Concerning the Mechanism of Diborane Reaction With Olefins

77388 sov/79-30-1-49/78

3R001031500021

Theoretically, a B atom can join either of the C=C carbon atoms and form isomers. According to D. Hurd, diborane gave with olefins equal amounts of isomers (X) and (XI); for example:

 $B_{2}H_{6} + 6 \frac{CH_{3}}{CH_{3}}C = CH_{2} \rightarrow 2B \begin{pmatrix} CH_{3} \\ CH_{3} \end{pmatrix} \begin{pmatrix} X \\ CH_{3$

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It was also reported (J. Am. Chem. Soc., 1956, Vol 78, p 5694; Chem. Eng. News, 1957, Vol 6, Nr 28) that the olefins, on reduction with sodium borohydride in the presence of AlCl₃, gave the corresponding primary alco-

hols. In view of the contradictory data on the order of diborane addition to olefins, the authors investigated the mechanism of this reaction. Propylene with diborane on heating to $230-250^{\circ}$ C gave tripropylboron in 91%

Card 2/3

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	AUTHORS:	Zhigach, A. F., Siryatskaya, V. N., Antonov, I. S., Makayeva, S. Z.	τι 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	TITLE:	Concerning the Mechanism of Diborane Reaction With Olefins	
	PERIODICAL:	Zhurnal obshchey khimii, 1960, Vol 30, Nr 1, pp 227-230 (USSR)	
	ABSTRACT:	Diborane reacts with excess olefins, and forms, successively, alkyldiboranes $(RB_2H_5; R_2B_2H_4; R_3B_2H_8; etc.)$	
		according to the reactions:	
0		$\begin{array}{c} B_2H_6 \xrightarrow{\sim} 2BH_3 (1V), \\ B_2H_0 \xrightarrow{\rightarrow} BH_3 \xrightarrow{\sim} B_3H_0 (V), \\ B_3H_0 + G_0H_{2n} \xrightarrow{\sim} BH_3 + B_2H_5G_0H_{2n+1} (VI), \end{array}$	
		$B_{3}\Pi_{0} + G_{n}\Pi_{2n} \longrightarrow B\Pi_{3} + B_{2}\Pi_{5}G_{n}\Pi_{2n+1} (\forall I),$ $B_{2}\Pi_{5}G_{n}\Pi_{2n+1} + B\Pi_{3} \longrightarrow B_{3}\Pi_{8}G_{n}\Pi_{2n+1} (\forall I),$	
		$B_{3}H_{8}C_{n}H_{2n+1} + C_{n}H_{2n} \rightarrow BH_{3} + B_{2}H_{4}(C_{n}H_{2n+1})_{2} (V11)$	
	Card 1/3	$B_{3}H_{4}(C_{n}H_{2n+1})_{5} + C_{n}H_{2n} \rightarrow BH_{3} + 2B(C_{n}H_{2n+1})_{5} (1X)$	



29020 S/038/61/025/005/001/001 C111/C222 The asymptotic behavior of the . . . where V(t, E) is the solution of $\frac{\mathrm{d}V}{\mathrm{d}t} = \frac{1}{\varepsilon} \mathbf{w} \left[\mathbf{v}(t, \varepsilon) \right] - \frac{1}{\varepsilon} \mathbf{w} \left[\mathbf{\overline{v}}(t) \right] + \mathbf{B} \left[\mathbf{\overline{\varphi}}(t, \varepsilon) + \mathbf{\overline{v}}, \mathbf{\overline{v}}(t) \right] \mathbf{v} \left(t_{0}, \varepsilon \right) = 0$ (2.25) $(\hat{\mathbf{M}} = \text{const}, \mathcal{E}_{0} \leq \mathbf{a}, \mathbf{D}_{0} - \mathbf{a}$ S-neighborhood of the solution $\overline{\mathbf{v}}(\mathbf{t})$ of the system system $\frac{\mathrm{d}\mathbf{v}}{\mathrm{d}\mathbf{t}} = \mathbf{\overline{V}}(\mathbf{v})$ (2.23) on $[t_0, L]; S > 0$ is so that $\overline{D}_0 \subset D)$. Two further theorems relate to the behavior of the solutions of (2.1) in the exceptional case where the system (2.2) has a non-degenerated whirl as its equilibrium position. Finally it is shown that the well-known older results by V.M. Volosov on the solutions of differential equations with a small parameter can be concluded from the author's theorem. The author mentions D. V. Anosov, Yu. A. Mitropol'skiy, L.S.Pontryagin, V.J. Smirnov, L.V.Rodygin, N.N. Bogolyubovand D.N.Zubarev. Card 11/12

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The asymptotic behavior of the ... $\frac{d\varphi}{dt} = \frac{1}{\xi} \quad w(v)$ $\frac{dv}{dt} = \tilde{V}(v)$ $(\frac{dv}{dt} = \tilde{V}(v)$ $(\tilde{V}(v) = \int_{0}^{1} V(\tilde{Y}, v, 0) d\tilde{Y}, \tilde{Y} > 0$ with the initial conditions $\tilde{\Phi}(t_{0}, \xi) = \tilde{\Psi}(v)$, $\tilde{V}(t_{0}) = v_{0}$. Let $\tilde{v}(t)$ remains in D on $[t_{0}, L]$. Then there exists an $\xi_{0} > 0$ so that $v(t, \xi)$ for every $\xi \in (0, \xi_{0}]$ and $t \in [t_{0}, L]$ remains in a certain closed bounded region $\tilde{D}_{0} \subset D$ and it holds $\left| v_{1}(t_{0}, \xi) - \tilde{v}_{1}(t) \right| \lesssim \stackrel{\circ}{M} \xi, \ 1 = 1, \dots, r, \\ |\tilde{\Psi}(t, \xi) - \tilde{\Psi}(t, \xi)| < \tilde{\Psi}(t, \xi)| \leq \stackrel{\circ}{M} \xi \cdot |V(t, \xi)| \leq \stackrel{\circ}{M} (2.21)$ Card 10/12

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RDP86-00513R001031500021 29020 s/038/61/025/005/001/001 C111/C222 The asymptotic behavior of the $\frac{\mathrm{d}\varphi}{\mathrm{d}t} = \frac{1}{\xi} \mathbf{w}(\mathbf{v}) + \mathbf{B}(\varphi, \mathbf{v}, \xi),$ (2.19) $\frac{\mathrm{d}\mathbf{v}}{\mathrm{d}\mathbf{t}} = \mathbf{V}(\mathbf{\varphi}, \mathbf{v}, \mathbf{\mathcal{E}}),$ where $\xi > 0$ is a small parameter, the functions w(v), $B(\phi, v, \xi)$, $V_1(\phi, v, \xi), \dots, V_r(\phi, v, \xi)$ together with their first partial derivatives are defined in $\varphi \in (-\infty, \infty)$, $v \in D$, $\varepsilon \in [0,a]$ and continuous (D-- open region of the Euclidean E of the variables v_1, \ldots, v_r), where $w(v) \neq 0$. The functions $B(\varphi, v, \varepsilon)$, $V_1(\varphi, v, \varepsilon)$,... ..., $V_r(\varphi, v, \varepsilon)$ are periodic in φ with the period 1. Let $\{\varphi(t, \bar{\xi}), v(t, \xi)\}$ be the solution of (2.19) corresponding to the initial conditions $\Psi(t_0, \mathcal{E}) = \Psi_0, v(t_0, \mathcal{E}) = v_0 \quad (v_0 \mathcal{E} \quad D, \ 0 < \mathcal{E} \leq a).$ Let $\{\varphi (t, \mathcal{E}), v(t)\}$ be the solution of the averaged system Card 9/12

The asymptotic behavior of the . . . C_{111}^{29020} $S_{038}^{61/025/005/001/00}$, $C_{111}^{t}C_{222}^{t}$ $+ \oint \left[\oint_{0}^{t} + \frac{1}{\epsilon} \int_{0}^{t} \frac{1}{T[\tilde{h}(r),\tilde{z}(r)]} dr + V, \tilde{h}(t), \tilde{z}(t), 0 \right], V(t_{0}, \epsilon) = 0$ where $\oint (\varphi, h, z, \epsilon) = \frac{1}{T(h, z)} \left[X(\tilde{x}, \tilde{y}, z, \epsilon) \frac{\partial y}{\partial h} - Y(\tilde{x}, \tilde{y}, z, \epsilon) \frac{\partial x}{\partial n} + \frac{1}{\epsilon} Z_{j}(\tilde{x}, \tilde{y}, z, \epsilon) \left(\frac{\partial x}{\partial h} \frac{\partial y}{\partial z_{j}} - \frac{\partial y}{\partial h} \frac{\partial x}{\partial z_{j}} \right) \right]$ The proof of the theorem is based on the properties of the solutions of (2.2) (under the assumptions of theorem 1), on the statement based on the latter that (2.8) represents a certain everaged system, and

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Averaging theorem: Given the system

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The asymptotic behavior of the . . . C111/C2222) The functions $x(t, \mathcal{E})$, $y(t, \mathcal{E})$ are identical with the functions

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$$\frac{*}{x} \left(\varphi + \frac{1}{\varepsilon} \int_{t_0}^{t} \frac{1}{T[\overline{h}(r), \overline{z}(r)]} dr + v(t, \varepsilon); \overline{h}(t), \overline{z}(t) \right),$$

$$\frac{*}{y} \left(\varphi_0 + \frac{1}{\varepsilon} \int_{t_0}^{t} \frac{1}{T[\overline{h}(r), \overline{z}(r)]} dr + v(t, \varepsilon); \overline{h}(t), \overline{z}(t) \right)$$

up to terms of the order $O(\mathcal{E})$. Here φ_{o} is determined from the relations: $\mathbf{x}_{o} = \mathbf{x} (\varphi_{o}, \mathbf{h}_{o}, \mathbf{z}_{o}), \mathbf{y}_{o} = \mathbf{y} (\varphi_{o}, \mathbf{h}_{o}, \mathbf{z}_{o}), |O(\mathcal{E})| \leq M_{o} \mathcal{E},$ $|\mathbf{v}(\mathbf{t}, \mathcal{E})| \leq M_{o}, M_{o} = \text{const}, \mathbf{v}(\mathbf{t}, \mathcal{E})$ is the solution of the equation $\frac{d\mathbf{v}}{d\mathbf{t}} = \frac{1}{\mathcal{ET}[\mathbf{h}(\mathbf{t}, \mathcal{E}), \mathbf{z}(\mathbf{t}, \mathcal{E})]} - \frac{1}{\mathcal{ET}[\mathbf{h}(\mathbf{t}), \mathbf{z}(\mathbf{t})]} + Card 7//12$

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$$\frac{29020}{S/038/61/025/005/001/001}$$
The asymptotic behavior of the . . . C111/C222
1) The solution { $x(t, \mathcal{E}), y(t, \mathcal{E}), z(t, \mathcal{E})$ } of (2.1) runs in G, and
the functions $h(t, \mathcal{E}), z_1(t, \mathcal{E}), \ldots, z_1(t, \mathcal{E})$ ($h(t, \mathcal{E}) = \mathbb{H}[x(t, \mathcal{E}), y(t, \mathcal{E}), z(t, \mathcal{E})]$) are identical up to terms of the order $O(\mathcal{E})$ with
the functions $\overline{h}(t), \overline{z}_1(t), \ldots, \overline{z}_1(t)$ being solutions of the following
autonomous system which is independent of \mathcal{E} :

$$\frac{dh}{dt} = \frac{1}{T(h, z)} \oint_{H(x, y, z)=h} \left[X(x, y, z, 0) \frac{\partial H(x, y, z)}{\partial x} + + Y(x, y, z, 0) \frac{\partial H(x, y, z)}{\partial y} + \sum_{j=1}^{l} Z_j(x, y, z, 0) \frac{\partial H(x, y, z)}{\partial z_j} \right] \times \\
\times \left[\left(\frac{\partial H(x, y, z)}{\partial x} \right)^s + \left(\frac{\partial H(x, y, z)}{\partial y} \right)^s \right]^{-\frac{1}{2}} ds, \\
\frac{\partial z_j}{dt} = \frac{1}{T(h, z)} \oint_{H(x, y, z)=h} Z_j(x, y, z, 0) \left[\left(\frac{\partial H(x, y, z)}{\partial z} \right)^3 + \frac{\partial z}{\partial z} \right]^s + \frac{\partial z}{\partial z} \right]$$
(2.8)

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The asymptotic behavior of the . . . C1

be the equation of the trajectory through $(\overset{0}{x}, \overset{0}{y}, \overset{0}{z})$. Let (2.4) lie completely in \widetilde{G} and let it be closed. Then it is shown that in E_{1+2}

there exists a neighborhood G of (2.4) with the following properties: 1) the phase trajectories of (2.2) going through the points of G are closed and lie completely in G. 2) For every pair (h,z) the equation (2.3) determines exactly one trajectory of (2.2) lying in G. 3) On each phase trajectory (2.3) of (2.2) one point $\{\infty, h, z\}, \beta(h, z), z\}$ can be given which depends smoothly on h,z.

The basic result of the paper is contained in Theorem 1: Let H(x,y,z), $\frac{\partial H(x,y,z)}{\partial x}$, $\frac{\partial H(x,y,z)}{\partial y}$ together with their partial derivatives up to the second order be continuous and defined in G. Let $X(x,y,z,\mathcal{E})$, $Y(x,y,z,\mathcal{E})$, $Z_1(x,y,z,\mathcal{E})$..., $Z_1(x,y,z,\mathcal{E})$ together with their first partial derivatives be continuous in G, $0 \leq \mathcal{E} \leq a$ (a > 0). Then there exists an $\mathcal{E}_0 > 0$ ($\mathcal{E}_0 \leq a$) so that for every $\mathcal{E} \in (0, \mathcal{E}_0]$ on the finite interval $[t_0, L]$ it holds: Card 4/42
$$\begin{split} & \begin{array}{c} 29020\\ & & & \\ & & & \\ & & \\ & & \\ & & \\ & & & \\ & & \\ & & \\ & & & \\ & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & &$$

 $\frac{29020}{s/036/61/025/005/001/001}$ The asymptotic behavior of the ... $g_{111}/222$ $\frac{dx}{dt} = \frac{\partial H(x,y,z)}{\langle x,y,z \rangle} + \langle \xi X (x,y,z,\xi) \rangle, \qquad (2.11)$ $\frac{dy}{dt} = -\frac{\partial H(x,y,z)}{\partial x} + \langle \xi Y (x,y,z,\xi) \rangle, \qquad (2.11)$ $\frac{dz}{dt} = \langle \xi Z(x,y,z,\xi) \rangle$ The system $\frac{dx}{dt} = -\frac{\partial H(x,y,z)}{\partial y} \rangle, \qquad (2.2)$ $\frac{dy}{dt'} = -\frac{\partial H(x,y,z)}{\partial x} \rangle, \qquad (2.2)$ $\frac{dy}{dt'} = 0$ arising from (2.11) for $\xi = 0$ is called the system of "quick motions" card 2/42

3R00103150002

EASE: 06/23/1 -RDP86-00513R001031500021-6 PPF PEI 29020 s/038/61/025/005/001/001 0111/0222 16,3400 Makayeva, G. S. AUTHOR : The asymptotic behavior of the solutions of differential equations with a small parameter the systems of "quick TITLE: motions" of which are Hamiltonian Akademiya nauk SSSR. Izvestiya. Seriya matematicheskaya, PERIODICAL: v. 25, no. 5, 1961, 685-716 TEXT: The author considers the system $\mathcal{E} \frac{\mathrm{d}x}{\mathrm{d}t} = \frac{\partial H(x,y,z)}{\partial y} + \mathcal{E} X (x,y,z,\mathcal{E}),$ $\mathcal{E} \frac{\mathrm{d}y}{\mathrm{d}t} = -\frac{\partial H(x,y,z)}{\partial x} + \mathcal{E} Y(x,y,z,\mathcal{E}),$ (2.1) $\frac{dz}{dt} = Z(x,y,z,\xi) (z = \{ z_1, \dots, z_1\}, Z = \{ Z_1, \dots, Z_1\} \}$ or, after the introduction of the quick time $T = \frac{t}{t}$ the system Card 1/16L

MAKAYEVA, G. S.: Master Phys-Math Sci (diss) -- "Asymptotic behavior of solutions of differential equations with small parameters, whose systems of 'rapid movements' are almost Hamiltonian". Moscow, 1959. 10 pp (Acad Sci USSR, Math Inst im V. A. Steklov), 185 copies (KL, No 12, 1959, 125)

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The Asymptotic Behavior of Solutions of Differential SOV/20-121-6-5/45 Equations With a Small Parameter Whose Systems of Rapid Motions" Are Close To the	
Hamilton Systems	
a sketched proof containing asymptotic properties for the solutions of (1) which correspond to the well-known results	
of Volosov /Ref 1,2,3,4,5] for systems with a quick time. Some misprints disturb the understanding. There are 5 Soviet references.	
ASSOCIATION: Matematicheskiy institut imeni V.A.Steklova Akademii nauk SSSR (Mathematical Institute imeni V.A.Steklov of the Academy of	
Sciences of the USSR) PRESENTED: April 18, 1958, by P.S.Aleksandrow, Academician SUBMITTED: April 17, 1958	
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MAKAYEVA, G.F.

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"Problem of Surgical Methods of Treating Varicose Veins of the Lower & tremitice and Their Lasting Results." Cand Med Sci, Second Moscow State Medical Inst insei I.V.Stalin, Moscow, 1955. (EL, Mo 16, Apr 55)

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SC: Sum.No. 704, 2 Nov 55 - Survey of Scientific and Technical Discertations Defended at USSR Higher Educational Institutions (16).






































EASE: 06/23/11 CIA-RDP86-00513R001031500021-6 FOR REI PPF **FD** 89973 s/133/61/000/003/007/014 Mastering the rolling of A054/A033 ings for the national economy in the low-alloy-sections are subjected to the heat treatment indicated. There are 8 figures and 4 tables. ASSOCIATION: Ni.zhne-Tagil'sk matallurgicheskiy kombinat (Nizhne-Tagil Metallurgical Combine) and Ural'skiy institut chernykh metallov (Ural Institute of Ferrous Metals) Card 4/6

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S/133/61/000/003/007/014 A054/A033

Mastering the colling of ...

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steels as compared with carbon steels. It was found, as regards temperature conditions, that low-alloy steels possess a higher deformation resistance at the final (lower) rolling temperatures, (750 - 850°C), than carbon steels. Therefore additional care has to be taken in adjusting the stand to obtain the required dimensions of the section. The standstills of the mill increased by about 10 % when rolling low-alloy steels, on account of changes of rolls and fixtures, so that the output of the mill dropped by about 10 %. However, the 09G2 steel, which is most suitable for light-weight sections, has a great strength in hot-rolled condition, as well as good welding properties and a lower ductility compared with St.3 steels. These properties of the 09G2 steel can still be improved by subjecting it to hardening and annealing at 580°C for 1,5 hours. As a result of heat treatment, the 09G2 steel obtains a fine grained ferrite-perlite structure; moreover, when annealed at 520°C, its strength increases further by about 10 - 20 %. 09G2 steel is also considerably tougher than the St. 3 steels (after complete heat treatment its toughness exceeds that of St. 3 steel at +20°C by 30%, at -40°C about three times.). Thus, with regard to the higher load of the motor and the reduced output of the mill, the production of light weight sections from low-alloy steels will yield actual sav-

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Mastering the rolling of

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sev, Yu. D. Korkodinow, S. V. Gubert, V, V. Skakun, V. V. Kutayev and V. S. Serebryakov. Beams and channels were rolled on the model "800" rolling mill. The parameters of the electromotors, the metalpressure on the rolls, the rolling temperature and the accuracy of the sections obtained were closely controlled. The same roll-pass designs were used as in the conventional process. The bloom were heated to 1280°C, rolled first in a "900" mill, next in the "800" mill, (with 3 - 5 passes on the first and 3 passes on the second stand) and then processed in the finishing mill. The roughing stands were actuated by a d-c 6200 hp motor (80 - 160 rpm, 55.5 TM rated torque), while the finishing stand was driven by a 2500 hp motor (rated torque: 22.4 TM). The energetic parameters were recorded on the tape of an OT-24 (OT-24) oscillograph, the metalpressure on the roll was registered by special YNYM (UIChM) dynamometer with wire pickups. The rolling temperature after the "900" stand was registered by a photoelectric pyrometer, before the finishing stand by a radiation pyrometer. Based on the test results it was found that the load on the motor increased by about 10 %, the rolling pressure by about 25 %, the specific electric power consumption by about 10 - 20 %, when rolling light-weight sections of low-alloy

Card 2/6

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	1.1300	also 1454, 1045	S/133/61/000/003/007/014 A054/A033			
	AUTHORS :	Makayev, S. V., Engineer; Rabinovich, D. M., Enginee Technical Sciences; Korshi	r; Shadrin, V. A., Candidate of			
	TITLE:		ight-weight sections of low-alloy	K i		
	PERIODICAL:	Stal', no. 3, 1961, 240 -	245			
2	TEXT: The new light-weight beams and channels (FOCT - GOST 8239-56 and GOST 8240-56) made of low-alloy steel have not the same strength as the corresponding sections made of carbon steel. In order to obtain the required strength, larger sizes of these sections are used and in this					
	way the savings otherwise effected are partly lost. This draw-back is compensated for by improving the mechanical properties of the steels of which the light-weight sections are made. In order to find suitable which the light-weight sections are made with the most current low-alloy steels:					
ŕ	methods to this end, tests were made with the one most of the CT.3 (St.3) grade 09r2 (09G2), 15XCHA (15KhSND) and compared with the CT.3 (St.3) grade steels. The tests were carried out with the cooperation of L. I. Putil't.					
	Card $1/6$					

RDP86-00513R001031500021 S/133/61/000/002/008/014 Volumetric Hardening of Rails in an Industrial ... A054/A033 Figure 2: Cross section of one of the ten compartments of the furnace for high-speed heating a - burner; b - air pipe; c - gas pipe; d - smoke pipe Card 8/8



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CIA-RDP86-00513R001031500021-6

The test rails were laid on the Sverdlovsk track, in heavy-duty sectors, in curves, and show great resistance to wear. Equipment for the heat treatment of the total Soviet rail production (1.2-1.5 million tons a year) for rails 25 m long, will be designed. The heat treatment costs about 10 rubles/ton, so that it is much cheaper than using alloyed steels. There are 5 figures and 2 Soviet references.

ASSOCIATION: Nizhne-Tagil'ski'y metallurgicheskiy combine (The Nizhne-Tagil Metallurgical Combine)

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Volumetric Hardening of Rails in an Industrial ... A054/A033

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Duration of heating, min 30-70 Holding time in air, sec Hardening temperature, in oil, °C 830-850 Oil temperature, during hardening **≼** 110 5-6 the rail, (Duration of hardening, min Annealing temperature, ^{°C} 450-480 Annealing temperature, Holding time for annealing, hours

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The heat treatment installation ensures such a straightness of the rails which cannot be obtained by any other equipment. Flat bending in vertical and horizontal planes does not exceed 80 mm and no torsion around the longi-tudinal axis was observed. The rails can be heated at a rate of 2° /sec between 20 and 900°C, despite the presence of screw holes. Cracks formed only after hardening in oil containing much water and when annealing was delayed after hardening. The comparison of characteristics of heat-treated and nonheat-treated rails show that the former are superior, attaining the values found in chrome-vanadium steel rails:

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S/133/61/000/002/008/014 Volumetric Hardening of Rails in an Industrial... A054/A033

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ity is equipped with oil conduits, air piping for the mixing of oil, supports for the rails, steam pipes for producing a vapour curtain when the oil is combusted. Above the container a welded metal beam construction is suspended. It is supplied with a roller runway and drive for lowering and lifting the beam. On the beam a cover is loosely fitted, which covers the container when the beam is lowered. After hardening the rail is removed by a winch from the beam structure onto a shelf provided with equipment for the removal of cil vapours. A bridge crane then carries it into the furnace for annealing. The uniformity of heating was checked by electronic potentiometers, indicating that the heating of the rails in the furnace is constant. The temperature differential along the rail does not exceed $80^{\circ}C$ ($50^{\circ}C$ on an average), above 900-950°C it even decreases to 30°C. The temperature drop can further be reduced by discharging the rails more quickly and making the furnace longer. Fairly uniform properties of the metal can be obtained by hardening the rail head at temperatures above Λ . The heat treatment is commised out under the following conditions: carried out under the following conditions:

900-920

Temperature of heating the rail in the compartment furnace, ^OC

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S/133/61/000/002/008/014 Volumetric Hardening of Rails in an Industrial... A054/A033

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This steel costs 31 rubles more than the M75 type and the rails made of it are twice as expensive as the conventional ones. However, tests carried out at the NTMK, in 1957-60, proved that rails with the required properties can be obtained from carbon-steel by volumetric hardening in oil with subsequent annealing. For this process a semi-industrial pilot installation has been designed, consisting of a 10-compartment, 50-ton furnace for rapid heating and a unit for oil-hardening. The furnace-compartments are arranged in one line, 1.600 mm apart. The spaces between the compartments are covered with drums under which water-cooled rolls for delivering the rails are mounted. Each compartment has eight two-conduit, short-flame turbulence burners of VNIIMT -design for coke-gas burning. The most uniform heat distribution in the furnace can be obtained by a chess-board arrangement of the burners on the upper and the lower level of each compartment, the thermal load being distributed between the upper and the lower burners at a 88-12% ratio. The furnace is provided with shelves and guiding mechanisms for feeding the rails to and discharging them from the furnace, moreover with control and measuring apparatus, sound and flashlight indicators. Uniform heating of the rails over their whole length can be obtained by continuously moving them forward and backward at a rate of 4 m/min. The hardening container of 30-ton capac-

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RDP86-00513R001031500021

S/133/61/000/002/008/014 A054/A033

AUTHORS: <u>Makayev, S.V.</u> Engineer, Gubert, S.V., Engineer, and Rabinovich, D.M., Engineer

RDP86-0051

TITLE: Volumetric Hardening of Rails in an Industrial Pilot Installation

PERIODICAL: Stal', 1961, No. 2, pp. 156-159

TEXT: Under the present operational conditions the service life of rails made of M75 type steels produced without heat treatment is insufficient. The strength of the rails should be increased to 100-120 kg/sq mm and their yield point to 80 kg/ sq mm and up, without deterioration of the plastic properties. This can be obtained either by alloying the rail steels or by a heat treatment consisting of volumetric hardening. Tests carried out at the Nizhne-Tagil Metallurgical Combine gave the following results: The properties of rails made of low-alloy steels without heat treatment were improved only slightly while the production became much more expensive. When the rails were made of alloy steels with a higher chromium and nickel content, their properties improved but the technological difficulties involved also Card 1/8

APPROVE	D FOR REL	EASE: 06/23/1	1: CIA-RI	DP86-00513	3R00103150	00021-6		
	Trends in the	Development of B	looming Mill		S/133/60/000/ A054/A029	010/006/013		
	ious specimen There are 6 f	s in the border an Igures, 4 tables a	nd the centra and 8 Soviet	l zones of th references.	ne products ar	e given.		
	ASSOCIATION:	Nizhne-Tagil ['] ski allurgical Plant	/ metallurgic	heskiy kombin	aat (<u>Nizhne-Ta</u>	gil [:] sk Met	 .	
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S/133/60/000/010/006/013 A054/A029

RDP86-00513R001031500021

Trends in the Development of Blooming Mills

tion between the longitudihal-vertical dimensions of the deformation center, 1/Haver (1 is the length of the arc of contact, Haver the average height) [Abstracter's note: Subscript aver (average) is the translation of the original cp (srednyaya)] and the changes in transverse deformation, $\Delta b/b$ were defined, giving the degree of deformation of the carcass sheets. The irregularities in longitudinal and vertical deformations were investigated in ingots with carcasses inside them, on which coordinates were plotted. The influence of the degree of reduction was examined in ingots and slabs cast in 7-ton molds, of boiling and killed steel. Mechanical, macro- and microstructural tests showed that an increase in the degree of reduction reduced the irregularities of deformation inside the sheets and the possibility of internal defects being formed, furthermore, that the mechanical properties and the structure of the products were improved. The conclusion was drawn that the output of the mill could be raised by increasing the degree of reduction to 100 - 110 mm per pass, while the optimum rolling speed is 75 rpm. The transport of the ingots from the soaking pit to the mill should not take more than 2 min and when increasing the degree of reduction, an edger should be operated for removing the angular cracks forming on both sides of the ingots, at least after every third pass. The values of $1/H_{aver}$, $\Delta b/b$ and other characteristics (expansion, indices of irregularities in expansion) cfvar-

S/133/60/000/010/006/013 A054/A029

RDP86-00513R001031500021

AUTHOR: Makayev, S.V., Engineer

TITLE: Trends in the Development of Blooming Mills PERIODICAL: Stal', 1960, No. 10, pp. 915 - 919

06/23/11

TEXT: In order to determine the possibilities of increasing the output of blooming mills by improving the quality of ingots and slabs as regards deformation, theoretical investigations and tests were carried out to define the laws governing transverse, vertical and longitudinal deformations in ingots, the distribution of the irregularities in deformation in its center and its influence on the stressed condition of the product. In the tests dealing with vertical and transverse deformations ingots containing carcasses were rolled; the carcass was formed by putting it in the empty ingot mold and by filling the mold with liquid steel by bottom casting. The carcass consisted of five sheets made of CT3 (ST3) type steel, 30 - 32 mm thick, 450 mm wide and 1,600 mm high. The distribution of vertical deformation was defined by the change in the distance between the sheets of the carcass, while the change in the distance between the notches made in the sheets showed the distribution of the transverse deformations. The rela-

Card 1/3





APPROVED FOR RELEASE: 06/23/11: CIA-RDP86-00513R001031500021-6 SOV/130-58-12-14/21 Reasons for the Formation of Corner Flaws on Blooms from Rimming-Steel Ingots 250 mm square billets which were then sectioned longitudinally and inspected. Ingots of one heat of type 3 kp steel were rolled, after delays of 1-4.5 minutes, into 300 x 320 mm billets which were retreated and rolled into 125 mm squares without intermediate dressing. Best results were obtained with cooling times of 1.0-1.5 minutes (corresponding to normal mill operation). The macrostructure of a specimen from a 250-mm square billet rolled from an ingot cooled for 5-6 min was normal and the maximal depth of surface fissures was 7-10 mm. No microstructural peculiarities were associated with the fissures. The author attributed the investigated flaws to longitudinal tensile forces due to uneven deformation. There is 1 figure and 1 table. ASSOCIATION: Nizhne-Tagil'skiy metallurgical combine Card 2/2

	ASE: 06/23/11: CIA-RDP86-00513R001031500021-6
	Makayev, S.V. Reasons for the Formation of Corner-Flaws on Blooms from Rimming-Steel Ingots (Prichiny obrazovaniya uglovykh rvanin na blyumakh iz slitkov kipyashchey stali)
PERIODICAI	L: Metallurg, 1958, Nr 12, pp 32-33 (USSR)
	When blooms and slabs are rolled from large ingots, especially those of rimming steels, serious fissures leading to rejects often appear on the corners. The author describes an experiment to confirm that an impor- tant cause of this is uneven temperature distribution due to cooling of the corners during pre-rolling delays. The 7-tonne rimming-steel experimental ingot was heated with the others in the soaking pit to 1320°C in 7 hours and on discharge was fitted with thermocouples placed in holes previously prepared in it. The cooling curves (Fig) thus obtained show that after 4 and 7 minutes the tempera- ture difference between centre and corners is 75 and 170°C respectively, and the author indicates that large differ- ences in resistance to deformation will result. To check this, top-poured, square 7-tonne rimming-steel ingots were rolled after various cooling times (1-7 minutes) into
	Torred after various cooring times (1-7 minutes) into

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 MAKAYEV, S.V. AUTHOR: Makayev, S.V., Kotel'nikov, G.V., Staroseletskiy, M.I. and Narutskaya, L.A., Engineers. TITLE: New Wheel-rolling Shop of the Nizhniy Tagil Metallurgical Combine (Novyy kolesoprokatnyy tsekh Nizhne-Tagil'skogo metallurgicheskogo kombinata) PERIODICAL: Stal', 1957, No.7, pp. 616 - 621 (USSR) ABSTRACT: A description of the wheel-rolling shop designed by Gipromez for the Production of 180 000 tons of wheels with their mechanical and thermal treatment is given. The distri- bution of equipment is shown in Fig.1. Main points: 14 ingot- cutting machines (at present capable of cutting 11-13 ingots per shift each), two four-zone ring furnaces with rotating bottoms for pre-heating semis before deformation (furnace capacity - 216 semis), 3 000-ton press for primary reduction and piercing, 7 000-ton press for the final forming of semis; wheel-rolling mill; 2 500-ton bending press. The duration of the whole operation on presses and rolling mill is 2.5 - 3 min. In order to prevent the formation of flakes, packets of 6 wheels with a temperature of 450 - 600 °C are transferred into soaking pits for isothermal treatment at 600 °C for 3 hours (altogether 48 soaking pits of 2 150 mm in diameter and 2 110 nm Card1/2 in epth). After cooling in air in peckets, the wheels are 							
 AUTHOR: <u>Makayev</u>, S.V., Kotel'nikov, G.V., Staroseletskiy, M.I. and Narutskaya, L.A., Engineers. TITLE: New Wheel-rolling Shop of the Nizhniy Tagil Metallurgical Combine (Novyy kolesoprokatnyy tsekh wizhne-Tagil'skogo metallurgicheskogo kombinata) PERIODICAL: Stal', 1957, No.7, pp. 616 - 621 (USSR) ABSTRACT: A description of the wheel-rolling shop designed by Gipromez for the Production of 180 000 tons of wheels with their mechanical and thermal treatment is given. The distri- bution of equipment is shown in Fig.1. Main points: 14 ingot- cutting machines (at present capable of cutting 11-13 ingots per shift each), two four-zone ring furnaces with rotating bottoms for pre-heating semis before deformation (furnace capacity - 216 semis), 3 000-ton press for primary reduction and piercing, 7 000-ton press for the final forming of semis; wheel-rolling mill; 2 500-ton bending press. The duration of the whole operation on presses and rolling mill is 2.5 - 3 min. In order to prevent the formation of flakes, packets of 6 wheels with a temperature of 450 - 600 °C are transferred into soaking pits for isothermal treatment at 600 °C for 3 hours (altogether 48 soaking pits of 2 150 mm in diameter and 2 110 mm 	/	MAKA	YEV, S.V.				
Combine (Novyy kolesoprokatnyy tsekh wizhne-Tagil'skogo metallurgicheskogo kombinata) PERIODICAL: Stal', 1957, No.7, pp. 616 - 621 (USSR) ABSTRACT: A description of the wheel-rolling shop designed by Gipromez for the Production of 180 000 tons of wheels with their mechanical and thermal treatment is given. The distri- bution of equipment is shown in Fig.1. Main points: 14 ingot- cutting machines (at present capable of cutting 11-13 ingots per shift each), two four-zone ring furnaces with rotating bottoms for pre-heating semis before deformation (furnace capacity - 216 semis), 3 000-ton press for primary reduction and piercing, 7 000-ton press for the final forming of semis; wheel-rolling mill; 2 500-ton bending press. The duration of the whole operation on presses and rolling mill is 2.5 - 3 min. In order to prevent the formation of flakes, packets of 6 wheels with a temperature of 450 - 600 °C are transferred into soaking pits for isothermal treatment at 600 °C for 3 hours (altogether 48 soaking pits of 2 150 mm in diameter and 2 110 mm		AUTHOR:	Makayev, S.V and Narutska	., Kotel'nikov Iya, L.A., Engi	v, G.V., Staros neers.		
ABSTRACT: A description of the wheel-rolling shop designed by Gipromez for the Production of 180 000 tons of wheels with their mechanical and thermal treatment is given. The distri- bution of equipment is shown in Fig.l. Main points: 14 ingot- cutting machines (at present capable of cutting 11-13 ingots per shift each), two four-zone ring furnaces with rotating bottoms for pre-heating semis before deformation (furnace capacity - 216 semis), 3 000-ton press for primary reduction and piercing, 7 000-ton press for the final forming of semis; wheel-rolling mill; 2 500-ton bending press. The duration of the whole operation on presses and rolling mill is 2.5 - 3 min. In order to prevent the formation of flakes, packets of 6 wheels with a temperature of 450 - 600 °C are transferred into soaking pits for isothermal treatment at 600 °C for 3 hours (altogether 48 soaking pits of 2 150 mm in diameter and 2 110 mm		' TITIE:	Combine (Nov	yy kolesoproka	tnyy tsekh wizh	' agil M etallurgical hne-Tagil'skogo	£
Gipromez for the Production of 180 000 tons of wheels with their mechanical and thermal treatment is given. The distri- bution of equipment is shown in Fig.1. Main points: 14 ingot- cutting machines (at present capable of cutting 11-13 ingots per shift each), two four-zone ring furnaces with rotating bottoms for pre-heating semis before deformation (furnace capacity - 216 semis), 3 000-ton press for primary reduction and piercing, 7 000-ton press for the final forming of semis; wheel-rolling mill; 2 500-ton bending press. The duration of the whole operation on presses and rolling mill is 2.5 - 3 min. In order to prevent the formation of flakes, packets of 6 wheels with a temperature of 450 - 600 °C are transferred into soaking pits for isothermal treatment at 600 °C for 3 hours (altogether 48 soaking pits of 2 150 mm in diameter and 2 110 mm		PERIODI	CAL: Stal', 1	.957, No.7, pp.	616 - 621 (US	SR)	
		6 5 5 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	Sipromez for the their mechanica oution of equip cutting machine per shift each) oottoms for pre- capacity - 216 and piercing, 7 wheel-rolling m the whole opera In order to pre- wheels with a to soaking pits for altogether 48	the Production of al and thermal oment is shown es (at present b, two four-zon e-heating semis semis), 3 000- 7 000-ton press atill; 2 500-to ation on press event the formation comperature of soaking pits of	of 180 000 tons treatment is g in fig.l. Mai capable of cut he ring furnace before deform ton press for of the final on bending pres and rolling ation of flakes 450 - 600 °C a creatment at 60 of 2 150 mm in	of wheels with iven. The distri- n points: 14 ingot- ting 11-13 ingots s with rotating ation (furnace primary reduction forming of semis; s. The duration of mill is 2.5 - 3 min. , packets of 6 re transferred into 0 °C for 3 hours diameter and 2 110 rm	

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APPROVED FOR REL EASE: 06/23/11: CIA-RDP86-00513R001031500021-6 MAKAYEV, N.A.; GEL'BERG, Ya.L (Vitebsk) On the road to technical progress. Shvein.prom. no.5:11-14 S-0 (MIRA 13:12) 160. (Clothing industry)




























SOV/3-59-3-37/48 The International Connections of the Higher School - Scientists of Foreign Countries in the USSR

Union. Professor S. Landa delivered lectures on chemistry at the Moskovskiy khimiko-tekhnologicheskiy institut imeni Mendeleyeva (Moscow Chemico-Technological Institute imeni Mendeleyev). Forty-five Instructors from countries of the people's democracies attended a seminar on the Russian language at the MGU. During the last 6 months of 1958 the USSR Ministry of Higher Education recieved 4 delegations from the USA: a delegation of presidents of American universities of 13 men headed by E. Litchfield, President of Pittsburg University, a delegation of American university professors headed by F. Brown, Director of a Department of the American Council on Questions of Education. The author mentions 2 other delegations, one of which was led by D. Turkevich, Professor of Princeton University, and the other by F. Lindwall, Professor of California University. The American specialists visited the Kuybyshev GES and familiarized themselves with the system of training engineers for

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22(1) #UTHOR:	Makav'yeva, N.A.	sov/3-59-3-37/48	
22(1) AUTHOR:	Makay'yeva, N.A.	SOV/3-59-3-37/48	
		5017 5-55 577 5	
TITLE:	(Manhamanadamma antigal)	ections of th e Higher School L vysshey shkoly) - Scientists h the USSR (Uchënyye zaru-	
PERIODICAL:		, 1959, Nr 3, pp 72-73 (USSR)	
ABSTRACT:	the USSR and other coun carried out on a large Ministry of Higher Educ by 672 foreign special: 700 scientists and about countries. The author workers of Albania T. nari and scientists fr V. Kylbova, S. Neykov, who visited agricultur 100 young scientists f	scientific cooperation between ntries was for the first time scale. The vuzes and the USS cation were visited last year ists, and in turn sent over ut 150 students to foreign mentions the young scientific Perpari, S. Chicho, G. Dzhi- om Bulgaria I. Georgiyev, I. Panchev and I. Terziyskiy al and medical vuzes. About rom Hungary spent from 1 to 4 increase their qualification, ty Minister of Education I.	SR c

AUTHOR: Makav'yeva, N.A. 3-58-7-29/36	
TITLE: Foreign Scientists in the Soviet Union (Zarubezhnyye uchenyye v Sovetskom Soyuze)	
PERIODICAL: Vestnik vysshey shkoly, 1958, Nr 7, pp 79-81 (USSR)	
ABSTRACT: In the last 5 months more than 150 scientists visited the Soviet Union. About 50 of them came from capitalistic countries. There is 1 photo.	
Card 1/1	

RDP86-00513R00103150002 Veterinary Medicine BULGARIA PAVLOV, N., Dr, MAKAVEYEVA, E., Dr, VESELINOVA, A., Dr, VIZPB/not identified7 "Disease of New- Born Lambs Caused By Neorickettsiae" Sofia, Veterinarna Sbirka, Vol 63, No 1, 1966, pp 3-6 Abstract: The virus abortion of sheep is a latent neorickettsiae infection. Lambs that are born alive exhibit symptoms of the infection. Tissues and organs of infected new- born lambs were subjected to a pathological, anatomic, and histologic investigation. Two strains of the causative factor were isolated and propagated in 6-day old chicken embryos on being injected into their yolk sac. The embryos perished on infection and showed presence of typical elementary bodies. Antigen obtained from chicken embryos had properties identical with those of antigen isolated from the placenta of aborting ewes. By using the antigen from chicken embryos, the reaction of complement fixation was carried out for diagnostic purposes. 1/1







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BULGARIA/Fa	rm Animals - Cattle. Q-3	
Abs Jour	: Ref Zhur - Biol., No 7, 1958, 30958	
Author	: Vladimirov Ivan, Makaveyev Tsvetan	
Inst Title	The Evaluation of Bulls According to Progeny. (Ob otsenke bykov po potomstvu).	
Orig Pub	: Selkostop. mis"1, 1957, 2, No 4, 231-214	
Abstract	: Examples are adduced where, in the absence of the evalua- tion of bulls according to the milkiness of their daugh- ters and in the selection of cows by the milk yield, the level of production according to milk composition remained without change for about 20 years. The methods for the testing of bulls and the technique used in dif- ferent countries are described. It has been noticed that the evaluation of sires by progeny must be repeated in the presence of essential changes in the herd structu- re, in the conditions of maintenance, management and	
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MAKAVEEV, IV.				
N	ing mixture for toba	oco leaves. Ratsic	nalizatsiia ll	
	(Tobacco)			
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ACCESSION NR: AP4004139

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No. 3, 1940), which employs a capillary and an annular balance. The smoothed data obtained from several sets of isotherms agree with the experimental values within 2%. Orig. art. has: 3 figures, 5 formulas, and 3 tables.

RDP86-00513R00103

1500021-6

ASSOCIATION: Moskowskiy energeticheskiy institut (Moscow Power Engineering Institute)

SUBMITTED: 03Jul63	DATE ACQ: 26Dec63	ENCL: 02
SUB CODE: AS, PH	NO REF SOV: 004	OTHER: 006

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ACCESSION NR: AP4004139

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s/0294/63/001/002/0191/0197

RDP86-00513R00103

AUTHORS: Makavetskas, R. A.; Popov, V. N.; Tsederberg, N. V.

TITLE: Experimental determination of the viscosity of helium and nitrogen

SOURCE: Teplofizika vy*sokikh temperature, v. 1, no. 2, 1963, 191-197

TOPIC TAGS: dynamic viscosity, viscosity, helium, helium viscosity, nitrogen viscosity, gas analyzer, gas analysis, gas property, gas viscosity, nitrogen, helium nitrogen mixture

ABSTRACT: With an aim at filling the temperature gaps in the existing experimental data, the coefficient of dynamic viscosity of helium, nitrogen, and their mixture was investigated experimentally in the temperature range 10--660°C and in the pressure range from 1 to 600 kg/cm² using the method of Professor D. L. Timrot (Izv. VTI,

Card 1/4













MARAVEST, Tavetan Pattening of the young bulls and oxen of the Red Danish crossbreed up to various live weights. Selskostop nauka I no.1011109-1116 '62. 1. Kompleksna opitna stantsila "Obrastsov chiflik" krai Ruse.

