





APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R00051872(





Ipatov, P.M., Candidate of Technical Sciences, and Sipaylov, G.A., Candidate of Technical Sciences. 110-6-4/24 A simplified thermal ventilation calculation for hydro-

TITIE: A simplified thermal ventilation calculation for hydrogenerators. (Uproshchennyy teplovoy ventilyatsionnyy raschet gidrogeneratorov.)

AUTHOR:

Card 1/2

PERIODICAL: "Vestnik Elektropromyshlennosti" (Journal of the Electrical Industry) 1957, Vol.28, No.6, pp. 6-10 (U.S.S.R.)

ABSTRACT: The Scientific Research Institute of the Ministry of Electro-technical Industry (NII MEP) has done a great deal of work on the experimental determination of the temperature, the flow and speed of air in various parts of the air ducts of existing hydro-generators. This material may be used to introduce certain corrections into the procedure of thermal calculations.

The present article proposed a procedure of thermal calculations based on the method of the equivalent thermal circuit and also a simplified procedure for determining the air flow. The article first considers at some length thermal calculations on the stator of a hydro-alternator. The information which is required for the purposes of the calculation is stated and the necessary equations are formulated. Heating of the rotor is considered much more briefly. The second part of the article is concerned with determin-

A simplified thermal ventilation calculation for hydrogenerators. (Cont.) 110-6-4/24

ation of the air flow. A formula is given for the head in the closed ventilating system. In order to compare the ventilating systems of different generators it is convenient to select a single characteristic section of the air duct, for instance, the section of the air gap, and to relate all the other sections to it. This is done in the article. Some of the factors that appear in the equations are difficult to determine analytically and simplified procedures for finding them are given. The procedure here described was used to make thermal calculations on a number of existing hydro-alternators. The theoretical and practical test results are compared in a table which shows that there is good agreement between the two.

Card 2/2 There are 3 figures and 4 references, 3 of which are Slavic.

ASSOCIATION: Elektrosila Works. (Zavod "Elektrosila")

SUBMITTED: December 24, 1956.

AVAILABLE:

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[PATdv, P.M. IPATdv, P.M., inzh.; KHUTORETSKIY, G.M., inzh. APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R000 Rated voltage of high capacity generators. Vest.elektroprom. 28 no.8:14-17 Ag '57.
(MIRA 10:10)

1.Zavod "Elektrosila."

(Electric generators)

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AUTHOR :	<u>Ipatov, P.</u> M., Candidate of Technical Sciences	SOV/105-58-7-2/32
TITLE:	Slot-Ripple Frequency Currents in th Additional Losses of an Alternator chastoty v dempfernoy obmotke i dobs generatora)	(Toki zubtsovoy
PERIODICAL:	Elektrichestvo, 1958, Nr 7, pp. 7 -	11 (USSR)
ABSTRACT: Card 1/3	The currents parallel to the transv the additional losses caused by the here. First an alternator with slan currents and the losses produced by the magnetic flux at t_2 =t with a wh and phase and with a damping windin mined. The formulae for the total c damping cage, for the maximum curre pole-length at x=0 and for the loss rods) at 75°C are determined. Then stator slots is investigated. In the occurs between the ends AB of the a	se currents are investigated ting slots is described. The them by the pulsation of ole number of slots per pole g with open slots are deter- urrent in the rods of the nt in the steel per 1 cm es in the copper-rods (armor an alternator without slanting is case, a drop of potential

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SOV/105-58-7-2/32 Slot-Ripple Frequency Currents in the Damping Winding and the Additional Losses of an Alternator in the armor rods is determined according to formula (17). After the determination of the currents in the rods, the losses may be determined according to formula (14). The problem of the generation of currents in the steel between the armor rods of the adjacent poles in the case of a stator-slot-slanting per slot pitch is of great importance. These currents may reach considerable values and lead to a destruction of the poles. In order to avoid sparking, a sufficiently reliable contact between the rods and the steel of the poles must be guaranteed. There are 4 figures and 2 references, 1 of which is Soviet. ASSOCIATION: Zavod "Elektrosila" im. Kirova ("Elektrosila"-Works imeni Kirov) SUBMITTED: January 21, 1958 Card 2/3

CIA-RDP86-00513R00051872

AUTHOR:	SOV/110-58-8-20/26 Ipatov, P.M. (Candidate of Technical Science)
TITLE:	Currents in the Damper-winding Bars of a Synchronous Machine with Asynchronous Fields (Toki v sterzhnyakh dempfernoy obmotki sinkhronnoy mashiny pri asinkhronnykh polyakh)
PERIODICAL	L: Vestnik Elektropromyshlennosti,1958,Nr 8,pp 68-70 (USSR)
ABSTRACT: Card 1/3	The damper-windings in salient-pole synchronous machines that may be used for asynchronous starting or for retar- dation are made short-circuited, but there are bars only in the pole-pieces. As there are no bars in the spaces between the poles, the current distribution in the damper- winding bars is not uniform during asynchronous operation. The bars near the edge of the pole-piece are most heavily loaded. In a published method of calculating the current distribution in this case it is assumed that the outer bars take up all the uncompensated part of the sinusoidally distributed linear load of the stator, which is rotating relative to the rotor. The actual current distribution is more favourable than this because of leakage of the damper-winding. This article describes a simplified

SOV/110-58-8-20/26 Currents in the Damper-winding Bars of a Synchronous Machine with Asynchronous Fields

approximate method of calculating the current distribution in the bars during asynchronous running or asymmetric loading. The method supposes that the space between the poles of the machine also contains damper-bars, so that the current distribution in the bars, including the imaginary bars, may be considered as sinusoidal in the longitudinal and cosinusoidal in the transverse axis. It further supposes that an e.m.f. is applied to the imaginary bars which sets up in them currents equal in .magnitude and opposite in phase to the initial currents; these additional currents would circulate through the real bars mounted on half of the pole-piece. The superposition of the two hypothetical current distributions corresponds to the real distribution. A mathematical analysis of the case is given on this basis and equations are derived for the additional current in each bar and the normal current. Theoretical and experimental

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Cureents Asynchron	SOV/110-58-8-20/26 ous Fields
	current distributions are compared in Fig 3 and agreement is seen to be good. Overloading of the outer bars is greater if the leakage is small and if the arc occupied by damper-bars is small. A numerical worked example of the calculations is given.
	There are 3 figures and 1 German reference.
SUBMITTED:	July 16, 1957
	1. Electric motorsCircuits 2. Electric motorsDesign 3. Mathematics Applications
ard 3/3	
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 V.V. (Engineer) TITLE: Current During Internal Short-circuits in Wave Windings of Synchronous Machines (Toki pri vnutrennikh korotkikh zamykaniyakh v volnovykh obmotkakh sinkhronnykh mashin). PERIODICAL: Vestnik Elektropromyshlennosti, Nr.11, 1958, pp.20-26, (USSR) 	AUTHORS:	SOV/110-58-11-5/28 Ipatov, P.M. (Cand.Tech.Sci.) and Dombrovskiy,
of Synchronous Machines (Toki pri vnutrennikh korotkikh zamykaniyakh v volnovykh obmotkakh sinkhronnykh mashin). PERIODICAL: Vestnik Elektropromyshlennosti, Nr.11, 1958, pp.20-26, (USSR) ABSTRACT: When short-circuits occur in the wave windings of a synchronous machine operating in parallel with a large power system, the currents in the two parts of the winding are in opposite directions. Therefore, two bars of the same phase in a single slot may carry currents in opposite directions, as shown in Fig.1, and the resultant mechanical forces due to these currents may cause damage. The currents in question are calculated with the simplifying assumptions that the winding has no parallel branches, and that the machine is connected to an infinitely large system. For further simplification,		V.V. (Engineer)
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Card 1/4 reactances due to higher harmonics in the field curve, and		resultant mechanical forces due to these currents may cause damage. The currents in question are calculated with the simplifying assumptions that the winding has no parallel branches, and that the machine is connected to an infinitely large system. For further simplification,
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SOV/110-58-11-5/28 Current During Internal Short-circuits in WaveWindings of Synchronous Machines. also the ohmic resistance of the winding, are neglected. A symmetrical internal short-circuit, illustrated in Fig.2, is first considered because although it is hardly likely to occur it must be investigated in order to analyse other forms of internal damage. A schematic diagram of the winding with internal short circuit is drawn in Fig. 3. Calculations are then made of the inductances of the two parts of the winding; expressions for the self-inductance are given in equations 4 and 5 and for the mutual inductance in equation 6. Equations are then obtained for the current in the different parts of the winding. The case of asymmetric short-circuits is then considered, with reference to Fig.5. In examining single- and twophase short-circuits, which are the most common forms, it is assumed that during the short-circuit a symmetrical system of reactances is formed in the windings. This is always true of single-phase short-circuits, but for two-phase short-circuits the same number of turns should be shorted in both phases. If these assumptions are made, Card 2/4

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sov/110-58-11-5/28 Current During Internal Short-circuits in Wave Windings of Synchronous Machines. the theory of symmetrical components can be used to calculate the currents and voltages. Equivalent circuits for various types of symmetrical internal short-circuit are depicted in Fig.6. Expressions are then derived for the symmetrical components of current in the different It is concluded that single-phase internal shortcases. circuit currents are never greater than the currents during three-phase short-circuits. Curves are plotted in Fig.7 for the initial values of current in the two parts of the winding for various positions of shortcircuit in hydro-alternators with known reactance values. These are averaged curves calculated from the formula given, and can be used to calculate the currents and stresses between winding bars during internal shortcircuits. A table gives values of short-circuit currents calculated by the method given in this article and values calculated by the previous methods for a hydro-alternator of known inductances. It may be seen from the curve Card 3/4

SOV/110-58-11-5/28 --Current During Internal Short-circuits in Wave Windings of Synchronous Machines. and the table that the results can explain certain types of failures that occur in these machines. There are 7 figures, 1 table and 7 references, of which 3 are Soviet and 4 English. SUBMITTED: October 2, 1957. 1. Generators--Operation 2. Electric circuits--Failure 3. Electric currents--Performance Card 4/4s firm

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IPATON, P.M.	
110-1-1/19	
AUTHOR: Rozovskiy, Yu.A., Candidate of Technical Sciences, Salita, P.Z., Engineer, and Ipatov, P.M. Candidate of Technical Sciences.	
TITIE: On the Constants of Hydro-alternators for Use with Long- distance Transmission Lines with Synchronous Compensators (O parametrakh gidrogeneratorov dlya dal'nikh elektro- peredach s podpornymi sinkhronnymi kompensatorami)	
PERIODICAL: Vestnik Elektropromyshlennosti, 1958, Vol.29, No.1, pp. 1 - 4 (USSR).	
ABSTRACT: When hydro-electric stations feed relatively short transmission lines, stability is enhanced by reducing the reactance of the generators and increasing their inertia. However, when the lines are so long that stability cannot be achieved without special arrangements (such as the use of series capacitors or synchronous compensators), the above measures may be less effective. Since 1955, the NIIPT, together with the staff of the Elektrosila Works and the Electrical Machines Faculty of the Leningrad Polytechnical institute (Leningradskiy politekhnicheskiy institut), have been investigating the stability of long-distance transmissi lines and the rational selection of characteristics for hydro-alternators and synchronous condensers. This article	ion

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110-1-1/19 On the Constants of Hydro-alternators for use with Long-distance Transmission Lines with Synchronous Compensators gives a brief outline of the main results of work relating to the Stalingrad Hydro-electric Station-Moscow transmission line. The stability of this line was investigated using the electro-dynamic model, the circuit and main characteristics of which are given in an article by Rokotyan in Elektricheskiye Stantsii, 1956, No.8. First, the influence on the steady-state stability of the installed output and location of the synchronous condensers was determined. If the improved values of hydro-alternator characteristics were used and if synchronous condensers with a total capacity of 280 MVA were installed in the first substation, an adequate steady-state stability limit is achieved even without series capacitors. This arrangement was accordingly made the basis of further work. Stability limits with various values of generator reactance are tabulated and it will be seen that the generator reactance has relatively little influence. Increase in the reactance of one section of the transmission system can largely be compensated by appropriate adjustment of the regulators. Card2/4 To increase the permissible time for disconnecting a fault,

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110-1-1/19 On the Constants of Hydro-alternators for Use with Long-distance Transmission Lines with Synchronous Compensators the inertia constant of the Stalingrad generators was selected as 16 sec. As it was not proposed to brake the generators, this solution was correct. However, electrical and mechanical braking is now proposed to improve the stability of the power station and extra inertia becomes necessary. Work done in the Institute by Candidate of Technical Sciences Ye.A. Marchenko showed that with suitable electrical braking of the generators, dynamic stability can be ensured with an inertia constant of the order of 10 sec. The cost and size of generators having extra reactance and inertia was calculated. The effect of the direct-axis transient reactance on the cost is most marked. An approximate formula is given for the relationship between this value and the weight and cost of the generator. The relationship between the machine constant and the transient reactance for a generator of 123.5 MVA, 13.8 kV and 68.2 r.p.m. is given in Fig.2. The relationship between the linear load and the transient reactance for a pole-pitch of 51 cm is given in Fig. 3. For a hydro-alternator of the type in question, the normal inertia for the given reactance is of the order of 8 or 9 sec; for an Card3/4

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 110-1-1/19 On the Constants of Hydro-alternators for Use with Long-distance Transmission Lines with Synchronous Compensators inertia constant of 15 - 16 sec., the rotor has to be made heavier. The inertia may be reduced by using high-tensile steel for the rotor or by other measures. If the Stalingrad generators are designed for normal inertia, they will weigh about 17% less than the current design. Manufacture and erection will be simpler and cheaper. Hydro-alternators with specially low reactance and high inertia are accordingly not advised for the Stalingrad-Moscow type of installation, because adequate steady-state and trans- ient stability can be achieved by appropriate excitation control of the synchronous condensers, combined with braking of the alternators. The power-factor of the alternators can be raised to 0.95. There are 3 figures and 5 Russian references. ASSOCIATION: MILPT - NAUCHNO-ISSLEDOUNTEL'SHY INSTITUT PESTRYANNOGO TOKA. SUBMITTED: January 18, 1957 AVAILABLE: Library of Congress Card 4/4 							
 On the Constants of Hydro-alternators for Use with Long-distance Transmission Lines with Synchronous Compensators inertia constant of 15 - 16 sec., the rotor has to be made heavier. The inertia may be reduced by using high-tensile steel for the rotor or by other measures. If the Stalingrad generators are designed for normal inertia, they will weigh about 17% less than the current design. Manufacture and erection will be simpler and cheaper. Hydro-alternators with specially low reactance and high inertia are accordingly not advised for the Stalingrad-Moscow type of installation, because adequate steady-state and trans- ient stability can be achieved by appropriate excitation control of the synchronous condensers, combined with braking of the alternators. The power-factor of the alternators can be raised to 0.95. There are 3 figures and 5 Russian references. ASSOCIATION: NIIPT - NAUCHNO - ISSLEDOWNTEL'SKIY INSTITUT POSTEYANNOGO TOKA. SUBMITTED: January 18, 1957 AVAILABLE: Library of Congress 							
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Card 4		ission inerti- heavie steel genera about erect: Hydro- inerti- type (ient s contro of the be rai refere ATION: TED:	ission Lines wi inertia consta heavier. The steel for the generators are about 17% less erection will Hydro-alternat inertia are ac type of insta- ient stability control of the of the alternat be raised to 0 references. ATION: NIIPT - TED: January	ission Lines with Synchron inertia constant of 15 - heavier. The inertia may steel for the rotor or by generators are designed f about 17% less than the c erection will be simpler Hydro-alternators with sp inertia are accordingly r type of installation, bec ient stability can be ach control of the synchronou of the alternators. The be raised to 0.95. There references. ATION: NIIPT - NAVCHNO-ISSLE FED: January 18, 1957	ission Lines with Synchronous Compens inertia constant of 15 - 16 sec., th heavier. The inertia may be reduced steel for the rotor or by other meas generators are designed for normal i about 17% less than the current desi erection will be simpler and cheaper Hydro-alternators with specially low inertia are accordingly not advised type of installation, because adequa ient stability can be achieved by ap control of the synchronous condenser of the alternators. The power-facto be raised to 0.95. There are 3 figu references. ATION: NIIPT - NauchNO - ISSLEDOUNTEL'SLY INSTIT TED: January 18, 1957	Constants of Hydro-alternators for Use with Lon ission Lines with Synchronous Compensators inertia constant of 15 - 16 sec., the rotor has heavier. The inertia may be reduced by using h steel for the rotor or by other measures. If t generators are designed for normal inertia, the about 17% less than the current design. Manufa erection will be simpler and cheaper. Hydro-alternators with specially low reactance inertia are accordingly not advised for the Sta type of installation, because adequate steady-s ient stability can be achieved by appropriate e control of the synchronous condensers, combined of the alternators. The power-factor of the al be raised to 0.95. There are 3 figures and 5 F references. ATION: NIIPT - NAUCHNO-ISSLEDOUNTEL'SLIP INSTITUT POSTEYANNOGO IED: January 18, 1957	Constants of Hydro-alternators for Use with Long-distance ission Lines with Synchronous Compensators inertia constant of 15 - 16 sec., the rotor has to be mad heavier. The inertia may be reduced by using high-tensil steel for the rotor or by other measures. If the Staling generators are designed for normal inertia, they will wei about 17% less than the current design. Manufacture and erection will be simpler and cheaper. Hydro-alternators with specially low reactance and high inertia are accordingly not advised for the Stalingrad-Mo type of installation, because adequate steady-state and t ient stability can be achieved by appropriate excitation control of the synchronous condensers, combined with brak of the alternators. The power-factor of the alternators be raised to 0.95. There are 3 figures and 5 Russian references. ATION: NIIPT - NAUCHNO - isstedownTel'ship institut posteyAnNode TokA. FED: January 18, 1957

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SOV/110-59-2-6/21 Additional Stator Iron Losses due to Pulsations of a Magnetic Flux Caused by the Damper Winding important in medium and small motors but that at high speeds machines with a large number of slots per ϕ olo and phase show small additional stray losses. Card 2/2There are 2 Soviet references. SUBMITTED: February 6, 1958





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IPATOV, Pavel Mikhaylovich, kand.tekhn.nauk Resistance of the circuit of a double and triple-throw armature winding for equalizing mrrents. Izv.vys.ucheb.zav.; elektromekh. (MIRA 15:2) 5 no.1:28-36 '62. 1. Ispolnyayushchiy obyazannosti dotsenta kafedry elektricheskikh mashin Severo-Zapadnogo zaochnogo politekhnicheskogo instituta. (Electric machinery--Windings) North west Conceptor Bol tech Sust. machinso

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IPATOV, P.M., kand.tekhn.nauk; KAZOVSKIY, Ye.Ya., doktor tekhn.nauk; KULIKOV, N.V., inzh.; LYUTER, R.A., doktor tekhn.nauk Research conducted at the Leningrad branch of the All-Union Scientific Research Institute of Electromechanics and the S.M. Kirov "Elektrosila" factory. Vest.elektrprom. 33 no.4:3-8 (MIRA 15:4) Ap '62. (Electric machinery)

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DOMBROV	VSKIJ, V.V. [Dobrovskiy, V.V.]; <u>IPATOV, P.M.</u> ; KAPLAN, M.J.; PINSKIJ, G.B. [Pinskiy, G. ^B .]	-
	Large hydroaltenators in the Soviet Union. El tech obsor 52 no.2:58-63 F '63.	
	1. Elektrosila, Leningrad.	



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"APPROVED FOR RELEASE: Thursday, July 27, 2000

IPATOV, Pavel Mikhaylovich; DANILEVICH, Ya.B., otv. red. [Multiplex armature windings of d.c. electric machines] Mnogokhodovye obmotki iakorei elektricheskikh mashin postoiannogo toka. Moskva, Nauka, 1965. 60 p. (MIRA 18:4)

CIA-RDP86-00513R00051872



IPATOV, P.M., kand. tekhn. nauk Performance of a d.c. machine with a multiplex armature winding under load. Elektrotekhnika 35 no.10:54-57 0 '64. (MIRA 17:11)

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AUTHOR:	Ipatov, P. M				35
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nators In cert harmoni For ins cate th mention	is discussed f ain cases, the cs could not b tance, use of e design of th ed that the al will have three and large coil	rom the standp usual methods e applied effi a fractional n e water-coolin ternator desig	oint of the a. available for ciently to the umber of state g system. In ned for the K e per phase.	id pole shoes in the reduction of design of machinary or slots rander in this connection rasnoyarsk Hydro- In case of heavy call for a high j	of these Ines. Intri- , it was -Power y satur-

ACC NR AT6000052 sion in designing and fitting the damper windings. It seems, therefore, that the use of solid poles or solid pole shoes without damper windings on become a radical method for suppressing the slot harmonics in water- wheel-type alternators. As to the additional losses in solid shoes, they are in many cases, not greater than in the laminated poles. These losses can be reduced by 50 to 70% in solid shoes with a corrugated sur- face. The expensive machinery and finishing of solid pole surfaces can partly be avoided by using clean surfaced castings. The author states that the trend developed by the "Uralelektroapparat" plant toward the use of solid poles appears to be a right decision. In order to investi- gate the effect of solid poles upon the emf wave shape, the author pre- sented a brief analysis of the currents induced in solid poles by the pulsating magnetic flux. The damper factor was also determined. The formulas for induced wave lengths and amplitudes were given for machines having integer number of stator slots per pole per phase. By using standard vector and equivalent circuit diagrams the damper factor for the transversal axis was formulated. The flux penetration depth was also expressed by a formula. For a better illustration, an example of calcu- lation for a DC-85-10-4 synchronous machines of 745 kva was presented. The calculations were made for the laminated poles with damper windings as well as for the solid poles without damper windings but with a short- tard 2/3		
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NIKOLAYEVSKIY, Te.Ta., insh.; ETDEL'NANT, L.B., inzh.; DAVYDOV, A.M., insh.; SIMACHEV, L.V., red.; BATENCEUX, A.H., insh.; red.; IPATOV, P.P., insh., red.; RIEGUY, V.A., insh., red.; PELSKUL, N.I., insh., red.; PITERSKOV, N.I., red.; SUBOY, L.B., red.
[Instructions for industrial safety measures in the assembly of technological equipment and piping] Instruktivnye ukaraniia po tekhniks besopasnosti pri montashe tekhnologicheskogo oboudovaniis i truboprovodov. Isd.2, perc. i dop. Noskva, TSentr. biuro tekhn.informstail, 1959. 160 p. (MIRA 13:6)
1. Bassia (1917- R.S.F.S.R.) Ministerstvo stroitel'stva. Glavmstallurgmontash. 2. Glavnyy inzhemer Glavmatallurgmontazha Winisterstva stroitel'stva REFSR (for Simachev). (Industrial safety)

RAYKO, V.V., nauchnyy sotrudnik; NIKBERG, I.M., nauchnyy sotrudnik; KHODAK, A.N., nauchnyy sotrudnik; NEVEDUSHCHIY, A.I., nauchnyy sotrudnik; VOLKOV, Ya.R., nauchnyy sotrudnik; PEYCHEV, G.P., otv. red.; IPATOV, P.P., red.; SHULYATSKIY, D.M., red.; BURKSER, L.D., red.; BALASEVICH, Yu.Yu., red.; SVETCHENKO, V.N., red.; ERYLOVSKIY, A.P., red.; SINYAVSKAYA, Ye.K., red.izd-va; ANDREYEV, S.P., tekhn.red.

[Regulations for operating the mechanical equipment of rolling mills] Pravila tekhnicheskoi ekspluatatsii mekhanicheskogo oborudovaniis prokatnykh tsekhov. Khar'kov, Gos.nauchno-tekhn.izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1959. 247 p. (MIRA 12:9)

1. Moscow. Vsesoyuznyy nauchno-issledovatel'skiy insitut organizatsii proizvodstva i truda chernoy metallurgii. 2. Vsesoyuznyy nauchno-issledovatel'skiy institut organizatsii proizvodstva i truda chernoy metallurgii (VNIIOChERMET) (for Rayko, Nikberg, Khodak, Nevedushchiy, Volkov). 3. Otdel glavnogo mekhanika byvshego Ministerstva chernoy metallurgii SSSR (for Ipatov, Shulyatskiy). 4. Zavod imeni Dserzhinskogo (for Burkser, Balasevich). 5. Zavod imeni Kirova (for Svetchenko). 6. Zavod imeni Voroshilova (for Krylovskiy). (Bolling mills--Equipment and supplies)

GINZBURG-SHIK, Lev Davidovich; IPATOV, P.P., insh., retsenzent; POLOZHINTSKY, V.R., insh., Fed.; TSOPIN, K.G., insh., red. izd-va; STROGANOV, L.P., inzh., red.izd-va; MODEL', B.I., tekhn.red. [Installation of boiler systems; brief reference book] Montash kotlosgregatov; kratkos spravochnos posobie. Moskva, Gos.nauchnotekhn.isd-vo mashinostroit.lit-ry, 1960. 231 p. (MIRA 13:11) (Boilers)

MIKHEYEV, Il'ya Il'ich; IPATOV, P.P., inzh., nauchnyy red.; SHIROKOVA, G.M., red. izd-va; OSENKO, L.M., tekhn. red. [Assembly of centralized systems of lubrication and hydraulic and pneumatic drives] Montazh tsentralizovannykh sistem smazki, gidravliki i pnevmatiki. Moskva, Gos. izd-vo lit-m po stroit., arkhit., i stroit. materialam, 1961. 240 p. (MIRA 14:11) (Lubrication and lubricants) (Oil-hydraulic machinery) (Pneumatic machinery)



IPATOV, F. F. <u>Ipatov, F. F.</u> "Analysis of the stud activity of the Gil'deyts stallion and further selection work with his descendants," Trudy Stavrop. s.-kh. in-ta, Issue 3, 191A, p. 267-86 So: U-3566 15 March, (Letopis 'Zhurnal 'nykh Statey, No. 13, 1949)

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"APPROVED FOR RELEASE: Thursday, July 27, 200 CIA-RDP86-00513R00051872
IPATOV, P. P.
20930 Ipatov, P. P. Voprosy podlotovki kadrov i nauchno-issledova tel' skaya
rabota po molochnomu delu v zooveterinarnykh . Sbornik dokladov Pervoy Vsesoyuz.
Konf-tsii po moloch. delu. M., 1949, s. 6-15
S0: LETOPIS ZHURNAL STATEY - Vol. 28, Moskva, 1949

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USSR/Forn initals. Horses.		
Abs Jour: Ref Zhur-Biol., No 20, 1958, 92567.		
Author : Ipatov, P.P		
tute.		
Orig Pub: Tr. Vses. skh. in-ta zaochn. obrazovaniya, 1957, vyp.	· ·	
Orig Pub: 4r. Vses. 5. 41. 1, 103-134.		
Abstract: It was established during the investigation of pul- nonary caseous metabolism in trotting horses that the pulse rate (PR) and respiration rate (R) are lower in horses with a speed of 2 min. 25 sec. and slower. Inmediately after a race at a distance of 1600 meters the PR reached 91 and 114 respectively while R attained		
Card : 1/3		

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USSR/Farm Animals. Horses. Abs Jour: Ref Zhur-Biol., No 20, 1958, 92567.

55 and 77. The inhalation intake was 6.6 and 6.0 liters, after 1 hour it was 4.6 and 3.2 liters, after 2 hours 4.5 and 3.8 liters respectively. The O₂ requirement for the fastest trotters was 0.211 liters (reater at rest than for the merely fast trotters, and inmediately after the race, one hour and two hours after racing, the greatest O₂ need was found in horses having the least speed. The O₂ utilization factor was higher in the fast horses both at rest and after running than in the slower ones, although the CO₂ acunulation factor was less in the former than in the latter. The oxygen restoration process lasts for two hours after the race in the slower trotters. The process is completed somer in faster trotters. The oxygen supply to tissues occurs at the expense of

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USSR/Farm Animals. Horses.

- A

Abs Jour: Ref Zhur-Biol., No 20, 1958, 92566,

cardiovascular system was at peak functioning capacity, the average DP scarcely varied before and after racing. The nost characteristic DP cuve may be regarded as the one where the curve comes to rest in the shortest possible time and its drop before coning to rest at the bottom does not exceed 10%. Blood pressure norms are given for trotters undergoing training at the track.

Card

: 2/2

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USSR/Farm Anima	ls - Horses.	7
Abs J ^O ur :	Ref Zhur - Biol., No 7, 1958, 3090	1
Author Inst Title Orig Pub Abstract	<pre>Ipatov P.P. Changes of the Blood Composition i Tests. (Izmeneniya v sostave krovi u ryst ispytaniyakh). Tr. Mosk. vet. akad., 1957, 19, N During the summer season of the r Trotters and 10 Russian Trotters indexes were studied: Hb, erythic count, reserve alkalinity, and 1 It was demonstrated that identic (test run of 1,600 m.) appears t (causing sharp variations in the count is then for the Russian)</pre>	o 1, 112-131. running tests on 10 Orel , the following blood rocyte and leukocyte eukocytal formula. al muscular exertion o be much more straining blood indexes) for the
	(causing sharp variations in the Orel Trotter than for the Russia	n Trotter.
Card 1/2	- 11 -	

est in an

USSR/Farm Anime	Ref Zhur - Biol., No 7, 1958, 30907	
Abs Jour :	The difference in the blood picture between the lively and quist Trotters within the breed groups was also studied. The quiet Trotters are distinguished by a lower index of reserve alkalinity, by a rapid spendin of it, and by a slower process of its restoration.	
Card 2/2		

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IPATOV, Petr Platonovich, inzh.; FINKEL', Abram Froymovich, inzh.; ZALENSKIY, V.S., inzh., nauchn. red.; PEREVALYUK, M.V., red.; SHEVCHENKO, T.N., tekhn. red. [Rigging operations and hoisting and conveying machinery used in assembling] Takelazhnye raboty i montazhnye pod"emno-transportnye mekhanizmy. Moskva, Stroiizdat, 1964. (1964 17:2) 246 p.



IPATOT, S.S. [Coordinate boring machines in precision instrument making] Koordinatno-rastochnye stanki v tochnom priborostroenii. Moskva, Oborongis, 1954. 196 p. (NLBA 7:11D)

CIA-RDP86-00513R00051872

IPATOV. S.S.; YERMILOV, Ye.F., red.; TIKHONOV, V.I., red.; GLADKIKH, N.N., tekhn. red. [Jig boring machines used in the precision manufacture of instruments] Koordinatno-rastochnye stanki v tochnom priinstruments] Koordinatno-rastoennye stanic borostroenii. Pod red. E.F.Ermilova. Moskva, Oborongis, (MIRA 16:9) 1954. 195 P. (Drilling and boring machinery) ١ (Instrument manufacture)

"APPROVED FOR RELEASE: Thursday, July 27, 200 CIA-RDP86-00513R00051872 <u>IPATOV, V.;</u> NOVIK, G.; RUSANOV, B.; STEPANOV, Yu.; LANSKOY, V.; IVANOV, A. Sports news. Kryl. rod. 15 no.7:27 Jl ¹⁶4. (MIRA 18:1)

SOV/120-58-2-22/37

AUTHORS: Ipatov, V. A., Pakhomov, L. P. TITLE: A Photoelectric Instrument for the Determination of the Concentration of Mercury Vapour in Air (Fotoelektricheskiy pribor dlya opredeleniya kontsentratsii parov rtuti v vozdukhe) PERIODICAL: Pribory i Tekhnika Eksperimenta, 1958, Nr 2, pp 91-94 ABSTRACT: A description is given of a portable instrument which can be used to determine quickly and conveniently the concentration of mercury vapour in air. The instrument is based on the absorption by a vapour of ultraviolet radia-tion having a wavelength of 2537 Å . The intensity of the radiation is measured by a photomultiplier. The out-put of the photomultiplier is fed to an electric circuit which uses only diode and triode transistors. The circuit used is shown in detail in Fig.3. The scale of the instrument is linear and full scale deflection corresponds to 120 µg/m³. A complete analysis of mercury vapour concentration in a given room can be carried out in 30-40 sec. Card 1/2



ACC NR: AP6018720	SOURCE CODE: UR/0057/66/036/006/0981/0987
UTHOR: Ipatov, V.A.; Kalmykov,	<u>, B.G.</u> 99
DRG: <u>Physicotechnical Institut</u> tekhnicheskiy institut AN SSSR)	te im, A.F. Ioffe, AN SSSR, Leningrad (Fiziko- B)
FITLE: Application of uhf diag	gnostic techniques to the investigation of the structure
SOURCE: Zhurnal tekhnicheskoy	fiziki, v. 36, no. 6,1966, 981-987
TOPIC TAGS: plasma diagnostics structure, electron density, as	s, uhf, microwave, plasma shock wave, shock wave rgon, SHOCK WAVE FRONT, SHOCK WAVE VELOCITY
electron density distribution	ployed a microwave interferometer to measure the in a shock front. The shock waves were produced in a aining argon at approximately 0.01 mm Hg by discharging
a 50 kV 12 microfarad capacito:	r through a two-turn conical winding at one end of the
a 50 kV 12 microfarad capacitor tube. Electrode erosion was a winding and carefully preparing fied by repeated discharges, and up to 14 kOe transverse magnet region, was provided by dischar	r through a two-turn conical winding at one end of the voided only by employing high grade steel for the g its surface. The apparatus was baked out and was puri- fter each of which it was pumped down to 19 ⁻⁶ mm Hg. An ic field, uniform within 3% over the 10 cm long working rging a 5 kV 1.05 microfarad capacitor through two
a 50 kV 12 microfarad capacitor tube. Electrode erosion was a winding and carefully preparing fied by repeated discharges, and up to 14 kOe transverse magnet region, was provided by dischar	r through a two-turn conical winding at one end of the voided only by employing high grade steel for the g its surface. The apparatus was baked out and was puri- fter each of which it was pumped down to 19 ⁻⁶ mm Hg. An ic field, uniform within 3% over the 10 cm long working

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times of two parallel microwave beams 4 cm apart that crossed the shock tube at right angles to its axis. The 8 mm wavelength microwave interferometer was located midway between the two microwave beams employed to measure the shock wave velocity. The trans mitting and receiving antennas were identical; each consisted of a horn and a 7 cm diameter hyperbolic double convex paraffin lens that focused the beam onto the axis of the shock tube. The local lengths of the two surfaces of each lens were 4 and 12.5 cm, respectively. The electron density was calculated from the phase shift of the transmitted beam. The resolving power of the interferometer in the axial direction was determined by moving a 3 cm diameter metal cylinder through the shock tube and observing the change with the position of the cylinder of the intensity of the transmitted beam; the resolution was found to be approximately 1 cm. In deriving the electron density from the interferometer data it was assumed that the electron density was constant in a coordinate system moving with the shock front and could be represented by a trapezoidal distribution function. The velocity of the shock front was about 107 cm/sec at 0.045 mm Hg; the velocity increased slightly with increasing voltage on the capacitor and decreased somewhat with increasing strength of the transverse magnetic field. The velocity was nearly 10⁸ cm/sec at 0.064 mm Hg, but the reproducibility was poor. The width of the shock front, defined as the distance in which the maximum electron density increased from 10^{12} to 1.7×10^{13} cm⁻³, increased rapidly with increasing velocity of the shock wave, and under some conditions it was as great as 20 cm. The observed velocity dependence of the shock front width is in conflict with the findings of H. Petschek and S. Byron (Ann. Phys., 1, 270, 1957) and H. Blackman and B. Niblett (The Card 2/3

ess, 1958 nged from ock front e width w at furthe), but it 140 to 8 decrease as defini r experin of a trap ter is a ial resol	is pointed ou 00, were diffe d somewhat wit tely not limit pents are desir pezoidal electr	rent in the h increasing ed by the el able to elim con density	netohydrodynamics, Si lach numbers, which in other experiments. 7 transverse magnetic lectron Larmor radius minate the necessity distribution, and tha rapidly changing ele of 1 cm. Orig. art.	The width of the field strength, but It is concluded for the arbitrary t the microwave ctron densities has: 2 formulas
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396-66 SOURCE CODE: UR/0142/65/008/003/0355/0357 AP5020927 ACC NR: Zyubenko, V. D.; Ipatov, V. I. AUTHOR: 6 ORG: none TITLE: A shock excitation oscillator circuit SOURCE: IVUZ. Radiotekhnika, v. 8, no. 3, 1965, 355-357 TOPIC TAGS: semiconductor diode, periodic pulse, shock wave, electron tube ABSTRACT: Two alternative semiconductor diode circuits are presented that form pulses of a sinusoidal wave by shock excitation. One has a positive, the other a negative initial half period. The diode generator is more advantageous at higher frequencies than the transistor and electron tube pulse forming circuits in that it has a much higher back breakdown voltage than the former and lower impedance than the latter. An experimental diode pulse forming circuit produced pulses of a sinusoidal voltage with a frequency of 10 Mc. Fig. 1 shows the schematic diagrams of the two alternatives, and fig. 2 shows the respective control and output voltages for both alternatives. Orig. art. has: 2 figures. Card 1/2 1902 01







IPATOV, V.P.; LOSEV, O.L.; SAKOVICH, O.Yu.

Study of the insecticide sensitivity of Anopheles maculipennis Sacharovi Favre and Anopheles hyrcanus pseudopictus Grassi mosquitoes in the Masally and Astrakhan-Bazar Districts of the Azerbaijan S.S.R. in 1960. Med.paraz.i paraz.bol. no.1:83-87 '62. (MIRA 15:5)

1. Iz otdela epidemiologii (i. o. zav. N.N. Dukhanina) i otdela entomologii (zav. - rmof. V.N. Beklemishev) Instituta meditsinakoy parazitologii i tropic...skoy meditsiny imoni Ye.I. Martsinovskogo (dir. - prof. P.G. Sergiyev) Ministerstva z dravookhraneniya SSSR. (AZERBAIJAN---MOSQUITOES) (INSECTICIDES)

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IPATOV, V.P.; SAKOVICH, O.Yu.

STATE OF STREET

Study of the insecticide sensitivity of malarial mosquitos in the Massaly and Astrakhan-Bazar districts of the Azerbaijan S.S.R. in 1961; results of the second year of observation. Med. paraz. i paraz. bol. 32 no.3:271-274 My-Je¹63 (MIRA 17:3)

1. Iz otdelov epidemiologii (zav. - prof. N.N. Dukhanina) i entomologii (zav. - prof. V.N. Beklemishev [deceased] Instituta meditsinskoy parazitologii i tropicheskoy meditsiny imeni Ye.I. Martsinovskogo Ministerstva zdravookhraneniya SSSR (dir. -prof. P.G. Sergiyev).

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CIA-RDP86-00513R00051872

TAREYEV, Ye.N., prof., red.; SHUBLAD2F, A.K., prof., red.; IPATOV, V.P., red. [Epidemic hepatitis; Botkin's disease] Epidemicheskii gepatit; bolezn' Eotkine. Moskva, Meditsina, 1964. 198 p. (MIRA 17:8) 1. Deystv:tel'nyy chlen AMN SFSR (for Tareyev).

CIA-RDP86-00513R00051872



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CIA-RDP86-00513R00051872

YECOROV, Mikhail Nikolayevich, prof.; LEVITSKIY, Leonid Markovich, doktor med. nauk; IPATOV, V.P., red. [Obesity] Ozhirenie. Izd.2., perer. i dop. Moskva, Meditaina, 1964. 305 p. (MIRA 18:1)

"APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R00051872

IPATOV. V.; ZELINSKIY, K. (REVIEWERS) dimester and "In the heart of living nature." IU.Dolgushin. Reviewed by V. Ipatov, K.Zelinskii. Bot.zhur.39 no.1:119-121 Ja-7 '54. (MLRA 7:3) (Origin of species) (Dolgushin, IUrii)

SHISHKIN, B.K., professor; ROMANKOVA, A.G., kandidat biologicheskikh nauk, starshiy nauchnyysotrudnik; MARKOV,G.S., doktor biologicheskikh namk, dotsent; DANILAVSKIY,A.S., kandidat biologicheskikh namk, dotsent; SHTETHERG, D.N., doktor biologicheskikh nauk; LONAGIN, A.G aspirant; SELL'-HERMAN, I.Y., mladshiy nauchnyy sotrudnik; ZHIMKIN, L.N., doktor biologicheskikh nauk, professor; IPATOV, V.S., student V kursa; KOELOV, V.Ye., kandidat biologicheskikh mank, Starshiy nauchnyy sotrudnik; KARTASHEV, A. I., kandidat biologicheskikh nauk, starshiy nauchnyy sotrudnik; MITSKHKO,A.A., starshiy nauchnyy sotrudnik; VASILEVSKAYA, V.K., doktor biologicheskikh nauk, dotsent; RYUMIN, A.V., kandidat biologicheskikh mauk; MAUNOV.D.V., kandidat biologicheskikh mauk, mladshiy nauchnyy sotrudnik; KHOZATSKIY,L.I. kandidat biologicheskikh nauk, dotsent; GOROHUTS, A.N., kandidat biologicheskikh nauk, starshiy nauchnyy sotrudnik; GODLEVSKIY, V.S. assistent; GERBIL'SEIY, E.L., doktor biologicheskikh nauk, professor; ALEESANDROV, A.D., professor; KOLODYAZHEYY, V.I.; TURBIN, N.V.; ZAVAD-SKIY,K.M.

[Theory of species and the formation of species]. Vest.Len.un. 9 no.10:43-92 0 '54. (NLRA 8:7)

1. Chlen-korrespondent Akademii nauk SSSR (for Shishkin, Aleksandrov)

(Condtinued on next card)

"APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-

CIA-RDP86-00513R00051872

SHISHKIN.B.K., professor; ROMANKOVA,A.G., kandidat biologicheskikh nauk, starshiy nauchnyy sotrudnik, and others.

[Theory of species and the formation of species]. Vest.Len.un. 9 no.10:43-92 0 '54. (MLRA 8:7)

2. Leningradskiy gosudarstvennyy universitet (for Shishkin, Romankova, Markov, Ipatov, Koslov, Kartashev, Godlevskiy, Gerbil'skiy, Aleksandrov) 3. Zoologicheskiy institut Akademii nauk SSSR (for Shteynberg, Haumov) 4. Kafedra entomologii Leningradskogo gosudarstvennogo universiteta (for Danilevskiy). 5. Kafedra darvinisma Leningradskoga gosudarstvennogo universitete (for Lomagin, Gorobets). 6. Kafedra geobtaniki Leningradskogo gosudarstvennogo universiteta (for Nitsenko). 7. Kafedra botaniki Leningradskogo gosudarstvennogo universiteta (for Vasilevskaya). 8. Kafedra zoologii posvonochnykh ^Leningradskogo gosudarstbennogo universiteta (for Khosatskiy). 9. Leningradskoge otdeleniye Vsesoyuznogo instituta udobreniy, agropochvovedeniya i agrotekhniki (for Sell'-Bekman) 10. Institut eksperimental'noy meditsiny Akademii meditsinskikh nauk SSSR (for Zhinkin)

(Origin of species)

"APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R00051872

IPATOV, V. S., Cand Biol Sci -- (diss) "Aspen forests of the Leningred Economic Rayon." Leningrad, 1960. 13 pp; (Academy of Sciences USSR, Bot-annical Inst im V. L. Komarov); 200 copies; price not given; (KL, 24-60, 130)

NAMES AND ADDRESS OF TAXABLE PARTY.





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IPATOV, V.S. and adapted the state of the st Types of aspen forests in the northwestern part of the R.S.F.S.R. (MIRA 13:1) Vest, IGU 15 no.3:23-40 '60. (Russia, Worthwestern--Aspen)

IPATOV, V.S.
"Comparative estimation of the participation of species in the structure of a meadow community" by V.M.Poniatovskaia, N.V. Syrokomskaia. Reviewed by V.S.Ipatov. Bot. zhur. 46 no.9: 1346-1348 S *61. (MIRA 14:9)
1. Leningradskiy gosúdárstvennyy universitet. (Pasture research) (Poniatovskaia, V.M.) (Syrokomskaia, N.V.)



CIA-RDP86-00513R00051872



IPATOV, V.S.
Comparison of some methods for determining the role of a species in the structure of the herbaceous cover of an oak forest. Bot. zhur. 47 no.3:360-368 Mr *62. (MIRA 15:3)
1. Leningradskiy gosudarstvennyy universitet. (Forest ecology) (Grasses)



IPATOV, V.S.; MIRKIN, B.M. "Floodland meadows of the Yenisey" by L.I.Nomokonov. Reviewed by V.S.Ipatov, B.M.Mirkin. Bot. zhur. 47 no.9:1388-1390 S '62. (MIRA 16:5) 1. Leningradskiy gosudarstvennyy universitet. (Yenisey Valley-Pastures and meadows) (Nomokonov, L.I.) ۰ <u>۲</u>. ۲ \mathcal{T}_{1}

MIRKIN, B.M.; IPATOV, V.S. Geobotany at the Second Interuniversity Conference "Contribution of Universities to Agriculture". Bot. zhur. 48 no.7:1088-1090 Jl '63. (MIRA 16:9 (MIRA 16:9) 1. Leningradskiy gosudarstvennyy universitet. (Phytogeography) (Botany, Economic)

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"APPROVED FOR RELEASE: Thursday, July 27, 2000 CIA-RDP86-00513R00051872

DROZDOV, Aleksandr Aleksandrovich; <u>IPATOV</u>, <u>Vladimir Vasil'yevich; MIGAY</u>, L.S., vedushchiy red.; POLOSINA, A.S., tekhn. red. [The SS-24P standard seismic station] Seriinaia seismicheskaia atantsiia SS-24P. Moskva, Gos. nauchmo-tekhn. izd-vo neft. i gorno-toplivnoi lit-ry, 1961. 89 p. (MIRA 14:10) (Seismic prospecting)

CIA-RDP86-00513R00051872

· 20ЦЦ2 в/115/61/000/003/006/013 в124/в204

26,2190

AUTHORS: Ipatov, V. V. and Magin, I. Ya.

TITLE: A miniature resistance thermometer for checking the service of bearings

PERIODICAL: Izmeritel naya tekhnika, no. 3, 1961, 19-20

TEXT: The service of the bearings in turbo-generators is usually controlled with the temperature of the oil emerging from the bearing, but this is not enough to avert the danger of breakdowns early enough. A more promising method of checking load and support bearings is direct measurement of the temperature of the bearing metal layer in the bearing. The controls showed that the temperature of the race depends on the type of design, amount of load, quantity, and temperature of the cooling oil, and that it usually varies between 70 and 90°C, whereas on critical conditions it may reach $110-140^{\circ}$. Thus, the apparatus for checking the service of bearings must be able to measure temperatures of up to $150^{\circ}C$. However, the usual resistance thermometers which are suited for this range, are too big and therefore cannot be attached to the casing of the

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A miniature resistance thermometer ...

support bearings. For this reason, a miniature thermometer with a diameter of 3.2 mm and a 12 mm long active part was developed at the laboratory of a turbine engine factory. This resistance thermometer (Fig.1) is a copper wire (0.05 mm in diameter) which is bifilarly wound upon the thermometer and covered with a layer of bakelite paper of the type $\Pi \Im \mathcal{N} \Gamma \mathcal{O} CT 2773-51$ (PRI GOST 2773-51). The resistance of the thermometer at $\mathcal{O}^{\circ} C$ is 53 ohms, its graduation the same as that of the copper thermometers 2a. Stability and measuring error of the thermometers cited meets the requirements of TOCT 6651-59 (GOST 6651-59) for third-class thermometers. Inertia of these resistance thermometers is low. The mounting of miniature resistance thermometers to the casings of the support bearing of a BNT-25-4 (VPT-25-4) type turbine and in the casings of the load bearings is shown in Fig.2. The resistance thermometers are placed in especially drilled openings (diameter of 3.4 mm) and fixed with $\overline{BP-2}$ (BF-2) adhesive. The terminals of the resistance thermometers are, over a plug, connected to a switch and a measuring instrument. As measuring instrument, the electron bridge JMB-11 (EMV-11) or JMAC-26 (EMDS-26) was used. There are 2 figures.

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5/589/62/000/063/011/021 E194/E436 Ipatov, Yu.S., Leykum, V.I., Oleynik, B.N., **AUTHORS:** Patovskaya, Z.K. Instruments for measuring thermal conductivity TITLE : USSR. Komitet standartov, mer i izmeritel'nykh priborov. Trudy institutov Komiteta. no.63(123). SOURCE : Moscow, 1962. Issledovaniya v oblasti teplovykh i temperaturnykh izmereniy. 143-150 In 1960 a need was pointed out for instruments to measure thermal conductivity quickly, though not necessarily with great accuracy. For this purpose the here described instrument A-21 The cylindrical specimen is in contact with an The measurements are carried out with a is suitable. insulated heater. Under such constant current passing through the heater. conditions the thermal flux passing through specimens is a function of their thermal conductivity, providing they have the same length.

heater. Microammeter M-95 measures the output from the thermocouples in the contact plates at the top and bottom of the test Card 1/3

In the base of the instrument is a transformer which supplies the

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s/589/62/000/063/011/021 E194/E436 Instruments for measuring thermal ... The influence on the readings of the pressure on the piece. specimen, the air temperature around the specimen and the cooling temperature were studied, using test pieces 15 mm diameter and 20 mm long made of fused quartz or of fluoroplast-4 (teflon). These specimens are longer than the optimum length of 5 to 10 mm and so the maximum stabilisation time could readily be determined, with quartz it was up to 125 minutes. Similar results were The specimen diameter is not obtained with fluoroplast-4. critical but it will probably be convenient to use a value of The mean standard error was + 1% and the overall 10 to 15 mm. error of measuring the coefficient of thermal conductivity of a specimen 10 to 15 mm diameter and 5 to 10 mm long is about + 2% 150 for a large number of tests or about + 3% for two or three measurements. These values apply for thermal conductivities in the range 0 to 1 W/(metre degree) but for materials of greater thermal conductivity the errors will be greater and indeed the A-21 instrument is not recommended for them. A somewhat improved version, type A-22, is of very similar performance. In order to extend the range of thermal conductivity that can be measured, Card 2/3

