occurred within 90 days. ⁴ It appears that the illoy welds is a result of <u>stress corrosion</u> under the	delayed
effect of air mositure. The	the optimum aging conditions for both alloys were 900	for
100 hr. Orig. art. has: 6	figures and 9 tables.	[TD]
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SUB CODE: 11, 13/ SUBM DAT	TE: none/ ORIG REF: 001/ OTH REF: 006/ ATD PH	RESS:5056
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ACC NRI AT6024922 (A, N)	ID/JH SOURCE CODE: UR/2981/66/000/004/0135/0142
AUTHOR: Fridlyander, I. N.; Setyukov, O. A Lashko, N. F.; Khromova; O. A.	.; Titarenko, I. I.; Barasheva, T. V.; 37 Br
ORG: none	4
TITLE: Study of the chemical inhomogeneity	
SOURCE: Alyuminiyevyye splavy, no. 4, 1966 (Heat resistant and high-strength alloys),	. Zharoprochnyye 1 vysokoprochnyye splavy 135-142
TOPIC TAGS: zinc containing alloy, magnesi aluminum alloy/ATSM <u>aluminum</u> alloy, ATSMU	um containing alloy, weld evaluation, aluminum alloy
tion of the weld joint depends on the compo	is shown that the average chemical composi- position of the base material and filler supply rate of filler wire, and is indepen-
content and drop in the zing content of the	of the sheets causes a rise in the magnesium e seam. Motallographic analyses of the ists of grains of base material fused at
Tuston zone snowed chat its solucould cond	
the boundaries; these grains gradually char Cord 1/2	nge into the cast grains of the seam. In

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	ACC NR: AT6024922 3
	the fused grains of the fusion zone and cast grains of the seam, liquation of zinc from the grain to the periphery is observed; the boundary regions are rich, the cen- tral ones poor in zinc. X-ray structural analysis showed the existence of the AlgMm phase in ATSM and ATSMU alloys if the <u>manganese</u> concentration did not exceed 0.26%. In ATSM and to a much lesser degree in ATSMU, which contains half as much Mm, coarse formations of the separated AlgMm phase are observed which promote the generation of <u>microcracks</u> and may increase the tendency toward a slow breakdown. Orig. art. has: 3 figures and 3 tables. SUB CODE: 11/ SUEM DATE: none
a a su a	welding of dissimilar metals
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$\frac{L + 27041-66}{ACC NR: AT6024923} $	4/0143/0151
AUTHOR: Fridlyander, I. N.; Kuznetsova, Ye. A.; Bubenshchikov, V. S.	36 B+1
ORG: none TITLE: Kinetics of <u>aging</u> of an alloy of the <u>Al-Zn-Mg</u> system $\frac{1}{272777777}$ SOURCE: Alyuminiyevyye splavy, no. 4, 1966. Zharoprochnyye i vysokoprochny (Heat resistant and high-strength alloys), 143-151	
TOPIC TAGS: aluminum alloy, zinc alloy, magnesium containing alloy, metal $A \perp \Delta G' = G' \leq F \leq T_{EM}$ AESTRACT: The kinetics of aging of an alloy of the Al-Zn-Mg system was stuvarious temperatures immediately after quenching (30 min at 450 °C, cooling and after two months of aging. The alloy had the composition (in \$): Zn 4. Mn 0.45, Zr 0.17, Fe 0.27, Si 0.17, Cu 0.021, bal. Al). The alloy was foun characterized by a very long aging period at 20°C, probably measured in yea set of mechanical properties and the nature of change in electrical conduct respond to the zone stage of aging. Transition to phase aging may occur at ture as low as 50-70°C; it is possible that if the holding time is increase transition will shift toward lower temperatures. Preliminary zone aging ha ciable effect on subsequent aging at high temperatures. It is postulated to into motastable particles, and the particles thus formed have a greator the	died at in water) 35, Mg 1.57, d to be rs. The ivity cor- a tempera- d, this s an appre- hat some of the zones)
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ity than those formed from the nuclei d or the effect of stepwise aging. Orig.	irectly in the matrix. This m art. has: 6 figures.	echanism accounts
UB CODE: 11/ SUBM DATE: none		
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$\frac{L 16968-66}{ACC NR: AT6024924} = \frac{(A,N)}{EMP(w)/EMP(v)/EMP(v)/EMP(v)/ETI IJP(c) JH/JD/HN}$	3
AUTHOR: Fridlyander, I. N.; Vlasova, T. A.; Skachkov, Yu. N.; Shiryayeva, N. V.; Surkova, Yu. I.; Gorokhova, T. A.; Ped', A. A.; Gur'yev, I. I.; Dzyubenko, M. V.	
ORG: none $\begin{pmatrix} 4 \\ 9 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	
TITLE: Weldability of high-strength alloys of the Al-Zn-Mg-Cu system $B+1$	
SOURCE: Alyuminiyevyye splavy, no. 4, 1966. Zharoprochnyye 1 vysokoprochnyye splav (Heat resistant and high-strength alloys), 152-158	r
TOPIC TAGS: aluminum zinc alloy, aluminum alloy property, weldability / V96 aluminum zinc alloy	n
ABSTRAOT: The object of the work was to study the weldability in the fusion welding of V96 alloy, and also to determine whether the weldability of this alloy can be im- proved by changing the chemical composition of the base metal and filler wire. Shee of V96 alloy 2.5 mm thick of the chemical composition 8.44% Zn, 2.72% Mg, 2.2% Cu,	
0.06% Mn, 0.13% Zr, 0.29% Fe, and 0.13% Si were used in the experiments. In order t decrease the tendency toward crystallization cracks, the welding should be carried o with Al-Mg alloy fillers (of type AMg6). The content of the main alloying elements	ut_ in
the base metal should be kept within the following limits: 6.5-7.5% Zn; 2.7-3.5% Mg 1.6-2.0% Cu; 0.15-0.22% Zr. However, even then the tendency of V96-type alloys to form cracks during welding remains higher than in commonly used alloys of the Al-Mg	
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	L h6963-66 ACC NR: A system (AM fected zon ing is 0.5 Weld joint aluminum a in welded	(1) g3, AMg6) e. The m -0.6 of t s of V96- lloys. S structure	nodulus of that of th -type allo The low <u>pl</u> es. Orig.	resist o base ys have asticit art. h	ance of we metal imme a lower b $y \circ f$ the j as: 4 tab	diatel; ending oints les.	y after we angle tha may cause	lding o n those a low s	or after ag	ring. weldable
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$\frac{16967.66}{\text{NCC} NRi AT6024925} (A,N)$	SOURCE CO	DE: UR/2981/66/000/004/0159/0169.
UTHOR: Drits, M. Ye.; Kadan Fridlyander, I. N.	ner, E. S.; Vashchenko,	A. A.; Shiryayeve, N. V.; 37
DRG: none	4	36 B+/
NITLE: Structure of weld jot	ints of W96-type alloys	
SOURCE: Alyuminiyevyye splay Noat rosistant and high-stre		rochnyye i vysokoprochnyye splavy
COPIC TAGS: aluminum zinc al luminum zinc alloy	lloy, aluminum alloy proj	perty, weld evaluation / V96
ing elements on the structure compositions. A definite rol o form hot cracks during wel- joint. As a rule, the struct seam in that it has coarser a boundaries; in most cases, the structure of the transition a character of the structure, a	o of V96-typo weld joint: lationship was found beta lding and the structure of ture of the transition zo agglomerates of second or hose phases form a contin zone, greater its extent and greater the enrichmen	the influence of various alloy- s by using filler wire of various ween the tendency of the alloys of the transition zone of the weld one differs from the center of the cess phases along the grain muous network. The coarser the , more pronounced the network at of the boundaries with brittle the alloys to form hot cracks dur-
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"APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000513720001-2 I 1/27/15 ACC NR: ATS024925 ing wolding. Conversely, a fine, regular structure of the transition motal zone and a discontinuity of the network of second phases correspond to lower values of the cracking coefficient. By selecting optimum wolding conditions, one can influence the process so as to obtain a favorable structure in the transition zone and thus reduce the danger of failure of the weld joints. Org. art. has: 7 figures. SUB CODE: 11/ SUEM DATE: none/ ORIG REF: 003/ OTH REF: 001 M Cord 2/2

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the plasticity decreases. In subsequent studies, a process for origustering of pres- sing semifinished products from SAA was developed. The <u>effect of temperature</u> , pres- sure, time of holding under pressure during briquetting, temperature and degree of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have	ACC NRI AT6024933		UR/2981/66/000/004/0219/0223
ORG: none TITLE: Properties of a <u>sintered</u> aluminum alloy with a low linear expansion coeffi- cient SOURCE: Alyuminiyevyye splavy, no. 4, 1966. Zharoprochnyye i vysokoprochnyye splavy (Heat resistant and high-strength alloys), 219-223 TOPIC TAGS: sintered alloy, aluminum alloy production / SAS-1 sintered alloy ABSTRACT: A process was developed for pressing sintered aluminum alloys (SAA) with low linear expansion coefficients, specifically, the <u>SAS-1</u> alloy, and the properties of the latter were studied. Analysis of the plastic properties showed that the plas- ticity maximum of SAS-1 is located in the 530-450 °C range, and that the plasticity is markedly affected by the temperature and rate of deformation: as the latter increases, the plasticity decreases. In subsequent studies, a process for briquetting and pros- sing semifinished products from SAA was developed. The <u>effect of temperature</u> pres- sure, time of holding under pressure during briquetting; temperature and degree of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have	AUTHOR: Krivenko, R. A.	; Klyagina, N. S.; Tsabrov, N. D.	; Fridlyander, 1. N.
TITIE: Properties of a <u>sintered</u> aluminum alloy with a low linear expansion coeffi- cient SOURCE: Alyuminiyevyye splavy, no. 4, 1966. Zharoprochnyye i vysokoprochnyye splavy (Heat resistant and high-strength alloys), 219-223 TOPIC TAGS: sintered alloy, aluminum alloy production / SAS-1 sintered alloy AESTRACT: A process was developed for pressing sintered aluminum alloys (SAA) with low linear expansion coefficients, specifically, the <u>SAS-1</u> alloy, and the properties of the latter were studied. Analysis of the plastic properties showed that the plas- ticity maximum of SAS-1 is located in the 530-450°C range, and that the plasticity is markedly affected by the temperature and rate of deformation: as the latter increases, the plasticity decreases. In subsequent studies, a process for briquetting and pres- sing semifinished products from SAA was developed. The effect of temperature of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have		1	. + 1
cient SOURCE: Alyuminiyevyye splavy, no. 4, 1966. Zharoprochnyye i vysokoprochnyye splavy (Heat resistant and high-strength alloys), 219-223 TOPIC TAGS: sintered alloy, aluminum alloy production / SAS-1 sintered alloy AESTRACT: A process was developed for pressing sintered aluminum alloys (SAA) with low linear expansion coefficients, specifically, the <u>SAS-1</u> alloy, and the properties of the latter were studied. Analysis of the plastic properties showed that the plas- ticity maximum of SAS-1 is located in the 530-450 °C range, and that the plasticity is markedly affected by the temperature and rate of deformation: as the latter increases, the plasticity decreases. In subsequent studies, a process for briquetting and pres- sing semifinished products from SAA was developed. The effect of temperature of pres- sure, time of holding under pressure during briquetting, temperature and degree of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have	TITIE: Properties of a	sintered aluminum alloy with a lo	w linear expansion coeffi-
(Heat resistant and high-strength alloys), 219-22) TOPIC TAGS: sintered alloy, aluminum alloy production / SAS-1 sintered alloy ABSTRACT: A process was developed for pressing sintered aluminum alloys (SAA) with low linear expansion coefficients, specifically, the <u>SAS-1</u> alloy, and the properties of the latter were studied. Analysis of the plastic properties showed that the plas- ticity maximum of SAS-1 is located in the 530-450 °C range, and that the plasticity is markedly affected by the temperature and rate of deformation: as the latter increases, the plasticity decreases. In subsequent studies, a process for briquetting and pres- sing semifinished products from SAA was developed. The effect of temperature, pres- sure, time of holding under pressure during briquetting, temperature and degree of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have	cient		
TOPIC TAGS: sintered alloy, aluminum alloy production / SAS-1 sintered alloy ABSTRACT: A process was developed for pressing sintered aluminum alloys (SAA) with low linear expansion coefficients, specifically, the <u>SAS-1</u> alloy, and the properties of the latter were studied. Analysis of the plastic properties showed that the <u>plas- ticity</u> maximum of SAS-1 is located in the 530-450 °C range, and that the plasticity is markedly affected by the temperature and rate of deformation: as the latter increases, the plasticity decreases. In subsequent studies, a process for briquetting and pres- sing semifinished products from SAA was developed. The effect of temperature, pres- sure, time of holding under pressure during briquetting, temperature and degree of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have	SOURCE: Alyuminiyevyye (Heat resistant and high	splavy, no. 4, 1966. Zharoprochr -strength alloys), 219-223	yye i vysokoprochnyye splavy
low linear expansion coefficients, specifically, the <u>SASAT</u> alloy, and the properties of the latter were studied. Analysis of the plastic properties showed that the plas- ticity maximum of SAS-1 is located in the 530-450 °C range, and that the plasticity is markedly affected by the temperature and rate of deformation: as the latter increases, the plasticity decreases. In subsequent studies, a process for briquetting and pres- sing semifinished products from SAA was developed. The effect of temperature of pres- sure, time of holding under pressure during briquetting, temperature and degree of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have	TOPIC TAGS: sintered al	loy, aluminum alloy production /	SAS-1 sintered alloy 17
of the latter were studied. Analysis of the plastic properties should only the <u>latter</u> ticity maximum of SAS-1 is located in the 530-450 °C range, and that the plasticity is markedly affected by the temperature and rate of deformation: as the latter increases, the plasticity decreases. In subsequent studies, a process for briquetting and pres- sing semifinished products from SAA was developed. The effect of temperature of pres- sure, time of holding under pressure during briquetting, temperature and degree of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have	 		
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sing semifinished products from SAA was developed. In <u>e effect of temperature</u> , pro- sure, time of holding under pressure during briquetting, temperature and degree of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have	1 1 17 - CC - to - 1 lose + he	tomponeture and rate of delormal	LIONI AS CHO LACCOL LHOLOGOUP,
sure, time of holding under pressure during briquetting, temperature and degree of deformation during pressing, rate of discharge of the metal, various types of lubri- cants, etc. on the compactability, mechanical properties, and structure of the alloy was determined. SAS-1 was found to soften slowly with rising temperature, and to have	- I DI I DI I DI I	to from SAA was developed. 100 (allact of competatuto, proc
cants, etc. on the compactability, mechanical properties, and schedule of the inclusion was determined. SAS-1 was found to soften slowly with rising temperature, and to have		Jaw www.aguwa duming hvidugtting	
was determined. SAS-1 was found to soften slowly with rising comparation, and co have		setability, machanical Drobbrulda	
	was determined. SAS-1	vas found to soften slowly with r	ising temperature, and to have
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	rength at 400 % tests showed						
1 A Alamaa	Luminum alloys: .25 (dry friction	unthout and	NCIC COAL	1 ng . U.27	(OLA TLICOT	011/9 HT011 H110	010
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L he976-66 ENT(m). T/EAP(t)/211 IJP(e) ACC NR. AT6024934 (AN)	JH/JD		
ACC NR: AT6024934 (A,N)	SOURCE CODE:	UR/2981/66/000/004/0224/0231	
AUTHOR: Muss, N. P.; Fridlyander, I. N.			
The second		38	
ORG: none	.1		
TITLE: Dilatometric studies of binary all	1^{1} oys of the <u>Al-Z</u>		
SOURCE: Alyuminiyevyye splavy, no. 4, 196 (Heat resistant and high-strength alloys),	6. Zharoprochn 224-231	yye i vysokoprochnyye splavy	
TOPIC TAGS: aluminum zinc alloy, thermal	expansion		
ABSTRACT: The purpose of the work was to a binary alloys of the Al-Zn system from 20° the pattern of variation of α in relation the alloys of this system, and also to fin to the dependence of α on the chemical com from 10.4 to 89.2% Zn. The dilatometric s range where the alloys exist in the solid the alloy was found to ca. 30 a continuous atures studied. A gradual increase in the range of testing temperatures. These regu of phase transformations, which are associ dence of α on the alloy composition does n Cord 1/2	C to the solidu to the phase tr d out whether t position. The tudies were car state. An incr and gradual inc: α of each allog larities were f ated with a lar	s temperature, to determine ansformations taking place in he law of additivity applies alloys ranged in composition ried out in the temperature ease in the zine content of rease in a at all the temper- y was observed with rising ound to hold in the absence ge volume effect. The depen-	

10230 L 46976-56 0 ACC NR: AT6024934 the temperature ranges studied. Orig. art. has: 6 figures and 2 tables. SUE CODE: 11/ SUEM DATE: none/ ORIG REF: 002 • . rest Card 2/2

	$L l_{1697l_{1-66}} = EMP(k)/EMP(e)/EMP(e)/EMP(t)/EPI IJP(c) JH/JD/WE$	
niju, s	ACC NR: AT6024941 (1,N) SOURCE CODE: UR/2981/66/000/004/0277/0287	
	AUTHOR: Komissarova, V. S.; Kireyeva, A. F.; Stepanova, M. G.; Fridlyander, I. N.	
	ORG: nono (U 1 TITLE: Corrosion resistance of SAP material B+1	
	SOURCE: Alyuminiyevyye splavy, no. 4, 1966. Zharoprochnyye i vysokoprochnyye splavy (Heat resistant and high-strength alloys), 277-287	
	TOPIC TAGS: sintered aluminum powder, corrosion resistance	
	ABSTRACT: The corrosion resistance of SAP-1 sintered aluminum powder material in the atmosphere and in 3% NaCl was studied in the presence of 0.1% H ₂ O ₂ as a function of the content of aluminum oxidel (1/to 16%) and <u>iron</u> (0.01 to 1%) on rods and sheets. It was found to be close to that of <u>pure AOO</u> gluminum. The iron admixture has an undesirable effect on the corrosion resistance of SAP material, and the iron content should therefore be limited to 0.2%. Above this value, the elongation loss after 10 months of tests in the atmosphere amounts to an average of 25-30%. Studies of the electrochemical behavior of SAP as a function of the aluminum and iron content showed the data on the corrosion resistance to be in full agreement with the results of electrochemical measurements: iron is an active cathodic inclusion, and its content above 0.2% is not permissible; aluminum oxide can also be regarded as a cathodic inclusion,	-
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AUTHOR	Fridlyander,	, I. N.			41 Rtl
ORG: no		and the second sec	4		811
			21	. /	٠.
TITLE:	Proposed nume	erical <u>designati</u>	ion of aluminum al	Loys C	· •
SOURCE: (Heat re	Alyuminiyevy sistant and h	ye splavy, no. high-strength al	4, 1966. Zharopro Lloys), 288-290	ochnyye 1 vysokopro	chnyye splavy
TOPIC TA	GS: factory	marking, alumir	num alloy production	on, sintered alumin	numpander
ABSTRACT	: Because of	the confusion	existing in the p	resent designation	of aluminum
alloys,	a numerical a	system is propos	od which consists "O" designates bra	of seven main grou ands of pure alumin	ps. In a um, including.
sintanad	ະດາພາຍການ ກວະ	der: the group	with second digit	"1" includes alloy	8 OI LNG SYS
En and /	N −Cu−Li−Mn−Cd	1: with second d	ligit "3," Al-Si,	2," alloys of the s Al-Mg-Si, and Al-Mg	-31-Cu. Ine
second d	Noit "4" desi	ignates allovs i	nose main allovin	g elements are comp	onents that
group of	allovs with	second digit "	5" consists of mag	, Al-Mn, Al-Cr, A-W nalium-type alloys.	Tue group
with sec	ond digit "9"	" includes alloy	78 of Al-Zn-Mg and	Al-2n-Mg-Cu system	S. 21 - 1971 - 1981
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SUB CODE	E: 11/ SUBM	DATE: none			

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L 04198-67 EWT(m)/EWP(w)/T/E#P(t)/ETI IJP(0) JD/JH ACC NR: AP6028583 (N) SOURCE CODE: UR/0129/66/000/008/0011/0014	
Author: Fridlyander, I. N.; Gerchikova, N. S.; Zaytseva, N. I.	
ORG: none 8	
TITLE: A study of aging kinetics in the alloy V92Ts of the Al-Zn-Ng system $\frac{77}{27}$ $\frac{1}{27}$ $\frac{1}{17}$	
SOURCE: Netallovedeniye i termicheskaya obrabotka metallov, no. 8, 1966, 11-14	
TOPIC TAGS: aluminum alloy, aging process, electron microscopy, heat treatment, pre- cipitation hardening, mechanical property, stress corrosion	
ABSTRACT: Transmission <u>electron microscopy</u> was used to study the aging kinetics in V92Ts in order to determine the cause of strengthening and delayed fracturing. The alloy composition was: 3.1% Zn, 4.1% Mg, 0.65% Mn, 0.15% Zr, 0.2% Fe, 0.10% Si, and Al as remainder. The original sheet material (2 mm thick) was rolled to 50 µ, heat treated and etched in a hydrochloric-acetic acid electrolyte by the "window" method. After quenching and zone aging for periods ranging from 3 days to 1 month at 20°C, dis- location loops and isolated dislocations formed. The greatest loop density after quenching from 550°C corresponding to the greatest degree of vacancy supersaturation. With aging the dissolved atoms and vacancies agglomerated, and Guinier-Preston zones formed after 6 months at 20°C. The mechanical properties and stress corrosion resist- ance of V92Ts are given as a function of aging after water quenching from 450°C. The	
UDC: 621.785.54.783.784:669.5'71'72	

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ACC NR: AP6028583		4
greatest strength (σ_v =	50 kg/mm ² and $\sigma_{0,2} = 40 \text{ kg/mm}^2$)	was obtained after step aging
at 20°C for 2 months + 7 es of V92Ts and ATsM all T-phase (Al ₂ Mg ₃ Zn ₃) appe the matrix and had a lat	0°C 1000 hrs or after aging at 20° oys were shown after different aging at 20°C for 1 hr tice orientation of (110) _M {112},	These were coherent with These $a_{\rm T} = 14.16$ Å. Cohe-
rent particles of T-phas	e formed along grain boundaries as	fter supplementary aging at because the sequently aging at 200°C a
highly dispersed precipi	tation of T-phase occurred, which	to stress corrosion was caused
	14-4144 AF EMBIL DEDTICIES OT 190	
	eten aging-even with prolonged h	eat at 70°C. Orig. art. nas:
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3	I. 110956-66 EWT(m)/EWP(k)/EWP(e)/EWP(t)/ETT IJP(c) JH/JG/WW/JD ACC NRI AT6024930 SOURCE CODE: UR/2981/66/000/004/0202/0207	
	AUTHOR: <u>Palatnik</u> , L. S.; Fedorov, G. V.; Klyagina, N. S.; Krivenko, R. A.; <u>D'yachenko, S. S.</u> ; F <u>ridlyander, I. N.</u> (Doctor of technical sciences) 5	
	ORG: none 371	
	TITLE: Obtaining highly dispersed metal powders by vaporization in argon 27	ŕ
	SOURCE: Alyuminiyevyye splavy, no. 4, 1966. Zharoprochnyye i vysokoprochnyye splavy (Heat-resistant and high-strength alloys), 202-207	
•	TOPIC TAGS: metal powder, ultra fine powder, powder, production, vAPOR CONDENSATION ALUMINUM ROWDER ABSTRACT: Certain processes associated with the condensation of <u>metal vapors</u> in an inert-gas atmosphere have been investigated. It was found that in the argon atmo- sphere, condensation of metal vapors takes place in a limited space-condensation zone, The size of the condensation zone decreases with increasing vaporization rate and inert-gas pressure. On an experimental scale, ultrafine powders of several metals were obtained. The <u>magnesium</u> cadmium, and zinc powders had an average particle size of 0.001 mm; the particle size of copper and aluminum powders was 0.00005. The size of copper and aluminum particles does not depend very greatly on the variation in the rate of vaporization and the pressure of inert gas, Orig. att. has: 7 figures. [TD]	
	SUB CODE: 11 / SUBM DATE: none/ ORIG REF: 004/ ATD PRISS: 5057	
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CC NRI AR7004889 SOURCE CODE: UR/0276/66/000/009/G011/G011	
AUTHOR: Nuss, N. P.; Fridlyander, I. N.	
TITLE: Dilatometric study of binary alloy of the system A1-Zn	
SOURCE: Ref. zh. Tekhnologiya mashinostroyeniya, Abs. 9G77	
REF SOURCE: Sb. Alyumin. splavy. M., Metallurgiya, vyp. 4, 1966, 224-231	
TOPIC TAGS: binary alloy, alloy system, aluminum alloy, dilatometric study, zinc alloy ABSTRACT: A determination of the coefficient of linear expansion α of alloys in	
the Al-Zn system was carried out in the 20-500 C range on samples 60 mm in diameter and 900 mm in length, using a laboratory set up for the semicontinuous casting. It was determined that α increases gradually in all temperature intervals	
when the Zn content in the alloy is increased; by raising the temperature range in testing, an increase of α is observed (with no phase transformation) i the	
dependence of α on the composition of alloys does not appear to be additive. The original article has 6 figures and a bibliography of 2 reference items. Ye. Borisov. [Translation of abstract] [AM]	
SUB CODE: 13, 11/ ud 1/1 UDC: 669, 715'5	
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FRZDLYA NOV, L. T. FRIDLYANOV, L.T., insh.

Experience designing buildings for "integral"-type hydroelectric power plants. Gidr.stroi.26 no.12:14-17 D '57. (MIRA 10:12) (Hydroelectric power stations)

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ZAKHAROV, I.A.; FRIDLYANSKAYA, I.I.

Isolation of auxotrophic mutants of Chlorella by replica plating technique. Vest. LGU 18 no.9:159-160 '63. (MIRA 16:6) (Algae--Cultures and culture media) (Botany--Variation)

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IGNATOVA, T.N.; FRIDLYANSKAYA, I.I.

Symposium on problems of genetics in human pathology. TSitologiia 7 no.2:282-284 Mr-Ap '65. (MIRA 18:7 (MIRA 18:7)

ene (14

VAKHTIN, Yu.B.; IGNATOVA, T.N.; FRIDLYANSKAYA, I.I.; SHVEMBERGER, I.N.

Intensity of selection and the frequency of sharp karyotypic variations in the populations of somatic cells during clonal multiplication. TSitologiia 7 no.2:258-259 Mr-Ap '65. (MIRA 18:7)

1. Laboratoriya tsitologii zlokachestvennogo rosta Instituta tsitologii AN SSSR, Leningrad.

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VAKHTIN, Yu.B.; IGNATOVA, T.N.; FRIDLYANSKAYA, I.I.; SHVEMBERGER, I.N.

Changes in tumor cell populations caused by cloning. TSitologia 7 no.3:393-400 My-Je 165. (MIRA 18:10)

1. Laboratoriya genetiki opukholevykh kletok Instituta tsitologii AN SSSR, Leningrad.

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SOV/84-58-11-22/58

AUTHOR: Fridlyanskiy, Al.
TITIE: Moscow - Alma-Ata (Moskva - Alma-Ata)
PERIODICAL: Grazhdanskaya aviatsiya, 1958, Nr 11, p 11 (USSR)
ABSTRACT: The author describes the first Tu-104 round trip flight on the Moscow - Sverdlovsk - Alma-Ata route. The 3,500 km distance to Alma-Ata took 4 hours 20 minutss, the return trip to Moscow 4 hours 45 minutes, at an average speed of 860 km per hour. Personalities mentioned include pilot lat class lvan Jvanevich Frolov, acting chief of Moscow Administration of Aircraft Trensportation (Moskovskoye upravleniye transportnoy aviatsit), in charge of the flight, chief pilot Patr Vasil'yevich Soldatov, navigator lat class N. Nosov, compilot Aleksey Akimovich Ryakhovskiy. There are 2 photographs.

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(MLRA 7:1)

SKRIPCHENKO, I.K.; FRIDLYANDSKIY, A.I. Contraction of the second Protective inhibition following brain injury; observations from practice. Zhur.nevr.i psikh. 54 no.1:52-53 Ja '54. (Brain--Wounds and injuries) (Inhibition)

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"APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000513720001-2 CONTRACTOR PORTAL STATE AND A DECEMBER OF THE STATE OF T No. State FRIDLYANSKIY, A.I., mayor meditsinskoy sluzhby (Vladivostok) Case of hysteric hydrophobia. Vrach.delo no.5:521 My '57. (MIRA 10:8) (HYSTERIA) 1.14





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L 04585-67 EWT(1) SCTB DD ACC NR: AP6033154 SOURCE CODE: UR/0238/66/012/005/0697/0699	
ACC NR: AP6033154 SOURCE CODE: UR/0238/66/012/009/009/	
AUTHOR: Morozov, O. P.; Fridlyans'kyy, V. Ya.	
ORG: <u>Physiology Institut im. O. O. Bohomolets</u> , Academy of Sciences URSR, Kiev (Instytut fiziolohiyi Akademiyi nauk URSR)	
TITLE: Plethysmographic method for recording respiration in white rats	
SOURCE: Fiziolohichnyy zhurnal, v. 12, no. 5, 1966, 697-699	
TOPIC TACS: plethysmography, biologic acceleration effect, oxygen consumption, respiratory system, bioinstrumentation, rat, animal experiment	
ABSTRACT: A detailed description is given of the apparatus and procedures for a plethysmographic study of respiration in white rats during centrifugation. The apparatus consists of a cylindrical sealed chamber (28 cm long and 5.5 cm in diameter), a centrifuge in which the plethysmographic chamber is located, a recording unit, and linkage. The chamber has a stand to which the rat is fastened. The respiratory system of the rat is connected by tracheotomy to the air cutside the chamber and has no connection with the chamber space. A general setup of the apparatus and two types of the plethysmographic chamber are shown in Figs. 1 and 2.	
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accuracy	proposed apparatus, the air intake and expiration may be most of 0.25 ml. Orig. art. has: 2 figures.	easured with an
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ard 3/3		
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FRIDMAN, A.

Mar 52 USSR/Electronics - Radio Amplifiers "An Amplifier for Reproduction of Phonograph Records," A. Fridman

"Radio" No 3, p 38

Describes a 3-w amplifier using 4 tubes, a 5Ts4S (524), a 62h8, a 652S, and a 6P3S. The amplifier boosts the low-frequency signals to compensate for their attenuation in recording and cuts off frequencies above 4-6 kc to eliminate needle noise.

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ACCESSION NR: AP5002362	22/0053/64/000/012/0639/0645
AUTHOR: Tanach, V.; Cojocaru, Z.; St	anciulea, L.; Fridman, A.; David, B.
TITLE: New developments in the field	of perminvar ferrites and their applications
SOURCE: Przeglad elektroniki, no. 12	25
TOPIC TAGS: ferrite, perminvar ferri permeability, quality factor	te, temperature dependence, field dependence,
purpose of establishing the connectio properties of perminvar ferrites. Th compositions, and the best results we	zinc ferrites with cobalt additive for the on between the production technology and the se tested ferrites covered a wide range of are obtained with ferrites in which the oxide of geothite. The ZnO/NiO ratio ranged from maintained constant. The resultant ferrites
0 to 2.45, and the Fe ₂ O ₃ excess was m had initial permeabilities up to 200 to 200 Mc. The initial permeability	G/Oe and very low losses (Q up to 2000) up was greatly affected by the sintering tem- field. Several applications of such per-

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L 22605-65 ACCESSION NR: AP5002362		2
minvar ferrites are discussed and television coils and filt lems concerning the mechanism influence of the temperature the question of the applicabi miniature circuits remains op ASSOCIATION: <u>Electronic Ente</u> Institute, Bucharest. SUBMITTED: 15Jul64	ers at various frequencies. of production of the permin and of the external field re lity of such ferrites for mi en. Orig. art. has: 4 tabl	Some theoretical prob- var structure and the main to be solved, and niature and micro- es.
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FRIP MAN, A.

RUMAN LA/Vi	.ro]	logy - Viruses of Man and Animals. D-3
Abs Jour	:	Ref Zhur - Biologiya, No 7, 10 April 1957, 26131
Autho:	:	Elias, Brukner, Marinesku, Brikman, Fridman, Teodoresku, Spiner.
Inst	:	
Title	;	Clinical Forms of Infectious Hepatitis among Children and Their Relation to Age.
Orig Pub	:	Pediatria, 1956, <u>5</u> , No 2, 168-183
Abst	:	No abstract.

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Fumania/Virology. Viruses of Man and Animals F, Abs Jour : Ref Thur-Biol., No 13, 1953, 57343 : Aderca I., Fridman A., Ianconescu M. Author : Not given Inst : The Growing of the Virus MM of Encephalomyo-Title carditis in Rotating Test Tubes : Studii si cercetari inframicriobiol., microbiol., Orig Pub si parazitol., 1957, 8, No 1, 49-55 Abstract : The virus which was cultivated in the ruscles and skin of a mouse embryo was found to have a cytopathogenic effect. The initial dilution of the virus was 5.10⁻⁵, the final--5.10⁻¹. By titrating the virus of the final passage in the brain of grown mice it was shown that the viru-lence of the virus decreases, a fact which in the opinion of the authors bears witness to the Card 1/2

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FRIDMAN, A. (A)

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Arifmetika. BSE, T. 3 (1926), 338-346.

SO: Mathematics in the USSR, 1917-1947 edited by Jurosh, A. G. Markushevich, A. L. Rashevskiy, P. K. Moscow-Leningrad, 1948

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FRIDMAN, A.A. 24741. FRIDMAN, A.A. Ob Odnom Istolkovanii Ponyatiya (Meshdu) I O Znachenii Aksiony Pasha V Gilbetovoy Systeme Aksion. Uchen. Zapiski Kazakh. Gos. Un-ta. Im Kirova, XII, 1949, S. 18-29--Bibliogr: 5 Nazv. SO: Letopis' No. 33, 1949