

ANFIMOV, A.S., inzh.; MANEVICH, I.V., inzh.

Band cantilever dumper. Bezop. truda v prom. 3 no.10:33
0 '59. (MIRA 13:2)

1. Trest Volchanskugol'.
(Coal mining machinery)

ANDRIANOV, K.A.; MANEVICH, I.Ya.

Synthesis and properties of acid salts of methylphosphinic acid.
Zhur.neorg.khim. 9 no.1:210-212 Ja '64. (MIRA 17:2)

1. Institut elementoorganicheskikh soyedineniy AN SSSR i Institut obshchey i neorganicheskoy khimii imeni N.S.Kurnakova AN SSSR.

ANDRIANOV, K.A.; MANEVICH, V.M.; RIBAYEV, Y.U.; MAT' S I., V.I.

Acid salts of methylphosphinic acid. Zhur. neorg. khim. 1965
no.3:596-600 Ns 165.

I. Institut elementarnoi chkhimi, sverdleniyu AN SSSR
Institut obshchey i zashchitnoy khimii, Sverdleniyu
Kurgan'ya N. SSSR.

MANEVICH, I.Z. (Ryazan')

Behavior of integral curves of a system of homogeneous differential equations with continuous right-hand parts. Izv. vys. ucheb. zav.; mat. no.3:117-120 '65. (MIRA 18:7)

"APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8

KLOPOTOV, B.; HANEVICH, I.; TSVENEV, V.

Combined premium-fixed wage system. Sets. trud no. 4:117-123 Ap '57.
(Wages)

APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8"

PETROV, K.M.; DYAKONOV, V.I.; FADEYEV, I.G.; SEMENENKO, P.P.; KRYUKOV, L.G.;
Prinimali uchastiye: PASTUKHOV, A.I.; SHISHKINA, N.I.;
PAZDNIKOVA, T.S.; CHIRKOVA, S.N.; KAREL'SKAYA, T.A.; LOPTEV, A.A.;
DZEMYAN, S.K.; ISUPOV, V.F.; BELYAKOV, A.I.; GUDOV, V.I.;
SUKHMAN, L.Ya.; SLESAREV, S.G.; GOLOVANOV, M.M.; GLAGOLENKO, V.V.;
ISUPOVA, T.A.; ZYABLITSEVA, M.A.; KAMENSKAYA, G.A.; POMUKHIN, M.G.;
UTKINA, V.A.; MANEVICH, L.G.

Vacuum treatment of alloyed open hearth steel. Stal' 22 no.2:113-
117 F '62. (MIRA 15:2)

1. Ural'skiy nauchno-issledovatel'skiy institut chernykh metallov
(for Pastukhov, Shishkina, Pazdnikova, Chirkova, Karel'skaya,
Loptev, Dzemyan). 2. Metallurgicheskiy kombinat im. A.K. Serova
(for Isupov, Belyakov, Gudov, Sukhman, Slesarev, Golovanov,
Glagolenko, Isupova, Zyablitseva, Kamenskaya). 3. 6-y Gosudar-
stvennyy podshipnikovyy zavod (for Pomukhin, Utkina, Manevich).

(Steel—Metallurgy)
(Vacuum metallurgy)

SHEVLYAKOV, Yu.A.; MANEVICH, L.I.

Certain cases of the stability of a flat bend. Dop. AN URSR
no.6:627-630 '58. (MIRA 11:9)

1.Dnepropetrovskiy universitet. Predstavil akademik AN USSR G.N.
Savin [H.M. Savin].

(Elastic rods and wires)

Report presented at the 1st All-Union Congress of Theoretical and Applied Mechanics,
Moscow, 27 Jan - 3 Feb '60.

148. G. D. Lekhnitskii (Birov): On stress distribution of columns
in the temperature field.
149. V. N. Leont'ev (Pezov): Fibrestress at room temperature.
150. V. A. Leont'ev (Pezov): Plasticity of metals under combined loading.
151. V. I. Lerner (Lerner): Some problems of nonstationary flow in compressible viscous (Newtonian) liquids.
152. A. I. Lerner (Lerner): Some problems of nonstationary flow law of an incompressible viscous-elastic (Kondratenko) medium.
153. V. I. Lerner (Lerner): The generalization of the torsion theory of inhomogeneous bars.
154. M. I. Leont'ev (Leont'ev): The development of mechanics of inhomogeneity.
155. Th. B. Levin (Fuchs): Plastic flow of elastic plates under tension and bending or compression and bending.
156. G. S. Leont'ev (Leont'ev): Torsion of an inhomogeneous bar in terms of equal elasticity constants of plates and squares.
157. A. B. Libavski (Perovskii): Free vibrations and stability of ordinary and generalized elastic reticular beams.
158. A. V. Likhanskii (Vlasov): Mathematical problems in connection with singular layers.
159. S. I. Lifshits (Fersman): On the application of matrix methods to the solution of large sets of linear equations of elasticity theory.
160. G. I. Lichten (Lichten): The selection of structural parameters for inhomogeneous plates of equal elasticity constants of plates and squares.
161. G. I. Lichten (Lichten): Large deflections of shallow shells of inhomogeneously elastic materials.
162. G. I. Lichten (Lichten): The choice of the relation of two dimensions of cylindrical shells of inhomogeneous materials.
163. G. I. Lichten (Lichten): Analysis of an orthotropic plate with a central circular hole as arbitrary load applied to a free edge.
164. G. I. Lichten (Lichten): On the experimental study of stresses in plates and shells.
165. G. I. Lichten (Lichten): Creep strains and responses of high polymers.
166. B. I. Lichten (Lichten): Vibrations of thin circular cylindrical shells.
167. A. I. Lichten (Lichten): Some problems of combined loading of cylindrical shells.
168. K. A. Litvinov (Litvin): The influence of structural elements in concrete on its strength.
169. A. G. Makarov (Barab): Investigation of the state of stress in square plates with central cylindrical holes under internal pressure.
170. O. A. Maksimovich (Makhlis): Minimization of plane elastic problem for anisotropic bodies by reduction to the problem of linear coupling with "displacement".
171. Iu. N. Matveev (Matveev): The theory of plastic shells in bending.
172. V. N. Moshchuk (Moshchuk): The influence of material properties on the mechanical behavior of laminated and reinforced composite materials.
173. V. N. Moshchuk (Moshchuk): Stress and strain in naturally twisted bars.
174. I. V. Nekrasov (Nekrasov): The problem of conformal mapping of a unit disk.
175. G. I. Nikishin (Nikishin): Plasticity of shells under external loads.
176. G. I. Nikishin (Nikishin): The theory of plastic shells under external loads.
177. G. I. Nikishin (Nikishin): Contribution to the theory of plastic shells under uniform strength.
178. G. I. Nikishin (Nikishin): On the bending of a simply supported parabolic plate.
179. G. I. Nikishin (Nikishin): Vibrations of a curved bar in statical walls and on elastic supports.
180. G. I. Nikishin (Nikishin): An experimental study of bars of large size.
181. G. I. Nikishin (Nikishin): On statically equivalent loadings.
182. M. G. Nikishin (Nikishin): Contribution to the theory of plastic shells under uniform strength.
183. G. I. Nikishin (Nikishin): On the bending of a simply supported parabolic plate.
184. G. I. Nikishin (Nikishin): Prediction of the rheological properties of plastic viscoelastic materials in statical walls and on elastic supports.

MANEVICH, L.I.

27049

244200 1327 1191 2808 2601 S/021/60/000/005/005/015
D210/D304

AUTHORS: Shevlyakov, Yu.A., and Manevych, L.I.

TITLE: The stability of a cylindrical shell under bending

PERIODICAL: Akademiya nauk ukrayins'koyi RSR, Dopovidi, no. 5, 1960,
605-608

TEXT: The article deals with determining the lower critical (buckling) stress of a thin-walled cylindrical shell under pure bending. The problem is solved by approximation using the basic non-linear equations of the theory of elasticity. The critical state is given by

$$\begin{aligned}\varepsilon_x^0 &= \frac{\partial u_0}{\partial x} = \frac{T_x^0}{Eh}, \\ \varepsilon_y^0 &= \frac{\partial v_0}{\partial y} - \frac{w_0}{R} = -\frac{v T_x^0}{Eh}, \\ \varepsilon_{xy}^0 &= \frac{\partial v_0}{\partial x} + \frac{\partial u_0}{\partial y} = 0.\end{aligned}$$

where $v = 0$ for $x = 0$ and

$x = \ell$. The x-axis lies along a generator, the y-axis along the tangent to the excess load, and the z-axis towards the center of curvature. $\varepsilon_x^0, \varepsilon_y^0, \varepsilon_z^0$

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are the deformations of the central plane, u_0 , v_0 , w_0 are the displacements in the x, y, z directions respectively, R and l are respectively the radius and length of the shell, ν is Poisson's coefficient, $\sigma_x^0 = T_x^0 = \frac{M}{h}$ is the normal stress. Also,

$\sigma_x^0 = \frac{M}{W} = \sigma_0 \cos \frac{y}{R}$ (3) where M is the bending moment, W is the support moment $\sigma_0 = \frac{M}{\pi R^2 h}$ h is the thickness

of the shell. Integration and substitution gives for the displacements $u_0 = \frac{\sigma_0}{E} \left(\frac{l}{2} - x \right) \cos \frac{y}{R}$, Investigation of the stability gives (Eqs. 5 and 6 see next card)

$$v_0 = \frac{\sigma_0}{2ER} x(l-x) \sin \frac{y}{R}, \quad (4)$$

$$w_0 = \frac{\sigma_0}{2ER} [x(l-x) - 2\nu R^2] \cos \frac{y}{R}.$$

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$$\nabla^2 \nabla^2 \Phi = Eh \left[\left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 - \frac{\partial^2 w}{\partial x^2} \cdot \frac{\partial^2 w}{\partial y^2} - \frac{1}{R^2} \frac{\partial^2 w}{\partial x^2} \right], \quad (5)$$

$$D \nabla^2 \nabla^2 w = \frac{\partial^2 \Phi}{\partial y^2} \cdot \frac{\partial^2 w}{\partial x^2} - 2 \frac{\partial^2 \Phi}{\partial x \partial y} \cdot \frac{\partial^2 w}{\partial x \partial y} + \frac{\partial^2 \Phi}{\partial x^2} \cdot \frac{\partial^2 w}{\partial y^2} - \frac{1}{R} \frac{\partial^2 \Phi}{\partial x^2}, \quad (6)$$

$$D = \frac{Eh^2}{12(1-\nu^2)}$$

is the cylindrical rigidity. w and Φ are written
 $w = w_1 + w_0$ where w_1 and Φ_1 are respectively the deflection
 $\Phi = \Phi_1 + \Phi_0$ with respect to the normal and the stress function
 which characterizes the bulging of the shell,

and $\Phi_0 = \phi_0 R^2 \cos y$. If $\ell > 1.5R$ the boundary
 conditions may be ignored. The first approximation for w_1 gives in the
 zone of compression

$$w_1 = f h \left(\cos \frac{\pi x}{l_x} \cos \frac{\pi y}{l_y} + a \cos \frac{2\pi x}{l_x} + b \cos \frac{2\pi y}{l_y} \right) \cos^2 \frac{y}{R}. \quad (10)$$

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and in the zone of tension $w_1 = 0$, λ_x and λ_y are longitudinal semi-waves in the x and y directions, f, a, b, are dimensionless parameters. Solving for ϕ_1 gives

$$\begin{aligned}
 & \left[\begin{aligned} & f_1 \phi_1 = \left[f_1 \cos^2 \frac{\pi}{L_x} + f_1 \cos \left(\frac{\pi}{L_x} + \frac{2}{R} \right) x + f_1 \cos \left(\frac{\pi}{L_x} - \frac{2}{R} \right) x + \right. \\ & \left. + f_1 \cos \left(\frac{\pi}{L_x} + \frac{4}{R} \right) x + f_1 \cos \left(\frac{\pi}{L_x} - \frac{4}{R} \right) x + f_1 \cos^2 \frac{2\pi y}{L_y} + \right. \\ & \left. + f_1 \cos \left(\frac{3\pi}{L_x} + \frac{2}{R} \right) x + f_1 \cos \left(\frac{3\pi}{L_x} - \frac{2}{R} \right) x + \right. \\ & \left. + f_1 \cos \left(\frac{3\pi}{L_x} + \frac{4}{R} \right) x + f_1 \cos \left(\frac{3\pi}{L_x} - \frac{4}{R} \right) x \right] \cos \frac{\pi y}{L_y} + \\ & + \left[f_{11} \cos \frac{\pi x}{L_x} + f_{12} \cos \left(\frac{\pi}{L_x} + \frac{2}{R} \right) x + f_{13} \cos \left(\frac{\pi}{L_x} - \frac{2}{R} \right) x + \right. \\ & \left. + f_{14} \cos \left(\frac{\pi}{L_x} + \frac{4}{R} \right) x + f_{15} \cos \left(\frac{\pi}{L_x} - \frac{4}{R} \right) x \right] \cos \frac{2\pi y}{L_y} + \\ & + \left[f_{16} \cos^2 \frac{\pi y}{L_y} + f_{17} \cos^2 \left(\frac{\pi}{L_x} + \frac{2}{R} \right) x + f_{18} \cos^2 \left(\frac{\pi}{L_x} - \frac{2}{R} \right) x + \right. \\ & \left. + f_{19} \cos^2 \left(\frac{\pi}{L_x} + \frac{4}{R} \right) x + f_{20} \cos^2 \left(\frac{\pi}{L_x} - \frac{4}{R} \right) x \right] \cos \frac{3\pi y}{L_y} + \\ & + \left[f_{21} \cos^2 \frac{2\pi y}{L_y} + f_{22} \cos^2 \left(\frac{\pi}{L_x} + \frac{2}{R} \right) x + f_{23} \cos^2 \left(\frac{\pi}{L_x} - \frac{2}{R} \right) x + \right. \\ & \left. + f_{24} \cos^2 \left(\frac{\pi}{L_x} + \frac{4}{R} \right) x + f_{25} \cos^2 \left(\frac{\pi}{L_x} - \frac{4}{R} \right) x \right] \cos \frac{4\pi y}{L_y} + \end{aligned} \right] \quad (11)
 \end{aligned}$$

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where the g_i are found from the boundary conditions in the usual way.The energy equation for a general system is $\mathcal{E} = \mathcal{E}_1 + \mathcal{E}_2 - V$, where \mathcal{E}_1 is the energy of deformation of the central plane, \mathcal{E}_2 is the energy of bending, and V is the potential of external forces. Ignoring small quantities

Abstractor's Note:
 Symbols not explained]. The energy criterion of equilibrium is Eq. 13
 (see next card)

$$\begin{aligned} \mathcal{E}' = \frac{16}{3} \frac{R}{Eh^3\pi l} \cdot \mathcal{E} = \frac{\xi^2}{\eta^2} \left\{ \xi^2 \eta^4 \left[\frac{(a+b)^2 + 4a^2b^2}{(1+\theta^2)^2} + \frac{a^2}{(1+9b^2)^2} + \right. \right. \\ \left. \left. + \frac{b^2}{(1+\theta^2)^2} + \frac{1}{128} + \frac{17}{12 \cdot 256} (1+8a^2)^2 \right] + \frac{1}{4} \frac{\theta^4}{(1+\theta^2)^2} - \right. \\ \left. - \frac{\theta^4}{(1+\theta^2)^2} \xi(a+b) + \frac{1}{128} (\xi - 8a)^2 \right\} - \frac{8}{3} \sigma_{01}^2 + \\ + \frac{1}{48(1-\nu^2)} \xi^2 [(1+\theta^2)^2 + 32(a^2\theta^4 + b^2)] - 0.225 \cdot \sigma_{01} \frac{\xi^2\theta^3}{\eta} (1+8a^2). \end{aligned} \quad (12)$$

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$$\frac{\partial \vartheta'}{\partial z} = \frac{\partial \vartheta'}{\partial q} = \frac{\partial \vartheta'}{\partial b} = \frac{\partial \vartheta'}{\partial a} = \frac{\partial \vartheta'}{\partial i} = 0.$$

(13) from which can be found
the relationship between
the load parameter for

pure bending and the uniform axial compression in the post-critical stage. Hence, the lower critical (buckling) stress may be found. The load parameter in this case is 0.26, and thus is obtained the approximation formula

$$\sigma'_0 = 0.26 \frac{Eh}{R} \quad (15) \quad \rho'_0 = 0.18 \frac{Eh}{R}. \quad (15A)$$

There are 2 Soviet-bloc references.

ASSOCIATION: Dnipropetrov's'kyj derzhavnyj universytet (State University of Dnepropetrovsk)

PRESENTED: by Academician AS UkrSSR H.M. Savin

SUBMITTED: June 17, 1959

Card 6/6

Manuevich, L.I.
BOROVSKIY, P. V.

PHASE I BOOK EXPLOITATION

SOV/6206 75

Konferentsiya po teorii plastin i obolochek. Kazan', 1960.

Trudy Konferentsii po teorii plastin i obolochek, 24-29 oktyabrya 1960. (Transactions of the Conference on the Theory of Plates and Shells Held in Kazan', 24 to 29 October 1960). Kazan', [Izd-vo Kazanskogo gosudarstvennogo universiteta] 1961. 426 p. 1000 copies printed.

Sponsoring Agency: Akademiya nauk SSSR. Kazanskiy filial. Kazanskiy gosudarstvennyy universitet im. V. I. Ul'yanova-Lenina.

Editorial Board: Kh. M. Mushtari, Editor; F. S. Isanbayeva, Secretary; N. A. Alumyaev, V. V. Bolotin, A. S. Vol'mir, N. S. Ganiyev, A. L. Gol'denveyzer, N. A. Kil'chevskiy, M. S. Kornishin, A. I. Lur'ye, G. N. Savin, A. V. Sachenkov, I. V. Svirskiy, R. G. Surkin, and A. P. Filippov. Ed.: V. I. Aleksagin; Tech. Ed.: Yu. P. Semenov.

PURPOSE: The collection of articles is intended for scientists and engineers who are interested in the analysis of strength and stability of shells.

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Transactions of the Conference (Cont.)

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SOV/6206

COVERAGE: The book is a collection of articles delivered at the Conference on Plates and Shells held in Kazan' from 24 to 29 October 1960. The articles deal with the mathematical theory of plates and shells and its application to the solution, in both linear and nonlinear formulations, of problems of bending, static and dynamic stability, and vibration of regular and sandwich plates and shells of various shapes under various loadings in the elastic and plastic regions. Analysis is made of the behavior of plates and shells in fluids, and the effect of creep of the material is considered. A number of papers discuss problems associated with the development of effective mathematical methods for solving problems in the theory of shells. Some of the reports propose algorithms for the solution of problems with the aid of electronic computers. A total of one hundred reports and notes were presented and discussed during the conference. The reports are arranged alphabetically (Russian) by the author's name.

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Transactions of the Conference (Cont.)	SOV/6206
Makarov, B. P. On the Nonlinear Flutter of a Plate Clamped by Its Circumference	220
<u>Manevich, L. I.</u> On the Stability of a Cylindrical Shell Under Nonuniform Axial Compression	226
Mitkevich, V. M. Symmetrical Deformation of a Stiffened Conical Shell	233
Mishenykov, G. V. On the Dynamic Stability of a Shallow Cylindrical Shell	239
Myursepp, P. V. On a Method for Investigating the Behavior of Shells After Plastic Buckling	246
Obolashvili, Ye. I. Positive Curvature Membrane Shells Acted on by Discontinuous External Forces	250
Pavlynen, V. Ya. Membrane State of Stress of [Circular] Translational Shells	254

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MANEVICH L. I.

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244200 1103, 1327, 1191

S/021/61/000/008/008/011
D210/D303

AUTHOR: Manevych, L. I.

TITLE: On the local stability of shells under non-uniform loads

PERIODICAL: Akademiya nauk Ukrayins'koyi RSR. Dopovidi, no. 8,
1961, 1018-1021

TEXT: 1) A thin cylindrical shell of medium length is considered, being in conditions of eccentric compression prior to loss of stability. According to the momentless theory, the normal stresses in the section is

$$\sigma = \sigma_0 + \sigma_1 \cos \beta = \sigma_0 (1 + \gamma \cos \beta) \quad (1)$$

σ_0 being the stress of uniform compression, σ_1 the maximum bending

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stress, β the angle counted from the plane of bending. If $\sigma_1 \rightarrow 0$, $r \rightarrow 0$ and $\sigma \rightarrow \sigma_0$: if $\sigma_0 \rightarrow 0$, $r \rightarrow \infty$ and $\sigma \rightarrow \sigma_1 \cos \beta$. 2) To investigate the stress, a system of non-linear equations is used which relate to each other the additional forces and displacements in buckling. The boundary conditions are satisfied in the integral sense. The additional radial buckling is imagined in the form

$$w_1 = f \cdot h \left(\cos \frac{\pi R \xi}{\lambda \varepsilon} \cos \frac{\pi R \beta}{\lambda \beta} + a \cos \frac{2\pi R \xi}{\lambda \varepsilon} + b \cos \frac{2\pi R \beta}{\lambda \beta} \right) \cos \frac{k \beta}{2} \quad (2)$$

where $\lambda_\xi, \lambda_\beta$ are half wavelengths in the directions ξ, β . Using the Ritz-Papkovich method, one must find the solutions for several values of k ($0, 2, 4, 6, 8, 10$). [Abstractor's note: An example of partial solution for the stress function with $k=2$ follows, consisting of 32 terms.] The coefficients g_1 are determined in the

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usual way. The terms $g_{31} \cos \beta$, $g_{32} \cos 2\beta$ correspond to the part of additional axial force which has a comparatively large period of change. The presence of such terms, due to the non-linear effect, determines the influence of inhomogeneity of the stressed state on lower critical force. To calculate the upper critical stress one puts $a=b=0$ and does not take into account the terms due to non-linearity of initial equations. The dimensionless parameter of total energy, computed according to the well known formulae, according to A.S. Volmir (Ref. 3: Gibkiye plastinki i obolochki (Flexible Plates and Shells), Gostekhizdat, 1956, 52), can be imagined in the form

$$\exists^* = \frac{0,25r^2\theta^4}{(1+\theta^2)^2\eta^2} + \frac{r^2(1+\theta^2)^2}{48(1-v^2)} - 0,25\alpha_1(k,r) \frac{r^2\theta^2}{\eta} \sigma^*$$

where

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$$\theta = \frac{\lambda_3}{\lambda_e}; \eta = \frac{\pi^2 R h}{\lambda_B^2}; r = f \cdot \eta; \sigma^* = \frac{R}{Eh} \sigma$$

The values of $\alpha_1(k, \gamma)$ are given in a table. The relation between the critical stresses of central and eccentric compression is

$$\sigma = \frac{1}{\alpha_1(k, \gamma)} \sigma_0 \quad (4)$$

When k increases, it is $\alpha_1(k, \gamma) \rightarrow 1$ for all values of γ , i.e. the upper critical stress does not depend on the eccentricity of load. The same result can be obtained by computing the energy corresponding to the zone of maximum compression $-\lambda_B/R < \beta < \lambda_B/R$,

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it being $\sigma_1 = 1$. In determining the lower critical stress one uses (2) and (3'). The dimensionless parameter of general energy (in the zone of maximum compression) is

$$\begin{aligned} \sigma^* = & \frac{r^2}{\eta^2} \left\{ r^2 \theta^4 \left[\frac{(a+b)^2 + 4a^2b^2}{(1+\theta^2)^2} + \frac{a^2}{(1+9\theta^2)^2} + \frac{b^2}{(9+\theta^2)^2} + \frac{1}{128} + \right. \right. \\ & \left. \left. + a_2(k)(1+8a^2)^2 \right] - \frac{\theta^4(r(a+b)-0.25)}{(1+\theta^2)^2} - \right. \\ & \left. - \frac{1}{128}(r-8a)^2 \right\} + \frac{r^2}{48(1-v^2)} [(1+\theta^2)^2 + 32(a^2\theta^4 + b^2)] - \\ & - 0.25 \frac{r^2\theta^4}{\eta} \sigma^* (1+8a^2). \end{aligned}$$

The values of $a_2(k)$ are given in a table. There are 2 tables, 1 figure and 4 Soviet-bloc references.

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ASSOCIATION: Dnipropetrov's'kyj derzhavnyj universytet (Dnipro-petrovsk State University)

PRESENTED: by Academician AS UkrSSR, H. M. Savin

SUBMITTED: December 23, 1960

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STEPANOV, M. M. [Stepanov, M. M.] (Dnepropetrovsk); TSVETKOV, M. M.
[Tsvetkov, M. M.] (Dnepropetrovsk); MANEVICH, L. I.
[Manevich, L. I.] (Dnepropetrovsk)

Stability of cylindrical shells reinforced with ribs. Prykl.
mekh. 9 no. 1:59-67 '63. (MIRA 16:4)

(Elastic plates and shells)

MANEVICH, L.M.

KLOPOTOV, B.Ye., inzhener; MANEVICH, L.M., inzhener; TSVENEV, V.L., inzhener.

Applying a bonus system to the payment of wages for regular assignments. Sudostroenie 23 no.4:37-39 Ap '57. (MLRA 10:5)
(Shipbuilding workers) (Wages)

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and Report of the Central Intelligence Agency
to Congress, 1970, Vol. 1

1. Report of the Central Intelligence Agency to Congress, 1970, Vol. 1

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CIA-RDP86-00513R001032120013-8"

MANEVICH, M.G.; BARIKO, I.A.

Burning crushed anthracite. Sakh. prom. 31 no.5:53-56 My '57.
(MLRA 10:6)
1. Gosudarstvennyy institut po proyektirovaniyu novogo stroitel'-
stva i rekonstruktsii predpriyatiy sakharnoy promyshlennosti.
(Combustion)

BAYANDINA, D.G.; MANEVICH, M.Ye.; MLDUNETSKAYA, E.B.

Development of a method for yomesan treatment of nymenoleptasis.
Med.paraz.i paraz.bol. 33 no.4:411-415 Jl-47 '84.

(MIRA 18:3)

i. Otdel gel'mintologii Instituta meditsinskoy parazitologii i
tropicheskoy meditsiny imeni Martsinovskogo i parazitologicheskiy
otdel sanitarno-epidemiologicheskoy stantsii Zhdanovskogo rayona,
Moskva.

MANEVICH, R.M., inzh.

Detection of short-circuited turns in the windings of operating
turbogenerator rotors. Elek. sta. 32 no.11:53-56 N '61.
(MIRA 14:11)
(Turbogenerators--Windings)

MANEVICH, Roman Mikhaylovich, inzh.; KUTAKOVA, L.I., inzh., red.;
POMICHEV, A.G., red. izd-va; GVIITS, V.L., tekhn. red.

[Location of short-circuits in the turns of rotating turbo-generator rotors] Obnaruzhenie vitkovykh zamykanii v obmotkakh vrashchajushchikhsia rotorov turbogeneratorov. Leningrad, 1962. 13 p. (Leningradskii dom nauchno-tehnicheskoi propagandy. Obmen peredovym opytom. Seriya: Pribory i elementy avtomatiki, no.9)
(Turbogenerators--Windings)

"APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8

MANEVICH, S. A.

MANEVICH, S. A. -- "Clinical Evaluation of the Results of an Investigation of the Stomach Contents During Certain Diseases of Horses. Latvian Agricultural Academy, 1950
(Dissertation for the Degree of Candidate of Veterinary Sciences)

SO: Izvestiya Ak. Nauk Latviyskoy SSR, No. 9, Sept., 1955

APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8"

3-361. Correlation Between Impact Resistance and Cross-Sectional Reduction.
Sh. S. Mangerich. Factory Laboratory
(U.S.S.R.). v. 13, April 1947, p. 479-481.
discussion, p. 481. (In Russian)

As a result of a statistical treatment
of data for 3000 specimens of high-
alloy structural steel, a mathematical
and graphical relationship is devel-
oped. Such relationship holds only
for high-strength steels.

430 31A METALLURGICAL LITERATURE CLASSIFICATION

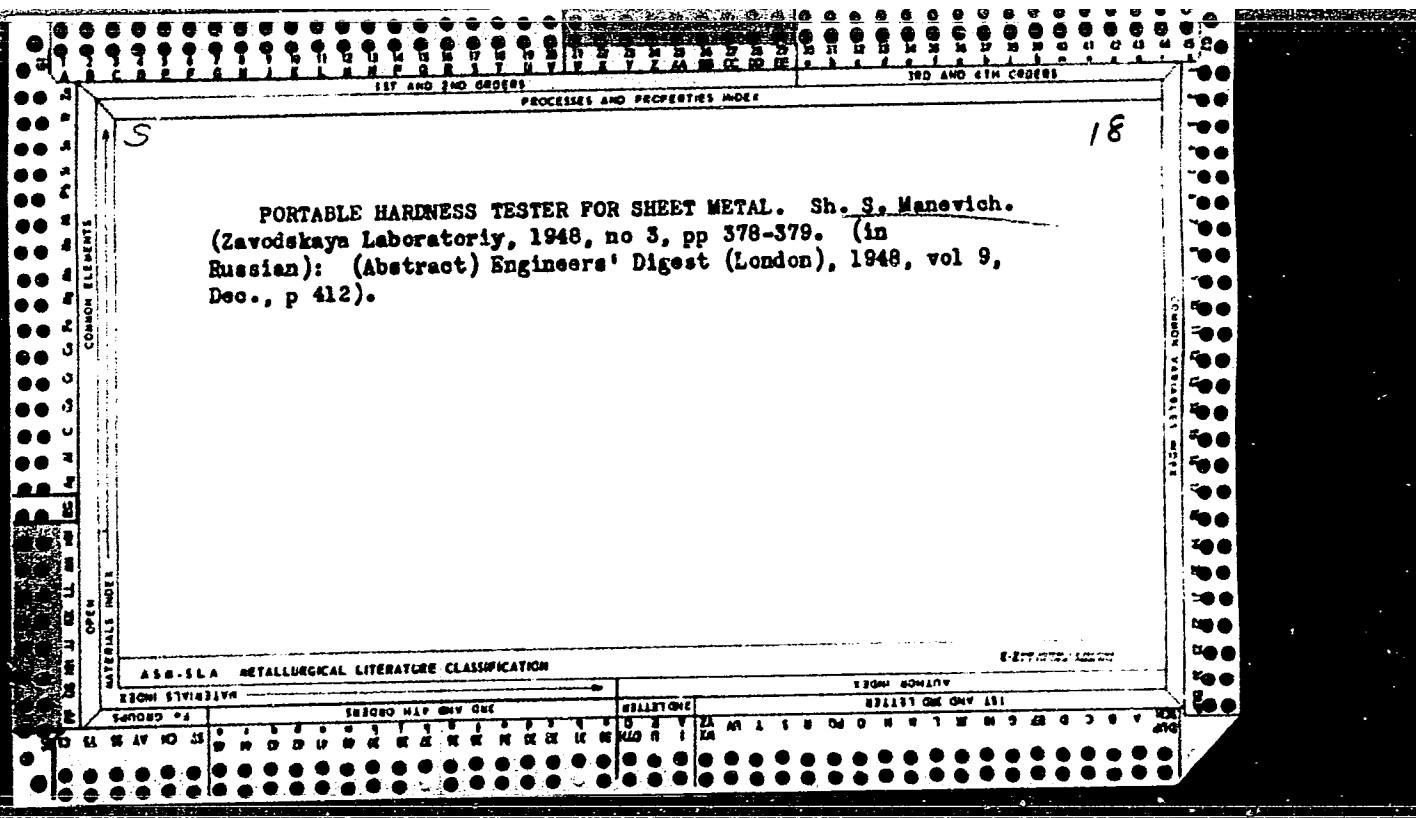
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PA 4/49 T37

MANEVICH, SH. S.

USB/R/Engineering

Feb 48

Detection, X-Ray

X-Rays - Measurements

"Simple Method of Determining the Depth of Defects Revealed by X-Ray," Sh. S. Manevich, B. V. Borshchev, 2 pp

"Zavod Lab" Vol XIV, No 2

Existing methods are complicated and little used. Diagrams show authors' simple method. Advantage is that it can be used by comparatively unskilled personnel. Only special equipment required is plexiglas rule with lead scale markings.

4/49 T37

Apr 48

USER/Engineering
Testing and Standardization
Testing Procedure

"Reply to the Questionnaire," Sh. S. Manovich,
Supervisor, Cer. Factory Lab., Kazan, 3 pp.

"Zavod Lab." Vol XIV, No 4

Considers division of mechanical properties into primary and secondary classes advisable. Yield point is basic characteristic; plasticity of second point is of secondary importance. Brittle fractures are comparatively frequent; instances of failures of connecting rods and crankshafts. Resilience is of use in connecting rods and crankshafts.

4/49T4

Apr 48

USER/Engineering (Contd.)

Properties usually determined are poor indication of behavior of metal during stamping, e.g., instances where hot-rolled sheets with high-ductility stamp worse than cold-rolled sheets with low ductility. Hardness readings by Vickers machines depend on load.

4/49T4

MANOVICH, Sh. S.

MANEVICH, SH. S.

PA 16/49T93

USSR/Metals
Plastics, Thermo-
Steel Alloys

Sep 48

"Studies of Thermoplastic Aftereffects in Metals
(Anomalous Case of Elastic Aftereffects)," Sh. S.
Manevich, 10½ pp

"Zavod Lab" Vol XIV, No 9

Establishes theory of thermoplastic aftereffect
and proves it by experiments. Effect is difference
in amount of residual deformation in deformed
specimens on heating. It varies according to type
of steel, and is of considerable importance in
springs.

16/49T93

S/058/61/000/002/004/018
A001/A001

Translation from: Referativnyy zhurnal, Fizika, 1961, No. 2, p. 263, # 2E130

AUTHOR: Manevich, Sh.S.

TITLE: On Tensile Strength of Solids

PERIODICAL: "Tr. Kazansk. s.-kh. in-ta", 1958, Vol. 1, No. 37, pp. 97 - 100

TEXT: The author proposes an approximate formula for determining tensile strength of solids using characteristics which are precisely measurable: $\sigma_{tens} = E \zeta + \alpha/x$, where E is the mean value of normal elasticity modulus, ζ is relative elongation of the material when heated from the test temperature to the melting point; α is coefficient of surface tension close to melting point; x is thickness of monomolecular layer. Based on the comparison of calculation and experimental data, the author comes to the conclusion that it will not be possible to obtain more heat-resistant alloys on Fe-base, but Zn- and Al-base alloys can be considerably improved. ✓

Yu. Dëmkin

Translator's note: This is the full translation of the original Russian abstract.

Card 1/1

S/058/61/000/002/005/018
A001/A001

Translation from: Referativnyy zhurnal, Fizika, 1961, No. 2, p. 281, # 2E273

AUTHOR: Manevich, Sh.S.

TITLE: On Relation Between Hardness and Other Physical Properties of Pure Metals

PERIODICAL: "Tr. Kazansk. s.-kh. in-ta", 1958, Vol. 1, No. 37, pp. 185-192

TEXT: It is presumed that there is a correlation connection between various physical quantities or their combination, if their dimensionalities are the same. In particular, there exists a correlation between hardness of metals and their surface energy, modulus of normal elasticity and ultimate strength. The author shows a close correlation between hardness and modulus of thermal elasticity, as well as between the latter and modulus of normal elasticity. It is possible to correct physical quantities, not precisely determinable, as e.g., hardness of absolutely pure metals, by using correlation connection.

Yu. Dëmkin

Translator's note: This is the full translation of the original Russian abstract.

Card 1/1

✓

S/058/60/000/006/016/04
A005/A001

Translation from: Referativnyy zhurnal, Fizika, 1960, No. 6, p. 195, # 14290

AUTHOR: Manevich, Sh.S.

TITLE: Energy Estimation Method of the Tear Resistance of Solids

PERIODICAL: Tr. Kazansk. s.-kh. in-ta, 1958, No. 39, pp. 111-115

TEXT: The author, starting from the assumption that the energy of mechanical splitting of a body into individual atoms is equal to the cohesion energy of this body, has derived a formula for estimating the magnitude of the resistance to tear. The numerical values of tear resistance calculated by the formula presented and by three others are similar. In contrast to other formulae, in this formula does not appear the magnitude of the surface energy. ✓

Author's summary

Translator's note: This is the full translation of the original Russian abstract.

Card 1/1

L 19657-63 EWP(k)/EWP(q)/EWT(m)/EWP(B)/BDS AFFTC/ASD Pf-4 JD
ACCESSION NR: AR3006997 S/0058/63/000/008/E077/E077

SOURCE: RZh. Fizika, Abs. 8E535

61
60

AUTHOR: Manevich, Sh. S.

TITLE: Effect of external actions on plastic deformation of metals

CITED SOURCE: Tr. Kazansk. s.-kh. in-ta, vy*p. 45, 1961, 76-78

TOPIC TAGS: metal plastic deformation, external influence,
heating, irradiation, ultrasound application

TRANSLATION: From the point of view of the fluctuation-shear theory of plastic deformation of metals, the resistance to deformation depends on the value of the interval of relative shear and the fluctuation coefficient. Their variation under the influence of external action such as heating, irradiation, and application of ultra-

Card 1/2

L 19657-63

ACCESSION NR: AR3006997

sound is considered. I. Gindin

DATE ACQ: 06Sep63

SUB CODE: PH

ENCL: 00

Card 2/2

10.7100

31010
S/124/61/000/009/051/058
D234/D303

AUTHOR: Maneyich, Sh.S.

TITLE: On the effect of fluctuations of elastic stresses
on plastic deformation

PERIODICAL: Referativnyy zhurnal. Mekhanika, no. 9, 1961, 45,
abstract 9 V418 (Tr. Kazansk. s.-kh. in-ta, 1959,
(1960), no. 42, 150-153)

TEXT: The difference between theoretical and actual
strength of materials is explained by fluctuation of elastic
stresses as a consequence of the influence of admixtures and dis-
tortions of crystal lattice. It is affirmed that in order to ob-
tain stronger materials one should not form materials without dis-
locations, but obtain thin-fiber materials consisting of very strong-
ly united homogeneous threads of metal; the metallic veneer made of
thin fibrous metallic foil must also be very strong. [Abstracter's
note: Complete translation]

Card 1/1

L 19658-63

EWP(q)/EWT(m)/EWP(B)/BDS AFFTC/ASD JD/HW

ACCESSION NR: AR3006996

S/0058/63/000/008/E077/E077

SOURCE: RZh. Fizika, Abs. 8E534

AUTHOR: Manevich, Sh. S.

TITLE: Fluctuation-shear theory of plastic deformation

CITED SOURCE: Tr. Kazansk. s.-kh. in-ta, vy*p. 45, 1961, 67-75

TOPIC TAGS: plastic deformation, fluctuation-shear theory

TRANSLATION: Starting from the fluctuation-shear concepts of the nature of plastic deformation of metals, according to which it is not the dislocations; but the fluctuations of the elastic stresses that are responsible for the low resistance to plastic deformation, an estimate is made of the cleaving stress necessary to initiate deformation; the experimental strain curve is explained; a system of equations is proposed to determine the behavior of the metal under

Card 1/2

L 19658-63

ACCESSION NR: AR3006996

the action of external forces; an attempt is made to relate the structure of fracture with the strain diagram of a metal. I. Gindin.

DATE ACQ: 06Sep63

SUB CODE: PH

ENCL: 00

Card 2/2

MINEVICH, S. G.

[Elements of mathematical statistics; textbook for students of agricultural schools of higher education] Elementy matematicheskoi statistiki; uchebnoe posobie dlja studentov sel'skokhoziaistvennykh vuzov. Kazan', Kazanskii gos'khoz. int-t, 1963. 160 p.

(MIA 10-1)

MININ, N.I., dotsent; BABIN, V.B.; KOFMAN, I.L.; MANEVICH, V.A.;
MIKHAIL'SON, V.A.; YUREVICH, V.M.

Concentration of ether in the blood during various types of
ether-oxygen anesthesia. Vest.khir. 85 no.9:95-100 S 160.
(MIRA 13:11)

1. Iz fakul'tetskoy khirurgicheskoy kliniki (zav. - prof. I.S.
Zhorov) sanitarno-gigiyenicheskogo fakul'teta 1-go Moskovskogo
ordena Lenina meditsinskogo instituta imeni I.M. Sechenova.
(ETHER (ANESTHETIC))

MANEVICH, V. A.

Call Nr: AF 1108825

Transactions of the Third All-union Mathematical Congress (Cont.) Moscow,
Jun-Jul '56, Trudy '56, V. 1, Sect. Rpts., Izdatel'stvo AN SSSR, Moscow, 1956, 237 pp.
Liber, A. Ye. (Saratov). To the Theory of Geometrical items.

Lyushkin, V. S. (Moscow). Vector Method of Transforming
the Systems into Simple Form of Differential Equation. 158-159

Manevich, V. A. (Moscow). On the Representation of
Elements of Collineation System of II and III Degree
As a Product of Two Polar Correspondences
and on Some Collineation Properties Connected With This
Problem. 160

There are 2 references, both of them USSR.

Nikolayenko, M. A. (Khar'kov). On Characteristics of
Monge Equation. 160

Norden, A. P. (Kazan'). On the Geometric Interpretation
of Certain Concepts of Spinor Analysis. 160

Card 51/80

AUTHOR: Manevich, V. A. (Moscow). 197

TITLE: On the representation of elements of systems of collineations of the second and third degree as products of two polar correspondences and on certain properties related to this problem. (O predstavlenii elementov sistem kollineatsiy vtoroy i tretiy stupeni v vide proizvedeniya dvukh polyarnikh sootvetstviy i o nekotorykh svoystvakh svyazannykh c etim voprosom).

PERIODICAL: "Matematicheskiy Sbornik" (Mathematical Symposium), 1957, Vol.41(83), No.2, pp.221-230 (U.S.S.R.)

ABSTRACT: By a ray of conic sections (K^2) is meant a set of curves of the second order passing through four points in general positions. If there are two rays of conic sections then two straight lines can be put into correspondence with each point of the plane (the polars of the points with respect to each ray), and two points can be put in correspondence with each line. The correspondence between one-parameter elements is a collineation, since it is the product of two correlations (polar correspondences) : $P_1 \cdot P_2 = C$. The representation of collineations in the form $P_1 \cdot P_2 = C$ is very convenient for the investigation of a number of problems. Hence it is important to investigate the possibility of representing any collineatory correspondence in the plane in such a form. This problem is discussed in the first part of the paper.

On the representation of elements of systems of 197 collineations of the second and third degree as products of two polar correspondences and on certain properties related to this problem. (Cont.)

Some related properties of collineations are also given. For example, it is shown that every correlative correspondence can be expressed as the product of three polar correspondences, and that the set of affine collineations can be represented as a polar system of some ray of conic sections having a general centre. In the second part of the paper is given the solution of the problem of representing collineations in space in the form of a product of two polar correspondences. Among related problems, the following are discussed:-
There are ∞^2 planes in space. Likewise, there are ∞^3 curves of the third order corresponding to these planes by one₂ and the same ray. On a curve of the third order are ∞^2 pairs of points each of which defines a unique collineation, which can be represented in the form of the product of two polar correspondences. Secondly, each ray of surfaces of the second order defines ∞^2 collineations, and so a system of collineations of the third degree can be regarded as a polar system relative to $\infty^1 = \infty^2 : \infty^2$ rays.
There are two references, both Russian.

Submitted 14/1/56.

"APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8

MANEVICH, V. A.: Master Phys-Math Sci (diss) -- "Some problems in linear geometry and their application to mechanics and aircraft building". Moscow, 1959.
(Min Educ RSFSR, Moscow City Pedagogical Inst im V. P. Potomkin), 150 copies
(KL, No 5, 1959, 125)

APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8"

MANEVICH, V.A.

A design of the attachment of a flap to airplane wings. Nauch.
dokl.vys.shkoly; mash.i prib. no.4:111-112 '58.
(MIRA 12:5)
1. Stat'ya predstavlena kafedroy "Nachertatel'naya geometriya"
Moskovskogo aviationskogo instituta.
(Airplanes--Wings)

46(+) 16.5000

66819

AUTHOR: Manevich, V.A.

SOV/155-58-5-9/37

TITLE: Some Questions Connected With the Quadratic Complex

PERIODICAL: Nauchnyye doklady vysshey shkoly. Fiziko-matematicheskiye nauki, 1958, Nr 5, pp 38-39 (USSR)

ABSTRACT: Theorem: Let the spherical space-curve of third order γ^3 be circumscribed to a given tetrahedron ABCD. The bisecants of γ^3 belong to a tetrahedral complex with the main tetrahedron ABCD.

Theorem : The geometrical position of the tops of cones of a quadratic complex, with respect to which two fixed points U and V are conjugate, is a surface of second order through U and V. Two further similar theorems are given.

ASSOCIATION: Moskovskiy ordena Lenina aviatsionnyy institut (Moscow Order of Lenin Aviation Institute) ✓

SUBMITTED: September 15, 1958

Card 1/1

AUTHOR: Manevich, V.A. SOV/41-10-2-9/13
TITLE: The Representation of the Collineations in the Plane as Products
of two Polar Correspondences (Predstavleniye kollineatsii na
ploskosti v vide proizvedeniya dvukh polyarnykh sotvetstviy)
PERIODICAL: Ukrainskiy matematicheskiy zhurnal, 1958, Vol 10, Nr 2, p 219(USSR)
ABSTRACT: The short note is a completion of a paper by the author [Ref 1]
published last year. The possibility of the considered repre-
sentation was already proved by Jung. The author gives a
constructive solution of the problem.
There is 1 Soviet reference.

1. Mathematics

Card 1/1

AUTHOR: Manevich, I.A. 1958, 10, 3, p. 333-334

TITLE: Polar Conjugacy With Respect to Some Figures of II-nd Order in the IV-Dimensional Space (Polyarnaya sverzhennost' otnositel'no nekotorykh obrazov II-ogo poryadka v IV-mernom prostranstve)

PERIODICAL: Ukrainskiy matematicheskiy zhurnal 1958, Vol 10, Nr 3
pp 333 - 334 (USSR)

ABSTRACT: The author starts from the notions axister and conoster in the projective geometry of Vlasov [Ref. 1] and proves the following theorems:
Theorem: An arbitrary plane of the IV-dimensional space intersects the axister in a curve of II-nd order.
Theorem: In the IV-dimensional space S_4 , a conoster intersects an arbitrary three-dimensional space along a surface of II-nd order.
Theorem: Let an axister be defined by the straight line a and by the curve of II-nd order α^2 . Then to every three dimensional space passing through a a plane passing through α^2 is polar conjugate with respect to the axister.
Theorem: The point A and the surface of II nd order F^2 are

Card 1/2

Polar Conjugacy With Respect to Some Figures
of II-nd Order in the IV-Dimensional Space SOV/4 'C-3-3/14

assumed to determine a concenter. Then to every three dimensional space through A a straight line through A is polar conjugate with respect to the concenter.
There is 1 Soviet reference.

SUBMITTED: September 17, 1957 (Moscow)

Card 2/2

AUTHOR: Manevich, V.A. (Moscow) 100/20-122-2-5/42

TITLE: A Straight Line Complex of 6-th Degree Generated by the Tetrahedral Complex (Kompleks pryamykh shestoy stepeni, porozhdayemyy tetraedral'nym kompleksom)

PERIODICAL: Doklady Akademii nauk SSSR, 1958, Vol 122, Nr 2, pp 183-185 (USSR)

ABSTRACT: The author gives a purely synthetic construction of a straight line complex of 6-th degree which is generated by a tetrahedral complex and formulates four properties of the system. There is 1 German reference.

ASSOCIATION: Moskovskiy aviatsionnyy institut imeni Sergo Ordzhonikidze (Moscow Aviation Institute imeni Sergo Ordzhonikidze)

PRESENTED: May 12, 1958, by F.S. Aleksandrov, Academician

SUBMITTED: April 8, 1957

Card 1/1

16(1)

AUTHOR: Manavich, V.A. (Moscow)

SOV/39-48-1-4/5

TITLE: On a Method of Descriptive Geometry (Ob odnom metode
nachertatel'noy geometrii)

PERIODICAL: Matematicheskiy sbornik, 1959, Vol 48, Nr 1, pp 105-116 (USSR)

ABSTRACT: A construction method of the descriptive geometry is based on
a one-to-one relation between the points of the space and
pairs of points of the plane which results from the properties
of the linear complex and the zero system. The method is
suitable for constructions of rules surfaces of second order.
There are 12 figures, and 2 references, 1 of which is Soviet,
and 1 German.

SUBMITTED: July 19, 1957

Card 1/1

MANEVICH, V.A. (Moskva)

Basic theorem of central axonometry. Mat.v shkole no.6:7-13 N-D
'62. (MIRA 16:1)
(Axonometric projection)

MANEVICH, V.A.

Three problems of central axonometry. Usp.mat.nauk 17 no.1:199-
203 Ja-F '62. (MIRA 15:3)
(Axonometric projection)

MANEVICH, V.A. (Moskva)

A remark on the study of T.G. Room "A problem in projective geometry". Cas pro pes mat 87 no.1:98 '62.

MANEVICH, V.A.

Cayley's generalized problem and some problems related to it.
Dokl. AN SSSR 143 no.6:1272-1273 Ap '62. (MIRA 15:4)

1. Moskovskiy institut inzhererov zheleznodorozhnogo transporta.
Predstavлено академиком P.S. Aleksandrovym.
(Conic sections) (Geometry, Analytic)

MANEVICH, V.A., kand. fiziko-matem. nauk, dotsent

One-to-one correspondences relative to rigid systems of points with
adjoint conical cross sections. Trudy MIIT no.190:138-161 '65.

Theory of multiple-value point correspondences. Ibid.:162-166

Hyperboloidal position of two plane quadrangles. Ibid.:167-169
(MIRA 18:8)

MANEVICH, V.B.

Nonuniform convergence of a series composed of nonnegative
functions, continuous on the segment. Uch. zap. AGU. Fiz.-mat.
i khim. ser. no.5:9-12 '60. (MIRA 14:11)
(Series)
(Functions, Continuous)

MANEVICH, V. F., inzh.

Machine for manufacturing clay cartridges for steaming blast holes.
Bezop. truda v prom. 4 no.11;34 N '60. (MIRA 13:11)
(Blasting—Equipment and supplies)

GREKOV, V.K., inzh.; MANEVICH, V.F.

Prevent longwall filling in coal mines. Bezop.truda v prom, 5
no.3:9-11 Mr '61. (MIRA 14:3)
(Coal mines and mining--Safety measures)

MANEVICH, V. F., inzh.

New safety measures for preventing mine fires. Bezop. truda v
prom. 5 no.11:37 N '61. (MIRA 14:11)
(Mine fires—Safety measures)

KAPELYUSHNIKOV, German Isaakovich; KLITSUNOV, Viktor Igant'yevich;
MANEVICH, Veniamin Fayyovich; PANKRATOV, Yu.A., inzh., retsen-
zent; ZASADYCH, B.I., retsenzent; FEDOTOV, A.N., otv. red.;
OKHRIMENKO, V.A., red. izd-va; IL'INSKAYA, G.M., tekhn. red.

[Safety measures in underground coal mining] Tekhnika bezo-
pasnosti pri podzemnoi dobyche uglia. Moskva, Gos. nauchno-
tekhn. izd-vo lit-ry po gornomu delu, 1962. 503 p.

(MIRA 15:4)

(Coal mines and mining—Safety measures)

(Coal miners—Diseases and hygiene)

MANEVICH, V.F., inzh.; CHERMASHENTSEV, Ya.N., inzh.

Conference on the use of short mechanized walls in working coal
and shale deposits. Bezop.truda v prom. 6 no.4:38 Ap '62.
(MIRA 15:5)
(Mining engineering)

MANEVICH, V.F., inzh.

Conference on the degassing of coal beds. Bezop. truda v proz. № 2:
38 F '63. (MIRA 16:2)
(Mine gases)

MANEVICH, V. L., Cand of Med Sci -- (diss) "Study of the Lymph Nodes
During Cancer of the Stomach," Moscow, 1959, 16 pp (Central Inst
for the Advanced Training of Physicians) (KL, 1-60, 126)

OSIPOV, B.K., prof.; MANEVICH, V.L.; SHIMELIOVICH, L.B.

Treatment of insufficiency of coronary circulation by bilateral
section of the a. mammariae internae. Terap.arkh. 31 no.12:60-63
D '59. (MIRA 13:4)

1. Iz 2-y kafedry klinicheskoy khirurgii (zav. - prof. B.K. Osipov)
TSentral'nogo instituta usovershenstvovaniya vrachey.
(CORONARY DISEASES surg.)

"APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8

MANEVICH, V.L.

Examination of the regional lymph nodes in operable gastric cancer.
Khirurgia 35 no. 11:47-54 N '59. (MIRA 14:1)
(STOMACH—CANCER) (LYMPHATICS)

APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8"

LITVAKOVSKAYA, G.A.; MANEVICH, V.L.

Cancer of the small intestine. Vest. rent. i rad. 35 no. 5:66-69
My-Je '60. (MIRA 14:2)

1. Iz 2-y kafedry rentgenologii (zav. - prof. Yu.N. Sokolov) i 2-y
kafedry khirurgii (zav. - prof. B.K. Osipov) TSentral'nogo
instituta usovershenstvovaniya vrachey na baze gorodskoy bol'nitsy
No.50 (glavnnyy vrach N.P. Brusova).

(INTESTINES--CANCER)

ROZANOV, I.B.; MANEVICH, V.L.

[Polyposis as precancer of the stomach] Polipoz kak predrak
zheludka. Moskva, TSentr. in-t usovershenstvovaniia vrachei,
1961. 166 p. (MIRA 15'6)

(STOMACH—CANCER)

MANEVICH, V.L.; SHIMELIOVICH, L.B.

Utilization of bilateral ligature of the internal thoracic arteries
in patients with pronounced coronary circulatory insufficiency
in preparation for severe surgical interventions on the organs of
the abdominal cavity. Trudy TSIU 2:143-146 '61. (MIRA 15:8)
(THORACIC ARTERY--LIGATION) (CORONARY HEART DISEASE)
(ABDOMEN--SURGERY)

MANEVICH, V.L.

Changes in the regional lymph nodes in operable cancer, polyposis
and peptic ulcer of the stomach. Trudy TSJU 2:202-214 '61.

(MIRA 15:8)

(STOMACH--CANCER) (LYMPHATICS) (PEPTIC ULCER)

MANEVICH, V.L.; ZAGNITKOVSKAYA, E.M.

Sarcoma of the intestines. Trudy TSIU 2:224-227 '61. (MIRA 15:8)
(INTESTINES--CANCER)

MANEVICH, V.L.; SHIMELIOVICH, L.B.

Abdominal syndrome in hemorrhagic vasculitis. Trudy TSIU 2:241-246
'61. (MIRA 15:8)
(PURPURA (ATHOLOGY)) (ABDOMEN--DISEASES)

MANEVICH, V.L.; PERKIN, E.M.

Primary cancer of the gall bladder and extrahepatic bile ducts.
Trudy TSIU 2:264-270 '61. (MIRA 15:8)
(GALL BLADDER--CANCER) (BILE DUCTS--CANCER)

"APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8

MANEVICH, V.L.

Technique for peridural anesthesia. Trudy TSIU 2:382-390 '61.
(MIRA 15:8)
(SPINAL ANESTHESIA)

APPROVED FOR RELEASE: 03/13/2001

CIA-RDP86-00513R001032120013-8"

MANEVICH, V.L.; LITVAKOVSKAYA, G.A.

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Ja-F '61. (MIRA 14:4)

1. Iz 2-y kafedry klinicheskoy khirurgii (zav. - prof. B.K. Osipov)
i 2-y kafedry rentgenologii (zav. - prof. Yu.N.Sokolov) na baze
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(ESOPHAGUS—TUMORS)

SOKOLOV, Yu.N., prof. (Moskva, Volokolamskoye shosse, d.1.kv.218);
MANEVICH, V.L., kand.med.nauk; ZAGNEUKOVSKAYA, L.M.

Excessive development of the folds of the mucosa of the stomach.
Vest. rent. i rad. 36 no.4:17-30 Jl-Ag '61. (MI.A 15:2)

1. Iz 2-y kafedry rentgenologii (zav. - prof. Yu.N.Sokolov) i
2-y kafedry khirurgii (zav. - prof. B.K.Osipov) Tsentral'nogo
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(STOMACH ABNORMALITIES AND DEFORMITIES)

MANIVICH, V.I., kand. med. nauk; T.D. "N.N." N.

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MANEVICH, V.L., kand. med. nauk

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