CIA-RDP86-00513R000930420019-3



APPROVED FOR RELEASE: 06/20/2000

INVENTOR: <u>Al'tman, M. B.</u> : <u>Ambartsumyan, S. M.</u> : <u>Kolobnev, I. F.</u> : <u>Lotareva, O. B.</u> ; <u>C</u> <u>Loktionova, L. I.</u> ; <u>Spiridonova, S. B.</u> ORC: none <u>M</u> TITLE: Cast <u>aluminum</u> -base alloy. Class 40, No. <u>183398</u> SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 13, 1966, 80 TOPIC TAGS: aluminum alloy, cast alloy, zinc containing alloy, magnesium containing alloy, manganese containing alloy, titanium containing alloy, iron containing alloy, beryllium containing alloy, stress corrosion, corrosion resistant metal ABSTRACT: An Author Certificate has been issued for a cast aluminum-base alloy con- taining zinc, magnesium, manganese and <u>titanium</u> . ¹ In order to reduce susceptibility to <u>stress corrosion</u> While retaining high mechanical properties, the content of alloyin elements should be kept within the following limits in X: zinc 3.5-5.5, magnesium 1.2-2.2, manganese 0.2-0.7, titanium 0.05-0.25, chromium 0.1-0.6, iron 1.0-1.6, and beryllium 0.01-0.5. The alloy may also contain silver, niobium, cobalt, nickel, molybdenum, boron, tungsten, and rare-earth metals in an amount up to 1.5X. [DV]	40374-66 ETI/EUP(t)/Eli(m) 1 C NR: AP6025629	1JP(c) JH/JD/WB/JT SOURCE CODE: UR/0413/66/000/013/0080/0080	
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SUE CODE: 11/ SUBM DATE: 12Jun64/ ATD PRESS: 5053	2-2.2, manganese 0.2-0.7, tita ad beryllium 0.01-0.5. The allo	anium 0.05—0.25, chromium 0.1—0.6, iron 1.0—1.6, loy may also contain silver, niobium,cobalt, nickel.	-
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S/689/61/000/000/017/030 D205/D303

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- AUTHORS: Isayev, V.I., Ivankin, I.A., Kulakov, V.I., and <u>Holdishov</u>, N.A.
- TITLE: Peculiarities of thermal treatment of manarive drop-forged articles of the 201 (D1) alloy
- BOURCE: Fridlyander, I.M., V.I. Dobetkin, and Ye.D. Zahlarov, edu. Deformiruyemyye alyuniniyevyye splavy; sbornik statey, Moscow, 1961, 131 - 156

TEXT: This paper is concerned with some peculiarities of the theman treatment of massive eluminum alloy (D1) articles and the influence of certain factors of the treatment on the values of the residual stresses and mechanical properties. The forgings were propured by axial hammering of the casting. Test specimons were cut out from the forged articles in various directions with respect to the fiber. Durge differences were revealed between the various specimens cut out from the same forging. The strength limit ranged from 31.8 to 41.8 kg/mm² and the relative elongation in samples cut out parallel to the Card 1/2

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fiber was more than twice as much as those of the transverse subjust. It was found that hardening from 490° C after 2 hours at that temper ture reduced cracking defects down to 0.2 %. Still better results arre obtained by quenching in hot hedia (30° C water on $145 - 155^{\circ}$ C solt melts in step herdening). It was shown that cracks develop because of residual thermal stresses which are formed during herdening and tend to concentrate at the passages from thin to thick sections of the articles. There are 2 figures, 3 tables and 1 Soviet-bloc reference.

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Reduction of warping of welded ...

<mark>\$/689/61/000/000/018/000</mark> D205/D303

200°C range (2 min) and then in water at 30°C; 3 - in salt baths at 160 - 180°C for 2 to 16 hours. In the first two cases, the specimens were aged after cooling at 165°C for 10 - 16 hours. All specimens, notwithstanding the differences in cooling conditions, had almost identical mechanical properties (about 40.5 Kg/nm2 strength limit, 50.5 kg/mm² yield point and 14 5 relative elongation). This indicates that the D20 alloy which contains copper in amounts exceeding the solubility limits is not sensitive to the lowering of the cooling rate during hardening. A-ray analysis has shown that the increase of the cooling temperature by 100 - 200°C lowers the defectivity of the grains, but does not entirely remove the general stresses. Correction tests were performed using welded specimens in a 3 % solution of MaCL The specimens fastened to a rotating wheel were periodically innersed during the 4.5 months. The specimens cooled in water at 20°C were destroyed after 14 - 16 days, while those cooled in boiling outer, calt baths and by the step regime remained intact after 130 days. Warping was 2 - 4 times less in the specimens cooled at higher tenperatures. It is concluded that the welding of D20 alloy sheets should be carried out in the hardened and not in the annealed state, because

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8/609/81/000/090/018/0) D205/D303 Reduction of warping of welded ... in this case the partial mardening occurring during wolding does not induce residual stresses near the joint. Anticus throught of plant ticity were measured for welded and non-welded spectrums, the provide indicating that the welded samples possess almost the arms planticle-ty as the non-welded, the fatigue limit at cyclical conding (20 m $^{\circ}$ cycles) was, however, superior in the non-wolded samples (12 kg/m²), as compared with the welded (5 kg/m²). Conclusiona: to lower streases and prevent warping, articles made of the D20 alloy should be quenched in a heated medium. In order to increase the strength of welded constructions they should be welded in mardened or hardened and aged state. There are 1 figure and 5 tables. Card 3/3

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					RESULTING DEPARTMENT	
				8/123/62/000/0 A004/A101)14/008/020	
	AUTHORS :	Isayev, V. I., Ivankin,	I. A., Kulakov, V	. I., Loktionova,	N. A.	
	TITLE:	The special features of I 1 (D1) alloy ,	the heat treatment	t of solid dies f	rom the	
	PERIODICAL:	Referativnyy zhurnal, Ma 14B158 (In collection: Oborongiz, 1961, 131 - 1	"Deformiruyemyye	no. 14, 1962, 28, alyumin. splavy".	abstract Moscow,	
	conditions a larly in the crease of th of 20°C). A 495 + 5°C, t cooling in m because of c	It was found that the ma id dies made of the D1 al are increased residual str ose places where thin cross he hardening temperature, a strict observation of th the use of hot water (80°C molten salts at 145 - 155° eracks to 0.2%. There are s note: Complete transla	uminum alloy under resses arising duri- s sections go over and the use of ab- the heat-treatment of) for cooling or a C made it possible 2 figures.	r large-scale pro ing the hardening r into thick ones rupt cooling aids conditions, harde a gradual hardeni	oduction , particu- , the in- (water ming at .ng with	\checkmark
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s/137/62/000/006/161/163 A057/A101 AUTHORS ; Loktionova, N. A., Kozlovskaya, V. P., Isayev, V. I. The decrease of warping of welded structures of \mathcal{A} 20 (D20) alloy TITLE: at thermal treatment FER(ODICAL: Referativnyy zhurnal, Metallurgiya, no. 6, 1962, 13, abstract 6E80 (V sb. "Deformiruyemyye alyumin. splavy", Moseow. Oborongiz, 1961. 137 - 143) Thermal stresses, which arise during quenching of welded articles FEXT: of D20 alloy, lead to warping of these articles and they have to be straightened after quenching. In order to develop measures for reducing thermal stresses, the effect of quenching in boiling water and in salt melts upon the stability of geometric dimensions of the welded articles and mechanical properties of the D20 alloy was investigated. As a result of the investigation the following conclusions were drawn. To reduce thermal stresses and avoid warping of articles of D30 alloy, quenching in hot medium (boiling water, salt melt) is recommended. The D20 alloy is little sensitive to the cooling rate during quenching in the Card 1/2

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The decrease of warping of welded	S/137/62/000/006/161/163 A057/A101	
temperature range $535 - 200^{\circ}$ C. In spite of the red son to quenching in water of a temperature of 20° C. "Atom is formed, which is able to strengthen during and in salt melt. In order to increase the streng alloy, they must be welded from a material in quence state.	, a supersaturated α-solid solu- aging and isothermic soaking th of welded structures of D20	
	V. Tarisova	
[Abstracter's note: Complete translation]		1
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CARLE I

5/129/62/000/010/004/006 E073/E335

AUTHORS: Loktionova, N.A., Candidate of Technical Sciences, Rastvorova, N.M. and Breslavtseva, O.P., Engineers TITLE: New heat-treatment regime for A. 19 (AL19)alloy castings PERIODICAL: Metallovedeniye i termicheskaya obrabotka metallov, no. 10, 1962, 53 - 57 TEXT: The mechanical properties were determined at 250 °C of 10-mm rods produced from 12-mm diameter specimens cast into earthen moulds. The composition of the melts was as follows: 4.5 - 5.3% Cu, 0.6-1% Mn, 0.25-0.40% Ti, < 0.3% Si, \leq 0.3% Fe. Prior to quenching the specimens were heated to 540 and 545 °C and held at that temperature for 6, 8, 10, 12, 16 and 20 hours. In addition, the influence of repeated quenching was investigated. Ageing was carried out at 150, 175, 200 and 225 °C with holding times of 3, 6, 12, 24 and 30 hours (after heating to 545 °C prior to quenching and holding at that temperature for 10-12 hours). The hardenability of massive castings was determined from tests with cubes of 100 mm side Card 1/2

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New heat-treatment

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length, cast into earthen moulds. Quenching was in water at 45 and 50 °C and in boiling water. Conclusions: the optimum heat-treatment is single-stage heating to 545 ± 5 °C, holding at that temperature for 10 - 12 hours, quenching, artificial ageing at 175 ± 5 °C for 3-6 hours. Quenching in boiling water reduces appreciably the deformation caused by quenching, which greatly helps in eliminating changes in the geometry and obviating the necessity of straightening the parts after heat-treatment. There are 3 figures and 3 tables.

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S/724/61/000/000/004/020

A New heat-treatment procedure for the AL19....

the AL19 alloy is practically insensitive to a reduction in the rate of cooling upon quench. The mechanical properties of the castings in the freshly quenched state, tested at room T. were practically invariable with an increase in water T from 45 to 96° , whereas in aged specimens tensile strength and relative elongation were somewhat reduced thereby. The mechanical properties at 250°C (short-term tests) were practically invariable with an increase in quench-water T up to 96° and were also independent of the type of heat treatment; (2) the total corrosional stability of the AL19 alloy quenched in water is practically the same with quench-water T of 45 and 96°, both in the freshly quenched state and after artificially accelerated aging; (3) the quenching of odd-shaped large castings in boiling water produces so insignificant a warping of the castings, that virtually no straightening is required after heat treatment. The adoption of quenching in boiling water for large odd-shaped castings has provided a cardinal solution of the problem of warpage, has reduced the amount of labor required, and has increased the quality of parts made of AL19 alloy; (4) quenching in boiling water does not require any additional major equipment and does not alter in any way the procedural schedule of the production line. Quenching in boiling water can be done with the utilization of ordinary vats and requires only a simple addition of equipment in which the water is heated by means of live steam. There are 2 figures, 4 tables, and 1 Russian-language Soviet reference.

Card 2/2

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5/724/61/000/000/012/020

AUTHORS: Kolobnev, I.F., Loktionova, N.A.

TITLE: The enhancement of the plastic properties of the alloy B300 (V300).

SOURCE:

Liteynyye alyuminiyevyye splavy; svoystva, tekhnologiya plavki, lit'ya i termicheskoy obrabotki. Sbornik statey. Ed. by I.N. Fridlyander and M.B. Al'tman. Mosvow, Oborongiz, 1961, 94-98.

TEXT: The paper describes various experimental approaches toward the improvement of the plasticity of the alloy B300 (V300) which excels by its elevated stress-rupture strength (7 kg/mm² for 100 hrs at 300°C and 4 kg/mm² for 100 hrs at 350°C), and an elevated creep strength (5 kg/mm² for 100 hrs at 300° and 2 kg/mm² for 100 hrs at 350°, with a residual strain of 0.2%, but which is severely limited in many applications by its low plasticity. The brittleness of the alloy is attributed to the presence in it of large particles of insoluble phases of the type of $Al_6Cu_3Ni_3$, $Al_3(GuNi)_2$, et al., containing Cr, Mn, and Fe. The present experimentation shows that a high plasticity can be attained in the V300 alloy with the following composition: 5% Cu, 3% Ni, no more than 1.2% Mg, no more than 0.3%

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The enhancement of the plastic properties

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rupture strength which satisfy the requirements of the Engineering Specifications. The plasticity of the V300 alloy can also be increased by means of a novel heattreatment procedure. The recommended procedure comprises a stepwise prequench heating, namely, heating to 500°C and 2-3-hr hold, an increase to 525-530° with a 2-3-hr hold. Quenching is then performed in saltpeter heated to 250-275°C, soaking at that temperature for 5 hrs, and avoidance of any artificially accelerated aging. This procedure affords a tensile strength in excess of 20 kg/mm^2 and a relative elongation of 1.2-2% with a stress-rupture strength that is still within the requirements of the Engineering Specifications. These conclusions are supported by a detailed description of the effect of the pre-quench heating temperature (fullpage tabulation) and the effect of the temperature of the quenching medium (tabulation). There are 2 figures and 2 tables; no references. The participation of L.V. Shvyreva in the experimental work on the effect of the chemical composition, that of L. V. Shvyreva and T. V. Boytsova in the experimental work on the effect of the pre-quench temperature, and that of N.S. Pantyushkova and T.V. Privezentsev in the experimental work on the effect of the quenching medium are acknowledged.

Card 2/2

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sional stat tended to v which are optimal an AA3 (AL3	The influence of anneal and cold treatment on the dimensional of die-cast Aluminum-alloy castings. Liteynyye alyuminiyevyye splavy; svoystva, tekhnologiya pla i termicheskoy obrabotki. Sbornik statey. Ed. by I. N. Frid and M. B. Al'tman. Moscow, Oborongiz, 1961, 111-117. The paper describes an experimental investigation intended t circumstances cold treatment of Al castings contributes to th bility of the castings. More especially, the work described her rerify the advisability of cold treatment under pressure of Al c not subjected to a strengthening heat treatment and also to dev nealing regime for castings and parts made of the Al alloys A bility of (AL9), a regime that would stabilize their dimensional and AA9 (AL9), a regime that would stabilize their dimension.	ivki, lit'ya ilyander to determine te dimen- re was in- tastings velop an A2 (AL2), ons after mensional	
casting an	d machining. The method used for the induced in the drawing of sho esulting from residual stresses consisted in the drawing were d	ort straight Irawn at a	
lines on 3 specified of Card 1/3	hitable portions of a part, and two transverse segmented acted distance from one another, in a manner that permitted repeate		

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The influence of anneal and cold treatment

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of the distance between the two lines as the process progressed. The measurements between the control lines were made with an accuracy of ± 0.01 mm. Both castings and machined parts were tested in that fashion. Cold treatment consisted in soaking at -50°C for 3, 6, 9, 12, 15, and 30 hrs. In the determations of the effect of holding time at 300° on the dimensional stability of the castings, the specimens were heated in air-circulation furnaces for 0.5, 2, 4, 6, and 8 hrs. Three cyclic procedures were also employed, as follows: (a) Anneal at $300 \pm 10^{\circ}$ C for 4 hrs; (b) anneal at $300 \pm 10^{\circ}$ for 4 hrs, followed by cold treatment at -50° C for 3 hrs; (c) cold treatment at -50° for 3 hrs, followed by anneal at $300 \pm 10^{\circ}$ for 4 hrs. The residual-stress investigation consisted of an anneal of the castings at 300° for 4 hrs, followed by machining according to the respective blueprints; the finished parts were again heated to 300°, and the various high- and low-temperature sequences outlined above were repeated. It was found that the second annealing of parts after machining is indispensable in the following cases: (a) When the part has a complex contour and, also, sharp variations in cross-section; (b) if the requirements for dimensional stability of a part are very stringent; (c) if the ratio of the machined surface to the unmachined surface is great. Following is the recommended heat treatment for a first-stage treatment for castings and for a second-stage treatment for some types of parts after machining to obtain the best possible dimensional stability: Anneal at $300 \pm 10^{\circ}$, holding for 2-4 hrs, and water cooling. Castings Card 2/3

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The influence of anneal and cold treatment $8/724/61/000/000/$ and parts must not be subjected to any kind of external dynamic ention, suc impact, shaking, compression, etc., either during or after anneal and also transportation. Cold treatment at -50° C of castings and parts made of AL and AL9 alloys, which have not been strengthened by heat treatment, have effect on the magnitude of the deformations. There are 6 figures and 1 ta no references. The participation of L. U. Rodicheva, A. F. Chuvikova, and Suvorova in the investigation is acknowledged.	ch as o during _2, -AL3, no able;
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LOKTIONOVA, N.A.; Prinimali uchastiye; PANTYUSHKOVA, N.S.; POBOCHINA, T.V.; KHASNOVA, A.I.; FEL'DMAN, F.Z.; INOZHAPSKAYA, L.A.; BOGUKHVALOVA, Z.V.; PRYTKOV, I.I. Increasing the dimensional stability of A19 alloy castings by heat treatment. Alium. splavy no.1:80-91 '63. (MIRA 16:11) APPROVED FOR RELEASE: 06/20/2000 CIA-RDP86-00513R000930420019-3"



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19306-2327

FETRUNIN, A.M.; LOKTIONOVA, N.A.; AL'TMAN, M.B., rukovoditel' raboty; Prinimali uchastiye: LOZHICHEVSKIY, A.S.; SHKROB, V.A.; POSTNIKOV, A.S.; ARBUZOV, B.A.; PANTYUSHKOVA, N.S.; FOBOCHINA, T.V.; PATRUSHEV, L.M. Mastering the production of large A18 alloy castings. Alium. splavy no.l:150-159 '63. (MIRA 16:11)

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ACCESSION NR: AP4019810 S/0279/64/000/001/00	85/0091	
AUTHOR: Loktionova, N. A. (Moscow)		
TITLE: Hardening of aluminum alloys in hot media		
SOURCE: AN SSSR. Izv. Metallurgiya i gornoye delo, no. 1, 1964, 85-91	lening,	
TOPIC TAGS: 'aluminum alloy, AK4-1 aluminum alloy, hardening, hot water hard salt bath thermal treatment, water hardening, cooling effect, cooling veloci residual stress effect		
ABSTRACT: The progress of the cooling process during the hardening of alumination of the progress of the cooling process during the hardening of alumination in metal properties and in residual stresses with respect to temp of the cooling medium. The AK4-1 aluminum alloy samples were heated in a point trate bath to 535C, and were subsequently cooled in boiling water and in room temperature. Formation of the vapor film and of separate vapor bubble studied cinematographically with the "Debri" camera (120 frames/sec). It was also been that metal hardening in hot media resulted in the formation of over a solid solution capable of further hardening during aging.	erature otassium water at s was as saturated	
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optimal temperature for the a Distribution of residual str of cooling regime during har decreased with the variation sional stability in large an	hardening in boiling water and in graded and for isothermal hardening esses in notal was independent of t dening, and of aging conditions. R in cooling rate. Hot water harden d complicated details during heat t ions. Orig. art. has: 1 table and	s was 190 I 10C. he alloy composition, esidual stresses ing secured dimen- creatment and during
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at 2000 were about equal for har optimal temperature for the grad Distribution of residual stress of cooling regime during harden decreased with the variation in sional stability in large and co subsequent mechanical operations	led and for isothermal harde es in metal was independent ing, and of aging conditions cooling rate. Hot water he omplicated details during he	enings was 190 L of the alloy com s. Residual stre ardening secured eat treatment and	10C. position, sses dimen-	
ASSOCIATION: none				
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AUTHOR: Loktionova, N. A.; Rastvorova, N. M.; Kovrizhny*kh, V. G.; Komarova, N. K.; Telis, M. Ya. TITLE: Ways to reduce warping of large parts made of alloy AK4-1 SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1964. Deformiruyemy*ye splavy* (Malleable alloys), 271-284 TOPIC TAGS: alloy AK4-1, extruded hollow cylinder, hollow cylinder warping, cooling stress, warping, alloy heat treatment, boiling water quenching, alloy mechanical property, aluminum alloy ABSTRACT: The authors report on a study designed to eliminate residual cooling stresses, which result in a rejection rate of up to 50% due to warping in machining. Inversely extruded and pierced hollow cylinders (wall thickness 32. 5-50.5 mm, outside diameter 591-855 mm, height 156-823 mm, weight 37 to 180 kg), manufactured in serial production from homogenized in lukewarm or 5 min. in boiling water) and aged 10 hrs. at 190C, then tested to determine effects of quenching in boiling water on mechanical properties, microstructure and warping.		BR
 Telis, M. Ya. TITLE: Ways to reduce warping of large parts made of alloy AK4-1 SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1964. Deformiruyemy*ye splavy* (Malleable alloys), 271-284 TOPIC TAGS: alloy AK4-1, extruded hollow cylinder, hollow cylinder warping, cooling stress, warping, alloy heat treatment, boiling water quenching, alloy mechanical property, aluminum alloy ABSTRACT: The authors report on a study designed to eliminate residual cooling stresses, which result in a rejection rate of up to 50% due to warping in machining. Inversely extruded and pierced hollow cylinders (wall thickness 32, 5-50, 5 mm, outside diameter 591-855 mm, neight 156-823 mm, weight 37 to 180 kg), manufactured in serial production from homogenized in lukewarm or 5 min. in boiling water) and aged 10 hrs. at 190C, then tested to determine effects of quenching in boiling water on mechanical properties, microstructure and warping. 	ACCESSION NR: AT4037668	S/2981/64/000/003/0271/0284
SOURCE: Alyuminiyevy*ye splavy*, no. 3, 1964. Deformiruyemy*ye splavy* (Malleable alloys), 271-284 TOPIC TAGS: alloy AK4-1, extruded hollow cylinder, hollow cylinder warping, cooling stress, warping, alloy heat treatment, boiling water quenching, alloy mechanical property, aluminum alloy ABSTRACT: The authors report on a study designed to eliminate residual cooling stresses, which result in a rejection rate of up to 50% due to warping in machining. Inversely extruded and pierced hollow cylinders (wall thickness 32.5-50.5 mm, outside diameter 591-855 mm, neight 156-823 mm, weight 37 to 180 kg), manufactured in serial production from homogenized ingots of alloy AK4-1, were hardened (45 min. in a niter bath at 528 ± 5C, quenched 2 min. in lukewarm or 5 min. in boiling water) and aged 10 hrs. at 190C, then tested to determine effects of quenching in boiling water on mechanical properties, microstructure and warping.	AUTHOR: Loktionova, N. A.; Rastvoro Felis, M. Ya.	va, N. M.; Kovrizhny*kh, V. G.; Komarova, N. K.;
alloys), 271-284 TOPIC TAGS: alloy AK4-1, extruded hollow cylinder, hollow cylinder warping, cooling stress, warping, alloy heat treatment, boiling water quenching, alloy mechanical property, aluminum alloy ABSTRACT: The authors report on a study designed to eliminate residual cooling stresses, which result in a rejection rate of up to 50% due to warping in machining. Inversely extruded and pierced hollow cylinders (wall thickness 32.5-50.5 mm, outside diameter 591-855 mm, neight 156-823 mm, weight 37 to 180 kg), manufactured in serial production from homogenized ingots of alloy AK4-1, were hardened (45 min. in a niter bath at 528 \pm 5C, quenched 2 min. In lukewarm or 5 min. in boiling water) and aged 10 hrs. at 190C, then tested to determine effects of quenching in boiling water on mechanical properties, microstructure and warping. Effects of aging temperature were evaluated in a separate series, where the latter was varied	FITLE: Ways to reduce warping of larg	e parts made of alloy AK4-1
warping, alloy heat treatment, boiling water quenching, alloy mechanical property, aluminum alloy ABSTRACT: The authors report on a study designed to eliminate residual cooling stresses, which result in a rejection rate of up to 50% due to warping in machining. Inversely extruded and pierced hollow cylinders (wall thickness 32.5-50.5 mm, outside diameter 591-855 mm, height 156-823 mm, weight 37 to 180 kg), manufactured in serial production from homogenized ingots of alloy AK4-1, were hardened (45 min. in a niter bath at 528 \pm 5C, quenched 2 min. In lukewarm or 5 min. in boiling water) and aged 10 hrs. at 190C, then tested to determine effects of quenching in boiling water on mechanical properties, microstructure and warping. Effects of aging temperature were evaluated in a separate series, where the latter was varied	SOURCE: Alyuminiyevy*ye splavy*, no. alloys), 271-284	. 3, 1964. Deformiruyemy*ye splavy* (Malleable
which result in a rejection rate of up to 50% due to warping in machining. Inversely extruded and pierced hollow cylinders (wall thickness 32.5-50.5 mm, outside diameter 591-855 mm, neight 156-823 mm, weight 37 to 180 kg), manufactured in serial production from homogenized ingots of alloy AK4-1, were hardened (45 min. in a niter bath at 528 \pm 5C, quenched 2 min. In lukewarm or 5 min. in boiling water) and aged 10 hrs. at 190C, then tested to determine effects of quenching in boiling water on mechanical properties, microstructure and warping. Effects of aging temperature were evaluated in a separate series, where the latter was varied	TOPIC TAGS: alloy AK4-1, extruded how warping, alloy heat treatment, boiling walloy	ollow cylinder, hollow cylinder warping, cooling stress, vater quenching, alloy mechanical property, aluminum
Card 1/2	which result in a rejection rate of up to and pierced hollow cylinders (wall thick height 156-823 mm, weight 37 to 180 kg ingots of alloy AK4-1, were hardened (4 in lukewarm or 5 min. in boiling water) effects of guenching in boiling water on	50% due to warping in machining. Inversely extruded ness 32.5-50.5 mm, outside diameter $591-855$ mm,), manufactured in serial production from homogenized 5 min. in a niter bath at $528 \pm 5C$, quenched 2 min. and aged 10 hrs. at 190C, then tested to determine mechanical properties, microstructure and warping.
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from 180 to 210C. Results are retention of properties adequat kg/mm ² , yield 29.3-34.3 kg/m degree obviating the the need for under the guidance of V. I. Dol G. F. Bulgakov, V. I. Pyatuni Veysman, N. N. Aper'yanova, in the work." Orig. art. has:	e for technical requirem m ² , elongation 12.0-17 or straightening procedu patkin; N. G. Vinokurov, a, S. M. Titkov, K. V. N. S. Pantyushkova and	ents (tensile .7%), but eli res. "The w Yu. N. Por Kalmy*koy.	strength 39. minates war ork was car nagaybo, I. N D. N. Brasl	ping to a ried out I. Perety*kina avskiv. S. Ya	< 19
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ACC NR: AT6024928 (A,N) SOURCE CODE: UR/2981/66/000/004/0187/0191	
AUTHOR: Loktionova, N. A.; Ovchinnikov, Yu. F.; Nikonorov, Ye. A.; Zamolodchikova, V. N.; Lapina, L. V.; Perevozchikov, A. V.; Potapov, P.I.,	
ORG: none 42	
TITIE: Residual stresses in weld joints of aluminum alloys B+1	
SOURCE: Alyuminiyevyye splavy, no. 4, 1966. Zharoprochnyye i vysokoprochnyye splavy (Heat resistant and high-strength alloys), 187-191	
TOPIC TAGS: tensile stress, compressive stress, aluminum alloy property, weld evalu- ation	
ABSTRACT: The residual stresses in various parts of a welded structure of ATSM alloy were determined by a mechanical method, and the influence of the artificial aging and tempering of the weld joints on the magnitude of these stresses was investigated. It was found that longitudinal residual stresses up to $10-11 \text{ kg/mm}^2$ and compressive re- sidual stresses up to $11-12 \text{ kg/mm}^2$ in the transverse direction arise in the zone of the weld joints. Artificial aging of the weld joints of ATSM alloy for 100 hr at 90° does not change the magnitude and character of the residual stresses in the heat-af- fected zone as compared to the residual stresses in the naturally aged state. Temper- ing of the zone of the weld joint by induction heating to 240-250 °C for 4-5 min fol- lowed by cooling of the heat-affected zone with water increases the magnitude of the Card $1/2$	

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ongitudinal te the same tim each 4 kg/mm ² .	nsile residual str w, the transverse Orig. art. has:	essos by 1.5-2 kg residual stresses 2 formulas.	g/mm ² , without changing change into compress	ng the sign. sive ones and
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AUTHOR: Loktionova, N. A.; Kulakov, V. I.; Isayev, V. I.
TITLE: Heat treatment of products of AK6 aluminum alloy in hot media
SOURCE: Alyuminiyevyye splavy, no. 4, 1966. Zharoprochnyye i vysokoprochnyye splavy (Heat resistant and high-strength alloys), 341-349
TOPIC TAGS: metal heat treatment, aluminum alloy property
ABSTRACT: A study of the mechanical, corrosion and microstructural properties of pressed billets and stampings of AK6 alloy showed that in quenching in hot media, depressed billets and stampings of AK6 alloy showed that in quenching in hot media, depressed billets and decrease in cooling rate/as compared to ordinary quenching in water at aging and isothermal holding in a salt melt at the temperature of artificial aging. Industrial tests showed that stepwise and isothermal quenching schedules can be used in hot water at 90 °C can be used for stampings with a cross-sectional thickness of no more than 15 mm. Cuenching 50 mm without any appreciable decrease in properties. The observed slight decrease in solid solution along the grain boundaries. For this reason, articles with a finely Cord $1/2$
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	L 46975-65 ACC NR: AT6024950 the cooling rate than articles with a coarse-grained recrystallized structure. Tree	
	general corrosion and stress corrosion after quenching in not media are practically the same as after ordinary quenching followed by artificial aging. Orig. art. has: 4 figures and 1 table.	
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GG/RM/GS EWT(m)/EPF(n)-2/EWP(j)/T/EWA(h)/EWA(1) SOURCE CODE: UR/0000/65/000/000/0037/0042 L 42974-66 (A) ACC NR: AT6006242 1-1 AUTHOR: <u>Dubrova, L. N.; Kachan, A. A.; Loktionova, R. A.; Chervyatsova, L. L.;</u> Kornev, K. A. (Doctor of chemical sciences) ORG: Institute of Chemistry of High Molecular Compounds, AN UkrSSR, Kiev, (Institut khimii vysokomolekulyarnykh soyedineniy AN (krSSR) TITLE: Radiochemical polymerization of allyl esters of certain N-methylol deriva-19,44,55 tives of acid amides SOURCE: AN UkrSSR. Modifikatsiya svoystv polimerov i polimernykh materialov (Modification of the properties of polymers and polymeric materials). Kiev, Naukova dumka, 1965, 37-42 TOPIC TAGS: <u>radiation polymerization</u>, organic amide, IR spectrum ABSTRACT: Allyl esters of N-methylol derivatives of acetamide, chloroacetamide, and benzamide were polymerized both in the pure state and in benzene and methanol solutions by irradiation with Co⁶⁰ gamma rays. Formation of the polymer was determined visually and also by means of viscosity and IR spectral measurements. In benzene 2 Card 1/2 CONTRACTOR OF

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and methanol, the effectiveness of the irradiation was one order of magnitude greater than in the bulk. IR spectra showed that even when doses of 1500 Mrad are used, no appreciable degradation of the allyl monomers takes place. The dependence of the content of allyl groups on the irradiation dose was determined. The decrease in the content of allyl groups observed indicates that the polymerization takes place at the double bonds. Orig. art. has: 2 figures, 3 tables.

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MIKHAYLOV, I.A.; LOKTIONOVA, Ye.L.

الصحابة بمديدة

Adsorption properties of molecular sieves during liquid phase sorption of hydrocarbons. Khim.i tekh.tcpl.i masel 3 no.11: 4-10 N '63. (MIRA 16:12)

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SUBACK CODE: 08/0065/65/000/0	008/0008/0012	2	
AUTHOR: Mikhaylov, I. A.; Polyakova, A. A.; Khmel'nitskiy, R. A.; Loktic Medvedev, F. A.			
Medvedev, F. A.	onova, 10. L.		
ORG: VNII NP	24		
TITLE: Hydrocarbon composition of dearomatized liquid paraffins	B		
SOURCE: Khimiya i tekhnologiya topliv i mascl, no. 8, 1965, 8-12 TOPIC TAGS: hydrocarbon aromatic hydrocarbon aromatic			
TOPIC TAGS: hydrocarbon, aromatic hydrocarbon, petroleum refining, petro ABSTRACT: The hydrocarbon composition of highly dearomatized liquid para	chemistry		·
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naphthene hydrocarbons up to 1% and anomatic budge and structure 3-4%,			
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structure paraffin hydrocarbons (90% and lower) and a high content of iso ffin hydrocarbons (from 8 to 17%). Distribution of normal-structure para			
	ame as quantitativa		
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OPIC TACS: horphorus	red phosphorus,	yellow phosphorus	(Gor'kiy), vy*p. , purity, vacuum d	istilletion,		
rom impuriti quivalent ac qual amounts cid for peri	es of mineral ac tion of 3 and 59 , was demonstrat ods of 12 hours,	HNO ₃ , H ₂ SO ₄ , and ed at 70-95°. Two followed by wash	echnical commercia entrations was stu HCl or their mixt o treatments of re ing with distilled total content of t as of vacuum disti	taken in the phosphorus water and the impurities	n with	
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technical yellow at a residual pr zation to the re impurities to be of two to three method of four d range 1.10 ⁻² -1.10	phosphorus, p essure of 1.10 d modification determined eq distillations. istillations. 0 ⁻⁴ mm of mercy	reliminarily purified of (-2-1.10-4 mm of mercury, was studied. Phosphorus ual to 5.10-4% and lower Spectrally pure phosphor No influence of the depth ury or of the variety of (From the authors' summary.	followed by its poly containing a sum of is obtained by the r rus is obtained by the h of the vacuum in the rlass on the curling	ymeri- f the method the		
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LOKTYUKHOV, M.; IVANOV, V. Widespread precast construction. Stroitel' no.6:3-8 Je '61. (MIRA 14:37) Upravlyayushchiy trestom Mosstroy No.3 (for Loktyukhov).
Sekretar' partorganizatsii tresta Mosstroy No.3 (for Ivanov). (Moscow-Construction industry) N





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LONTYUSTEA, L. A.

Loktyushina, L. A.

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"The Concept of Mass in the Physics Course at the Intermediate School." Moscow State Pedarogical Inst imeni V. I. Lenin. Moscow, 1955. (Dissertation for the Degree of Candidate in Pedagogical Science)

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DERA, J.; SZCZEBIEWSKI, B.; LOKUCIJEWSKI, B.

Radioactive contamination of sea water in the North European region. Acta geophys pol 10 no.2:173-182 '62.

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•	s/058/63/000/002/030/070 A062/A101	•
AUTHOR:	Varshavskaya, N. B., Levenberg, T. M., Lokutsiyevskaya, L. K.	
TITLE:	On the requirements regarding the exposure conditions in motion- -picture photography on multilayer materials in the case of utilizing intermediate contratyping	
PERIODICAL:	Referativnyy zhurnal, Fizika, no. 2, 1963, 99 - 100, abstract 2D644 ("Uspekhi nauchn. fotogr.", 1962, v. 8, 172 - 178)	
graphing is posed accord graphing obj terioration when changin contratyping a wide range	It is shown that in the direct negative-positive process and in the contratyping by the reversal method, the exposure reserve in photo- on the average the same. For films $\square C - 2$ (DS-2) and $\square H - 3$ (LN-3), ex- ing to the technical conditions, it is about 1.4 - 1.5 when photo- ects of an average contrast. For original color positives, the de- noted in the quality of the colored image as compared to the optimum, g the exposure, is as a rule gradual. But with positives obtained from , the quality of the color image, remaining nearly the same within of exposures, sharply decreases behind that range. In negatives cor- o original positives, still satisfactory as to their quality of color	

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reproduction, and to positives from contratyping, use is almost always made of the curvilinear portions of the characteristic curves of the negative material. Positives quite unsatisfactory as to the quality of reproduction are usually obtained when in one or in two layers of the negative film the straight-line portions of the characteristic curves are but little utilized, while the initial or terminal portions thereof are utilized almost completely. The convenience control of negatives for contratyping can be carried out on the color-light passport of the original negative. Changes of exposure in photography within rather wide limits have little effect on the quality of color reproduction in both the direct negative-positive process and in the process with intermediate contratyping on the reversed film.

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AUTHORS:	Balabukha, D. K., Levenberg, T. M., Lokutsiyevskaya, L. K., Khristinina, G. N.	
PITLE:	Sensitometric test for controlling color reproduction. I. Construc- tion principles of the test	
PERIODICAL:	Referativnyy zhurnal, Fizika, no. 3, 1963, 87, abstract 3D589 ("Tr. Leningr. in-ta kinoinzhererov", 1961, no. 6, 91 - 98)	2
ses. The a rimetric ev the measure all the sta gradation s production	This is a report on elaborated construction principles of a test gating and controlling color reproduction in color photography proces- pplication of such a test permits to replace the physiological colo- aluation of the color reproduction by a physical evaluation, based on ment of the dye concentrations. The investigation, by this test, of ges of a color photography process (color separation, synthetic and tages) in their mutual relationship permits to describe the color re- as an objective process property characterized by the configuration r reproduction bands. The test provides the possibility to judge on	

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the intermediate images, obtained at the differ- the color separation and gradation characterist the aid of the test, it is possible to determine logical factors in the formation of the quality that by the test it is possible to compare object graphy processes and different technological van	of a color image. It is shown	
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LEVENBERG, T.M.; LOKUTISYEV3KAYA, L.K.

Determining the macrograininess of monochromatic color fields by means of the photographic projection method. Usp.nauch.fot. 10:195-201 ¹64. (MIRA 17:10)

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LOKUYSIYL/SUIY, O. V.

LOKUTSITYEVSKIY, O. V. -- "Certain Problems in the Theory of Continuous Representations (Reflections) of Closed Sets." Sub 20 Feb 52, Sci Res Inst of Mechanics and Nathematics, Mescow Order of Lenin State U imeni M. 7. Lomonosov. (Discertation for the Decree of Candidate in Physicomathematical Sciences).

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SO: Vechernaya Moskva January-December 1952

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SALVADORI, Mario, G.; LOKUTSIYEVSKIY, O.V.[translator]; SEMENDYAYEV, K.A., redaktor; ACHANOVICH, M.S., redaktor; SHAPOVALOV, V.I., tekhnicheskiy redaktor.

> [Numerical methods in engineering.Translated from the English] Chislennye metody v tekhnike. Perevod s angliiskogo O.V.Lokutsievskogo. Pod red. K.A.Semendiaeva. Moskva, Izd-vo inostrannoi lit-ry, 1955. 247 p. (MLRA 9:4) (Numerical calculations) (Engineering--Tables, calculations, etc.)

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Continuous flow of overburden in open mines of the north Bohemian lignite basin. Uhli 5 no.6:208-209 Je ¹63.

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LOKVENC, T.

Specimens of trees, foreign to the area of Krkonose (Riesengebirge). p. 183 (Ochrana Frirody Vol. 11, no. 6, July 1956 Praha)

SO: Nonthly List of East European /ccession (EEML) IC, Vol. 6, no. 7, July 1957. Uncl.

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The Alpine forest line in the Krkonose Mountains. Rozpravy mat CSAV 72 no.1:1-65 '62.

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LOKVENC, V.

Froper heights of the crest of a dam at diverging and navigable lateral canals. p. 124. VODNI HCSFODARSTVI. (Ustredni sprava vodniho hospodarstvi) Praha. No. 5, 1954.

SOURCE: East European Accessions List, (EFAL). Library of Congress. Vol. 5 no. 12, December 1956

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Vol. 3, No. 6, 1955 SCVETSFA VEDA: VCDNI STAVITELSTVI. TICHNOLCGY Praha, Czechoslovakia

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SOURCE: East European List (TEAL) Library of Congress, Vol. 6, No. 1, January 1957

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MYSHEO, D., redaktor; ASEYEV, Yu.; BEVZO, A.; VINTOROV, A.; GRISHEO, N.; DOROSHENKO, Ye.; YEVTUSHEDKO, A.; IGMATKIN, I.; KOZYKENKO, W.; LOIA, A.; LYSENKO, A.; LYSENKO, M.; PANKEYEV, V.; POLUPANOVA, I.; TELECIE, D.; CHUDNOVSKAYA, I.; DEHEVYANKO, G., tekhnicheskiy redaktor. [Kiev; a guidebook] Kiev; spravochnik-putevoditel'. Kiev, Gos. isd-vo polit, lit-ry USSR, 1954. 284 p. [Microfilm] (MLEA 8:2) (Kiev--Guidebooks)

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LOLA, A.T.

Some criteria of the activity of the tubercular process in pulmonary tuberculomas. Vrach.delo no.3:135-136 Mr '63. (MIRA 16:4)

1. Kliniko-dispansernyy otdel (zav. - prof. V.P.Rudin) Ukrainskogo nauchno-issledovatel'skogo instituta tuberkuleza i grudnoy khirurgii.

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LOHN V.N. 133-10-14/26 Filonov, V. A., Ksenzuk, F. A., Lola, V. H., and AUTHOR: Khudas, A. L. Engineers. Production of Hot Rolled Plates from the Kh18N25S2 Steel. TITLE: (Proizvodstvo Goryachekatanogo Lista Iz Stali X18H25C2). FERIODICAL: Stal', 1957, No.10, pp. 917-918 (USSR). ABSTRACT: Heating of 10.5 t. ingots from X18H2502 steel and their rolling into slabs, as well as subsequent heating of slabs and their rolling into plates was investigated in order to determine the most suitable practice. According to POCT-5632-51, the above steel should have the following composition: 0.30 - 0.40% C; 41.5% Mn; 2.0-3.0% Si; ≤0.035% P; ≤0.025% S; ≤17.0-20.0% Cr; 23.0-26.0% Ni. The following heating practice was adopted; temperature of the pit during charging 950°C; rate of heating until soaking period 80-100°C/hr, the temperature of walls during soaking 1200-1220°C; duration of soaking 2 hours 45 min.; total heating time 6 hours 10 min. Two invotes were realled into slobe (135 6 hours 10 min. Two ingots were rolled into slabs (115 x 1050 mm) from one heating in 39 and 35 passes respectively. One ingot was rolled with intermediate heating after 16 passes (thickness 400 mm) for 1 hour 20 min. at 1220°C and subsequent finishing in 23 passes. The maximum value of absolute reduction per pass did not exceed 10-15 mm. Card1/2 The surface quality of all ingots was approximately the

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Marken V. N.

AUTHORS: Filonov, V.A., Podgorodetskiy, A.A., Ksenzuk, F.A. and Lola, V.M. (Engineers)

TITLE: From Experience in Production of Two Layer (Clad) Ingots and Slabs (Opyt proizvodstva dvusloynykh slitkov i slabov)

PERIODICAL: Stal', 1958, Nr 2, pp.188-191 (USSR)

ABSTRACT: The technology of production of clad ingots and slabs from steels 20K and X18H12M27 developed on the Zaporozhstal' Works is described. The method consists of teeming steel 20K into an ingot mould into which a plate from stainless steel was fixed (Figs.1, 2). The preparation of stainless plate, heating (Table 2) and rolling clad ingots, dimensions of clad slabs (Table 2) and mechanical properties of clad plate produced (Table 3) are given. There are 3 tables and 4 figures.

ASSOCIATION: Zaporozhstal' Works (Zavod "Zaporozhstal'")

AVAILABLE: Library of Congress.

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KSENZUK, F.A., inzh.; LOLA, V.N., inzh.; PAL'CHIK, W.V., inzh. Investigating the heating and rolling of electrical steel slabs. Stal' 20 no.8:738-739 Ag '60. (MIRA 13:7) 1. Zavod "Zaporozh'stal'." (Rolling(Metalwork))

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s/133/63/000/001/009/011 A054/A126 Filonov, V. A. (Deceased), Lola, V. N., Pavlishchev, V. B., AUTHORS: Petrenko, I. S., Engineers Flame cleaning of stainless steel ingots and preparing slabs for TITLE: rolling PERIODICAL: Stal', no. 1, 1963, 73 - 75 The surface defects of 12-ton stainless steel ingots (maximum cross section: 640 x 1,100 mm, height: 2,200 mm) produced at the zavod "Dneprospetsstal'" ("Dneprospetsstal'" Plant) and rolled at the zavod "Zaporozhstal'" (Zaporozhstal'" Plant) could not be removed by conventional planing and grinding methods. In 1961, tests were carried out (in co-operation with L. N. Soroko, F. M. Dolmatov, M. Ye. Kugayenko, V. G. Antipenko, F. A. Yevtushenko, V. K. Barziy, N. V. Pal'chik, N. P. Cherkashina, V. I. Kalabukhov, V. I. Kiselev, A. V. Sysoyev, Yu. V. Zagorul'ko, B. M. Tsirlin, V. D. Klipinitser, Engineers, et al.) to remove the surface defects of the ingots by flame-cleaning. Based on the construction of the PP -53 (RR-53) type flame cutter a special - .1 Card 1/3

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Flame cleaning of stainless steel ingots and...

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apparatus was designed, in which the burning substance ejected from the head of the apparatus consisted of crushed dalcium silicate and the so-called NAM-4 (PAM-4) powder (50% aluminum and 50% magnesium) in a volume ratio of 2 : 1. The heat developed by the burning mixture is sufficient for both carbon and stainless steels. Calcium silicate in the mixture has a fluxing effect on the highsmelting components, it makes the slag layer fluid and promotes its removal. The powder mixture is ejected through a jet of oxygen of 99.0% purity under a pressure of 10 atm. The cutter head is also supplied with natural gas (calorific value: 8,340 cal/stand m³) under a pressure of 3 atm. One run of the flame cleaner cleans the ingot surface to a depth of 3 - 7 mm and over a width of 150 - 200 mm. Then follows the secondary cleaning, which removes the remaining deeper defects to a depth of 20 - 30 mm. After flame cleaning, the metal surface is slightly corrugated with ridges not higher than 3 mm. The metal loss in flame cleaning is 10 - 30 kg/ton of flawless metal, whereas in the planing process: up to 51 kg/ton. However, as flame cleaning alone did not produce the required flawless ingot surface and as it requires much labour, tests were carried out to combine it with other finishing processes, i.e. I. flame cleaning + local removal of single defects by grinding, II. flame cleaning + continuous

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