Problems of the Economics of Utilization of Reserve Capacities (cont.)

unsatisfactory organization of the work, as well as violations of the proper thermal and process technology. The planning of heat times and tapping times is arbitrary in most cases, without consideration of the state of each particular heat or of the capabilities of the individual shop. Therefore, the number of heats tapped on schedule is not over 30-50%. Particularly long delays occur during the period of hot-metal addition, charging, and servicing; they are due to the fact that this time coincides with the similar periods at other furnaces and also to poor supply of the metal portions of the charge, inadequacy of molten iron in the mixers, and unsatisfactory preparation of the mixer materials for the heat. At some plants, there is a shortage of ladle cranes, charging machines, and other auxiliary equipment, while the essential pool of cranes and transportation equipment is utilized to only 50-60% of capacity and is capable of serving the open-hearth furnaces even if their rate of production is increased by 25%. A number of open-hearth shops require reconstruction, with an increase in the traffic capacity of their pouring stockyards and other bottlenecks.

V. G.

Card 2/2

MEDVEDEV, [redacted]; KOBYLYAKOV, I.I.; TARKYKO, N.A.; DUBINA, Yu.G.

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1. Dnepropetrovskiy metallurgicheskiy institut i Zavod imeni Dzerzhinskogo.
(Open-hearth furnaces—Equipment and supplies)

KOBYLYAKOV, I. I.

MEDVEDEV, I. A.; KOBYLYAKOV, I. I. [Kobylyakov, I. I.]; TARKIKO, N. A. [Tarcyko, N. A.]; DUBINA, I. G. [Dubina, Yu. G.]

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KOBYLYAKOV, I.I.

Some problems of industrial organization in modern open-hearth plants. Izv. vys. ucheb. zav.; chern. met. 4 no.12:185-190 '61. (MIRA 15:1)

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(Open-hearth furnaces) (Industrial organization)

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1. Dneprodzerzhinskiy metallurgicheskiy zavod-vtuz.
(Steel industry—Accounting) (Bannyi, N.P.)

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Efficiency of the oxygen-blown converter process of steelmaking. Izv. vys. ucheb. zav.; chern. met. 5 no.8:200-206 '62. (MIRA 15:9)

1. Dneprodzerzhinskiy metallurgicheskiy zavod imeni Lenina. (Bessemer process) (Oxygen—Industrial applications)

BRYUKHANENKO, B.A., dotsent, kand. ekonom. nauk; BEN', T.G.; GERSHTENKERN, S.Ya.; KAGAN, I.S.; PRAVDIN, M.V.; STOGNIY, A.F.; KHAKHALINA, A.N.; CHERNIKHOV, V.S.; KOBYLYAKOV, I.I., dotsent, kand. ekonom. nauk; SHIRYAYEV, P.A., kand. ekonom. nauk

"Economic aspects of ferrous metallurgy" by N.P. Bannyi, V.B. Brodskii, IA.A. Oblomskii, V.V. Rikman, L.N. Roitburd. Reviewed by B.A. Briukhanenko and others. Stal' 22 no.6: 562-565 Je '62. (MIRA 16:7)

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(Iron industry) (Steel industry)
(Brodskii, V.B.) (Oblomskii, IA.A.)
(Rikman, V.V.) (Roitburd, L.N.)

KOBYLYAKOV, I.I.

Determining the coefficient of work rhythmicity in modern open-hearth furnace plants. Izv. vys. ucheb. zav.; chern. met. 6 no.10:184-187 '63. (MIRA 16:12)

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KOBYLYAKOV, I.I.

Economic advantages of organizing production in converter plants. Izv. vys. uchab. zav.; chern. met. 8 no.7:56-62 '65. (MIRA 18:7)

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OTRESHKO, Anatoliy Ivanovich, doktor tekhnicheskikh nauk, professor, redaktor; IVYANSKIY, A.M., kandidat tekhnicheskikh nauk, dotsent; SHMURNOV, K.V., kandidat tekhnicheskikh nauk, dotsent; ALEKSEYEV, V.M., redaktor; KOBYLYAKOV, L.M., redaktor; PERESYPKINA, Z.D., tekhnicheskiy redaktor; BALUEV, K.I., tekhnicheskiy redaktor.

[Hydraulic engineering structures] Inzhenernye konstruktsii v gidromeliorativnom stroitel'stve. Pod obshchei red. A.I.Otreshko. Moskva, Gos.izd-vo sekhos. lit-ry, 1955. 551 p. (MLRA 9:1)
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BOGDASHIN, A.S.; BOGORODSKIY, A.A.; VINOGRAD, M.B.; GORBUNOV, V.I.; GORBUNOV, V.R.; DUROV, V.K.; YERMAKOV, A.L.; IVANOV, A.A.; KARAKOVA, N.I.; KOBYLYAKOV, L.M.; KOZLOVSKIY, M.I.; MARAKHTANOV, K.P.; MIRUMYAN, G.N.; NECHAYEV, G.P.; NOVIKOV, A.G.; OL'KHOVSKIY, K.I.; PESTRYAKOV, A.I.; POLAPANOV, A.V.; SKLYAREVSKAYA, Ye.Kh.; SOLDATENKOV, S.I.; SOROKIN, Ye.M.; TRUSHINA, Z.V.; FEDOROV, P.F.; FEDOSEYEV, A.M.; FROG, N.P.; SHAMAYEV, G.P.; YANOVSKIY, V.Ya.; ORLOVOV, A.D., spetsred.; ISAYEVA, V.M., tekhn.red.

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(Agricultural machinery)

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(Acrylic acid) (Hydroquinone) (Polarography)

L 16799-66 EWT(1)/EWT(m)/EWP(w)/EPF(n)-2/ETC(m)-6 JD/EM
ACC NR: AP6004119 SOURCE CODE: UR/0120/65/000/001/0021/0025

AUTHOR: Kobylyanskiy, A. A. 74 B

ORG: Kharkov Aviation Institute (Khar'kovskiy aviatsionnyy institut)

TITLE: Computation of initial heating of a two-layer plate with second order boundary conditions 24

SOURCE: Kharkov. Aviatsionnyy institut. Samoletostroyeniye i tekhnika vozdushnogo flota, no. 1, 1965, 21-25

TOPIC TAGS: thermal effect, thermal conductivity, thermal property, thermodynamics, heat conduction, thin plate, Laplace transform

ABSTRACT: The one-dimensional problem of initial heating 21,44,55 of a bi-layered plate is solved. The plate consists of metal sheets protected from heat by a layer of insulation. Heating occurs from the side of the insulation by means of a time-varying heat current which is approximated by the m^{th} degree polynomial

$$q(\tau) = \sum_{m} b_m \tau^m,$$

where the b_m are polynomial coefficients. The thermo-physical characteristics of

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the layers are constant and independent of temperature, and it is assumed that the thermal current goes only into the heating of the plates. Furthermore, it is assumed that the internal surface of the plate is thermally insulated and that the facing temperature is independent of coordinate, but dependent on time only. Under these assumptions the problem reduces to the integration of the linear differential equation of heat conduction

$$\frac{\partial t_1(x, \tau)}{\partial \tau} = a_1 \frac{\partial^2 t_1(x, \tau)}{\partial x^2},$$

where $t_1(x, \tau)$ is the temperature of the insulation; x is a coordinate direction; and $a_1 = \frac{\lambda_1}{c_1 \gamma_1}$ is the temperature conductivity of the insulation; λ_1 is the thermal conductivity of the insulation; c_1 is the unit heat capacity of the insulation, and γ_1 is its unit weight. Boundary conditions are

$$\lambda_1 \frac{\partial t_1(-\delta_1, \tau)}{\partial x} + \sum_1^m b_m \tau^m = 0,$$

$$\lambda_1 \frac{\partial t_1(0, \tau)}{\partial x_1} + C_m \frac{\partial t_1(0, \tau)}{\partial \tau} = 0,$$

$$t_1(0, \tau) = t_2(\tau).$$

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$t_1(x, \rho) = t_2(0) = t_0$.

These conditions are plotted in Fig. 1 (the subscript 2 refers to the metal sheets).

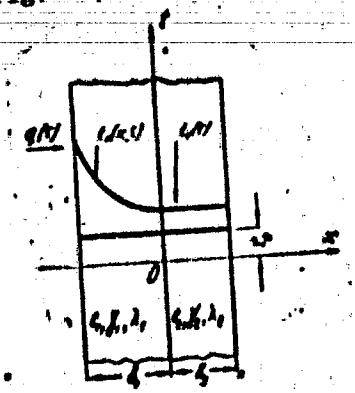

Fig. 1.

The problem is solved through the use of an operational method involving the use of a Laplace transform

$$T_1(x, s) = L[t_1(x, \tau)] = \int_0^\infty t_1(x, \tau) e^{-s\tau} d\tau.$$

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ACC NR: AP6004119

A general solution is found of the form

$$T_1(x, s) - \frac{f_0}{s} = A \operatorname{ch} \sqrt{\frac{s}{a_1}}\, x + B \operatorname{sh} \sqrt{\frac{s}{a_1}}\, x ,$$

where s is the transform parameter. Temperature expressions are developed in transforms. Use is made of transform multiplication theory, and the resulting temperature expressions are in series form. A table of coefficient values for the temperature formulae is given. Orig. art. has: 19 equations, 1 figure, and 1 table.

SUB CODE: 20 SUBM DATE: none/ ORIG REF: 003

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ACCESSION NR: AP4033046 S/0147/64/000/001/0105/0111

AUTHOR: Koby*lyanskiy, A. A.

TITLE: Calculation of the heating of a two-layer unlimited plate

SOURCE: IVUZ. Aviatsionnaya tekhnika, no. 1, 1964, 105-111

TOPIC TAGS: thermal insulation, convection, lamina heat resistance, heat transfer, heat flow, thermal conductivity,

ABSTRACT: The author considered the single-dimension problem of the heating of a twin-layer lamina, consisting of thermal insulation and a metal skin, with the lamina subjected to convective heating from the insulation side. It is noted that similar conditions arise during the heating of the skin of aircraft, protected externally by a heat-resistant covering. The thermo-physical characteristics of the layers are assumed to be independent of temperature. The heat transfer factor is taken to be constant, with the environmental temperature a function of time

$$t_c(\tau) = \sum_{1}^{m} b_m \tau^m + t_0. \qquad (1)$$

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ACCESSION NR: AP4033046

It is likewise assumed that the convective heat flow, transmitted from the boundary layer to the outer surface of the insulation, goes only to heat the lamina; the inner plate surface is considered to be heat insulated. The temperature in the skin depends practically on time alone, and not on the coordinate. This assumption is equivalent to $\lambda_2 = \infty$ and permits a considerable simplification of the problem of heating a two-layer lamina. With these assumptions, the solution of the problem is reduced to the solution of the heat conductivity differential equation:

$$\frac{\partial t_1(x, \tau)}{\partial \tau} = a_1 \frac{\partial^2 t_1(x, \tau)}{\partial x^2} \quad (2)$$

with boundary conditions (see Table 1 of the Enclosure):

$$\lambda_1 \frac{\partial t_1(-\delta_1, \tau)}{\partial x} + \alpha \left[\sum_1^m b_m \tau^m + t_0 - t_1(-\delta_1, \tau) \right] = 0; \quad (3)$$

$$\lambda_1 \frac{\partial t_1(0, \tau)}{\partial x} + C_m \frac{\partial t_1(0, \tau)}{\partial \tau} = 0, \quad (4)$$

$$t_1(0, \tau) = t_2(\tau), \quad (5)$$

$$t_1(x, 0) = t_2(0) = t_0 = \text{const}, \quad (6)$$

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ACCESSION NR: AP4033046

where $C_m = c_2\gamma_2\delta_2$. The problem is solved through the use of a Laplace transformation. An expression for the temperature is first found in a representational form:

$$T_1(x, s) - \frac{t_0}{s} =$$

$$= -\sum_1^m \frac{b_m m!}{s^{m+1}} \frac{a\left(\lambda_1 \operatorname{ch}\sqrt{\frac{s}{a_1}}x - C_m\sqrt{sa_1}\operatorname{sh}\sqrt{\frac{s}{a_1}}x\right)}{\sqrt{\frac{s}{a_1}}\left(\lambda_1^2 + C_m a_1 a\right)\operatorname{sh}\sqrt{\frac{s}{a_1}}h_1 + \lambda_1(C_m s + a)\operatorname{ch}\sqrt{\frac{s}{a_1}}h_1}, \quad (7)$$

which is then transposed from the original through the use of the theorem of multiplication of representations, to the form:

$$\int_0^\tau e^{s\theta}\sum_1^m m b_m \theta^{m-1}\,d\theta = e^{s\tau}(a_0 + a_1\tau + \ldots + a_{m-1}\tau^{m-1}) - a_0, \quad (8)$$

$$a_0 = \sum_1^m \frac{(-1)^{m+1} m! b_m}{0!\lambda^m}, \quad a_1 = \sum_1^m \frac{(-1)^m m! b_m}{1!\lambda^{m-1}}, \ldots$$

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The final expressions for the temperature of the thermal insulation and the skin take the form:

$$t_1(x, \tau) = t_c(\tau) - \sum_{n=1}^{\infty} \left\{ B_n (\cos \mu \bar{\delta}_1 + K_0 \mu \sin \mu \bar{\delta}_1) \sum_{1}^{m} p_m b_m \tau^m \right\}. \quad (9)$$

$$t_2(\tau) = t_c(\tau) - \sum_{n=1}^{\infty} \left\{ B_n \sum_{1}^{m} p_m b_m \tau^m \right\}. \quad (10)$$

The author points out that the use of the latter two equations is inconvenient, since the determination of μ and B_n requires double integration for Bi and K_0. The results of a previous work (J. H. Grover, W. H. Holter. Solution of the transient heat-conduction equation for an insulated, infinite metal slab. Jet Propulsion, 1957, XII, v. 27, No. 12) and verification calculations show that for a practical range of values Bi = 0.1 - 20 and K_0 = 0.05 - 20; the above two equations are approximated with an accuracy of 3% by expressions:

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$$t_1(x, \tau) = t_0(\tau) - \sum_{n=1}^{\infty} \left\{ A_n (\cos \mu_n \bar{x}_1 + K_c \mu_n \sin \mu_n \bar{x}_1) \sum_{1}^{m} p_m b_m \tau^m \right\}, \quad (11)$$

$$t_2(\tau) = t_0(\tau) - \sum_{n=1}^{\infty} \left\{ A_n \sum_{1}^{m} p_m b_m \tau^m \right\}, \quad (12)$$

where

$$A_n = (-1)^{n+1} \frac{2\sqrt{1 + \beta^2 \mu_n^2}}{\mu_n (1 + \beta + \beta^2 \mu_n^2)}, \quad (13)$$

$$\operatorname{ctg} \mu = \beta \mu, \quad (14)$$

$$\beta = \frac{1}{Bi} + K_c + \frac{1}{Bi} K_c. \quad (15)$$

In this way the determination of the skin temperature is reduced to the question of finding the proper values of k, A_n and p_m according to tables and carrying out certain operations of multiplication. Orig. art. has: 27 formulas and 1 table.

ASSOCIATION: None

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1.Nauchno-issledovatel'skiy institut zhivotnovodstva Lesostepi i Poles'ya USSR.
(Feeding and feeding stuffs)

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[Establishing standards for material consumption and stocks in the petroleum industry] Normirovanie raskhoda i proizvodstvennykh zapasov osnovnykh materialov v neftianoi promyshlennosti. Moskva, Gos.nauchno-tekhn.izd-vo neft. i gorno-toplivnoi lit-ry, 1959. 252 p. (MIRA 12:12)

(Petroleum industry--Standards)

KOBYLYANSKIY, D., kand. tekhn. nauk

Comfortable clothing for cooks. Obshchestv. pit. no.12:31-32 D '62. (MIRA 16:1)

1. Zaveduyushchiy laboratoriyey standartizatsii TSentral'nogo nauchno-issledovatel'skogo instituta shveynoy promyshlennosti pri Vsesoyuznom sovete narodnogo khozyaystva.

(Clothing, Protective)

KOBYLYANSKIY, D., kand.tekhn.nauk

From the exposition halls into life! Okhr.truda i sots.strakh. 5 no.12:29 D '62. (MIRA 16:2)

(Clothing industry)

KOBYLYANSKIY, D., kand. tekhn. nauk; BONDIN, Yu.; MAYMAN, I.; RAYKHMAN, S.

Technological information. Okhr. truda i sots. strakh. 6 no.3:33-37 Mr '63. (MIRA 16:4)

(Industrial safety) (Work clothes)

YURENKOVA, M.; KOBYLYANSKIY, D., kand. tekhn. nauk; ZOLOTAREV, B.

With their brakes down. Okhr. truda i sots. strakh. no.4:27-29 Ap '63. (MIRA 16:4)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut shveynoy promyshlennosti (for Yurenkova). 2. Chlen obshchestvennogo soveta redaktsii "Okhrana truda i sotsial'noye strakhovaniye" (for Kobylyanskiy). 3. Korrespondent zhurnala "Okhrana truda i sotsial'noye strakhovaniye" (for Zolotarev).

(Rublevo, Moscow Province—Clothing industry)

1. KOBYLYANSKIY, D. A.

2. USSR (600)

4. Clothing Industry

7. Controlling the fitness of fabrics for steaming. Leg. prom. 12 no. 10, 1952

9. Monthly List of Russian Accessions, Library of Congress, January 1953. Unclassified.

KOBYLYANSKIY, D.A., kandidat tekhnicheskikh nauk.

Use of twisted cotton yarn instead of thread. Leg.prom.14 no.2:39-41 F '54. (MLRA 7:5)
(Cotton yarn)

KOBYLYANSKIY, D.A., kandidat tekhnicheskikh nauk.

Faulty recommendations for grading textiles. Leg.prom.14 no.12:18-19 D '54. (MLRA 8:2)
(Textile fabrics--Specifications)(Bardadymova, N.A.)
(Abarinova, A.I.)

KOROTKOV, S.N.; KOBYLIANSKY, D.A.

The pattern of designed men's suits for mass production. Leg. prom. 15 no.10:20-26 O '55. (MLRA 9:1)
(Tailoring)

KOLESNIKOV, Petr Alekseyevich; [redacted]; MARGOLIN, Lazar' Yakovlevich; ISLANKINA, T.P., redaktor; MEDVEDEV, L.Ya., tekhnicheskiy redaktor

[Technical control in the clothing industry] Tekhnicheskii kontrol' v shveinom proizvodstve. Moskva, Gos.nauchno-tekhn. izd-vo lit-ry po legkoi promyshl., 1957. 343 p. (MIRA 10:11)
(Clothing industry)

KOBYLYANSKIY, D.A., kand. tekhn.nauk

Establish more suitable standards for fabrics. Leg.prom. 18 no.7:15-18 Jl '58. (MIRA 11:9)
(Textile fabrics--Standards)

DALIDOVICH, A.S., prof.; KOBYLYANSKIY, D., kand.tekhn.nauk

"Materials used in the garment industry" by T.A. Modestova, L.N.Flerova, B.A.Busov. Reviewed by A.S. Dalidovich, D.Kobylianskii. Leg.prom. 18 no.12:43-49 D '58. (MIRA 11:12)
(Textile fabrics)
(Modestova, T.A.) (Flerova, L.N.) (Busov, B.A.)

KOBYLYANSKIY, D., kand.tekhn.nauk

New firemen's uniform. Pozh.delo 5 no.9:22-23 S '59.
(MIRA 13:1)
(Clothing, Protective)

KOBYLYANSKIY, D.A., kand.tekhn.nauk

New types of professional clothing for special purposes. Shvein. prom. no.6:27-30 N-D '59. (MIRA 13:4)
(Clothing, Protective)

POPKOV, V.I., kand. tekhn. nauk; TER-OVAKIMYAN, I.A.; KOBYLYANSKIY, D.A.; KOLESNIKOV, P.A.; PERTSEV, G.V.; MARAKUSHEV, Ye.A.; RUSAKOV, S.I., retsenzent; PLEMYANNIKOV, M.N., red.; SHAPENKOVA, T.A., tekhn. red.

[Handbook for the clothing industry worker] Spravochnik shveinika. Moskva, Izd-vo nauchno-tekhn. lit-ry RSFSR. Vol.1. 1960. 335 p. (MIRA 15:1)

(Clothing industry)

KOBYLYANSKIY, D.A.; SINYAKOV, A.B. (Moskva-Leningrad)

For advanced standards in the quality and grading of clothing and fabrics. Shvein.prom. no.3:13-17 My-Je '60. (MIRA 13:7)

(Clothing industry) (Textile fabrics)

KOBYLYANSKIY, D.A. (Moskva)

New styles for warm work clothes. Shvein.prom. no.2:25-30 Mr-Ap '60. (MIRA 13:11)

(Work clothes) (Dressmaking--Pattern making)

KOBYLYANSKIY, D.A.

Improve the quality of ready-made clothing. Standartizatsiia 24 no.6:39-40 Je '60. (MIRA 13:7)
(Clothing industry--Management)

KOBYLYANSKIY, D., kand.tekhn.nauk

Strong, light and comfortable. Pozh.delo 7 no.11:26 N '61.
(MIRA 14:11)

1. Zaveduyushchiy laboratoriyey standartizatsii TSentral'nogo nauchno-issledovatel'skogo instituta shveynoy promyshlennosti.
(Clothing, Waterproof)

KOBYLYANSKIY, D., kand.tekhn.nauk

Comments on several recommended technical specifications. Sov.torg. 35 no.4:21 Ap '62. (MIRA 15:4)
(Textile industry--Production standards)

KOBYLYANSKIY, D., kand.tekhn.nauk

For the operators of hydraulic giants. Sov.shakht. 11 no.11:37 N '62. (MIRA 15:11)

(Clothing, Protective)

KOBYLYANSKIY, D., kand. tekhn. nauk

Standards and aesthetic requirements. Sov. torg. 36 no.2: 13-15 F '63. (MIRA 16:4)

(Clothing and dress specifications)

KOBYLYANSKIY, D.A.

Improved standards for protective gloves. Shvein. prom. no.1: 36-37 Ja-F '63. (MIRA 16:4)

(Protective clothing—Standards)

KOBYLYANSKIY, D.A.

Modification of the methods of labeling shirts. Shvein. prom. no.1:36 Ja-F '63. (MIRA 16:4)

(Latvia--Labels)

KOBYLYANSKIY, D.A. (Moskva)

Quality of the production of protective clothing. Shvein. prom. no.3:28-30 My-Je '63. (MIRA 16:8)

BAZHENOV, Vladimir Ivanovich; KOHYLYANSKIY, D.A., retsenzent; RYZHNIKOVA, A.M., retsenzent; BELOKOSKOVA, N.A., retsenzent; MINKIEVA, V.I., retsenzent; POD"YEMSHCHIKOVA, K.K., retsenzent, GABOVA, D.M., red.

[Study of materials used in the clothing industry] Materialovedenie shveinogo proizvodstva. Moskva, Legkaia industriia, 1964. 374 p. (MIRA 18:4)

KOBYLYANSKIY, G.

RMP-62 respirator. Okhr. truda i sots. strakh. 7 no.2:40 F '64.
(MIRA 17:2)

KOBYLYANSKIY, I.

The OdA3-869 passenger semitrailer. Avt.transp. 42 no. 4:43-44 Ap '64. (MIRA 17:5)

KOBILYANSKIY, I.

New semitrailers manufactured at the Odessa Automobile Assembly Plant. Avt.transp. 41 no.4:46-48 Ap '63. (MIRA 16:5)
(Odessa—Truck trailers)

34853
S/135/62/000/003/005/0
A006/A101

18.1151

AUTHORS: Kobylyanskiy, I. F., Engineer, Peshekhonov, V. D., Technician

TITLE: Properties of welded joints of heat resistant ВЖ100 (ЭП126) [VZh100 (EP126)] steel

PERIODICAL: Svarochnoye proizvodstvo, no. 3, 1962, 26- 28

TEXT: The authors studied the properties of weld joints of grade VZh100 steel produced by argon arc and resistance welding of 100 x 300 mm plates. Tests were made to determine the mechanical properties of joints, the effect of deviations from the welding parameters, and the effect of "rigid" or "soft" welding conditions on the quality of the welds. The following results were obtained: The VZh100 steel can be satisfactorily welded by argon-arc or resistance process. Its weldability is analogous to that of ВЖ98 (VZh98) steel. It is recommended to perform resistance welding under "soft" conditions. The deviation of welding parameters should not exceed ±5%. The hardness of the weld joint in manual argon arc and resistance welding is HV 240 - 260, which is 12 - 25% more than the hardness of the base metal. Weld-adjacent zones show also a higher hardness, varying within 3 - 20%. The strength of weld joints at 20 - 800°C temperature is 90 -

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X

KOBYLYANSKIY, I. F., insh.; PESHEKHONOV, V. D., tekhn.

Mechanical properties of welded joints in OT4-1 with BT5-1 titanium alloys. Svar. proizv. no.10:12-14 O '62. (MIRA 15:10)

(Titanium alloys—Welding)
(Welding—Testing)

S/135/63/000/001/014/016
A006/A101

AUTHORS: Kobylyanskiy, I. F., Engineer, Peshekhonov, V. D., Technician

TITLE: Argon-arc welding of vacuum-tight joints in a heat exchanger

PERIODICAL: Svarochnoye proizvodstvo, no. 1, 1963, 40

TEXT: An investigation was made of using argon-arc welding without filler wire to join heat-exchanger tubes with tubular plates. After assembling the tubes with the plates, special attention was given to the consecutive application of the weld joints. Initially the tubes were welded along the least concentric circumference, and then by one row in a radial direction from the center to the edges. The rows were arranged with 45° spacing. The following concentric circumferences were then welded in the same direction until the tenth row; finally the last row was welded (Figure 2). Welding was performed on direct polarity 60 amps d-c, with 1.5 mm tungsten electrode diameter, and 4 l/min argon consumption. Welding of heat exchangers by the described method yielded structures without deformations. The vacuum tightness of the welds showed one untight joint of 1,428 welds. Tests with a helium flaw detector revealed 3 un-

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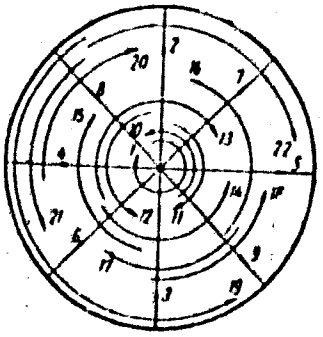
tight welds. They were repaired by additional welding. There are 3 figures.

Figure 2. Consecutive welding of tubes



KOBYLYANSKIY, I.F., inzh.; [illegible], V.D., tekhnik

Argon arc welding of heterogenous heat-resistant steels and alloys. Svar. proizv. no.11:18-21 N'63. (MIRA 17:5)

ACCESSION NR: AP4009825 S/0135/64/000/001/0021/0022

AUTHOR: Koby*lyanskiy, I. F. (Engineer); Peshekhonov, V. D. (Technician)

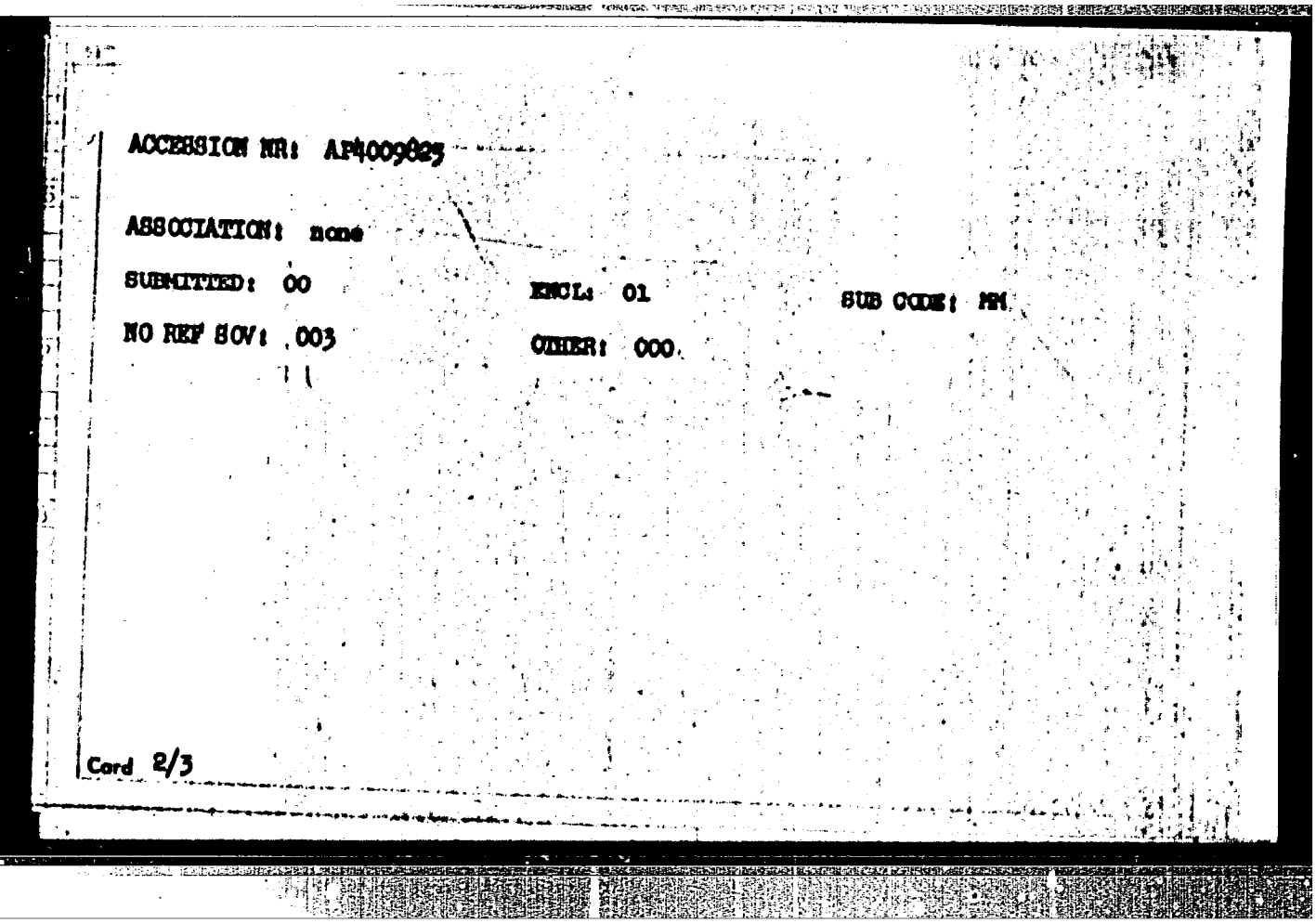
TITLE: Spot and seam welding of heat resistant steels and alloys

SOURCE: Svarochnoye proizvodstvo, no. 1, 1964, 21-22

TOPIC TAGS: spot welding, seam welding, steel welding, heat resistant steel, dissimilar material welding, alloy welding, VZh100 alloy, VZh98 alloy, EI703 alloy, 1Kh18N9T steel

ABSTRACT: The feasibility of resistance welding VZh100 alloy to VZh98 and EI703 alloys and 1Kh18N9T steel was tested on the MTP 150/1200 spot welder and the MShPR 300/1200 seam welder, using MTs4 alloy electrodes. Welding procedures were selected which insured adequate strength of the joints at room and high temperatures (up to 1000C), and x-ray control showed freedom from cracks and other defects. An example of the relationship between the strength of spot welds and the test temperature for three combinations of alloys is shown in Fig. 1 of the enclosure. The welding of such alloys should be carried out at high electrode pressures. "Z. F. Shirshova and E. N. Moloditsova took part in the work." Orig. art. has: 1 table and 3 figures.

Card 1/3



ACCESSION NR: AP4009825

ASSOCIATION: none

SUBMITTED: 00 ENCL: 01 SUB CODE: MM

NO REF SOV: 003 OTHER: 000

Card 2/3

ACCESSION NR: AP4019877 S/0135/64/000/003/0016/0017

AUTHOR: Koby*lyanskiy, I. F. (Engineer); Peshekhonov, V. D. (Technician)

TITLE: Resistance welding of steel OKh16N15M3B (EP376)

SOURCE: Svarochnoye proizvodstvo, no. 3, 1964, 16-17

TOPIC TAGS: EP376 steel, resistance welding, seam welding, spot welding, steel resistance welding

ABSTRACT: Steel EP376 is Nb stabilized, austenitic after annealing and rapid cooling, and highly corrosion resistant with tensile strength ≥ 55 kg/mm² and elongation δ ~50% at room temperature, compared to 50 kg/mm² and 25% respectively at 600C. Sheets 0.2—3.0 mm thick were spot and seam welded on the MTP-200 and MShP-150 units, respectively. An x-ray spotcheck indicated the welds to be free of pores or flaws. Tests at room temperature (see Fig. 1 in the Enclosure) and at temperatures up to 700C (Fig. 2) indicate that strength factor values for welded seams were above 0.9 over the range of 20—700C. Good quality of joints was assured by the selected operating

Card 1/4

ACCESSION NR: AP4019877

technique. "The mechanical tests were carried out by E. N. Molodtsova and N. G. Alisov." Orig. art. has: 2 figures and 2 tables.

ASSOCIATION: None

SUBMITTED: 00 ATD PRESS: 3045 ENCL: 02

SUB CODE: MM NO REF SOV: 000 OTHER: 000

Card 2/4

ACCESSION NR: AP4019877 ENCLOSURE:01

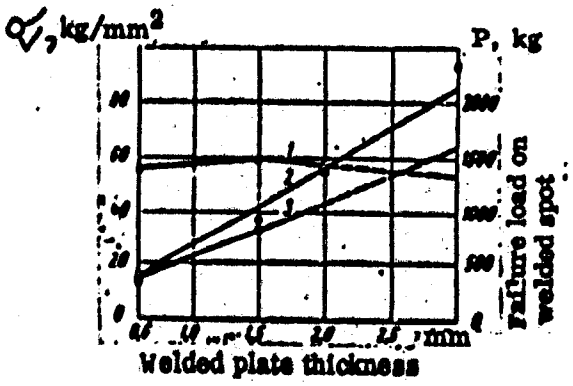


Fig. 1. Relationship between joint strength and plate thickness

1 - Seam welding; 2 - spot welding, shear test; 3 - same, rupture test

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Card 4/4

ACCESSION NR: AP4029387

S/0135/64/000/004/0026/0027

AUTHOR: Koby*lyanskiy, I. F. (Engineer); Peshekhonov, V. D. (Technician)

TITLE: The tendency of welded joints of certain high-temperature and heat-resistant steels and alloys toward intercrystallite corrosion

SOURCE: Svarochnoye proizvodstvo, no. 4, 1964, 26-27

TOPIC TAGS: intercrystallite corrosion, 1Kh18N9T steel, VZh100 alloy, VZh98 alloy, EI703 alloy

ABSTRACT: There has been no information concerning the durability of VZh100, VZh98 and EI703 alloys to intercrystallite grain corrosion. Tests were made on different thicknesses of VZh100 (1.2 mm), VZh98 (1.0 mm), EI703 (1.2 mm), and 1Kh19N9T (1.5 mm) in accordance with GOST 6032-58 by the AM method. This provides for the testing of samples in an aqueous solution of copper sulphate and sulfuric acid in the presence of copper shavings for 24 hours. The solution contains 160 g of copper $CuSO_4 \cdot 5H_2O$+100 ml of sulfuric acid with a density of 1.35/liter of water and copper shavings. The results are depicted in microphotographs. The materials VZh100, VZh98, EI703 and 1Kh18N9T, their homogeneous welded joints made by argon arc welding without welding rod and the inhomogeneous joints of VZh100+VZh98, VZh100+EI703, and VZh100+1Kh18N9T welded with and without a welding rod of VZh100, were found to be resistant to

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ACCESSION NR: AP4029387

intercrystallite grain corrosion in the initial state, as well as after tempering at 650° for 2 hours. In some samples, increased corrosion in the grain boundaries of the surface is observed; however, this may not be evaluated as a tendency toward corrosion. Orig. art. has: 2 figures and 1 table.

ASSOCIATION: none

SUBMITTED: 00 DATE ACQ: 28Apr64 ENCL: 00

SUB CODE: ML NO REF SOV: 000 OTHER: 000

Card 2/2

ACCESSION NR: AP4040700 S/0135/64/000/006/0021/0022

AUTHOR: Koby*lyanskiy, I. F.(Engineer); Peshekhonov, V. D.(Technician)

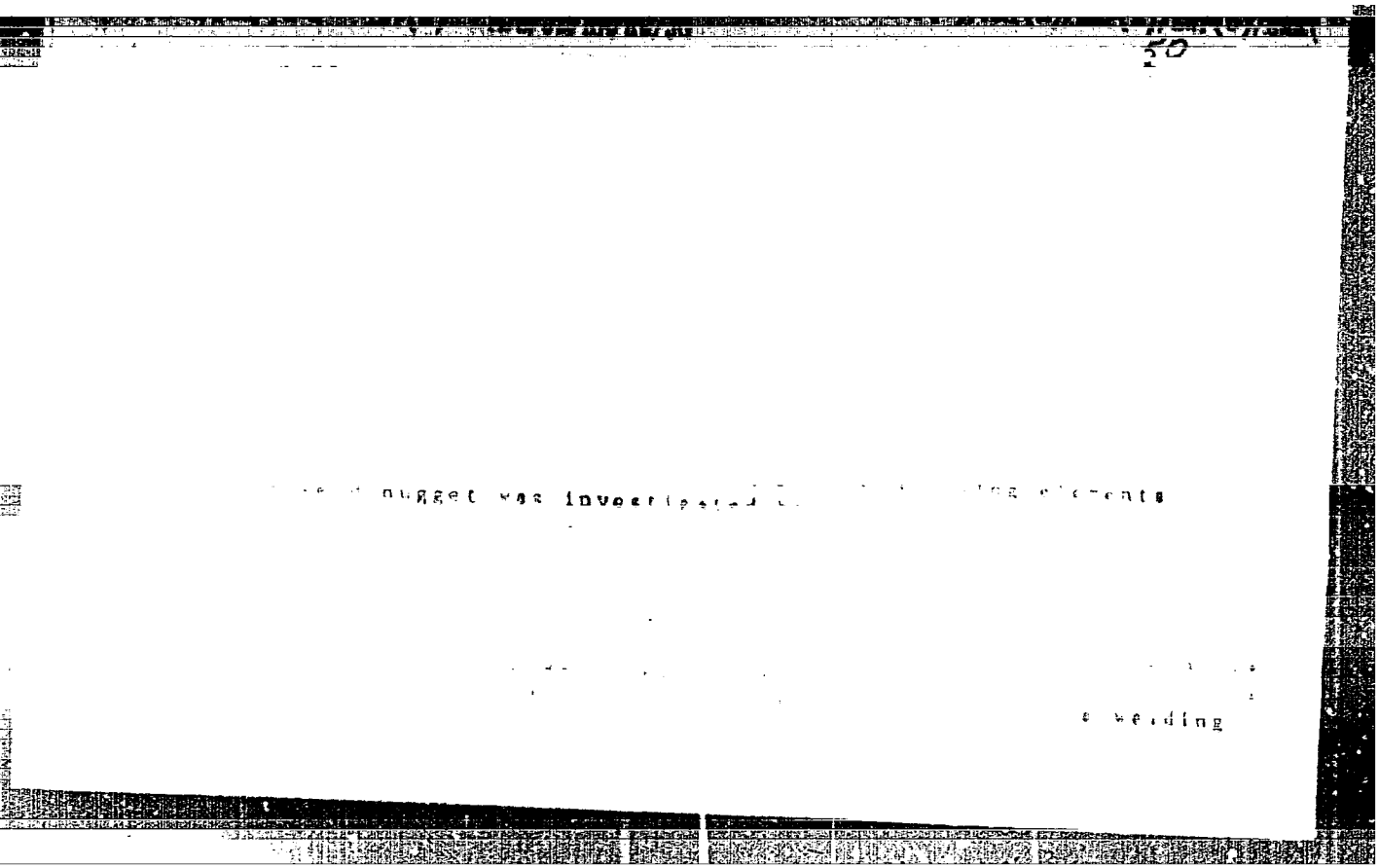
TITLE: Resistance welding of aluminum 0.1—0.2 mm thick

SOURCE: Svarochnoye proizvodstvo, no. 6 (630), 1964, 21-22

TOPIC TAGS: aluminum foil, foil welding, spot welding, seam welding, foil weld, spot weld, seam weld, weld property

ABSTRACT: Aluminum foil 0.1—0.2 mm thick can be seam and spot welded successfully with VZh98 alloy inserts 0.6 mm thick placed between the electrode and the foil. This insert prevents overheating of the electrodes and increases the concentration of heat at the contact zone. Seam welding at a current of 5400 amp, an electrode pressure of 100 kg, and a welding time of 0.01—0.02 sec produced seams 3.5—4.0 mm wide. Spot welding at a current of 4600 amp, an electrode pressure of 100 kg, and a welding time of 0.01—0.02 sec produced spot welds with nuggets 2.5—3.00 mm in diameter. Insert thickness can be increased up to 1.2 mm, but such increases must be

Card 1/2



ACCESSION NR: AP5012643

current and the squeezing force applied to the electrodes. The weld time within the limits of 0.1—0.3 sec does not appreciably affect the uniformity of the distribution of the alloying elements. Orig. art. has: 2 figures. [MS]

ASSOCIATION: none

SUBMITTED: 00 ENCL: 00 SUB CODE: MM

NO REF SOV: 002 OTHER: 000 ATD PRESS: 4005

Card 2/2

L 11508-66 EWT(m)/EWA(d)/EWP(t)/EWP(k)/EWP(z)/EWP(b) IJP(c) MJW/JD/HW/JG

ACC NR: AP6003282 SOURCE CODE: UR/0135/66/000/001/0014/0016

AUTHOR: Peshekhonov, V. D. (Engineer); Kotylyanskiy, I. F. (Engineer); Dubitskiy, A. K. (Engineer)

ORG: none

TITLE: Welding of sheet joints of copper and Kh18N10T steel

SOURCE: Svarochnoye proizvodstvo, no. 1, 1966, 14-16

TOPIC TAGS: sheet metal, copper, steel, arc welding, resistance welding, bimetal / Kh18N10T steel

ABSTRACT: The fabrication of certain products (evaporators, heat exchangers, etc.) requires joining sheet copper to Kh18N10T steel, i.e. joining metals which differ markedly in their physicochemical properties and hence are difficult to weld together. In this connection, the authors experimentally developed a technique for joining 0.3-1.5 mm thick M2 sheet copper to sheets of steel Kh18N10T of the same thickness. Of the welding methods investigated, the two most suitable methods proved to be argon arc and resistance welding. Prior to welding the steel specimens were degreased and the copper specimens pickled. In the case of argon arc welding, treatment of the weld with Ni or with Ml Cu improves the weld structure. Contact welding requires using as

Card 1/2

Card 2/2

KOBYLYANSKIY, I. I.

USSR/Engineering - Dump trucks

Card 1/1 : Pub. 12 - 6/16

Authors : Kobylyanskiy, I. I.

Title : Dump trucks, type GAZ-93D, for farm use

Periodical : Avt. trakt. prom. 6, 17-19, June 1954

Abstract : The Odessa Automobile Plant started the mass production of dump trucks designed for agricultural use. General description of the GAZ-93D dump truck is presented, together with drawings and illustrations depicting its various components.

Institution : .....

Submitted : .....

KOBYLYANSKIY, T. M.

Experience in open-pit mining of thin coal seams. Ugol' 37 no.10:31-32 O '62. (MIRA 15:10)

1. Glavnyy geolog Leninskogo tresta kombinata Kuzbassugol' Ministerstva ugol'noy promyshlennosti SSSR.

(Kuznetsk Basin—Strip mining)

KOBYLYANSKIY, V.B. [Kobylyans'kyi, V.P.] ; SHN'KIV, M.T.

Radiation dispersion of electrons. Dop. ta pov. L'viv. un. no.7 pt.3:237-238 '57. (MIRA 11:2)
(Electrons)

GLAUBERMAN, A.Ye.; KOBYLYANSKIY, V.B.; TAL'YANSKIY, I.I.

Distribution of neutrons in media with a cyclindrical interface and an off-axis source. Atom.energ. 10 no.5:513-515 My '61.
(MIRA 14:5)

(Neutrons)

ACC NR: AP6026312 (A) SOURCE CODE: UR/0113/66/000/005/0029/0031

AUTHOR: Genbom, B. B. (Candidate of technical sciences); Kobzlyanskiy, V. N.; Kirman, A. M.; Gudz, G. S.; Ryabov, A. V.; Gomma, E. F.; Starinskiy, A. D.; Atoyan, K. M. (Candidate of technical sciences)

ORG: L'vov Polytechnical Institute (L'vovskiy politekhnicheskiy institut); L'vov Bus Plant (L'vovskiy avtobusnyy zavod)

TITLE: Experimental investigation of the power capacity of brake mechanisms

SOURCE: Avtomobil'naya promyshlennost', no. 5, 1966, 29-31

TOPIC TAGS: vehicle braking system, test stand, vehicle component

ABSTRACT: The authors describe a combination stand developed at the L'vov Polytechnical Institute to be used for both inertial and constant braking tests. A diagram of the installation is shown in the accompanying figure. The principal elements of the stand are: .100 kw electric motor 1; clutch and gearbox 2 mounted on the clutch bracket; flywheel 3 with a moment of inertia of 16 kg·sec^2; brake mechanism 4 with the drum mounted on the flywheel shaft while the disc and shoes are mounted on the clutch shaft 5 which is coaxial with the flywheel shaft. The stand is equipped for measuring the braking moment and the moment on the release shaft, the temperatures of the brake linings and drum, the rotational velocity of the drum, the pressure in the brake chamber and rod travel. Provision is made for programmed control of brake operation. The device may be used for studying the effect of a variety of factors on the power capacity of braking mechanisms. Orig. art. has: 4 figures, 3 tables.

Card 1/2

SUB CODE: 13/ UDC: 629.11.013.001.5

Card 2/2 vlr

KOBYLYASHNYY, A.A.

Use capital assets with maximum efficiency and gain in time.
Shakht. stroi. 7 no.6:7-8 Je '63. (MIRA 16:7)

1. Sverdlovskaya oblastnaya kontora Stroybanka SSSR.
(Mining industry and finance)

KOBYLYATSKIY, I.

Lateral femoral hernia. Khirurgiia Jupplement:45 '57. (MIRA 11:4)

1. Iz Yur'yevskoy rayonnoy bol'nitsy Dnepropetrovskoy oblasti.
(HERNIA)

KOBYLYATSKIY, S.F., kand. tekhn. nauk

Equidimensional cylindrical projection possessing characteristics of the Tissot projection. Uch. zap. Pens. inzh.-stroi. inst. no.21 77-80 '62. (MIRA 17:11)

KOBYLYANSKIY, V.D.

Vernalization stage in wild barley species. Agrobiologiia no.3: 448-449 My-Je '62. (MIRA 15:10)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut rasteniyevodstva, Leningrad.

(VERNALIZATION) (BARLEY)

KOBYLYATSKIY, S. F., Candidate Tech Sci (diss) -- "Equal-scale perspective-conic projections for compiling large-scale agricultural maps". Khar'kov, 1959. 17 pp (Min Agric USSR, Khar'kov Order of Labor Red Banner Agric Inst im V. V. Dokuchayev), 150 copies (KL, No 25, 1959, 134)

RABINOVICH, Avram Nakhimovich, doktor tekhn. nauk; YAKHNOVICH, Vladimir Aleksandrovich, inzh.; BOYECHKO, Bogdan Yulianovich, kand. tekhn. nauk. Prinimali uchastiye: KOBYLYUKH, B.F.; GAVRILYUK, V.I.; KAMYSHNYY, N.I., doktor tekhn. nauk, retsenzent; CHERNIS, N.Kh., inzh., retsenzent

[Automatic vibratory feed mechanisms] Avtomaticheskie zagruzochnye ustroistva vibratsionnogo tipa. Kiev, Tekhnika, 1965. 379 p. (MIRA 18:3)

RABINOVICH, A.N., doktor tekhn.nauk; KOBYLYUKH, B.F.

Pulsating pneumatic drive for vibratory feed mechanisms.
Mashinostroitel' no. 4:13-15 Ap '61. (MIRA 14:4)
(Feed mechanisms)