Determination of the phase...

S/207/62/000/005/003/012 B108/B186

SUBMITTED:

July 11, 1962

Legend to Table 7: (1) p, kg/cm<sup>2</sup>; (2) graphite

1	β.10•							
<b>Φ</b> , κΓ/cπ <sup>3</sup>	РЬ	AgCi 17—132°C	графит 21—134°С	BN 23-130	T1 22-133	Hi		
p, at just	20-123°C					25-100	110	[1,2]
	20-12-0	11-1:12 0	21-134-0	•c	•c	•0	8	3)-75 °C
5000 10000 15000 20000 25000 30000	90 80 71 58 44 45 37	28 21 56 74 73 55 20	25 25 21 15 8 5	35 20 9 1 2 2 3	92 88 85 80 74 69 62	40 23 22 32 32 58	40 32 27 22 24 22	40 38 46 62 86 125

Card 2/2

LIVSHITS, L.D.; GENSHAFT, Yu.S.; MARKOV, V.K.

Diagram of state of cerium in the range 20 to 350°C at pressures up to 80.103 Kg./cm<sup>2</sup>. Zhur. eksp. i teor. fiz. 43 no.4:1262-1267 0 62. (MIRA 15:11)

1. Institut khimicheskoy fiziki AN SSSR. (Phase rule and equilibirum) (Cerium) (High-pressure research)

LIVSHITS, L.D.; MARTYNOV, Ye.D.

Laboratory apparatus for compressing liquids at pressures up to 20 kat. Prib. i tekh. eksp. 8 no.3:161-164 My-Je '63. (MIRA 16:9)

1. Institut khimicheskoy fiziki AN SSSR. (High-pressure research-Equipment and supplies)

L 10660-63 EWP(q)/EWT(m)/BDS--AFFTC/ASD--JD

ACCESSION NR: AP3001209

S/0078/63/008/006/1302/1306

AUTHOR: Livshits, L. D.; Genshaft, Yu. S.; Ryabinin, Yu. N.

TITLE: Phase diagram of crystal hydrates MgSO sub 4 at high pressures

SOURCE: Zhurnal neorganicheskoy khimii, v. 8, no. 6, 1963, 1302-1306

TOPIC TAGS: phase diagram, crystal hydrates of MgSo sub 4, polymorphic transition, phase transitions, MgSO sub 4

ABSTRACT: A phase diagram of the crystal hydrates of MgSO sub 4 was constructed from measurements obtained by the "piston displacement" method; data was obtained at 20 degrees by volume compressibility of salts which were previously dehydrated at 200 degrees. A polymorphic transition in the region of 4500 kg/sq.cm. pressure was discovered. The phase transition in the crystalline hydrates is sensitive to the quantity of water of crystallization; by decreasing the content of bonded water, the discontinuities in the volume upon compression are blurred, down to a complete disappearance of separate transitions. There is a limit in the piston displacement method above which the liberated water interferes with the measurement of change in volume decrease with pressure. Actual crystalline conditions of the salt under pressure can be studied by X-rays, but it may be assumed that

**Card** 1/2

NASARI MERKATSERI SARARI ME

L 10660-63

ACCESSION NR: AP3001209

رد

significant volume change with the transitions indicates important structural changes in the material. Orig. art. has: 3 figures.

ASSOCIATION: Institut khimicheskoy fiziki Akademii nauk SSSR (<u>Institute of chemical Physics</u>, <u>Academy of Sciences SSSR</u>). Institut fiziki Zemli Akademii nauk SSSR (<u>Institute of Earth Physics</u>, <u>Academy of Sciences SSSR</u>)

SUBMITTED: 28May62

DATE ACQD: 01Jul63

ENCL: 00

SUB CODE: 00

NO REF SOV: 004

OTHER: 003

kes/2-

HYABININ, Yu.N.; PETROV, V.P.; MARKOV, V.K.; LIVSHITS, L.D.; DELITSIN, I.S.

Additional data on the conditions governing the formation of the dense modifications of silica at high pressures and temperatures. Izv. AN SSSR.Ser.geol. 28 no.8:3-10 Ag '63. (MIRA 17:2)

1. Institut fiziki Zemli AN SSSR i Institut geologii rudnykh mestorozhdeniy, petrografii, mineralogii i geokhimii AN SSSR, Moskva.

ACCESSION NR: AP4025911

8/0056/64/046/003/0821/0824

AUTHORS: Livshits, L. D.; Genshaft, Yu. S.

TITLE: Nonlinear dependence of the magnetic transformation temperatures of two invar alloys on the hydrostatic pressure

SOURCE: Zhurnal eksperimental'noy i teoreticheskoy fiziki, v. 46, no. 3, 1964, 821-824

TOPIC TAGS: Curie temperature, magnetic transformation temperature, phase transition, second order phase transition, invar, coelinvar, elinvar, Curie temperature pressure dependence, high pressure ferromagnetic transformation, ferromagnetic transformation

ABSTRACT: The pressure dependence of the Curie temperature of the elinvar and coelinvar alloys was studied at pressures up to 20 kbar as part of an investigation of second-order phase transitions under pressure. The relation

Card 1/43

7 (3/1

ACCESSION NR: AP4025911  $\Delta\theta = \theta_p - \theta = -ap - bp^4,$ ( $\Theta$  — temperature of magnetic transformation at pressure p,  $\Theta$  — temperature, a and b — constants) is found to hold for both alloys. Although such a nonlinear relation follows from the theory, previous experiments yielded only linear relations, probably owing to the smallness of the range of variation of the pressures employed and in some cases to the smallness of the effect itself. A tentative value  $d\Theta/dR = 3--3.5 \times 10^{11}$  deg/cm is obtained for both alloys (R — interatomic radius, on the order of 2.5 Å). "The material for the samples was graciously furnished by G. I. Katayev, to whom the authors are deeply grateful. They also thank Yu. N. Ryabinin and R. Z. Levitin for interest in this work." Orig. art. has: 3 figures, 4 formulas, and 1 table.

ACCESSION NR: AP4025911

ASSOCIATION: Institut fiziki zemli AN SSSR (Institute of Physics of the Earth, AN SSSR)

SUBMITTED: 14Aug63 DATE ACQ: 16Apr64 ENCL: 01

SUB GODE: PH NO REF SOV: 006 OTHER: 001

ACCESSION NR: AP4010755

\$/0020/64/154/001/0086/0087

AUTHOR: Livshits, L. D.; Ryabinin, Yu. N.; Beresnev, B. I.; Marty\*nov, Ye. D.

TITLE: A new relationship between the elastic limit and pressure

SOURCE: AN SSSR. Doklady\*, v. 154, no. 1, 1964, 86-87

TOPIC TAGS: elastic limit, high pressure metallurgy, axial tension of materials, rate of deformation

ABSTRACT: The authors have investigated the elastic limits of various steels and of brass under high pressure. Their method of investigation differs from that previously used by a very high rate of deformation. The elastic limit E (the natural logarithm of the ratio of areas of the specimen cross sections before and after rupture) was measured as a function of pressure p. In the previous work (mainly by Bridgman), a proportionality between E and p has been

Card 1/2

ACCESSION NR: AP4010755

found in many metals and alloys. It is shown in the present work, that in some materials there is a relationship of a new type between E and p. At lower pressures, there is almost no effect of p on E. The rate of axial deformation has no effect on the dependence of the elastic limit on pressure. Orig. art. has: 2 figures.

ASSOCIATION: Institut fiziki Zemli im O. Yu. Shmidta Akademii Nauk SSSR (Institute for the Earth Physics).

SUBMITTED: 05Apr63

DATE ACQ: 10Feb64

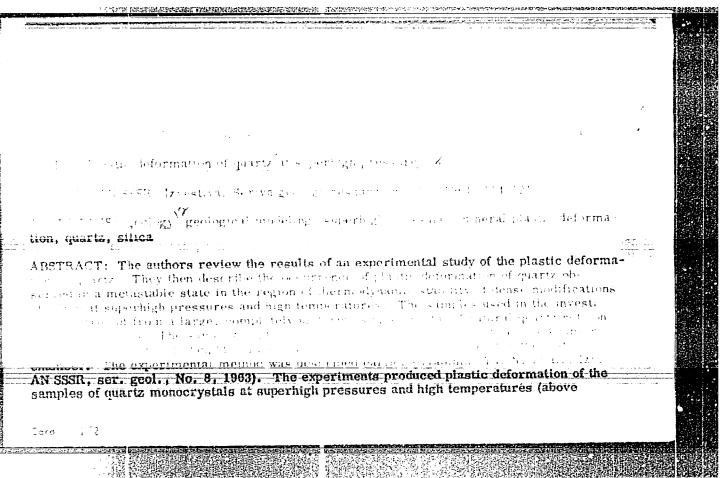
ENCL: 00

SUB CODE: PH, ML

NO REF SOV: 003

OTHER: 001

Cord 2/2



L 25621-65 ACCESSION NR: AP4049998 The deformation within a single sample was quite complex, as can be judged and the state of the control of the The state of the s develops for the most part either paramento me piane on the option and of an terial or perpendicular to it. "The authors wish to thank . I. Lukin and V.F. Cherny\*shey for examination of the polished sections and hiscussion of this laper." Originart has 4 figures. ASSOCIATION: Institut fiziki Zemli AN SSSR (Institute of Physics of the Earth, AN S.SR); Institut geologii rudny\*kh mestorozhdeniy, petrografii, mineralogii i geokhimii AN SSSR, Moscow (Institute of the Geology of Ore Deposits, Petrography, Mineralogy and Geochemstry AN SSSR) SUB CODE: Ex 10 ENCL: 00 SUBMITIED: 25Mar64 OTHER TH - R/ V - 008

# "APPROVED FOR RELEASE: 06/20/2000 CIA-R

CIA-RDP86-00513R000930310006-9

EAT(n)/EMA(d)/EAP(t)/EAP(k)/EAP(t)JT/4M/JO 1 271-5-65 most/45/035/902/9348/0354 ACCESSION NR: AP5005241 AUTHOR: Livshits, L. D.; Ryabinin, Yu. N.; Beresnev, B. I. TITLE: Effect of pressure on the ductility of metals SOURCE: Zhurnal tekhnicheskoy fiziki, v. 35, no.2, 1965, 348-354 chromium, chromium ductility, hydrostatic pressure, ductility pressure dependence ABSTRACT: To determine the effect of high hydrostatic pressure on the ductility of metals, specimens of pure forged chromium were subjected to tensile tests at ambient hydrostatic pressures of up to 18,000 kg/mm<sup>2</sup>. The curves of the ultimate deformationpressure dependence showed that pressures of up to  $4000-5000~{\rm kg/mm^2}$  have little or no effect on the ultimate elongation, but with a further increase in the pressure the elongation sharply increases. An analysis of the results showed that similar behavior is exhibited by a number of other brittle and low-ductility metals. The metal grain size appears to have no effect on the e-p dependence. This indicates the major role of the condition of grains and the secondary importance of grain boundaries. To obtain a more exact evaluation of the effect of individual deformationpressure factors, further investigation is required. Orig. art. has: 6 figures. Card 1/2

L 27188-65

ACCESSION NR: AP5005241

ASSOCIATION: Institut fiziki čemli im. O. Yu. Shmidta AN SSSR, Moscow (Institute

of Physics of the Earth, AN SSSR)

SUBMITTED: 09Mar64

ENCL: 00

SUB CODE: MM

NO REF SOV: 003

OTHER: 002

ATD PRESS: 3191

20.10.5%的中国68.5%的特别的基础的特别的10.0%。

JD/JG EVIT (m)/EVIP(t)/EWP(b) IJP(c) ACCESSION NR: AP5010496 UR/0056/65/048/004/1050/1053 AUTHOR: Livshits, L. D.; Genshaft, Yu. S. Shift of Curie temperature of gadolinium under hydraulic compression up to TITLE 35 Kbar SOURCE: Zhurnel eksperimental'noy i teoreticheskoy fiziki, v. 48, no. 4, 1965, 1050-1053 TOPIC TACS: gadolinium permeability, gadolinium Curie point, gadolinium permeability pressure shift, gadolinium Curie temperature shift ABSTRACT: The pressure dependence of permeability was plotted at a constant temperature at a frequency of 500 cps and an effective field intensity of 5-6 fe. The pressure was applied through a silver on order medium by the fistin displa ement The specimens were miniature to make of polycrystalline metal turned from and the original gadolinium with the following almixtures. It and The 18 (3) 18%), Fe (0.01%), and Cu (0.005%). The temperature fluctuations during the experiment did not exceed 0.5-1C. The pressure dependence curve of the Curie point was plotted on the basis of twelve independent determinations of the pressure or a ser which the specimen changed to the paramagnetic state. As expected this 1/2 Card the state . 

L 41068-65 ACCESSION NR: AP5010496		
curve was a straight line with kbar. The mean deviation of the straight temperature and 0.6 kb traight kbar pressure range inys fev., 1.4, 1964, A187), 1 formula.	he experimental points from ar in pressure. A disconting of the surve, as described	the straight line was uity of the ourse within by Pobinson and others
ASSOCIATION: Enstitut fiziki the Earth, Academy of Sciences		stitute of Physics of
EUBKITTED: 09Nov64	ENCL: 00	SUB CODE: SSEM
NO PEF SOV: 005	CTHER: 007	ATD PRESS: 3232

r 40284245 ACCESSION I	ENT(E)/ENP(k) R: AP5011530	)/EMA(c)/T/EMP(b)/E	WA(d)/EMP(*)/EMP(16	Pf-4 IJP(c) 1/005/1077/1080	
AUTHOR: L	venits. L. D.; Be	eresnev, B. I.; Ryab:	nin, Yu. N.	8	
TITLE Tu	etility of the 50	ats Bi-50 ats In al	loy in tension under	a high pressure	
SOURCE: A	N SSSR. Doklady,	v. 161, no. 5, 1965	, 1077-1080		
TOPIC TAGS	: bismuth alloy, lity relationship	tin containing allo , brittleness ductil	y, alloy ductility, ity transition		
ARGURACU:	Binary Bi-Sn all	oy containing 50 at	Hi was air cooled '	or water quenoued. ature at pressures	
naturally	agen and then so	bjected to tension to the all the second tree because here	loy fracture was br	ittle. With a	
further in 1400—1500 4.5%, and the alloy increased	trease in pressur kg/cm <sup>2</sup> range the the reduction of ductility decrease agein to the second ty to zero in	e the fracture became alloy ductility sha area was 99.9%. With sed, passed through and maximum at a protect 11,000—11,500 ,000—20,000 kg/cm², e, while above 20,000	arply increased, the the further increase minimum at a press source of 10,000—11, kg/cm² range. With	e in pressure ure of 6500 kg/cm <sup>2</sup> , 000 kg, and dropped an increase in	
Card 1/2	union, aprilia	- · · · · · · · · · · · · · · · · · · ·			

### "APPROVED FOR RELEASE: 06/20/2000

#### CIA-RDP86-00513R000930310006-9

1. 49284~65

ACCESSION NR: AP5011530

and the fracture became brittle. Thus, the experimental results revealed a new phenomenon—the existence of pressure ranges within which a material can have a nigher or a lower ductility. It is assumed that this phenomenon is associated with permitarities of the p, T-diagram of the alloy. Orig. art. has: 2 figures. [MS]

ASSOCIATION: Institut fiziki zemli im. O. Yu. Shmidta Akademii nauk SSSR (Institute of Physics of the Earth, Academy of Sciences, SSSR)

SUBMITTED: 210ct64

ENCL: 00

SUB CODE: MM

NO REF SOV: 008

OTHER: 004

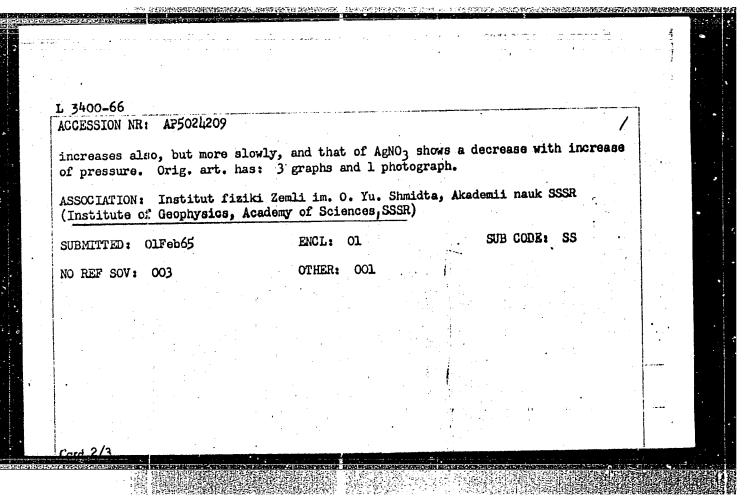
ATD PRESS:

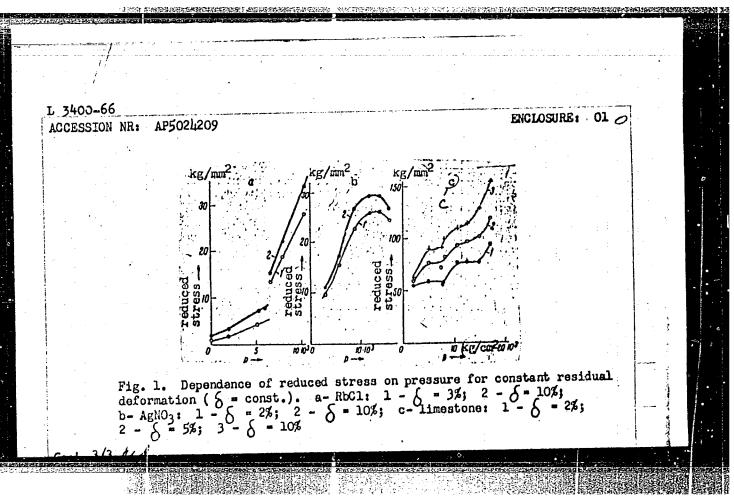
4005

BJB

Card 2/2

	the state of the s
3400-66 EPA(s)-2/EWT(m)/EWP(w)	)/EPF(c)/EPF(n)-2/T/EWP(t)/EWP(b)
3400-66 EPA(8)-2/EWT(M)/EWP(W) CCESSION NR: AP5024209	UR/0020/65/164/003/0541/0544
UTHORS: Livshits, L. D.; Beresnev	, B. I.; Genshaft, Yu. S.; Ryabinin, Yu. N.
Annual Control of the	1 substances in the region of polymorphic 32 B
OURCE: AN SSSR. Doklady, v. 164, n	10. 3, 1965, 541-544
OPIC TAGS: polymorphic transition, alcium carbonate	rubidium chloride, silver nitrate, limestone,
investigation is an extension of presuthors (DAN, 161, 5, 1965). Axial high hydrostatic pressures. The speciameter, and had a length-to-diameter are presented and see Fig. 1 on the Enclosure). It is a second and the second are presented and see Fig. 1 on the Enclosure and the second are presented and see Fig. 1 on the Enclosure are presented as the second are pres	n RbCl, AgNO3, and limestone was studied. The evious work on Bi-Sn alloys published by the compression of specimens was determined at ecimens were of cylindrical shape, 8-10 mm in ter ratio of 1 to 1.5. Photographs of the stress-strain curves are shown graphically is concluded that pressure affects the strength during polymorphic transitions. Thus the increases with pressure, that of limestone
ard 1/3	





MARKOV, V.K.; LIVSHITS, L.D.; BELITSIN, I.S.; RYABINIE, Yu.N.; HITROV, V.P.

Conversions in magnesium metasilicate under high pressures and temperatures. Tzv. AN SSSR. Ser. geol. 30 no.7:38-49 51 '65.

(MIFA 18:7)

1. Institut fiziki Zemli AN SSSR, i Institut geologii rudnykh mestorozhdeniy, petrografii, mineralogii i geokhimii AN SSSE, Moskva.

LIVSHITS, L. C., Engr. Gand. Tech. Noi.

Dissertation: "Theoretical and Experimental Substantiation of the High Cooling Fates of Babbits B-83, B-N and B-T During Their Pouring into Peerings." All-Union 5:1 Res Inst of Mechanization and Electrification of Agriculture - "VNE" 1 Jul 47.

S0: Vechernyaya Moskva, Jul, 1947 (Project #17836)

ASSES MATERIAL AND PROPERTY OF THE PROPERTY OF LIVEHITE, L. G. PA 18/4/TV1 USSR/Metals Dec 48 Steel, Chromium-Nickel Steel, Structural "Low-Alloy Structural Steel, " L. G. Livshits, Cand Tech Sci, G. A. Torpanovc, Engr, TeNIICherMET, 4 pp "Stal'" No 12 Some alloy structural steels (in particular, those containing molybdemum) can be successfully replaced in many cases by proposed lowalloy steels of low chromium and nickel content. Includes nine diagrams, one microphotograph, and three tables. <u> 18/49791</u>

LIVSHITS, L. G.

O metodakh povysheniia iznosostoikosti detalei traktornykh dvigatelei. (Vestn. Mash., 1950, no. 10, p. 30-32)

Methods of increasing the resistance to wear of traction engine parts.

DLC: THA.V4

SO: Manufacturing and Mechanical Engineering in the Soviet Union, Library of Congress, 1953.

ARTEM YEV, Yu.N., kandidat tekhnicheskikh nauk; ALEKSEYEV, I.A., inzhener; ASTVATSATUROV, G.G., inzhener; BISNOVATYY, S.I., inzhener; BONDAREN-KO, A.F., inzhener; GURAL'NIK, Ye.L., inzhener; GORBUNOV, M.F., inzhener; ZIATKOVSKIY, A.P., kandidat tekhnicheskikh nauk; KATTS, N.V., inzhener, KITAYEV, A.S., inzhener; KOZLOV, A.M., inzhener; LEOHOV, P.T., inzhener; LIVSHITS, L.G., kandidat tekhnicheskikh nauk; LIBERMAN, A.R., inzhener; LINNIK, Ye.M., inzhener; LUKANOV, M.A., inzhener; MOROZOV, S.A., inzhener; POGORELYY, I.P., kandidat tekhnicheskikh nauk; PETROV, S.A., kandidat tekhnicheskikh nauk; PYATETSKIY, B.G., inzhener; RABOCHIY, L.G., kandidat tekhnicheskikh nauk; SELIVANOV, A.I., kandidat tekhnicheskikh nauk; FERBERG, B.S., kandidat tekhnicheskikh nauk; CHISTYAKOV, V.D., inzhener; CHUNIKHIN, V.M., inzhener; SHIRYAYEV, A.I., inzhener; SHCHUPAK, A.D., inzhener; KUCHUMOV, P.S., inzhener, redaktor; PETROV, S.A.; PESTRYAKOV, A.I., redaktor; BALLOD, A.I., tekhnicheskiy redaktor.

[Handbook of equipment for repairing tractors and agricultural machinery] Spravochnik po oborudovaniiu dila remonta traktorov i seliskokhosiaistvennykh mashin. Moskva, Gos. izd-vo selkhos. lit-ry, 1954. 646 p. (MLRA 7:11)

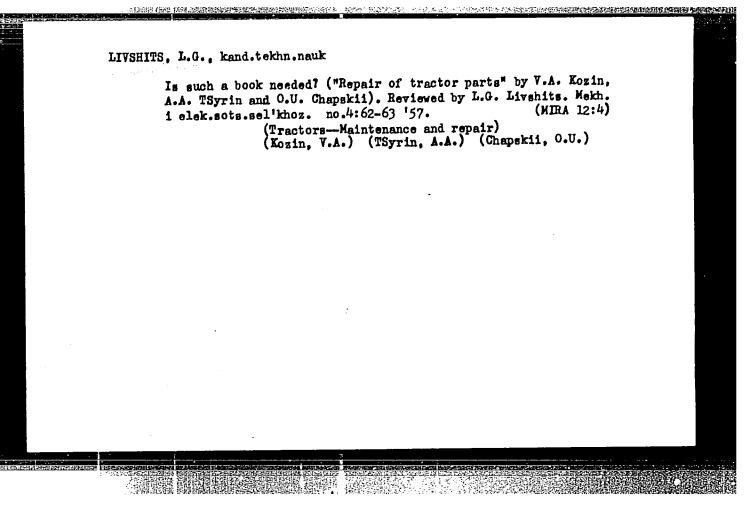
(Tractors -- Repairing) (Agricultural machinery -- Maintenance and repair)

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930310006-9"

KUTOVOY, I.D.; DEPARMA, V.N.; LIVSHITS, L.G.; KOROLEV, N.V.; DEMIN, V.S., insheher, redakter; OGIUBLIN, K.S., redaktor; MAYBORODA, M., tekhnicheskiy redaktor.

[Repair equipment for machine-tracter stations. Apparatus, devices and tools shown at the All-Union Agricultural Exhibit; a reference manual] Rementace obscudevanie masterskei MTS. Pribety, prispesselemiia i instrumenty, ekspeniruemye na VSEhV; spravechnik. Moskva, Gos.isd-ve kul'turno-prosvetitel noi lit-ry, 1955. 175 p. (MRA 9:6)

1. Moscow. Vsesoyuznaya seliskokhozyaystvennaya vystavka, 1954-. (Agricultural machinery--Repairing)



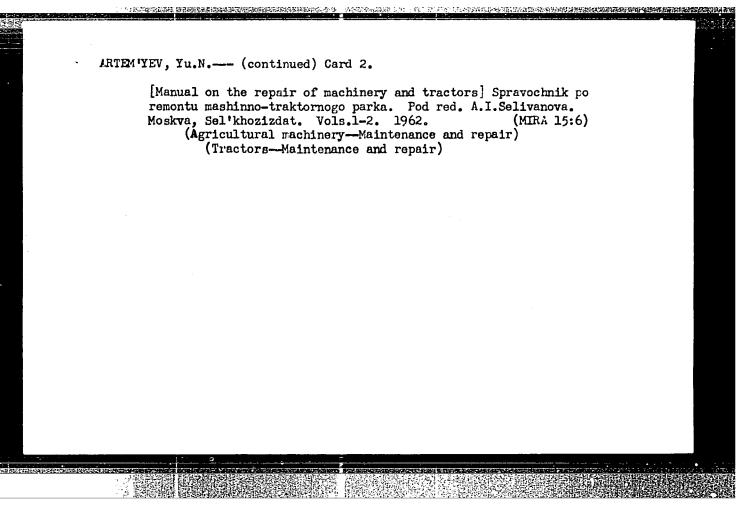
NOTE: The Control of the Control of

LIVSHITS, L.G., Fund.tekhn.nauk; KOROLEV, N.A., inzh.

ar riserranian communic

Gold welding of cast iron agricultural machinery parts. Svar. proizv. no.10:38-40 0 '61. (MIRA 14:9)

ARTEMIYEV, Yu.N., kand. tekhn. nauk; ASTVATSATUROV, G.G., inzh.; BARABANOV, V.Ye., inzh.; BARYKOV, G.A., inzh.; BISHOVATYY, S.I., inzh.; GALAYEVA, L.M., inzh.; GAL'PERIN, A.S., kand. tekhn. nauk; GAL'CHENKO, I.I., inzh.; GONCHAR, I.S., kand. tekhn. nauk; DEGTYAREV, I.L., kand. tekhn. nauk; DYADYUSHKO, V.P., inzh.; YERMAKOV, I.N., inzh.; ZHOTKEVICH, T.S., inzh.; ZUSMANOVICH, G.G., inzh.; KAZAKOV, V.K., inzh.; KOZLOV, A.M., inzh.; KOROLEV, N.A., inzh.; KRIVENKO, P.M., kand. tekhn. nauk; LAPITSKIY, M.A., inzh.; LEBEDEV, K.S., inzh.; LIBERMAN, A.R., inzh.; LIVSHITS, L.G., kand. tekhn. nauk; LOSEV, V.N., inzh.; LUKÁNOV, M.A., inzh.; LYUBCHENKO, A.M., inzh.; MAMEDOV, A.M., kand. tekhn. nauk; MATVEYEV, V.A., inzh.; ORANSKIY, N.N., inzh.; POLYACHENKO, A.V., kand. tekhn.nauk; POFOV, V.P., kand. tekhn. nauk; PUSTOVALOV, I.I., inzh.; PYTCHENKO, P.I., inzh.; PYATETSKIY, B.G., inzh.; RABOCHIY, L.G., kand. tekhn. nauk; ROL'BIN, Ye.M., inzh.; SELIVANOV, A.I., doktor tekhn. nauk; SEMENOV, V.M., inzh.; SKOROKHOD, I.I., inzh.; SLAHODCHIKOV, V.I., inzh.; STORCHAK, I.M., inzh.; STRADYMOV, F.Ya., kand. tekhn. nauk; SUKHINA, N.V., inzh.; TIMOFEYEV, N.D., inzh.; FEDOSOV, I.M., kand. tekhn. nauk; FILATOV, A.G., inzh.; KHODOV, L.P., inzh.; KHROMETSKIY, P.A., inzh.; TSVETKOV, V.S., inzh.; TSEYTLIN, B.Ye., inzh.; SHARAGIN, A.M., inzh.; CHISTYAKOV, V.D., inzh.; BUD'KO, V.A., red.; PESTHYAKOV, A.I., red.; GUREVICH, M.M., tekhn. red. (Continued on next card)



KR SECT DOCUMEN DESCRIPTION OF THE PROPERTY OF

LIVSHITS, L.G., kand. tekhn. nauk; POLYACHENKO, A.V., kand. tekhn. nauk; DMITRIYEV, I.N., red.; MAKHOVA, N.N., tekhn. red.; SOKOLOVA, N.N., tekhn. red.

[Reconditioning motor-vehicle and tractor parts]Vosstanovlenie avtotraktornykh detalei. Moskva, Sel'khozizdat, 1962. 319 p. (MIRA 15:10)

1. Gosudarstvennyy vsesoyuznyy nauchno-issledovatel'skiy tekhnologicheskiy institut remonta i ekspluatatsii mashinnotraktornogo parka (for Livshits, Polyachenko). (Tractors—Maintenance and repair)

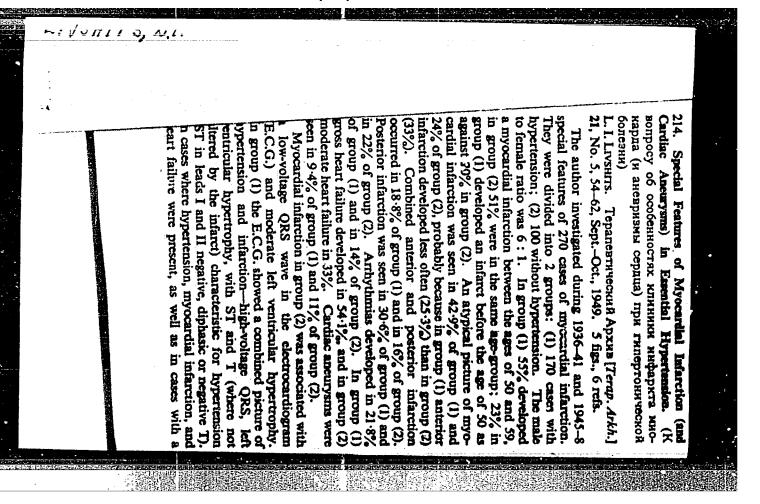
(Motor vehicles-Maintenance and repair)

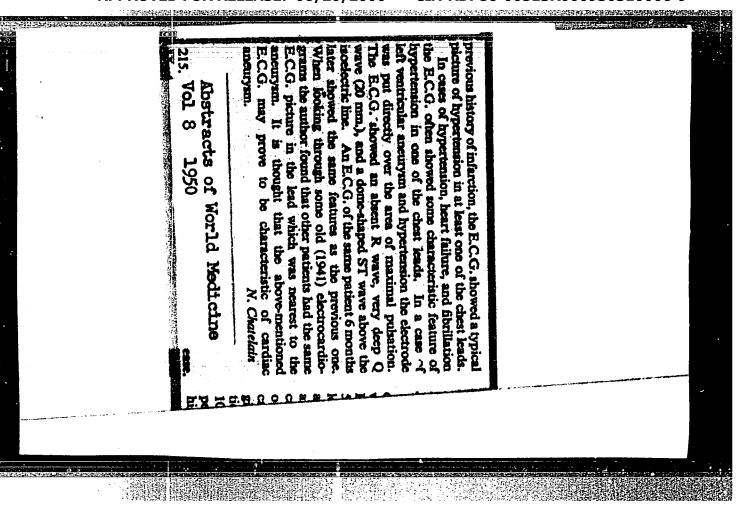
ABELEVICH, A.A.; ARTEM'YEV, Yu.N.; VLASOV, A.P.; GAL'PERIN, A.S.; YEVSIKOV,
A.V.; IVANOV, G.P.; KOROLEV, N.A.; LEVITSKIY, I.S.; LIVSHITS, L.G.;
MELKOV, M.P.; NAZAROV, H.I.; NOVIKOV, M.P.; POPOV, V.Ta.; TEPLOV,
A.G.; BAKHAREV, A.P., inzh., retsenzent; SAVEL'YEV, Ye.Ya., red. 1zdva; MODEL', B.I., tekhm. red.; EL'KIND, V.D., tekhm. red.

[Technological aspects of the repair of crauler vehicles] Tekhnologiia remonta gusenichnykh mashin. Moskva, Gos. nauchno-tekhn. izdvo mashinostroit. lit-ry 1960. 466 p.

(Crauler vehicles—Maintenance and repair)

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930310006-9"





PINGUIIO, Pri

Category : USSR/Magnetism - Experimental methods of magnetism

F-2

Abs Jour : Ref Zhur - Fizika, No 1, 1957 No 1389

Author : Korsunskiv, M.I., Fogel ', Ya.M., Bykova

: Korsunskiy, M.I., Fogel\*, Ya.M., Bykova, G.A., Livshits, L.I., Lozovskiy, N.S.

Chovnik, A.A.

Title : Investigation of the Topography of the Inhomogeneous Plane Magnetic Field

of a Six-Pole Electromagnet.

Orig Pub : Zh. tekhn. fiziki, 1956, 26, No 2, 1222-1232

Abstract : A procedure is described for the investigation of the topography of an

inhomogeneous plame magnetic field of a six-pole electromagnet, used to focus particles that have a magnetic moment. The cited measurement results show that the above field can be produced without substantial distortion in

a circle 10 cm in radius.

Card : 1/1

1. 上京中华人,在市场大学的企业的企业的企业的企业的企业的企业的企业的企业的企业的企业的企业。

SHUL'MEYSTER, Boris Iosifovich: LIVSHITS, L.M., inzh., retsenzent; MELEYEV, A.S., inzh., red.; SAVEL'IEV, Ye.Ya., red.izd-va; TIKHANOV, A.Ya., tekhn.red.; EL'KIND, V.D., tekhn.red.

[Repair and assembling of stationary diesel engines] Remont i montazh statsionarnykh dizelei. Moskva, Gos.nauchno-tekhn. izd-vo mashinostroit.lit-ry, 1959. 267 p. (MIRA 13:1) (Diesel engines--Maintenance and repair)

# LIVSHITS, L.M. Redesigning the slag cars by changing the cinder ladle from 11 to 16.5 m. Metallurg 9 no.1:12-14 Ja '64 (MIRA 18:1) 1. Metallurgicheskiy zavod im. Petrovskogo.

KOVALENKO, N.I., inzh. (Minsk); LIVSHITS, L.M. (Minsk)

Gutter spout funnels on the sloping roofs of industrial buildings. Vod. i sun. tekh. no.3s9.11 '64 (MIRA 18:2)

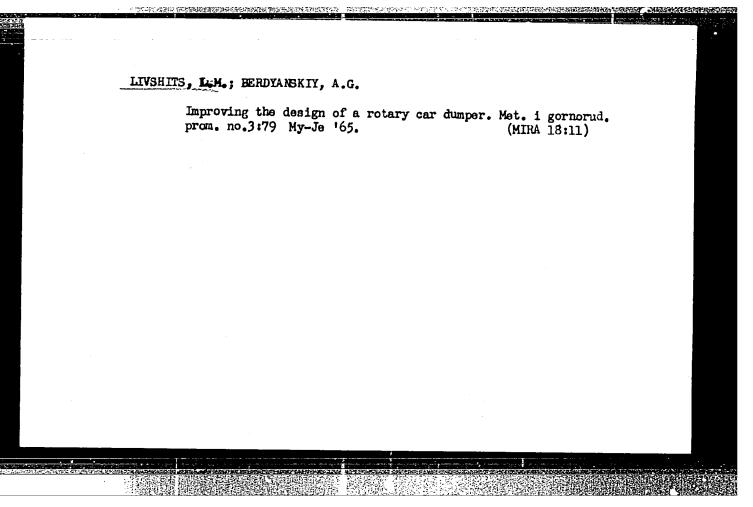
LIVSHITS, L.N., inzh.; PETROV, V.P., inzh.; VALGE, I.A., inzh.; BERESNEV, A.T., inzh.

THE RESERVE THE PARTY OF THE PA

Manufacture of welded beams of the V92-T aluminum alloy. Prom. stroi. 40 no.12:23-28 '62. (MIRA 15:12)

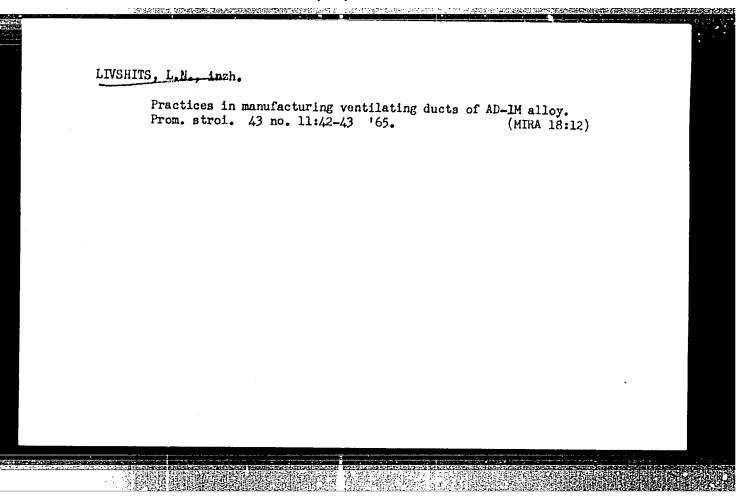
1. Chelyabinskiy zavod metallokonstruktsiy imeni Ordzhonikidze (for Livshits).

(Aluminum alloys) (Beams and girders)



LIVSHITS, L.M., inzh.

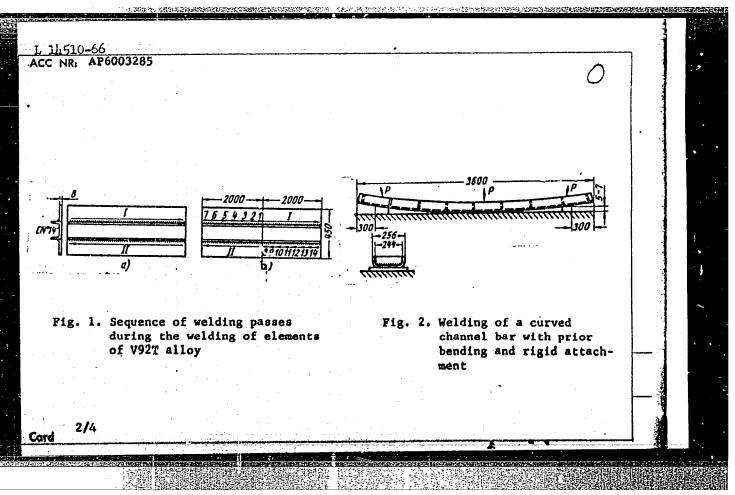
Mechanization of labor-consuming operations in a metallurgical plant. Mekh. i avtom. proizv. 18 no.10:17-20 0 '64. (MIRA 17:12)

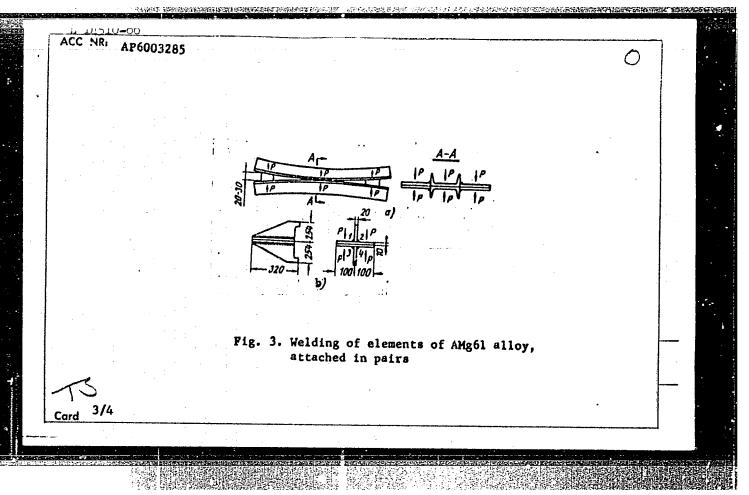


### "APPROVED FOR RELEASE: 06/20/2000 CIA-RDI

CIA-RDP86-00513R000930310006-9

EWT(m)/EWA(d)/T/EWP(v)/EWP(t)/EWP(k)/EWP(z)/EWP(b) IJP(c) I. 11510-66 ACC NRI AP6003285 SOURCE CODE: UR/0135/66/000/001/0026/0028 AUTHOR: Livshits, L. N. (Engineer) Chelyabinsk Metal Structural Elements Plant im. Ordzhonikidze (Chelyabinsk zavod metallokonstruktsiy ) TITLE: Instances of the prevention and elimination of deformations during the fabrication of welded structural elements of aluminum 47,55 2/ SOURCE: Svarochnoye proizvodstvo, no. 1, 1966, 26-28 fabricated structural metal, aluminum, welding technology, material TOPIC TAGS: deformation ABSTRACT: The fabrication of welded structural elements of aluminum alloys involves difficulties due to the easy deformability of aluminum -- a metal that, compared with steel, displays a lower modulus of elasticity, greater shrinkage on solidification, and a higher coefficient of linear expansion. In this connection, the effect of various design and technological factors on the deformation of welded structural elements of AMg6, AMg61 and V92T aluminum alloys was investigated at the Chelyabinsk Metal Structural Elements Plant and, as a result, the following techniques for the prevention and elimination of deformations have been developed: 1. The welding is 41,55 19 UDC: 621.791.015:624.014.25:669.715 Card 1/4

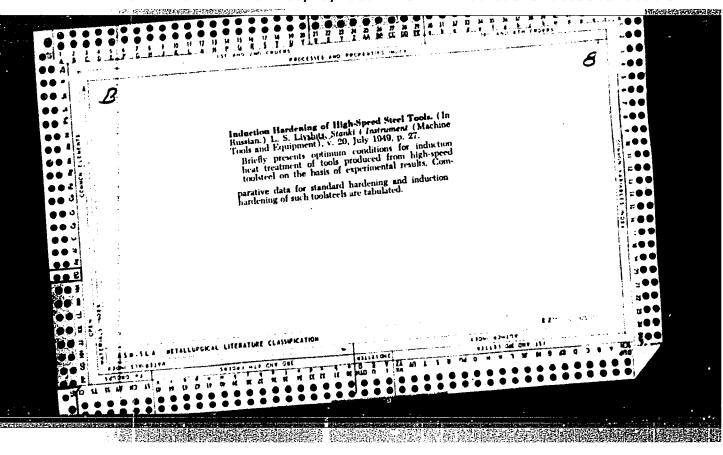


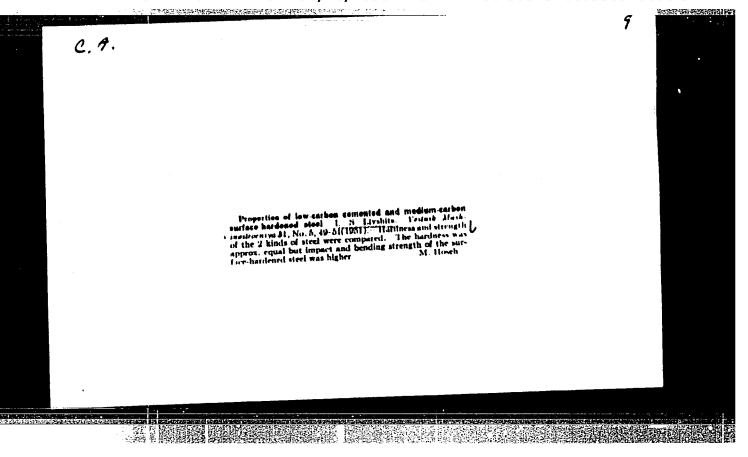


**2011年時中世界中央市場中央中央市場中央市場等在**161 "是一定是是是你还可以到的自己的是是是是一个,我们可以是一个 <u>i 14510-66</u> ACC NR: AP6003285 commenced at center of the element and proceeds toward its ends (Fig. 1, b). This confines the deformation to permissible limits (10-15mm) compared with the 120-150 mm deformation produced by conventional welding sequence (Fig. 1, a). 2. The welding is carried out in a rigid strap assembly and with prior bending of the H-beam (Fig. 2). This technique reduces residual deformation 3-5 times. 3. Welding of elements attached in pairs, e.g. T-beams (Fig. 3). Further, the effect of the combination of parts of various thickness in the weldment on its residual deformation was investigated. The welding of such parts is complicated, since then the thinner parts, with their smaller rigidity, greatly overheat so that residual deformations increase considerably. In this case it is best to perform welding by the semiautomatic consumable-electrode method which results in a more intensive local heating and hence in a faster welding rate which, in its turn, leads to a contraction of the zone of plastic deformations and the concomitant general decrease in residual deformations. The most effective method of preventing any marked residual deformations is the component-by-component method of fabricating structural elements which involves the division of the product into the largest possible number of symmetric or insignificantly asymmetric components which are separately assembled and welded together. Moreover, since it is not always practical, to carry out the cold straightening of deformed loadbearing structural elements of aluminum, it is advisable to apply hot straightening as based on the use of three heat sources: gas flame, electric arc and, particularly, "idle welds" applied by means of nonconsumable (tungsten) electrodes. Orig. art. has: 8 figures. SUB CODE: 11, 13/ SUBM DATE: none/ ORIG REF: 000/ OTH REF: 000

TO THE TOTAL PROPERTY OF THE P

EWP(k)/EWT(m)/EWP(w)/EWP(v)/EWP(t)/ETI L 11310-07 IJP(c) JD/H1 ALC NR: AR6022164 SOURCE CODE: UR/0137/66/000/003/E016/E016 AUTHOR: Livshits, L. N. TITLE: Prevention and elimination of deformations in manufacturing welded when SOURCE: Ref. zh. Metallurgiya, Abs. 3E111 REF SOURCE: Sb. Novoye v tekhnol. svarki stroit. konstruktsiy. M., 1965, 47-51 TOPIC TAGS: aluminum welding, metal deformation, consumable electrode ABSTRACT: The author studies the effect of various design alternatives and technological factors on deformability in making structural elements for bridges from Mg-6, AMg-61 and V92-T aluminum alloys. Among the factors investigated were the sequence in which the joints were made, selection of the welding method, welding in clamping fixtures and jigs, prebending, welding elements fastened in pairs, eliminating the effect of differences in thickness between the sheets to be welded, breaking down finished assemblies into separate subunits and straightening the finished product. It is concluded that tilting jigs should be used in making welded aluminum structural elements. The subunit method should be used for making complex aluminum structures. Deformation may be reduced by welding with a consumable electrode. Heating is effective for straightening aluminum structural elements although the work capacity of the element must be checked after this method is used. V. Fomenko. [Translation of abstract] SUB CODE: 11, 13 Card 1/1 bab UDC: 621.791.011:539.4.014.13.669.715





USER/Metallurgy - Welding, Steel,  Electrodes  Number of Kh5M Steel, "A.G. Mazel',  L.S. Livshits, Candidates Tech Sci, M. Ya. Chushen kova, Engr, MIStroynett' [Sci Res Inst for Construction of Enterprises of the Gas and Petroleum Indi]  "Avtogen Delo" No 7, pp 1-6  Investigates several types of electrodes for velding pipelines made of Kh5M Cr-Mo steel, videly used at petroleum refineries and working under pressure up to 70 atm and at temps up to 550° C.  233735  Experimentally establishes that electrodes made of 18-8 steel provide for obtaining velds with luwest teddency to hot crack formation and with highest erovelled. Editors disagree with authors, stating that their conclusions relate only to certain heats of 18-8 steel and cannot be generally accepted without preliminary test of electrodes.  233735
Pipes Made of Kn5M Steel," A.G. M. Shits, Candidates Tech Sci, M. Ya. Gr., NIIStroyneft' /Sci Res Inst for of Enterprises of the Gas and Pelo" No 7, pp 1-6  Lines made of Kn5M Gr.Mo steel, with the steel of Kn5M Gr.Mo steel, with the formation and working well of 70 atm and at temps up to 50 atm and at temps up to 51 hot crack formation and with high ance without preheating of pipes that electrodes relate only to certain heat tent of electrodes.
·

LIVSHITS, L. S., Mazel, A. G., and Chushenkova, M. Ya.

"The Welding of Chromium (42 per cent)-Molybdenum Steel Tubes" (Avto. Delo, 1952, 23, July, p. 1)

Type Kh5M ( $4\frac{1}{2}$  per cent Cr-Mol) steel is a creep-resisting steel used in the oil industry for tubular assemblies working at up to 70 atmospheres and 550 degrees C. In assembly shops, it may be welded with electrodes of the same wire composition and a low hydrogen lime-ferritic coating, but must be fully heat treated after welding. For site-welding, a molybdenum-bearing 18-8 austenitic electrode giving a duplex weld metal structure (i.e., containing some ferrite) must be used.

A hot cracking test is described, in which newly completed welds are impact tested; the criterion is the number of seconds during which the cooling weld still fractures brittle (cf. hot cracking test in ref. 18)

HI

XISLYUK, F.I., doktor tekhnicheskikh nauk; MAZEL', A.T. kandidat tekhnicheskikh nauk; FAL'KEVICH, A.S. 'inzhener; ANUCHKIN,'M.S., kandidat tekhnicheskikh nauk; LIVSHITS, L.S. kandidat tekhnicheskikh nauk; NEYFEL'D, inzhener; DANUMAKH, L.P., inzhener; POLYAKOVA, P.B., inzhener.

Welding with electrode cluster. Section of the All-Union Scientific Engineering Technological Association of Welders in the All-Union Scientific Research Institute for Petroleum Industry Construction. Avtog. delo 24 (MIRA 6:5) nc.6:30 Je '53. (Electric welding)

LIVSHITS, L.S., kandidat tekhnicheskikh nauk; MAXEL', A.G., kandidat

tekhnicheskikh nauk; CHUSHESKOWA, M.Ya., inzhener; BAKHRAKH, L.P.,
inzhener

Welding pipes of 12Eh5MA heat-resistant chromium molybdenum steel.
Svar. prolav. no.3:8-10 Mr 55. (MIRA 8:9)

1. VEIIStroyneft'
(Pipe, Steel--Welding)

LIVSHITS, L.S., kandidat tekhnicheskikh nauk

Austenite and perlite fusion zones. Svor.proizv. no.10:14-16 0'55.

(MERA 8:12)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut Stroyneft'

(Austenite--Welding) (Perlite--Welding)

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930310006-9"

PAL'ENVICH, A.S., kandidat tekhnicheskikh nauk; LIVSHITS, L.S., kandidat tekhnicheskikh nauk; PANICH, S.I.

Methods of assessing the susceptibility of steel te brittle fracture in welded storage tanks. Svar.preisv.ne.12:8-10 D '55.

(MERA 9:2)

1.Vsessyuznyy nauchne-issledevatel'skiy institut stroitel'ney nefti.

(Tanks--Welding) (Steel--Brittleness)

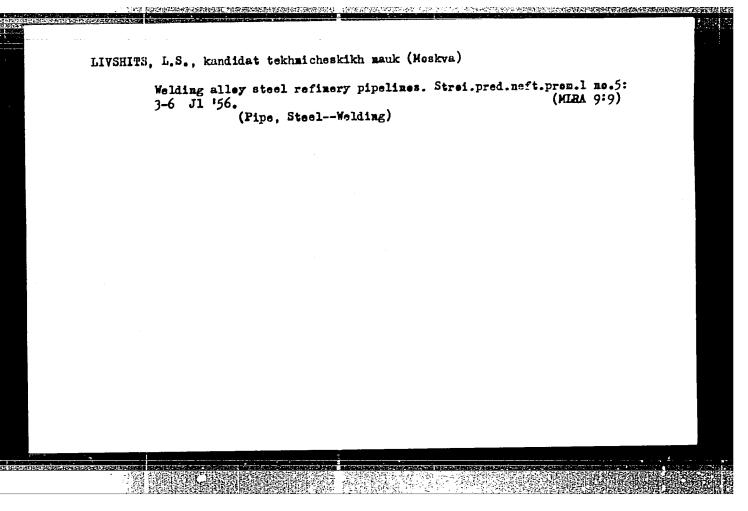
AL'TOAUZEN, O.N., kandidat fiziko-matematicheskikh nauk; BERNSHTEYN, M.L., kandidat tekhnicheskikh nauk; BLANTER, M.Ye., doktor tekhnicheskikh nauk; BOKSHTEYN, S.Z., doktor tekhnicheskikh nauk; BOLKHOVITIHOVA, Ye.N., kandidat tekhnicheskikh nauk; BORZDYKA, A.M., doktor tekhnicheskikh nauk; BUNIN, K.P., doktor tekhnicheskikh nauk; VINOGRAD, M.I., kandidat tekhnicheskikh nauk; VOLOVIK, B.Ye., doktor tekhnicheskikh nauk [deceased]; GAMOV, M.I., inzhener; GHLLER, Yu.A., doktor tekhnicheskikh nauk; GORELIK, S.S., kandidat tekhnicheskikh nauk; GOL'DENBERG, A.A., kandidat tekhnicheskikh nauk; GOTLIB, L.I., kandidat tekhnicheskikh nauk; GRIGOROVICH, V.K., kandidat tekhnicheskikh nauk; GULYAYEV, B.B., doktor tekhnicheskikh nauk; DOVGALEVSKIY, Ya.M. kandidat tekhnicheskikh nauk; DUDOVTSEV, P.A., kandidat tekhnicheskikh nauk; KIDIN, I.N., doktor tekhnicheskikh nauk; KIPNIS, S.Kh., inzhener; KORITSKIY, V.G., kandidat tekhnicheskikh nauk; LANDA, A.F., doktor tekhnicheskikh nauk; LEYKIN, I.M., kandidat tekhnicheskikh nauk; LIVSHITS. L.S., kandidat tekhnicheskikh nauk; L'VOV, M.A., kandidat tekhnicheskikh nauk; MALYSHEV, K.A., kandidat tekhnicheskikh nauk; MEYERSON, G.A., doktor tekhnicheskikh nauk; MINKEVICH, A.N., kandidat tekhnicheskikh nauk; MOROZ, L.S., doktor tekhnicheskikh nauk; MATANSON, A.K., kandidat tekhnicheskikh nauk; MAKHIMOV, A.M., inzhener; NAKHIMOV, D.M., kandidat tekhnicheskikh nauk; POGODIN-ALEESEYEV, G.I., doktor tekhnicheskikh nauk; POPOVA, N.M., kandidat tekhnicheskikh nauk; POPOV, A.A., kandidat tekhnicheskikh nauk; RAKHSHTADT, A.G., kandidat tekhnicheskikh nauk; ROGEL BERG, I.L., kandidat tekhnicheskikh nauk; (Continued on next card)

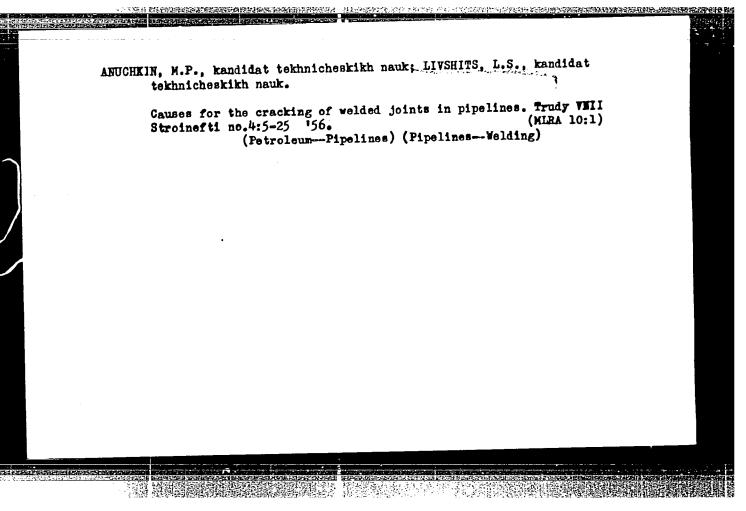
AL'TGAUZEN, O.N.--- (continued) Card 2.

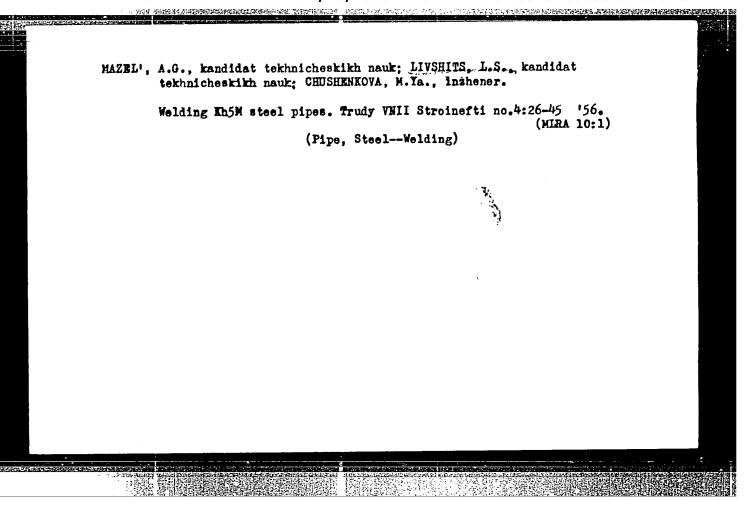
SADOVSKIY, V.D., doktor tekhnicheskikh nauk; SALTYKOV, S.A., inzhener; SOBOLEV, N.D., kandidat tekhnicheskikh nauk; SOLODIKHIM, A.G., kandidat tekhnicheskikh nauk; UTEVSKIY, L.M., kandidat tekhnicheskikh nauk; FRIDMAN, Ya.B., doktor tekhnicheskikh nauk; KHIMYSHIN, F.F., kandidat tekhnicheskikh nauk; KHRUSHCHEV, M.M., doktor tekhnicheskikh nauk; SHAPIRO, M.M., inzhener; SHKOL'NIK, L.M., kandidat tekhnicheskikh nauk; SHRAYBKR, D.S., kandidat tekhnicheskikh nauk; SHCHAPOV, N.P., doktor tekhnicheskikh nauk; GUDTSOV, N.T., akademik, redaktor; GORODIN, A.M. redaktor izdatel'stva; VAYNSHTEYN, Ye.B., tekhnicheskiy redaktor

[Physical metallurgy and the heat treatment of steel and iron; a reference book] Metallovedenie i termicheskaia obrahotka stali i chuguna; spravochnik. Pod red. N.T.Dudtsova, M.L.Bernshteina, A.G. Rakhshtadta. Moskva, Gos. nauchno-tekhn. izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1956. 1204 p. (MLRA 9:9)

1. Chlen -korrespondent Akademii nauk USSR (for Bunin)
(Steel--Heat treatment) (Iron--Heat treatment)
(Physical metallurgy)







LIVSHITS, L.S., kandidat tekhnicheskikh nauk; MAZKL', A.G., kandidat tekhnicheskikh nauk; CHUSHENKOVA, M.Ya., inzhener; BAKHRAKH, L.P., inzhener.

Welding 12Kh5MA steel pipes. Trudy VNIISTROINEFT' no.7:86-97 '56.

(Pipe, Steel--Welding)
(Heat resistant alloys)

1-11511175

123-1-539

Translation from: Referativnyy Zhurnal, Mashinostroyeniye, 1957, Nr 1, p. 86 (USSR)

AUTHORS:

Livshits, L.S., Chushenkova, M.Ya.

TITLE:

Welding Pipes Made of Non-Molybdenum Substitutes of 12 X 5 MA Steel (Svarka trub iz bezmolibdenovykh

zameniteley stali marki (2 X 5 MA).

PERIODICAL: Tr. Vses. n.-1. in-ta po str-vu, 1956, Nr 7, pp.98-107

ABSTRACT:

The authors present results of their study of properties of welded joints of non-molybdenum steels 12 X 5 and 12 X 53 pgrades, which are designated as the material for pipe-lines in refineries in replacement of the 12 X 5 MA steel which contains Mo (molybdenum). The evaluation of welded joint properties was conducted according to the indices for hardness and toughness in various spots of the welded joints after their technological ageing at 400° during 1,000 hours and without ageing,

Card 1/2

and according to a critical temperature of brittleness

VNIISTROINEFT

· "可以,你可能们是所有的全性的特殊。"

123-1-539

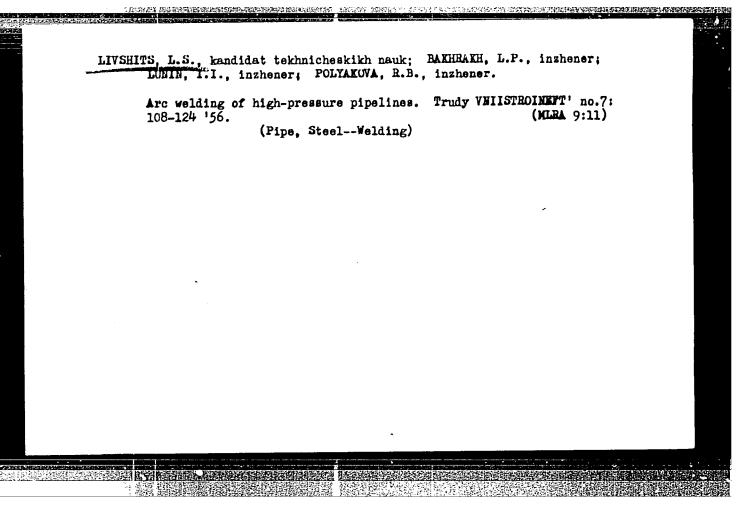
THE RESERVED TO SERVE THE PROPERTY OF THE PROP

Welding Pipes Made of Non-Molybdenum Substitutes (Cont.)

in the area with lowest properties. The welding was done by austenite electrodes with the U.S.-3 M and 9MTY-3 coatings, and by the U.L.-17 electrodes. They have established that the properties of welded joints of the 12 X 5 and 12 X 5 pp steels are equivalent to those of the 12 X 5 MA steel. It is recommended to weld the above-named steels in pipe lines with austenite electrodes having core of the X25H15 or OX18H9 steels without subsequent heat-treatment of the welded joints, or weld them by the 11-17. electrodes; in the latter case heat treatment of welded joints is imperative.

Card 2/2

Z.V.N.



Livshits, 1,3.

AID P - 5604

Subject

: USSR/Engineering

Card 1/2

Pub. 107-a - 4/12

Authors

Livshits, L. S., Kand. of Tech. Sci., N. M. Savvina, Kand. of Tech. Sci., L. P. Bakhrakh, Eng. and I. I.

Lunin, Eng.

Title

: Endurance of welded joints of 20 and 30KhMA steels

Periodical

Svar. proizv., 12, 14-16, D 1956

Abstract

The authors present the results of tests given to two types of welded pipes: a) the 35mm thick, 229mm in diameter, 20-steel pipes automatically butt-welded by Sv-08A electrode wire of 2mm gage, the AN-348 flux, and tempered at 550-560°C [in which the weld has higher strength than the base metall and b) the 52mm thick 30KhMA-steel pipes of the same diameter, automatically butt-welded by the Sv-Kh5M electrode of the 2mm gage, using AN-15 flux, and tempered at 650-660°C in which the joint turned out to be lower in strength than the

AID P - 5604

THE PROPERTY OF THE STATE OF THE PROPERTY OF T

Svar. proizv., 12, 14-16, D 1956

Pub. 107-a - 4/12Card 2/2

welded pipes. Three tables, 2 graphs, 1 macro-picture and 1 drawing.

All-Union Scientific Research Institute for Building of Institutions:

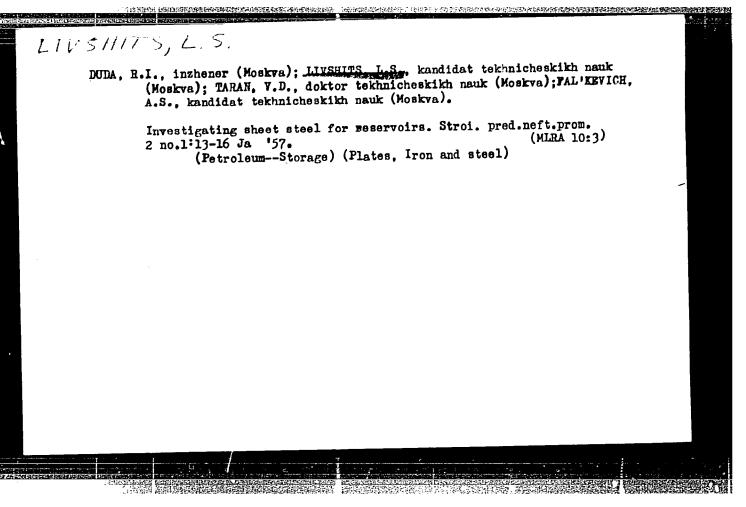
Petroleum Enterprises (VNIIStroyneft'), Central Sci-

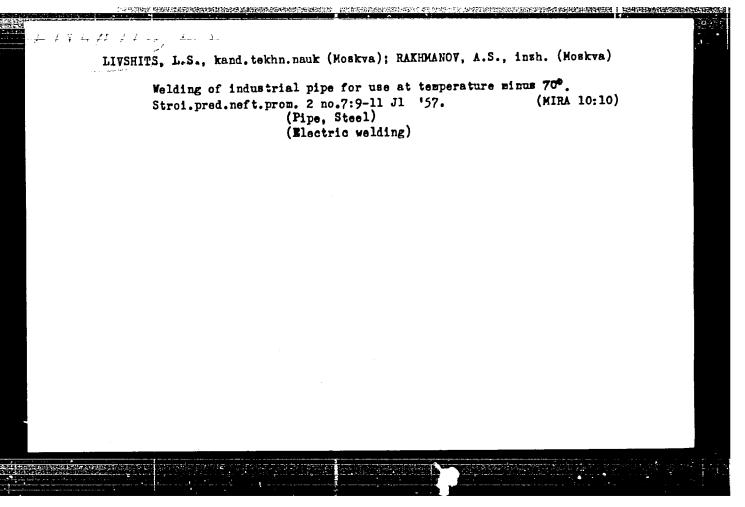
entific Research Institute of Machine-Building Technology

(Taniitmash).

Submitted | : No date

> CIA-RDP86-00513R000930310006-9" APPROVED FOR RELEASE: 06/20/2000





Livshits, LS.

SUBJECT:

USSR/Welding

135-8-11/19

AUTHORS:

Livshits, L.S., Candidate of Technical Sciences, and Bakhrakh,

L.P., Engineer.

TITLE:

Arc Welding of Thick-Walled High-Pressure Pipes (Dugovaya svarka

tolstostennykh trub vysokogo davleniya).

PERIODICAL

"Svarochnoye Proisvodstvo", 1957, #8, pp 29-31 (USSR)

ABSTRACT:

The article represents recommendations by VNIIStroyneft' for welding pipes of steel "20" and "30XMA", with 229 mm outside diameter and 52 mm wall thickness. The recommendations are based on experimental investigations of butt joints welded under various technological conditions.

The illustrations show the chamfering of butts and the special flux-retaining arrangement used. Experimental welding was

performed without supporting rings.

It is recommended to use multi-layer welds with section areas of single beads not over 70 mm<sup>2</sup>. For manual welding of steel "20" electrodes "YOHV-13/45", and for steel "30XMA" electrodes "43-19XM" are recommended. The proper electrode diameter for straight butts is 3 mm, for butts on bends - 4 mm. For semi-

Card 1/2

135-8-11/19

TITLE:

Arc Welding of Thick-Walled High-Pressure Pipes (Dugovaya svarka tolstostennykh trub vysokogo davleniya).

automatic welding of steel "20" the wire "CB-08A" and flux "AH -348" for semi-automatic welding of steel "30XMA" wire "CB-18XM" and flux "AH-15" are recommended.

Mechanical properties of welded joints equal to properties of base metal can be required, with the additional condition that impact resistance at temperature of  $-50^{\circ}$ C is to be not below 4 kg/cm<sup>2</sup>.

The article contains 4 sketches, 2 photographs, and 4 tables.

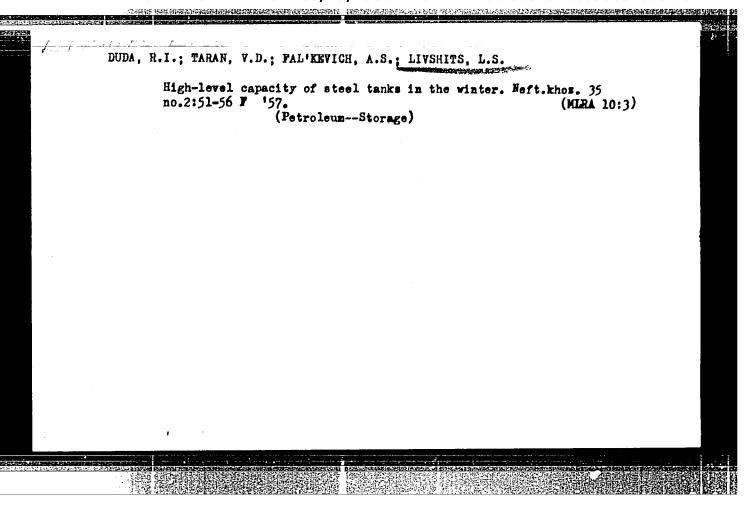
ASSOCIATION: "VNIIStroyneft".

PRESENTED BY:

SUBMITTED:

AVAILABLE: At the Library of Congress.

Card 2/2



SELECTION CONTROL CONT

LIVSHITS, Lev Semenovich, kand. tekhn. nauk; BAKHRAKH, Lidiya
Petrovna, inzh.; RAGAZINA, M.F., inzh., ved. red.; SHTERLING,
S.Z., dots., red.; SOROKINA, T.M., tekhn. red.

[Welding of EI578 and EI579 steel structures]Svarka konstruktsii iz stalei EI578 i EI579. Moskva, Filial Vses. in-ta nauchn. i tekhn. informatsii, 1958. 9 p. (Peredovoi nauchno-tekhn. i pro-izvodstvennyi opyt. Tema 12. No.M-58-281/24) (MIRA 16:3) (Steel, Heat-resistant-Welding)

CLUBHIB, LID

129-1-6/14

AUTHORS: Livshits, L.S., Candidate of Technical Sciences, and

Bakhrakh, L.P., Panich, S.I., Engineers.

TITLE: On the Non-uniformity in the Zone of Fusion of Welded

Joints (O neodnorodnosti v zone splavleniya svarnykh

soyedineniy)

PERIODICAL: Metallovedeniye i Obrabotka Metallov, 1958, No. 1, pp. 26 - 29 (USSR).

ABSTRACT: For studying the influence of manganese in the seam on the non-uniformity of fusion, strips of "Steel 3" (0.18% C, 0.45% Mn) were welded by means of a wire under flux. The manganese content in the seam was varied by introducing different quantities of ferro-manganese in the coating and thus a number of weld joints were obtained containing different quantities of manganese, whilst the content of other elements remained approximately unchanged. Some of the results obtained are given in Table 1, p.27. Experiments were also made with welding the chromium-manganese steel 30XMA with electrodes of such composition as to obtain an equal strength of the welds and the base material; the chemical compositions of the base metal and the welds are given in Table 2, p.28. Some of the results are entered in Table 3, p.28. On the basis of the Card 1/3

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930310006-9"

0n the Non-uniformity in the Zone of Fusion of Welded Joints.

obtained results, the following conclusions are arrived at: in welds of pearlitic steels with differing chemical compositions of the metal in the weld and the base metal, the formation is possible of a structural and chemical nonuniformity in the melting zone which is characterised by the formation of decarburised and carburised zones; the formation of these non-uniformities proceeds in the solid state due to displacement of carbon atoms from one zone of the weld into the other, whereby the carbon displacement takes place only in the sections which are close to the fusion zone, namely, it proceeds from the sections containing elements which produce less stable carbides to those sections which contain elements producing more stable carbides, i.e. from the sections with lower content of carbide-forming elements into the section with higher content of such elements. The direction of displacement of the carbon does not depend on its relative concentration in the neighbouring regions and is determined by the qualitative and quantitative difference in the content of carbide-forming elements in the weld and in the base metal and, therefore, frequently the carbon moves away from zones Card2/3 with low carbon content; immediately after welding, the weld

129-1-6/14

在1000mm 1200mm 1200mm

On the non-uniformity in the Zone of Fusion of Welded Joints.

does not always have an appreciable non-uniformity in the fusion zone. The non-uniformity occurs during heating to temperatures slightly below the Ac, point. Displacement of carbon and

formation of the above mentioned type of non-uniformities take place at heating temperatures at which the iron is in the  $\alpha$  state. There are 3 tables and 3 figures, and 4 Slavic references.

ASSOCIATION: VNIISTROYNEFT'

THE PERSON OF THE PROPERTY OF THE PERSON OF

AVAILABLE:

Library of Congress.

Card 3/3

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930310006-9"

Livshits, L.S.

135-58-4-7/19

AUTHORS:

Livshits, L.S., Candidate of Technical Sciences, and Panich,

S.I., Technician

TITLE:

Formation of Non-Homogeneity in Fusion Zones of Welds in Heating up to 500 - 700°C (Obrazovaniye neodnorodnosti v zone splavleniya svarnykh soyedineniy pri nagreve do

500 ~ 700°)

PERIODICAL:

Svarochnoye Proizvodstvo, 1958, Nr 4, pp 22-25 (USSR)

ABSTRACT:

In the works published thus far on the problem Ref 1-5, the non-homogeneity of metal structure of welded joints is explained by the difference in the content of the carbide-forming elements in portions of weld joints. This article gives information of the results of experimental investigation carried out recently by VNIIStroyneft, which prove that the aforementioned conception is wrong. The conclusion is that the non-homogeneity, forming at the temperature of 500 - 700° C, is caused by the presence and migration of excessive atoms (not bound in carbides) from one portion of the weld joint into another, i.e. when there is an excess of free atoms of a carbide-forming element in one portion of the weld, and an excess of free carbon atoms

Card 1/2

135-58-4-7/19

Formation of Non-Homogeneity in Fusion Zones of Welds in Heating up to 500 - 700° C

> in the other. A calculation principle is suggested which permits the determination of the possibility of the formation of carbon non-homogeneity in the fusion zone by the content (in atomic percentage) of the alloying elements in the seam and in the base metal. The uniform distribution of carbon and liquidation of the non-homogeneity can be obtained by a subsequent (after heating to 500 -700°C) heating to 950°C. The information includes a detailed description of the processes as observed in experiments, and microphotographs. The chemical composition of the alloy steel is shown in tables. There are 5 figures, 2 tables and 5 references, 2 of which are Soviet, 2 English and 1 Japanese.

ASSOCIATION: VNIIStroyneft1

AVAILABLE:

Library of Congress

Card 2/2

SOV-125-58-10-10/12

CHARLES OF THE PARTY OF THE PAR

AUTHORS:

Livshits, L.S., and Bakhrakh, L.P.

TITLE:

On the Relation Between the Hardness and the Microstructure of the Fusion of Austenitic Joint in Perlite Steel and the Chemical Composition of the Steel and Weld Joints (O svyazi mezhdu tvërdost'yu i mikrostrukturoy splavleniya austenitnykh shvov na perlitnykh stalyakh i khimicheskim

sostavom stali i shvov)

PERIODICAL:

Avtomaticheskaya svarka, 1958, Nr 10, pp 81 - 85 (USSR)

ABSTRACT:

Problems relating to the transition of carbon in the fusion zone in solid condition, and the passage of metals in various structure classes are discussed. The microstructure and microhardness of the fusion zone in commercially pure iron (about 0.03% C), carbon steel (up to 22% C), and "12Kh5M" steel (up to 0.15% C, 5 - 6 % Cr, 0.45 - 0.65 % Mo) were investigated. It was proved that hardness and structure of the fusion zone in austenitic seams on perlite steel can be controlled in a large range by changing the chrome and nickel content in the seams and the carbide forming elements in the base metal. It is concluded that hardness and probably also brittleness in the fusion zone

Card 1/2

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930310006-9"

On the Relation Between the Hardness and the Microstructure of the Fusion SOV-125-58-10-10/12 of Austenitic Joints in Perlite Steel and the Chemical Composition of the Steel and Weld Joints

> are reduced by a smaller carbon content in the steel and chromium content in the austenitic seam, as well as by an increased content of nickel in the seam, and of elements forming in the base metal stabler carbides than chromium. To reduce hardness and improve homogeneity in the fusion zone, the use of "18 Cr-8 Ni" electrodes, which do not contain niobium, titanium, molybdenum and tungsten, is recommended for welding steel alloyed with molybdenum, tungsten and vanadium (separately or in combination) in quantities ensuring binding of the carbon into carbide. There are 5 microphotos, 1 graph and 7 references, 3 of which are Soviet and 4 English.

SUBMITTED:

January 6, 1958

1. Steel alloys--Arc welding

2. Arc welding--Metallurgical effects

Card 2/2

3. Steel--Chemical properties 4. Welds--Chemical properties

LIVSHITS, L.S.; RAKHMANOV, A.S.

Determination of the resilience of steel at low temperatures.

Zav. lab. 24 no.5:622-625 158. (MIRA 11:6)

1. Vsesoyuznyy nauchno-issledovatel skiy institut po stroitel stvu predpriyatiy gazovoy i neftyanoy promyshlennosti.

(Steel-Testing)

SOV/135-59-1-6/18

SOUTH TO THE SECOND SEC

AUTHORS: Livshits, L.S., Candidate of Technical Sciences,

and Bakhrakh, L.P., Engineer

TITLE: The Radiographic Investigation of Niobium Distri-

bution in Stainless Steel (Radiograficheskoye issledovaniye raspredeleniya niobiya v nerzhave-

yushchey stali)

PERIODICAL: Svarochnoye proizvodstvo, 1959, Nr 1, pp 20-22

(USSR)

ABSTRACT: In connection with intercrystalline corrosion in

the use of "18-9 Ti" and "18-9 Nb" stainless steels, it was assumed that the stabilizing effect of Nb and Ti depends on their condition in the alloy and that satisfactory corrosion resistance is obtained if Nb (or Ti) is present in the form of carbide, binding the contained carbon. Information is given on the effect of heating conditions for

"18-9" grade stainless steel containing Nb, on the

Card 1/3 formation and dissolving of Nb-carbides, with the

SOV/135-59-1-6/18

The Radiographic Investigation of Niobium Distribution in Stainless Steel

use of an Nb-95 radioactive isotope. The tests led to the following conclusions: to ensure intercrystalline corrosion resistance in heating up to temperatures of 550 - 650°C, the use of stainless steel with a higher Nb content

$$\left(\frac{\text{Nb}}{\text{C}} \approx 10 - 13\right)$$

is recommended. In hardening stainless steel with a reduced Nb content, heating over 1200°C must be avoided. In the case of heating up to 1300°C, zones adjacent to the weld are less resistant to corrosion than remote portions. Best results in raising corrosion resistance can be obtained, by heating up to 850 - 900°C for 3 hours, ensuring a satisfactory Nb carbide formation. Maximum temperatures for steels containing Ti are lower

Card 2/3

SOV/135-59-1-6/18

The Radiographic Investigation of Niobium Distribution in Stainless Steel

than for Nb-containing steels. There are 5 microphotos, 1 table and 4 references, 3 of which

are Soviet and 1 English.

ASSOCIATION: VNIIST

Card 3/3

LIVSHITS, L.S., kand. tekhn. nauk; RAKHMANOV, A.S., inzh.

Using aluminum alloys pipes for building pipelines. Svar. proizv.
no.2:16-17 F '59. (MIRA 12:1)

1. Vsesoyuznyy nauchno-issledovatel'skiy institut tverdykh splavov.

(Pipelines) (Aluminum alloys--Velding)

SUV/129-59-6-3/15

THE KIND OF THE PROPERTY OF TH

Livshits, L.S. (Cand. Tech. Sci.) AUTHOR:

Displacement of Carbon in a-Iron and Solubility of TITLE:

Carbon in Ferrite (Peremeshcheniye ugleroda v al'fa-

zheleze i rastvorimost' ugleroda v ferrite)

PERIODICAL: Metalloyedeniye i termicheskaya obrabotka metallov,

1959, Nr 6, pp 13-17 (USSR)

ABSTRACT: As a result of heating in the temperature range 500 to 700 °C, displacement of carbon and side by side

formation of decarburized and carbon-enriched zones can be observed in cartain weld joints of perlitic steels; thereby the iron was in the a-state (Refs 1-3). Such a displacement of the carbon is attributed to differing contents of carbide forming elements in the metal of the weld joint and the weld metal. For the purpose of establishing the lews governing the displacement of carbon in the ariron, the fusion zones of several weld joints were investigated for six steels with compositions, as given in the table on page 13, which also contains the composition of the weld metal. direction of the displacement of the carbon was

evaluated metallographically from the formation and Card1/4 change in the dimensions of the decarburized and

SOV/129-59-6-3/15

NAME OF THE PARTY OF THE PARTY

Displacement of Carbon in a-Iron and Solubility of Carton in Ferrite

CELECTOR DESCRIPTION DE LA CONTRACTION DEL CONTRACTION DE LA CONTRACTION DEL CONTRACTION DE LA CONTRACTION DE LA CONTRACTION DE LA CONTRAC

carburized zones. The specimens were investigated after welding and also after welding followed by heating for 2, 10, 100, and 1000 hours at 600 and 700 °C. obtained results have shown that presence in one of the parts of the weld joint of small quantities of more 'potent' carbids-forming elements (Mo and W) than in other parts, is insufficient for causing displacement of carbon atoms in the a-iron. However, a great difference in the contents of elements which can produce carbides of higher stability than iron carbides, does bring about a displacement of the carbon into the zone of accumulation of carbide forming atoms (Fig 1). On the basis of the obtained results the following conclusions are arrived at: 1) solubility of carbon in the ferrite depends on the character and the degree conclusions are arrived at: of alloying of the steel. 2) Provided that the content of the alloying carbide forming element is high enough and the entire carbon is combined into stable carbides and there are excess carbide forming atoms, the content of carbon in the ferrite should be lower than the limit of solubility. However, if the

Card2/4

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930310006-9"

THE REPORT OF THE PROPERTY OF

SOV129-59-6-3/15 Displacement of Carbon in a-iron and Solubility of Carbon in Ferrite

content of the alloying element is low and is insufficient for combining the available earbon, the content of carbon in the ferrite reaches the limit of solubility. 3) The more stable the carbides formed by an alloying element, the lower will be the carbon concentration of the ferrite, provided that the content of the alloying element in the alloy is high enough. 4) In metallic joints (produced by welding or cladding) With differing contents of carbids forming alloying elements of the sections in contact, conditions are created which are favourable for the displacement of the carbon from the spots containing less stable carbides (high concentration of carbon in the ferrite) into spots containing more stable carbides (lower concentration of carbon in the ferrite). 5) Displacement of the carbon in the ferrite from the higher concentration to the lower concentration is appreciable at 550 to 700 °C and is accompanied by the

Card3/4

Displacement of Carbon in a-iron and Solubility of Carbon in Ferrite

decomposition of less stable and the formation of more stable carbides.

There are 3 figures, 1 table and 3 references, 2 of which are Soviet and 1 English.

ASSOCIATION: VNIIST

Card 4/4

18. 9300 15.2220 66889

AUTHOR: Livshits, L. S.

sov/126-8-1-6/25

TITLE:

On the Mechanism by Which Carbon Dissolves in and Diffuses Through Ferrite

PERIODICAL: Fizika metallov i metallovedeniye, 1959, Vol 8, Nr 1, pp 31-37 (USSR)

An investigation carried out by the authors on the ABSTRACT: diffusion of carbon in  $\alpha$ -iron has led them to assume that the solubility of carbon in ferrite and its rate of diffusion does not depend only on the qualitative difference in alloy elements; on alloying with the same carbide-forming elements these properties are associated with the concentration of the latter. The level of solubility of carbon in alloy ferrite most frequently determines the possibility of occurrence of reaction diffusion of carbon in  $\alpha$ -iron. These assumptions are based on the following facts: It was noticed that in welded joints, in which the seam and the welded metal differ in their carbide-forming element contents, transfer of carbon, on lengthy heating in the range 500-700°C, takes place in the direction of elements Card 1/4 forming more stable carbides (Refs 3 and 4).

· 中,因此特别在特别的首都的自然的基本有数据的特别的基础的国际的对一。例如《

66889

SOV/126-8-1-6/25

On the Mechanism by Which Carbon Dissolves in and Diffuses Through Ferrite

in which the seam unites with the basis metal, regions of considerable carburization form in those parts where there is an element capable of forming the most stable carbides in a given system, and a sharp de-carburization occurs in that part where decreasing element contents give less stable carbides (Fig 1). In the example shown in Fig 1 of a chromium steel weld, the presence of molybdenum in the seam led after 10 hours' heating (700°C) to transfer of carbon from the welded steel to the seam. In a welded carbon steel containing 0.15% carbon two types of seam were made, one containing 0.4 and the other 0.9% V. For seams of the first type no signs of transfer of carbon from the welded steel into the seam could be observed after lengthy heating at 700°C. (Fig 2). In the second case a considerable transfer of carbon had taken place from the basis metal into the seam and a drastic structural non-uniformity in the welded portion was observed (Fig 3). The same transfer of carbon was observed also in other experiments when a seam with high Card 2/4 vanadium content was obtained in chromium and molybdenum

66889

sov/126-8-1-6/25

On the Mechanism by Which Carbon Dissolves in and Diffuses Through Ferrite

Zav'yalov et al. (Ref 2) have published data steels. for the solubility of carbon in ferrite after lengthy heating at various temperatures, of several steels containing separately manganese, chromium, tungsten, If the atomic composition of molybdenum and vanadium. the alloys and the types of carbides found by the authors in each of these alloys are considered, it can be seen that in all cases there is a considerable excess of carbon as compared with that which can be associated with the alloy element contents. That is why an increased solubility of carbon in ferrite was found in all cases. As an example, a case is considered where a seam has been obtained on a carbon steel which contained more vanadium than required for the formation of stable carbides (Fig 4). The relationship between the absorbed energy and the relative increase in electrical resistance of sulphur is shown as another example. The author arrived at the following conclusions:

Card 3/4 Migration of carbon atoms in ferrite takes place if there

On the Mechanism by Which Carbon Dissolves in and Diffuses

THE PROPERTY OF THE PROPERTY O

is a difference in concentration. The difference in concentration of carbon in ferrite in various portions of the steel is due to the non-uniformity in carbideforming alloy element content. In portions containing a high percentage of a stable carbide-forming element a ferrite zone, impoverished in carbon, forms in low-carbon steel because of the great affinity of this element to carbon. Carbon atoms migrate into this zone from the remaining ferrite. If a steel, containing carbide-forming elements, has a high carbon content, equilibrium conditions between combined and free carbon lead to an increase in the quantity of carbon dissolved in the ferrite.

There are 4 figures and 4 Soviet references.

SUBMITTED: March 13, 1958

Card 4/4

APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930310006-9"

14(11)

507/32-25-2-32/78

AUTHORS:

Livshits, L. S., Rakhmanov, A. S.

TITLE:

Mechanical Testing Methods (Mekhanicheskiye metody ispytaniy ). On the Low Temperature Resilience Determination and the Tendency of Metals to Form and Develop Cracks (Ob opredelenii udarnoy vyazkosti pri nizkikh temperaturakh i sklonnosti

metalla k zarozhdeniyu i razvitiyu treshchin)

PERIODICAL:

Zavodskaya Laboratoriya, 1959, Vol 25, Hr 2,

pp 190 - 192 (JSR)

ABSTRACT:

The causes which led to the destruction of a 5000 cu. m cylindrical steel container were investigated, and a number of peculiarities were observed which may be used for determining the brittleness after resilience (R) changes at low temperatures. The article explains the advantages of the described method for the determination of the deformation and tearing process in impact-bending tests as criteria for the brittleness. The container mentioned above consisted of dead melt steel MSr.3 (0.20% C, 0.19-0.20% Si, 0.35-0.38% Mn, 0.042% S and 0.019% P). The air temperature at the

Card 1/3

Mechanical Testing Methods. On the Low Temperature SOV/32-25-2-32/78Resilience Determination and the Tendency of Metals to Form and Develop Cracks

moment of destruction was -27°, soil temperature -31°. The metal properties were as follows: or B = 45.9 kg/mm<sup>2</sup>,  $6_{S} = 27 \text{ kg/mm}^2$ , 6 = 27% and  $\phi = 61.4\%$ . Serial (R) tests at ifferent temperatures of the two container rings furnished varying results (Fig 1); of the first container ring, however, only longitudinal, while of the second ring only transversal samples could be produced. Investigations of the samples of the first container ring (Fig 2) showed that the main component of the deformation process is the plastic deformation process, while the share of elastic deformation is small. Investigations regarding the dependence of the tearing process of the temperature prevailing during the test (Fig 3) point to the fact that the container was destroyed by decomposition due to brittleness. A high (R) value of a metal is in such cases nothing but proof of great tensile strength, if the values of the deformation and tearing process are also high. Otherwise, here may be little resistance to cracking (high tearing process but little

Card 2/3

Mechanical Testing Methods. On the Low Temperature SOV/32-25-2-32/78
Resilience Determination and the Tendency of Metals to Form and Develop Cracks

deformation process), or a tendency towards a fast development of cracks (high deformation process, little tearing process). There are 4 figures and 2 Soviet references.

ASSOCIATION:

Vsesoyuznyy nauchno-issledovatel'skiy institut po stroitel'stvu magistral'nykh truboprovodov (All-Union Scientific Research

THE PERSON NAMED AND PARTY OF THE PERSON NAMED AND PARTY.

Institute for the Construction of Trunk Pipe Lines)

Card 3/3

LIVSHITS, L.S.

# PHASE I BOOK EXPLOITATION SOV/5596

- Neyfel'd, I. Ye., A. S. Fal'kevich, and L. S. Livshits
- Kontrol' kachestva svarki na stroitel'stve (Quality Control in Field Welding) Moscow, Gostroyizdat, 1960. 163 p. 8,000 copies printed.
- Scientific Ed.: V. L. Tsegel'skiy, Engineer; Ed. of Publishing House: L. S. Lytkina; Tech. Ed.: T. M. Gol'berg.
- PURPOSE: This book is intended for engineers, technicians, and skilled weldors engaged in field welding and its quality control.
- COVERAGE: Modern welding methods, types of welded joints used in construction and erection, and specifications for weldments are described. Particular attention is given to the following methods of weld inspection: X-ray, gamma-ray, magnetic, ing methods of weld inspection: X-ray, gamma-ray, magnetic, ultrasonic, mechanical, metallographic, and corrosion. Data concerning methods of inspecting welds for tightness are also

Card 1/7

sov/5596

Quality Control in Field Welding presented. The author thanks L. P. Bakhrakh, S. I. Panich, G. N. Shubert, and V. M. Lubov for their assistance in the work performed at VNIIST (Vsesoyuznyy nauchno-issledovatel'-skiy institut po stroitel'stvu magistral'nykh truboprovodov --All-Union Scientific Research Institute for the Construction

CONTRACTOR OF THE PROPERTY OF

of Main Pipelines). Chapters I, II, III, VI, VII, and X were written by A. S. Fal'kevich, Candidate of Technical Sciences; Chapters IV, V, and IX, by I. Ye. Neyfel'd, Engineer; and Chapter VIII, by L. S. Livshits, Candidate of Technical Sciences. There are 33 references, all Soviet.

## TABLE OF CONTENTS:

Foreword		3
Ch. I.	Modern Welding Methods and Types of Welded Joints Used in the Field	-

1. The significance of welding in the field 2. Characteristic features of welding under field conditions

Card 2/7

6147 ·

8/125/60/000/05/02/03

/8.7Z o authors:

Livshits, L. S., Grinberg, N. A., Panich, S. I., Shamonov, S. I.

TITLE:

The Nature of Chemical Non-Homogeneity of the Fusion Zone in

Some Pearlite Steels

PERIODICAL: Avtomaticheskaya svarka, 1960, No. 5, pp. 11-16

TEXT: Local spectral analysis with "three standards" was employed in investigating the distribution of carbon and other elements in the fusion zone of welded joints. The article gives the most characteristic results of investigation of welds with 1.9% Cr, and with 1.7% V. A "PMT-3" apparatus (Fig. 2) was slightly changed for local analysis with the use of a manganese needle electrode, i. e. the diamond was replaced by this electrode. The other electrode was a lead cone. The cylindrical needle 1-mm in diameter was of pure magnesium produced by electrolysis with 10-12 volt, a-c in electrolyte consisting of 90 cm of 10% Na<sub>2</sub>HPO solution and 10cm H<sub>2</sub>SO<sub>4</sub>. Sharpening the needle to 0.01-0.015 mm took 20 to 25 sec. After every photograph with the "ISP-28" spectrograph, the needle was immersed for 2-3 sec into 10% HNO<sub>3</sub> solution to remove oxides, then was

Card 1/3

W