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IST PARAMETER DATE AND A DESCRIPTION OF THE PARAMETER S/136/61/000/001/007/010 18.1245 1416, 1454 0-14 E021/E206 **AUTHORS:** Mikheyev, I. M. and Smirnova, Ye. I. TITLE: Wrought Semi-fabricated Articles of the Magnesium Alloy MA10 Tsvetnyye metally, 1961, No. 1, pp. 79-82 PERIODICAL TEXT: This article deals with the melting, ingot casting, extrusion, welding and corrosion resistance of the MA10 magnesium base alloy, which contains aluminium, cadmium, silver and manganese (% content not specified). According to the authors, melting, ingot casting and extrusion procedures for this alloy do not differ markedly from those used for other magnesium alloys. Aluminium and manganese are added during melting, while cadmium and silver are added in the mixer. Ingots are cast by a semicontinuous process and then conditioned by machining. Round billets are 345 mm in diameter and 600-1100 mm long; flat billets are 160 x 540 x 700 mm. Bars, panels and strip were extruded on a horizontal press. Tubes were prepared from the bars on a vertical press. Forgings and stampings were also prepared from the bars. Extruding the bars, panels and strip at rates of flow greater than Card 1/3

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Wrought Semi-fabricated Articles of the Magnesium Alloy MA10

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0.3 m/min., and tubes at greater than 0.5 m/min. resulted in transverse tears. Extruding at 350-400°C at lower rates of flow gave a good surface and a uniform fine grain. The forgings and stampings also had a good surface and a similar structure. Microinvestigations showed that the semi-fabricated articles consisted of complex solid solutions of cadmium, silver, aluminium and manganese in magnesium and chemical compounds of complex nature. The strength of the MAIO alloy at all temperatures up to 300°C is superior to all other magnesium alloys; at 250°C the strength of the alloy is equal to, and at 300°C superior to, that of the B95 (US7075) aluminium alloy. Alloy MAIO is recommended for short-time service at temperatures below 300°C. Data on the mechanical properties of this alloy are given in Table 1. Corrosion resistance of the alloy is somewhat lower than that of the MA8 alloy (a wrought magnesium alloy containing 1.5-2.5% manganese and 0.5 0.35% cerium).

Card 2/3

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Wrought Semi-fabricated Articles of the Magnesium Alloy MA10

MAIO is also susceptible to stress corrosion. Corrosion resistance can be improved to the level of the MAÖ alloy by oxidizing treatment, and susceptibility to stress corrosion can be reduced by metallizing and lacquer coating. Preheated to 300-350°C, the alloy can be welded with the argon-shielded arc. Final heat treatment must be done after welding. Strength of welded joint is 70% of that of the heat-treated weld metal. There are 3 tables and 3 figures.

		Table 1		
	Tensile strength, kg/mm ²	Yield strength. kg/mm ²	Elongation, %	
As-extruded	33-39	24-28	8-15	
Solution heat treated	36-39	22-26	8-14	
Solution heat treated and aged	40-49	28-36	4 - 8	

Card 3/3

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-	ACCESSION HR: AP5019050		669.721.5		 1
	AUTHOR: Kovalev, I. G.; Mikhe Mishkin, V. L.			<u>v.;</u> 27. B	
	TITLE: High-strength magnesiu	malloy. Class 40, N	0. 172050		
	SOURCE: Byulleten' izobreteni	y I tovarnykh znakov,	no. 12, 1965, 77		
	TOPIC TAGS: magnesium alloy, magnesium weldable alloy	an the second	دیک در دیک در دیک در		
4	ABSTRACT: This Author Certific taining zinc, cadmium, and zin weldability, the alloy contain 0.5-2% lanthanum, and the remain	ng 2-4% zinc, 12%	h-strength magnes improve mechanics admium, 0.3-1%	ium alloy con- al properties and tirconium, [WW]	
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INVENTOR: Pevzner, L. V.; Akutin, M. S.; Mikheyev, I. P.; /? Faydel', I. Ya.; Sokolov, A. D.; Timofeyev, A. V. E
ORG: none
TITLE: Method for obtaining compacts. Class 39, No. 179466
SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 5, 1966, 69
TOPIC TAGS: polyvinyl chloride, phenolformaldehyde, compact
ABSTRACT: An Author Certificate has been issued for a method of ob- taining compacts by combining <u>phenol resin</u> with <u>polyvinyl chloride</u> in the filler, using a mechanochemical method. Phenol resins and aniline- phenolformaldehyde resins are used to obtain materials which are <u>impervious to water, chemical, and tropical conditions.</u> [NT]
SUB CODE: 11, 07/ SUBM DATE: 27Nov64/
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	/Engineering - Heat, Heat T		<u>52</u>	
	t Transfer in Turbulent Flo s, ^M M. A. Mikheyev, Corr Me	m Aced 801 0998	3	
157 z	Ak Nauk, Otdel Tekh Nauk N	o 10, pp 1448-1454	ford.	
Anal	yzes experimental data for	air, water, alcoho	ol,	
aget	cone, benzene and mineral oi nge in their physical proper	ls with wide range	e 01	
	$v_{elocity}$ (Re = 1.10 ⁺ -2.10 ^o	and M = U.2 - U.9()	temp	
Droc	ssure, and heat flow. Devel cess of heat transmission in	turbulent 1100 0	1	
flui	lds in straight pipes and chapping and chapping for any cross-sec	tion shape, inclu	mula	
slot	tted $(a/b = 4-40)$ and annular	$(d_2/d = 1 - 2)$	3147	
			<u> </u>	



ranslation	from: Referativnyy Zhurnal, Mekhanika, 1957, Nr 11, p 72 (USSR)
UTHOR:	Mikheyev, M. A., Baum, V. A., Voskresenskiy, K. D., Fedynskiy, O. S.
ITLE:	Heat Transfer by Molten Metals. (Teplootdacha rasplavlennykh metallov)
PERIODICA	L: V sb.: Reaktorostroyeniye i teoriya reaktorov. Moscow, Izd-vo AN SSSR, 1955, pp 139-151 (Also, in English, Progr. Nuclear Energy, 1956, Ser. 4, No. 1, pp 223-232)
ABSTRACT	measuring techniques, and testing methods. Investigated was the heat transfer by mercury, tin, lead, bismuth, sodium, and bismuth-lead and sodium-potassium alloys. The flow velocities varied from 0.1 to 20 m/sec, the Reynolds num- ber from 1×10^4 to 6.5×10^5 , the Prandtl number from 4×10^{-3} to 3.2×10^{-2} , and the specific heat flux from 2×10^4 to 1×10^6 kg-cal/m ² .hr. The Authors offer criteria for pure and oxidized surfaces based on 600 test points.
Card 1/2	A comparison is made between the test data and existing theories.

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• 124-11-12810 Heat transfer by molten metals (continued). From an evaluation of a variety of test data a new criterion is proposed in the form of a formula which applies to molten metals as well as to "common" liquids in which the Prandtl number exceeds 0.7. Investigations were also performed on the heat transfer in conditions of natural convection on heated plates and tubes for heavy and alkaline molten metals and their alloys. As a result of the evaluation of the test material, and also from available data on liquids exhibiting low heat conductivity, the Authors submit a single criterion formula for the heat transfer in large volumes, applicable over a wide range of Grashof and Prandtl numbers. The data relative to the hydrodynamic resistance in the flow of liquid metals show that the general formulas of hydrodynamics are (V. N. Krylov) Card 2/2

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NITHE YEV, W.A. 24(8) PHASE I BOOK EXPLOITATION SOV/3501 P.2 Akademiya nauk SSSR. Energeticheskiy institut Voprosy teploobmena (Heat-Exchange Problems) Moscow, 1959. 237 p. Errata slip inserted. 2,800 copies printed. Resp. Ed.: M.A. Mikheyev, Academician; Ed. of Publishing House: G.B. Gorshkov; Tech. Ed.: I.F. Kuz'min. PURPOSE. This collection of articles is intended for scientific workers, engineers, and postgraduate students specializing in thermodynamics. COVERAGE: The collection reviews problems of heat transfer and explores possibilities of intensifing heat exchange. The heat exchange theory is outlined, and Russian scientists who contributed to its development are mentioned. Thermophysical properties of some molten metals and alloys are analyzed, and methods used to determine them presented. Equipment used for measuring thermal conductivity, heat capacity, and kinetic viscosity of these metals are discussed. Results of experimental study of the intensified heat exchange for a water flow in an annular channel are analyzed and the instruments used along with the pilot plant for studying convection heat exchange in contacting nonmiscible fluids are described. Instruments and equipment used for determining the linear expansion Card 1/4

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Heat-Exchange Problems	SOV/3501
of metals, the consumption of a liquid, and the absor are also described and illustrated. A number of equa thermodynamic problems are presented. Each article is the majority of which are Soviet.	ations for solving various
TABLE OF CONTENTS:	
Editorial Foreword	3
Mikheyev, M.A. Development of the Science of Heat Excha Forty Years	ange During the Last 5
Nikol'skiy, N.A., N.A. Kalakutskaya, I.M. Pchëlkin, T.V. Vel'tishcheva. Thermophysical Properties of Some Molter	. Klassen, and V.A. n Metals and Alloys 11
Pchëlkin, I.M. Heat Capacity of Molten Metals	46
Sidorov, E.A. Radiation and Convection Heat Exchange in	n an Absorbing Medium 49
Fedynskiy, O.S. Intensification of Heat Exchange for th Annular Channel Card 2/4	ne Flow of Water in an 53

50V/3501	
eat-Exchange Problems	
Peryugin, V.M., and O.S. Fedynskiy. Convection Heat Exchange in a Direct Convection Heat Exchange in a Direct Co	
irillov, P.L., V.I. Subbotin, M.Ya. Suvorov, and M.F. Troyanov. Study of rangier to Sodium-Potassium Alloy in a Pipe	Heat 80
Condrat'yev, N.S. Average Heat Transfer for a Turbulent Flow of Eutectic	96
Ivanovskiy, M.N. Accelerated Method for Determining the Coefficient of Ave	
Adrianov, V.N. Application of Electroanalogy to the Solution of Problems of Rediant Heat Exchange	
Lel'chuk, V.L. and B.V. Dyadyakin. Heat Transmission From a Wall to a Tur lent Air Flow in a Pipe and the Hydraulic Resistance at High-Temperature P sure Heads	12)
Minashin, M.Ye., V.I. Subbotin, P.A. Ushakov, and A.A. Sholoknov. Utiliza of a Microthermocouple in Studying Heat Transfer Card 3/4	tion 193

Heat-Exchange Problems SOV/3501	
Pchëlkin, I.M. Instrument for Determining the Coefficient of Linear Expans of Metals	200
Korotkov, Yu.A. Unit for Metallization Carried out by Sublimation of Metal in a Vacuum	s 202
Korotkov, Yu.A. Instrument for Measuring the Consumption of a Liquid	206
Buleyev, N.I. Distribution of Velocity and Temperature for a Turbulent Liquid Flow in a Circular Pipe	208
Khrustalev, B.A. Instrument for Determining the Absorption Capacity of a Surface	233
AVAILABLE: Library of Congress	
Card 4/4	TM/sfm 5-1 3- 60

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"APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R001134120002-7 MIKHEYEV, Mikhail Aleksandrovichi MIKHEYEVA, Iriza Mikhaylovas; SKVORTSOV, S.A., red.; BORUNOV, N.I., tekhn. red. [Brief course in heat transfer] Kratkii kurs teploperedachi. Moskva, Gos.emerg.izd-vo, 1960. 206 p. (MIRA 15:2) (Heat-Transmission)

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Convection and Radiation Heat Exchange SOV/4396 the special experimental conditions under which the data were established. No personalities are mentioned. References follow most of the articles. TABLE OF CONTENTS: Editor's Foreword Voskresenskiy, K.D.,/Ye.S. Turilina. Influence on Heat Transfer of Internal 5 Sources of Heat Acting in a Flow of a Liquid in a Pipe 7 Motulevich, V.P. Heat Exchange in the Frontal Point of Blunt Bodies in a Mikheyev, M.A. Heat Transfer and Hydraulic Resistance of a Plate 16 Mikheyev, M.A., S.S. Filimonov, and B.A. Khrustalev. Investigation of Heat 25 Exchange and Hydraulic Resistance of Water Moving in Pipes 33 Card 2/5

APPROVED FOR RELEASE: 06/14/2000

Pchelkin, I.M. Heat Transfer in Vertical Pipes in Natural Convection56Alad'yev, I.T., and L.D. Dodonov. Critical Thermal Currents in Boiling Underheated Water in Channels of Complex Form (100 ata pressure)65Alad'yev, I.T., L.D. Dodonov, and V.S. Udalov. Experimental Data on Heat Transfer in Bubbling Boiling of Underheated Water in Pipes79Usmanov, A.G. Generalization of Experimental Data on Viscosity and Heat Conductivity of Liquid Metals97Adrianov, V.N., and S.N. Shorin. Investigation of the Process of Combined Heat Exchange in a Combustion Chamber107Polyak, G.L. Radiation Heat Exchange of Bodies With Arbitrary Indicatrices of Surface Reflection118Filimonov, S.S., B.A. Khrustalev, and V.N. Adrianov. Measurement of the Components of Combined Convection and Radiation Heat Exchange by the Method of Two Radiometers133Card 3/5133	Convection and Radiation Heat Exchange SOV/4396	
Alad'yev, I.T., L.D. Dodonov, and V.S. Udalov. Experimental Data on Heat65Alad'yev, I.T., L.D. Dodonov, and V.S. Udalov. Experimental Data on Heat79Usmanov, A.G. Generalization of Experimental Data on Viscosity and Heat97Adrianov, V.N., and S.N. Shorin. Investigation of the Process of Combined107Polyak, G.L. Radiation Heat Exchange of Bodies With Arbitrary Indicatrices118Filimonov, S.S., B.A. Khrustalev, and V.N. Adrianov. Measurement of the Components of Combined Convection and Radiation Heat Exchange by the Method of Two Radiometers133	Pchelkin, I.M. Heat Transfer in Vertical Pipes in Natural Convection	56
Instance Instance <td< td=""><td>Alad'yev, I.T., and L.D. Dodonov. Critical Thermal Currents in Boiling Underheated Water in Channels of Complex Form (100 ata pressure)</td><td></td></td<>	Alad'yev, I.T., and L.D. Dodonov. Critical Thermal Currents in Boiling Underheated Water in Channels of Complex Form (100 ata pressure)	
97 Adrianov, V.N., and S.N. Shorin. Investigation of the Process of Combined Heat Exchange in a Combustion Chamber 107 Polyak, G.L. Radiation Heat Exchange of Bodies With Arbitrary Indicatrices of Surface Reflection 118 Filimonov, S.S., B.A. Khrustalev, and V.N. Adrianov. Measurement of the Components of Combined Convection and Radiation Heat Exchange by the Method of Two Radiometers	Alad'yev, I.T., L.D. Dodonov, and V.S. Udalov. Experimental Data on Hea Transfer in Bubbling Boiling of Underheated Water in Pipes	
107 Polyak, G.L. Radiation Heat Exchange of Bodies With Arbitrary Indicatrices of Surface Reflection 118 Filimonov, S.S., B.A. Khrustalev, and V.N. Adrianov. Measurement of the Components of Combined Convection and Radiation Heat Exchange by the Method of Two Radiometers 133	Usmanov, A.G. Generalization of Experimental Data on Viscosity and Heat Conductivity of Liquid Metals	
Filimonov, S.S., B.A. Khrustalev, and V.N. Adrianov. Measurement of the Components of Combined Convection and Radiation Heat Exchange by the Method of Two Radiometers 133	Adrianov, V.N., and S.N. Shorin. Investigation of the Process of Combin Heat Exchange in a Combustion Chamber	
of Two Radiometers 133	Polyak, G.L. Radiation Heat Exchange of Bodies With Arbitrary Indicatri of Surface Reflection	
	components of complified convection and Radiation Heat Frehence by the Wet	hod
	Card 3/5	.,,,

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Convection and Radiation Heat Exchange		
Adrianov, V.N. Radiometric Instrument for Measuring the Flow of Radiation		
Dul'nev, G.N. Theory of the Heat Regime of Some Constructions of Radio-	145	
Dul'nev, G.N., G.P. Pokrovskaya, and A.I. Smirnov. Engineering Method for Calculating the Heat Regime of Radioelectronic Equipment	150	
Baum, V.A. Thermal Modeling of the Heat-Producing Elements of an Atomic Reactor	161	
Usmanov, A.G., and A.I. Berezhnoy. Investigation of Molecular and Thermic Diffusion by the Similarity Method	176	
Minashin, V.Ye., V.I. Subbotin, P.A. Ushakov, and A.A. Sholokhov. Measuring Error Connected With the Distortion of Isotherms in the Region of the Lo- cation of Thermocouples	188	
Card 4/5	205	
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 "APPROVED FOR RELEASE: 06/14/2000
 CIA-RDP86-00513R001134120002-7

 Convection and Radiation Heat Exchange
 SOV/4396

 Pilimonov, S.S., and B.A. Khrustalev. Calculation of Heat Exchange and Hy-
draulic Resistance in Laminar Motion of Fluids in Fipes
 221

 Alad'yev, I.T. Heat Transfer in Bubbling Boiling
 233

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ACC NRI AP6034275 (N) SOURCE CODE: UR/0281/66/000/005/0096/0104 AUTHOR: Mikheyev, M. A. (Moscow)		
ORG: None		
TITLE: Empirical formulas for convective heat exchange		
SOURCE: AN SSSR. Izvestiya. Energetika i transport, no. 5, 1966, 96- 04		
TOPIC TAGS: convective heat transfer, heat transfer theory		
ABSTRACT: The author presents a basis for the selection of the determining dimension. In the case of heat exchange in tubes, this dimension is assumed to be the working distance of the heat transfer surface instead of the diameter. It is shown that mol- ten metals are commonly used heat transfer agents which conform to general neat trans- fer laws. Empirical heat exchange formulas are made more accurate for the following cases: heat exchange of a plate in a fluid stream; heat exchange during the flow of heat exchange of a tube cluster in a transverse flow and heat exchange of bodies under conditions of free convection. Orig. art. has: 5 figures, 21 formulas.		
SUB CODE: 20/ SUBM DATE: 17Jun66/ ORIG REF: 005		
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MIRHEYEV, M. N. 36161 Magnitnyy Kontrol' Kachestva termicheskoy i termoKhimicheskoy obrabotki stal'nykh 12delly pri pomoshehi Knertsitimetra s pristavnymi elektromagnitami. Trudy In-ta 'iziki metallov, vpp. 12, 1949, S. 157-91--Bibliogr: 25 nazv. SC: Letopis' Zhrunal'nykh Statey, No. 49, 1949

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Marnetic Control of the Depth of the Hardened Layer and of the Hardness of Steel Tools Mardened by High-Freeuency Currents
A mobile coercivity motor of M. N. Mikheyev's design for magnetic control of the depth of the hardened layer, treated by high freeuency currents, is described. Experiments proved that the depth of the hardened layer, its hardness well as that of the core are in constant ratio with the readings of the coercivity meter. (R2hFiz, No. 8, 1055) Tr. in-ta Fiziki Matallov Uralsk Fil. AN SSSR No. 14, 1954, 43-47.
So: Sum, No. 744, 8 Dec 55 - Supplementary Survey of Soviet Scientific Abstracts (17)

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1955

MIKHEYEV. M. N., ZHUKOVA, P. N., AND TOMILOV, G. S.

Magnetic and Electric Properties of Alloyed Steels After Various Thermal Treatmont

Coercive force, maximum magnetic permeability, saturation of magnetization, specific electric resistance, and hardness depending on thermal treatment of various steel alloys were studied for establishing best qualities of ready products. The causes of defects of steels 30 XOS, 41-34, 5 XBC, 40 CX were established. (RZhFiz, No. 8, 1955) Tr. in-ta Fiziki Metalloy Uralsk. Fil AN SSSR, No. 15, 1954, 90-102

SO: Sum. No. 744. 8 Dec 55 - Supplementary Survey of Soviet Scientific Abstracts (17)

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MIKHEYEV, M. N. AUTHOR: Mikheyev, M. N. 1: 6-1-7/40 On the selection of optimum geometrical dimensions of TITLE: attachable electromagnets of coercivity meters designed for controlling the quality of heat and chemical-heat treatment of steel and iron components. (U vybore optimal'nykh geometricheszikh razmerov pristavnykh elektromagnitov koertsitimetra, prednaznachennogo dlya kontrolya kachestva termicheskoy i khimiko-termicheskoy obrabotki stal'nykh i chugunnykh izdeliy). PERIODICAL: Fizika Metallov i Metallovedeniye, 1957, Vol.5, No.1, ABSTRACT: At present there are two basic methods of regulating the depth of magnetisation in components when measuring the average magnetic properties at a given depth from the surface and, consequently, two methods of designing magnetic control apparatus for determining the thickness of such surface layers in steel and iron components. A.C. operated magnetising systems of a suitable frequency can be used or d.c. operated magnetising systems with appropriately chosen geometrical sections (cross section of the poles, distance between the poles, etc.). The Card 1/6 thickness values of the surface layers of steel and iron

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126-1-7/40 On the selection of optimum geometrical dimensions of attachable electromagnets of coercivity meters designed for controlling the quality of heat and chemical-heat treatment of steel and iron components.

components, which are of interest from the point of view of quality control after various types of chemical and heat treatment, are enumerated in a table on p.45. The author deals with magnetisation by means of a.c. fields, since in this case the depth of magnetisation of the checked specimens can be regulated to any desired value within the range enumerated in the table (up to 20 mm). Earlier experimental study (Ref.18) of the topography of magnetic induction in massive steel components magnetised by means of attachable electromagnets indicates that the depth of the surface layer which is magnetised to high induction values, depends on the geometrical dimensions of the magnet. The results of the distribution of magnetic induction with the depth from the surface of the component measured by a ballistic method is graphed in Fig.3 for various pole cross sections. Applying these or analogous experimental data for electromagnets with known geometrical dimensions, it is possible to determine by Card 2/6 means of the analogy theory the dimensions of the electro-

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CIA-RDP86-00513R001134120002-7

On the selection of optimum geometrical dimensions of attachable electromagnets of coercivity meters designed for controlling the quality of heat and chemical-heat treatment of steel and iron

> magnets which are necessary to ensure sufficiently high induction values to a given depth from the surface. By means of instruments of the given type, the average coercive force is measured for the same depth from the surface as the depth of high induction magnetisation. On the basis of this, conclusions can be made on the structure and the mechanical properties of the surface layer of the tested components, since there is a great difference between the magnetic properties of the surface layer and the core of the component. Information which is adequate for practical purposes of select-ing the optimum geometrical dimensions of the attachable poles of coercivity meters (intended for magnetic quality control of heat treatment and for determining the thickness of carburised, nitrided, decarburised and hardened layers of steel components) can be obtained by means of the simplified investigation of the distribution of the magnetic flux in the components to be tested, presented in this paper. The depth of magnetisation to

Card 3/6

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126-1-7/40 On the selection of optimum geometrical dimensions of attachable electromagnets of coercivity meters designed for controlling the quality of heat and chemical-heat treatment of steel and iron components.

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values approaching saturation cannot be larger than the thickness of the pole d of the electromagnet even if the induction B in the pole reaches the saturation value and even if the lateral leakage of the magnetic flux is almost completely absent. On the basis of the calculations contained in the paper, the author formulates the following recommendations: the thickness d of the poles should be made equal to the thickness of the surface layer in which it is desired to determine the average coercive force; the width c of the poles when testing relatively thin layers (from 1 to 2 mm onwards) should, in the extreme case, be three times as large as the thickness d of the poles of the electromagnet; for quality control of thin layers (below 0.5 mm) the width c of the poles should not exceed their thickness d; the distance between the poles and the height b should in all cases be as small as possible, just large enough to accommodate the magnetising coils and the indicator equipment in the form of a moving

Card 4/6

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CIA-RDP86-00513R001134120002-7

On the selection of optimum geometrical dimensions of attachable electromagnets of coercivity meters designed for controlling the quality of heat and chemical-heat treatment of steel and iron

coil or any other indicating equipment. For magnetic control right through the heat treated components, the geometrical dimensions of the electromagnet poles should be selected on the basis of the same principles, namely, of characterising the components to be checked according to their magnetic properties at a certain depth from the surface if such defects as soft core, inadequate tempering, etc. are to be revealed and the influence of surface decarburisation on the readings coercivity meter are to be eliminated. In Fig.8, p.51, the photographs are reproduced of two electromagnets, one of which is intended for measuring the average coercive force at a depth of 8 to 10 mm, the other for a depth of 3 to 4 mm from the surface. intended respectively for checking the through heat treatment and the carburisation depth. In Fig.9 the dependence is graphed of the average coercive force (expressed in units of the demagnetisation current) on the thickness of the surface hardened layer.

Card 5/6

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CIA-RDP86-00513R001134120002-7

On the selection of optimum geometrical dimensions of attachable electromagnets of coercivity meters designed for controlling the quality of heat and chemical-heat treatment of steel and iron

There are 9 figures, 1 table and 22 references, 21 of which are Slavic.

SUEMITTED: January 8, 1957.

ASSOCIATION: Institute of Physics of Metals, Ural Branch of the Ac.Sc. USSR. (Institut Fiziki Metallov Ural'skogo Filiala AN SSSR).

AVAILABLE: Library of Congress.

Card 6/6



CIA-RDP86-00513R001134120002-7

Mikheyev 181.10 Vonsovskij, S.V., Jores, Charles in upe of the Academy AUTHORS: of Sciences USSR, Mikheyev, M.N., Candidate of Technical Sciences Analysis of Mignetic Structure (M. hithy, strukturny, analis) TITLL: Zavodskaya Laboratorija, 1957. Vol 23, Nr 10, pr. 1/21-1226 (USSR) PERIOD ICAL: ABSTRACT : The chapter of the paper: Developmint of the methods of analysis of magnetic structure begins by assistantian in terms - coviet, as well as American, German, and French sci-ntists who contributed to the development of the method referred to in the title.Amon; them are: Arkad'yev, Frenkel, Dorfman, Akalov, Kondorskiy, Landiu Lifshits and Yanus (USSA), further Bozopt and ditter (USA), Fring (Germany) and Keel (Frince). The elaborate studies of Soviet scientists in the field of as motic control of the materials are declared to be of greatest importance, and that in the sense of their practical application in industrial enterprises. The most important studies in this fleid are mentioned here, most of them with the application of a covercia ter in the control me-+ ods and finally a special method which is called here "magnetic metallography" with which the investigation of the structure of the phases is judged according, to the picture of the deposit

of the hagnetic powder on the ground sections of the metals (ac-

cording to Toremin, N. I.). In the following chapter: Ratio betw

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CIA-RDP86-00513R001134120002-7

Analysis of Magnetic Structure

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ween magnetic or certical and atomical state of clustinge the chiract-ristic property of interaction of the lectrons and positive ions of the crystalline lattice of the substance is taken as a basis for the investigation of this ratio. With this, it is also explained that the community in the shorical and $_{P}$ and $_{P}$ and $_{P}$ ture of the substance and various states of their structure in their magnetic characteristic becaus effective and that they detersine the beion ing of the substance to one of the magnetic groups. (Dianagnetica, pura-, or ferromagnetica). Taking account of the variations of saturation, or of the Curie Point, with respect to the changes in composition, the degree of order of the atoms in the alog and disturbances in discerbones, it therefore results a possibility of elaborating a measuring met on for these valuations in atomic structure of the substance. The same can be officed with respect to the structural dependence of magnetic parimeters which are in proportion to the tecnnical As a tigation surve (criginal ind maximum $x \in \mathbb{R}^n$ sty, sourcive force, final we stigation, etc.). Corres of x = 0 works ina rum the in taking principles there in by references, ³ of a rolling provide.

AVAILAJLL: Card 2/2

Librar, J. C. Largas 1. Magnetic properties-Analysis

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٠	Akademiya nauk SSSR. Ural'skiy filial. Institut fiziki metallov
	Trudy, vyp. 20 (Transactions of the Institute of the Physics of Metals, Ural Branch, Academy of Sciences USSR, No. 20) Sverd- lovsk, 1958. 402 p. Errata slip inserted. 1,000 copies printed.
	Resp. Eds.: S.V. Vonsovskiy, Corresponding Member, Academy of Sciences USSR, and V I. Arkharov, Doctor of Technical Sciences.
	PURPOSE: This book is intended for scientists working in the field of physical metallurgy.
	COVERAGE: This is a collection of 28 articles written by members of the Institute of the Physics of Metals, Ural Branch of the Academy of Sciences USSR, on problems investigated at the Institute. Studies at the Institute have concentrated on two basic problems: 1) developing a theory of metals and alloys and finding ways to improve the
	Card 1/6

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Transactions of the Institute (Cont.)

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properties of engineering materials; and 2) developing new physical methods for investigating and controlling the quality of materials and metal articles. In connection with these basic problems the articles in the collection treat the following subjects; problems of the multielectron quantum-mechanical theory of solids; the laws of distribution and diffusion of admixtures in various metallic alloys (internal adsorption theory); strength and plasticity of polycrystalline materials in relation to interatomic binding forces, distortions in the crystal lattice; structural theory of diffusion reaction, i.e. diffusion due to chemical reactions in solid phases; theory of the magnetic structure of ferromagnetic substances; theory of the heat treatment of steel; and the physical theory of magnetic measurements (magnetic flaw detection and structural analysis). The first article gives a description of the work being done by the Institute and a list of departments and laboratories along with their chief personnel. Several persons are cited for their work at the Institute. References accompany each article.

TABLE OF CONTENTS:

IN WARDEN STREET

Mikheyev. M.N. Summary and Prospects of Scientific Activity at the Card 2/6

APPROVED FOR RELEASE: 06/14/2000

sov/3847 Transactions of the Institute (Cont.) 5 Institute of the Physics of Metals Vonsovskiy, S.V. Problems in the Quantum Theory of Solids 13 Orlov, A.N. and A.N. Men'. Statistical Theory of Binding Forces 43 in Transition Metal Oxides With Cubic Lattice Sokolov, A.V. Quantum Theory of the Optical Properties of Metals 53 Vlasov, K.B. Problems in the Theory of Mechanical, Magnetic, Thermal, Magnetomechanical, Thermomagnetic and Thermoelastic Prop-erties of a Magnetoelastic Medium 71 Vlasov, K.B. Problems in the Quantum-Mechanical and Phenomenological Theory of Ferromagnetism, Antiferromagnetism, and Ferrimagnetism Irkhin, Yu.P. Anomalies in the Electrical Conductivity of Anti-95 ferromagnetics Near Néel's Point Turov, Ye.A., and V.G. Shavrov. Phenomenological Theory of Ferro-Card 3/6

APPROVED FOR RELEASE: 06/14/2000

SOV/3847 Transactions of the Institute (Cont.) 101 magnetic Phenomena Shur, Ya.S. Magnetic Structure of Highly Coercive Ferromagnetics 111 Startseva, I.Ye., and Ya.S. Shur. Magnetic Structure of Iron 125 Silicide Crystals in a State of Residual Magnetization Shur, Ya.S., M.G. Luzhinskaya, K.B. Vlasov, O.I. Shiryayeva, and V.A. Zaykova. Relationship Between the Magnetic Properties and Sensitivity of Magnetostrictive Receivers 131 Yanus, R.I. Methods of Checking the Magnetic Properties of Steel 141 for Electrical Equipment Shturkin, D.A. Comparative Tests of Ferrite Probes With Longi-153 tudinal and Lateral Excitation <u>Mikheyev, M.N.</u> Magnetic Checking of the Structure and Mechanical Properties of Steel Articles 163 Card 4/6

APPROVED FOR RELEASE: 06/14/2000

Transactions of the Institute (Cont.) SOV/3847 Nemnonov, S.A. Use of X-Ray Spectroscopy in the Study of the Energy Spectrum of Electrons and Atomic Bonds in Solids 169 Trapeznikov, V.A. Method of Absorbing X-Rays for Solving Certain Problems in Solid-State Physics 187 Arkharov, V.I. Internal Adsorption in Solid Solutions 201 Arkharov, V.I. Physical Mechanism of Diffusion Reactions as Reflected in the Structural Pattern of the Reaction-Product Layers 229 Pavlov, V.A. Study of the Regular Patterns of Plastic Deformation 245 Yakovleva, E.S. Microscopic Study of the Mechanism of Plastic Deformation of Metals and Alloys 265 Rodionov, K.P. Effect of High Pressure on Some Physical Properties 273 Buynov, N.N. Investigation of Decomposition in Supersaturated Metallic Solid Solutions Card 5/6 283

APPROVED FOR RELEASE: 06/14/2000

	· · · · · •
Transactions of the Institute (Cont.) SOV/3847	
Sadovskiy, V.D. Structural Mechanism of Phase Over-Crystalliza- tion During the Heating of Steel	
	303
Gorbach, V.G. and V.D. Sadovskiy. Effect of Preliminary Heat Treatment of Steel on the Transformation Kinetics of Supercooled Austenite	
	311
Kompaneytsev, N.A., and V.D. Sadovskiy. Correcting the Structur and Fracture of Cast Alloyed Steel Through Heat Treatment	e 329
	J29
Malyshev, K.A., N.A. Borodina, V.A. Mirmel'shteyn. Strengthening Metastable Austenite Alloys by Means of Phase Hardening	339
Rodigin, N.M. High-Speed Heating for Investigating Electrotherma Freatment and Other Purposes	al 349
Bibliography of Works by Members of the Institute of the Physics of Metals, Ural Branch of the Academy of Sciences USSR for the Tears 1932-1956	515
	357
VAILABLE: Library of Congress (TN607.A4)	
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SOV/126-6-4-9/34

Arkharov, V.I., Belenkova, M.M., **▲**UTHOR: Moiseyev, A.I. and Polikarpova, I.P. Mikheyev, M.N.,

- The Effect of Small Additions of Antimony and Boryllium TITIE: on Ageing of the Copper-Silver Alloys (Part 1V. On the Problem of Causes of the Effects of Small Alloying Additions on the Kinetics of Ageing of Alloys) (O vliyanii malykh primesey sur'my i berilliy: na stareniye splavov med' - serebro (k voprosu o prichinakh vliyaniya malykh primesey na kinetiku stareniya splavov. 1V))
- PERIODICAL: Fizika metallov i metallovedeniye, 1958, Vol 6, Nr 4, pp 633-642 (USSR)
- In his previous work (Ref.1-3) the result of which **ABSTRACT:** indicated that small additions of horophilic elements (elements showing preference for the grain boundaries) present in a supersaturated solid solution could affect the kinetics of its decompositon by the mechanism of adsorption enrichment of the structurally distorted zones linking the nuclei of decomposition with the solid Card 1/11 solution matrix, Arkharov studied the effects of single

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SOV/126-6-4-9/34

The Effect of Small Additions of Antimony and Beryllium on Ageing of the Copper-Silver Alloys (Part 1V. On the Problem of Causes of the Effects of Small Alloying Additions on the Kinetics of Ageing of Alloys)

The object of the present investigation was to study the simultaneous effect of two horophilic additions. The experimental alloys whose detailed additions. chemical analysis is given in a table on p 633, contained 6% Ag with 0.2 - 0.5% Sb and 0.02 - 0.3% Be added either separately cr jointly. The alleys were melted in a H.F. induction furnace, in a graphite crucible with borax used as the covering flux. The cast ingots were heated under charcoal to 800°C, held at the temperature for 2 hrs and cooled in the furnace They were then rolled to strip 5 mm thick which, after a homogenising treatment consisting of 50 hours at 800°C was used for the preparation of the experimental test pieces. The process of ageing was studied by measuring the variation of hardness, magnetic susceptibility and electrical resistance The Card 2/11 measurements of Rockwell hardness were taken at

APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R001134120002-7

The Effect of Small Additions of Antimony and Beryllium on Ageing of the Copper-Silver Alloys (Part 1V. On the Problem of Causes of the Effects of Small Alloying Additions on the 15-30 minute intervals on specimens solution treated at 780 - 790°C and aged at 370°C. Magnetic susceptibility was measured with the aid of a magnetic balance at room temperature and at 370, 400 and 420°C. The measurements were taken at 10-15 minute intervals and in every case the value of relative magnetic susceptibility was determined, i.e. the force acting on the investigated specimen was compared with the force acting on a standard nickel sulphate specimen placed in an identical magnetic field. Electrical resistance was measured by the comparison of potential drop method, using a potentiometer and a sensitive galvanometer. In this case, both the solution treatment and ageing (at 370°C) were carried out in vacuum and the measurements were taken at 15 minute intervals. From the experimental data the average rate of ageing Card 3/11 $(\mathbf{v}_{cm} = \text{the ratio of the maximum increment of the studied})$

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501/126-6-4-9/34 The Effect of Small Additions of Antimony and Peryllium on Ageing of the Copper-Silver Alloys (Part 1V. On the Problem of Causes of the Effects of Small Alloying Additions on the Kinetics of Ageing of Alloys) property to the length of time required to effect this variation) was calculated for various investigated alloys and the results were reproduced graphically. Figl shows how vcm (assessed on the basis of hardness measurements) of alloys with a constant Sb content aged at 370°C varied with increasing Be content. The variation of vcm (calculated from the data on magnetic BUSCeptibility) of alloys containing 0.2% Sb and aged at 370, 400 and 420° with increasing Be content is shown in Fig.2, while Fig.3 shows the effect of Be on Vcm (determined on the basis of electrical resistance measurements) of the 0.2% Sb alloy aged at 370°C. The effect of the Sb and Be additions on the course of the ageing process in its various stages was determined on the basis of the measurements of magnetic susceptibility, since this property could be masured Card 4/11

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SOV/126-6-4-9/34 The Effect of Small Additions of Antimony and Beryllium on Ageing of the Copper-Silver Alloys (Part 1V. On the Problem of Causes of the Effects of Small Alloying Additions on the Kinetics of Ageing with higher accuracy and without the necessity of of Alloys) interrupting the heat treatment. To this end, graphs showing the time-dependence of $\Delta \times$ were constructed, Δx being the difference between the values of the relative magnetic susceptibility of two alloys aged for a given period at 370°C: one with and the other without the addition(8), the effect of which was being examined. In this way the effect of Sb and Be (added separately) on the ageing process of the Cu-Ag alloy is shown on Fig.4. It can be seen that while antimony accelerates ageing at every stage of this process (this effect being most pronounced at t = 30 min) the effect of beryllium is quite different: In the first stages of the ageing treatment this addition accelerates ageing, but beginning from a certain moment, it slows the process down. (The higher the Be content the varlier is the moment at which its delaying effect comes into operation Card 5/11

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SOV/126-6-4-9/34

The Effect of Small Additions of Antimony and Beryllium on Ageing of the Copper-Silver Alloys. (Part 1V. On the Problem of Causes of the Effects of small Alloying Additions on the Kinetics of Ageing of Alloys)

and the greater is the magnitude of the effect.) The effect of 0.2% Sb on ageing of Cu-Ag alloys containing 0.02 and 0.1% Be (Fig.5) is similar to its effect on the binary Cu-Ag alloy. The same applies to the effect of simultaneous additions of Sb and Be, except that in this case the maximum value of $\Delta \chi$ decreases with increasing Be content (Fig.6). The effect of Be on kinetics of ageing of the Cu-Ag alloy effect of Be on kinetics of ageing of the Cu-Ag alloy icontaining 0.2% Sb is much more complex. At small concentrations (0.02%) beryllium accelerates ageing of the Cu-Ag-Sb alloy (graph 1) in all stages of the process, $\Delta \chi$ reaching its maximum after 1 hr. 0.1% Be allows the process down in its initial stage and slows the process down in the final stage. When accelerates it slightly in the final stage. When accelerates it slightly is the final stage and blows the ageing process of the Cu-Ag-Sb alloy at every down the ageing process of the Cu-Ag-Sb alloy at every

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The Effect of Small Additions of Antimony and Beryllium on Ageing of the Copper-Silver Alloys. (Part 1V. On the Problem of Causes of the Effects of Small Alloying Additions on the Kinetics of Ageing stage, its effect being most pronounced at t = 30 min. of Alloys) The following interpretation of the obtained results is offered by the present authors: The average rate, Vcm, of the isothermal decomposition of a supersaturated solid solution of silver in copper is markedly affected by small simultaneously present additions of Sb and Be, even when these elements are present in concentrations considerably lower than their respective solid solubility limits. When added separately, antimony accelerates and beryllium slows down the process of decomposition. However, these effects are not additive when Sb and Be are present simultaneously: At a given Sb concentration Vcm increases at first with the increasing Be content reaches a maximum and then slowly decreases (Fig.1-3). The higher the content of antimony the higher are the values of v_{cm} for any given beryllium concentrations Card 7/11

APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R001134120002-7

SOV/126-6-4-9/34 The Effect of Small Additions of Antimony and Beryllium cr. Ageing of the Copper-Silver Alloys. (Part 1V. On the Problem of Causes of the Effects of Small Alloying Additions on the Kinetics of Ageing including those corresponding to the maximum values of Vcm. These effects can be explained on the basis of of Alloys) a hypothesis of internal adsorption of the Sb and Be atoms in structurally distorted zones linking the nuclei of decomposition with the solid solution matrix, it being postulated that the alloying elements can be adsorbed not only as separate atoms but also in the form of complexes containing atoms of beth additions. As a result of the adsorption of complexes the free energy of the distorted zones is decreased in regions where owing to the specific character of the distortion - it would not be decreased by adsorption of single atoms. The extent to which adsorption of complexes affects the kinetics of decomposition of the Bolid Solution varies with time since, as a result of adsorption, the total concentration of both alloying elements in the adsorption zone is altered to a degree depending on the Card 8/11

APPROVED FOR RELEASE: 06/14/2000

The Effect of Small Additions of Antimony and Beryllium on Ageing of the Copper-Silver Alloys. (Part 1V. On the Problem of Causes of the Effects of Small Alloying Additions on the Kinetics of Ageing of Alloys)

overall concentration of the additions present Simultaneously in the alloy: At a given Sb concentration, beryllium - when present in small quantities - is absorbed mainly in the form of complexes with the result that the concentration of Sb in the adsorption zone is increased and its accelerating effect on the decomposition of the solid solution is multiplied. On the other hand, when the Be content is high, it is adsorbed in the form of single atoms which increases its concentration in the adsorption zones with the result that the rate of decomposition is slowed down. The effects of Be and Sb on the course of the ageing The effects of Be and Sb on the initial stages of the process when formation of nuclei of decomposition is the predominant factor affecting the kinetics of nucleation due to local lattice distortions in the

Card 9/11

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CIA-RDP86-00513R001134120002-7

SOV, 126-6-4-9/34

The Effect of Small Additions of Antimony and Beryllium or agains of the Copper-Silver Alloys. (Part 1V. On the Problem of Jauses of the Effects of Small Alloying Additions on the Kinetics of Ageing of Alloys)

vicinity of the solute atoms are non-additive because - owing to the fact that Be atoms are smaller and St atoms larger than the colvent atoms - the lattice distortions caused by the atoms of either element present separately are more severe than those caused by the complexes formed when the two alloying additions are present simultaneously. In the later stages of the ageing process when growth of the decomposition centres affected by the adsorption of the alloying elements in the surrounding zones is the predominating factor, the non-additive character of the effects of Sb and De is evidently due to the fact that at first beryllium is preferentially adsorbed, while adsorption of antimony takes place mainly in the later stages. This time-lag in the adsorption activities of the two elements is probably associated with the fact that with the growth Card 10/11 of the decomposition nuclei the character and magnitude

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SUV/1-0-7-1-5/20 Kuznetsov, I.A. and Mikheyev, M.L. **AUTHORS:** Magnetic, Electrical and Mechanical Properties of TITLE: Steels with High Chromium Content After Various Heat Treatments PERIODICAL: Fizika metallov i metallovedeniye, 1959, Vol 7, Nr 4, pp 513-526 (USSR) The first object of the investigation described in ABSTRACT: the present paper was to study the effect of various heat treatment procedures on hardness, H_{Rc} (Rockwell, C scale), coercive force, H_C(oersteds), maximum magnetic permeability, μ_{max} (gauss/oersteds), intensity of magnetisation, 1_S (gauss), electrical resistivity, q (ohm cm), impact strength, a_k (kgm/cm²) and the proportion of retained austenite, A(%), of two chromium steelsKil2M and Khl2Fl whose chemical analysis is given in Table 1. The second object was to establish which is the most reliable method of determining the proportion of retained austenite in heat treated specimens, this characteristic being of particular importance since it determines the dimensional stability of articles made of steels of this type. The experimental specimens, Card 1/12

APPROVED FOR RELEASE: 06/14/2000

CIA-RDP86-00513R001134120002-7

SOV/120-7-4-5/26 Magnetic, Electrical and Mechanical Properties of Steels with High Chromium Content After Various Heat Treatments measuring 10 x 10 x 66 mm, were protected from decarburization at high heat treatment temperatures by a 15 - 20 microns thick layer of electro-deposited chromium which was removed after the heat treatment by grinding each face of the specimen to a depth of 1 mm. Quenching was done at room temperature either in oil or in a stream of air. The intensity of magnetization was measured in on electromagnet in a field of approximately 4500 gauss. For the sake of greater accuracy, the differential ballistic method of measurement was used, i.e. in each test two specimens (a standard specimen of known I_s , and the investigated specimen) were used. Fig 1 shows the circuit diagram of the apparatus used with the standard and investigated specimens denoted by \mathbf{i} and \mathbf{x} , respectively. The deflection, a, of the galvanometer is proportional to the difference between the magnetic fluxes in \Im and x. If the cross-section areas, S_3 and S_X , of the two specimens are nearly the same and if the difference Card 2/12 between the magnetic fields $H_{\mathbf{y}}$ and $H_{\mathbf{x}}$ is not large,

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