

MINKER, F.; KONTAI, M.

The effect of dihydroergotoxine on the acetylcholine reaction of the cat's nictitating membrane. Acta physiol. Acad. sci. Hung. 25 no.3:285-293 '64

1. Institute of Pharmacology, University Medical School, Szeged.

MINKER, E.; KOLTAI, M.

Effect of protamine sulphate on the transmission process in
peripheral sympathetic ganglia. Acta physiol. acad. sci.
Hung. 24 no. 3: 365-371 '64

1. Institute of Pharmacology, Medical University, Szeged.

*

NOVAK, Istvan; BUZAS, Geza; MINKER, Emil; KOLTAI, Matyas; SZENDREI, Kalman

Crystalline active ingredients of Ruta graveolens. Acta pharm.
Hung. 35 no.2:90-95 Mr '65.

VLASOV, A.G., dots.; MINKEV, I.M., inzh.

Determining the electric field in a dielectric in connection with high-frequency heating. Izv.vys.ucheb.zav.; energ. 3 no.3:47-55 Mr '60. (MIRA 13:3)

1. Gosudarstvennyy ordena Lenina opticheskiy inatitut ineni S.I.Vavilova.

(Dielectrics) (Induction heating)

MINKEVICH, A. N., FISAREV, N. N. AND SOLODIKHIN, A. G.

"Nitriding as a Method of Protecting Steel from Corrosion," ISTEIN, Moscow, 1940.

1ST AND 2ND ORDERS

PROCESSES AND PROPERTIES INDEX

7

M

Research Progress (Surface Treatment of Steel with Aluminium).
(Light Metals, 1940, 2, (26), 66-67).—An account is given of recent work by
 Minkevich and Zudin (*Vestn. Metallopromish.*, 1939, 8, 67) on the diffusion
 of aluminium into iron when the iron is heated at 600°–1000° C. for 3–12 hrs. in
 contact with a powder consisting of aluminium (or its alloys), an inert material
 such as quartz or fireclay, and ammonium chloride. Results are given in
 graphical form.—H. W. L. P.

ASME-55-A METALLURGICAL LITERATURE CLASSIFICATION

SECTION 1: STEEL

SECTION 2: ALUMINUM

SECTION 3: COPPER

SECTION 4: ZINC

SECTION 5: NICKEL

SECTION 6: IRON

SECTION 7: TITANIUM

SECTION 8: MAGNESIUM

SECTION 9: ZIRCONIUM

SECTION 10: NIOBIUM

SECTION 11: MOLYBDENUM

SECTION 12: CHROMIUM

SECTION 13: MANGANESE

SECTION 14: SILICON

SECTION 15: BORON

SECTION 16: FLUORINE

SECTION 17: CHLORINE

SECTION 18: SULFUR

SECTION 19: PHOSPHORUS

SECTION 20: CARBON

SECTION 21: HYDROGEN

SECTION 22: OXYGEN

SECTION 23: NITROGEN

SECTION 24: ARGON

SECTION 25: NEON

SECTION 26: HELIUM

SECTION 27: LITHIUM

SECTION 28: SODIUM

SECTION 29: POTASSIUM

SECTION 30: RUBIDIUM

SECTION 31: CESIUM

SECTION 32: BARIUM

SECTION 33: STRONTIUM

SECTION 34: CALCIUM

SECTION 35: MAGNESIUM

SECTION 36: ZINC

SECTION 37: CADMIUM

SECTION 38: MERCURY

SECTION 39: COPPER

SECTION 40: SILVER

SECTION 41: GOLD

SECTION 42: PLATINUM

SECTION 43: IRIDIUM

SECTION 44: RHODIUM

SECTION 45: PALLADIUM

SECTION 46: NICKEL

SECTION 47: COBALT

SECTION 48: IRON

SECTION 49: RUTHENIUM

SECTION 50: RHODIUM

SECTION 51: PALLADIUM

SECTION 52: SILVER

SECTION 53: GOLD

SECTION 54: PLATINUM

SECTION 55: IRIUM

SECTION 56: OSMIUM

SECTION 57: NICKEL

SECTION 58: COBALT

SECTION 59: IRON

SECTION 60: RUTHENIUM

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SECTION 62: PALLADIUM

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SECTION 65: PLATINUM

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SECTION 89: OSMIUM

SECTION 90: NICKEL

SECTION 91: COBALT

SECTION 92: IRON

SECTION 93: RUTHENIUM

SECTION 94: RHODIUM

SECTION 95: PALLADIUM

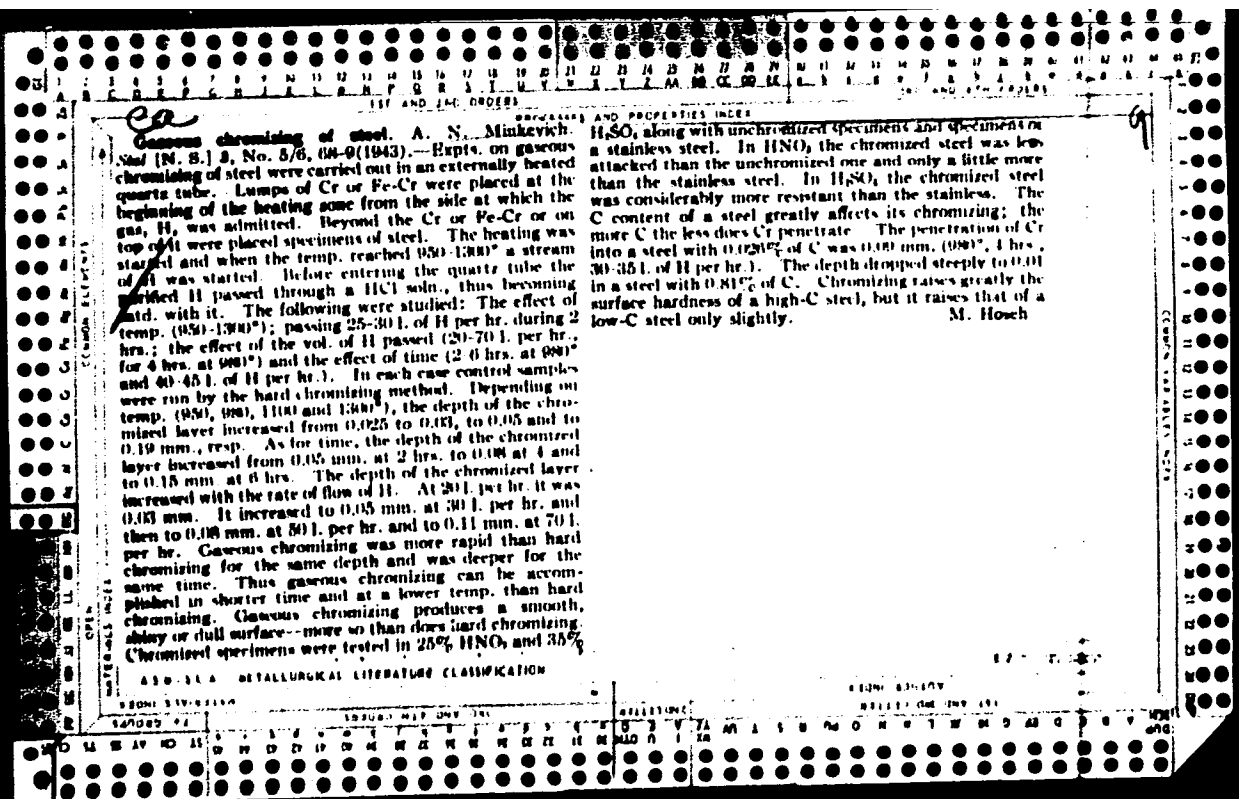
SECTION 96: SILVER

SECTION 97: GOLD

SECTION 98: PLATINUM

SECTION 99: IRIUM

SECTION 100: OSMIUM



MINKEVICH, A. N.

"Chemico-Thermal Treatment of Steel" Gosudarstvennoye Nauchno-Tekhnicheskoye Izdatel'stvo Mashinostroitel'noy Literatury. Moscow (1950). 432 pp.

It is perhaps noteworthy that Dubinin (in "Ceramic Method of Gaseous Chromizing Steel", 1953) considers gaseous methods the most technically perfected means of chromizing; whereas, in 1950, Minkevich stated chromizing in liquid or gaseous media was nonindustrial although this is a difference of viewpoint or a real commercial development that has taken place between 1950 and 1953.

B-77554

MINKEVICH, A.N.

17185 Surface Impregnation of Steel With Beryllium. A.
N. Minkevich. Henry Brewer, Alhambra, Calif. Translation
From book "Surface Impregnation of Steel",
Chapter X. Published by Mashgiz, Moscow, 1950.)
Pack and gas diffusion coating. Effects on hardening, micro-
structure, corrosion, and heat resistance. Micrographs, graphs,
tables. 4 ref.

MINKEVICH, A. IV.

17186 Surface Impregnation of Steel With Molybdenum.
A. N. Minkovych, Henry Bratcher, Altadena, Calif., Translation
from book "Surface Impregnation of Steel".
Chapter XI. Published by Mashgiz, Moscow, 1950.)
Gas and pack molybdizing of Fe and steel. Microstructure.
Micrograph, graphs, 4 ref.

MINKEVICH, A.N.

17157 Surface Impregnation of Steel With Tungsten. A. N. Minkovich, Henry Bratcher, Alhambra, Calif., Translation no. 8848, a part of a book "Surface Impregnation of Steel", Chapter XII. Published by Mashgiz, Moscow, 1950.) Pack, gas, and electrolytic tungstenizing. Microstructure and hardness. Graphs, micrograph, table. 6 ref.

MINKOVICH, A. N.

372 Surface Impregnation of Steel With Vanadium. A. N. Minkovich, Henry Bratcher, Altadena, Calif.. Translation from book "Surface Impregnation of Steel", Chapter XIII. Published by Mashgiz, Moscow, 1950.)
Effect of impregnation time in ferro-vanadium powder upon case depth of vanadized Fe. Microstructure and hardness.
Tables, micrographs, graph.

off

MINKEVICH, A. N. and KALININ, A. T.

"Development of the Process of Liquid Carburizing (Cyaniding) Steel,"
pp 81/99 in Modern Methods of Heat Treating Steel by Dom Inzhenera i Tekhnika
imeni F E Dzerzhinskovo. Gosudarstvennoye Nauchno-Tekhnicheskoye Izdatel'stvo
Mashinostroitel'noy Literatury, Moscow (1954) 404 pp.

Evaluation B-86350, 30 Jun 55

AL'TGAUZEN, O.N., kandidat fiziko-matematicheskikh nauk; BERNSTEYN, M.L., kandidat tekhnicheskikh nauk; BLANTER, M.Ye., doktor tekhnicheskikh nauk; BOKSHTAYN, S.Z., doktor tekhnicheskikh nauk; BOLKHOVITINOVA, Ye.N., kandidat tekhnicheskikh nauk; BORZDYKA, A.M., doktor tekhnicheskikh nauk; BUNIN, K.P., doktor tekhnicheskikh nauk; VINOGRAD, M.I., kandidat tekhnicheskikh nauk; VOLOVIK, B.Ye., doktor tekhnicheskikh nauk [deceased]; GAMOV, M.I., inzhener; GELLER, Yu.A., doktor tekhnicheskikh nauk; GORELIK, S.S., kandidat tekhnicheskikh nauk; GOL'DENBERG, A.A., kandidat tekhnicheskikh nauk; GOTLIB, L.I., kandidat tekhnicheskikh nauk; GRIGOROVICH, V.K., kandidat tekhnicheskikh nauk; GULYAYEV, B.B., doktor tekhnicheskikh nauk; DOVGAL'EVSKIY, Ya.M., kandidat tekhnicheskikh nauk; DUDOVTSYEV, P.A., kandidat tekhnicheskikh nauk; KIDIN, I.N., doktor tekhnicheskikh nauk; KIPNIS, S.Kh., inzhener; KORITSKIY, V.G., kandidat tekhnicheskikh nauk; LANDA, A.F., doktor tekhnicheskikh nauk; LEYKIN, I.M., kandidat tekhnicheskikh nauk; LIVSHITS, L.S., kandidat tekhnicheskikh nauk; L'VOV, M.A., kandidat tekhnicheskikh nauk; MALYSHEV, K.A., kandidat tekhnicheskikh nauk; MEYERSON, G.A., doktor tekhnicheskikh nauk; MINKOVICH, A.N., kandidat tekhnicheskikh nauk; MOROZ, L.S., doktor tekhnicheskikh nauk; NATANSON, A.K., kandidat tekhnicheskikh nauk; NAKHIMOV, A.M., inzhener; NAKHIMOV, D.M., kandidat tekhnicheskikh nauk; POGODIN-ALEKSEYEV, G.I., doktor tekhnicheskikh nauk; POPOVA, N.M., kandidat tekhnicheskikh nauk; POPOV, A.A., kandidat tekhnicheskikh nauk; REKHSHTADT, A.G., kandidat tekhnicheskikh nauk; ROZEL'BERG, I.L., kandidat tekhnicheskikh nauk;

(Continued on next card)

AL'TGAUZEN, O.N.----- (continued) Card 2.

SADOVSKIY, V.D., doktor tekhnicheskikh nauk; SALT'YKOV, S.A., inzhener; SOBOLEV, N.D., kandidat tekhnicheskikh nauk; SOLODIKHIN, A.G., kandidat tekhnicheskikh nauk; UMANSKIY, Ya.S., kandidat tekhnicheskikh nauk; UTEVSKIY, L.M., kandidat tekhnicheskikh nauk; FRIDMAN, Ya.B., doktor tekhnicheskikh nauk; KHIMYSHIN, F.F., kandidat tekhnicheskikh nauk; KHEUSHCHEV, M.M., doktor tekhnicheskikh nauk; CHERNASHKIN, V.G., kandidat tekhnicheskikh nauk; SHAPIRO, M.M., inzhener; SHKOL'NIK, L.M., kandidat tekhnicheskikh nauk; SHRAYBER, D.S., kandidat tekhnicheskikh nauk; SHCHAPOV, N.P., doktor tekhnicheskikh nauk; GUDTSOV, N.T., akademik, redaktor; GORODIN, A.M., redaktor izdatel'stva; VAYNSHTAYN, Ye.B., tekhnicheskiiy redaktor

[Physical metallurgy and the heat treatment of steel and iron; a reference book] Metallovedenie i termicheskaya obrabotka stali i chuguna; spravochnik. Pod red. N.T.Dudtsova, M.L.Bernshteina, A.G. Rakhshadta. Moskva, Gos. nauchno-tekhn. izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1956. 1204 p. (MLRA 9:9)

1. Chlen -korrespondent Akademii nauk USSR (for Bunin)
(Steel--Heat treatment) (Iron--Heat treatment)
(Physical metallurgy)

MINKEVICH A.N.

MINKEVICH, A.N., kandidat tekhnicheskikh nauk; TAYMER, A.D., inzhener; ZOT'YEV, Yu.A., inzhener.

Nitriding titanium in ammonia gas. Metalloved. i obrabot. met. no. 7:39-48 J1
'56. (MIRA 9:9)

1. Moskovskiy institut stali imeni I.V. Stalina.
(Concentration (Metallurgy)) (Titanium)

137-58-6-12795

Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 6, p 229 (USSR)

AUTHOR: Minkevich, A.N.

TITLE: Current Status and Problems in the Field of Thermochemical Treatment (Sovremennoye sostoyaniye i zadachi v oblasti khimiko-termicheskoy obrabotki)

PERIODICAL: V sb.: Sovrem. napravleniya v obl. tekhnol. mashinostr. Moscow, Mashgiz, 1957, pp 290-312

ABSTRACT: In recent years several new carburizable steels have been studied and introduced into production: boron-containing Cr-Mn steel, 20KhGR (0.0045% B), 30KhGT steel with Zr 18KhGTTs and 30 KhGTTs (0.09-0.18% Zr), which differ from similar steels without Zr, such as 15KhGNTA, etc., by a lower tendency towards growth of the grain. For the cementation of steels new carburizers are being used: "sintin", a liquid mixture of hydrocarbons, a by-product of the treatment of solid fuel, and triethanolamine, a colorless fluid containing (weight %) N 9.4, C 48.5, H 10, O 32.1. Included are plans of equipment for the production of neutral gas (diluting gas) and of kilns for the gas cementation and cyanidation of parts.

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137-58-6-12795

Current Status and Problems in the Field of Thermochemical Treatment

Aggregates for rapid gas cementation of gears with high-frequency heating have been developed and introduced into the industry (automobile plant im. Likhachev). [A drawing of the installation is included.] A new process of low-temperature nitriding has been introduced. The possibility of applying rapid nitriding of Mg-cast iron with spheroidal graphite is noted. The wide use in the industry of the processes of carburizing and sulfidizing of steel and cast iron and chromization and boronization of steel are pointed out. In the very near future thermochemical treatment of metals and alloys on nonferrous base will be used widely: nitriding of Ti and surface hardening of Ti by means of oxidation. Among the promising processes to be named are also the thermochemical treatment of steel with heating in the electrolyte by the method of I. Z. Yasnogorodskiy. Bibliography: 24 references.

A.B.

1. Steel--Thermochemistry
2. Steel--Materials
3. Steel--Properties

Card 2/2

Minkevich A. N. 129-12-8/11
AUTHORS: Minkevich, A.N., Candidate of Technical Sciences and
Shul'ga, Yu. N., Engineer.
TITLE: Surface hardening of titanium by treatment in molten borax.
(Poverkhnostnoye uprochneniye titana obrabotkoy v
rasplavlennoy bure)
PERIODICAL: Metallovedeniye i Obrabotka Metallov, 1957, No.12,
pp.53-61 (USSR)
ABSTRACT: The results are described of the study of oxidation of
titanium in molten borax applying electric protection
and borating inside metallic boron powder in vacuum.
The experiments were made with forged titanium, smolten
from commercial titanium in a vacuum furnace with a
graphite crucible, containing 0.5 to 0.6% C; a forged
titanium alloy containing 0.5% W (produced by smelting
of commercial titanium in an arc furnace inside an argon
atmosphere), forged commercial titanium and, finally,
a titanium alloy containing 2.5% Cr and 2% Al. To
prevent oxidation of the titanium in the molten oxygen
containing salts and to protect the surface from
corrosion damage, electro-chemical₂ protection was applied,
the current density being 0.1 A/cm², the voltage
Card 1/5 12 to 15 V, the titanium specimen the cathode and

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Surface hardening of titanium by treatment in molten borax.

graphite rods serving as anodes. After removal from the bath the specimens were covered with a layer of the solidifying borax. The graphs, Fig.1, show the distribution of the micro-hardness with the depth of the diffusion layer for one of the tested alloys as a function of the duration and the temperature of the process; the graph, Fig.2, shows the change with depth of the diffusion layer as a function of the duration of the process at various temperatures; Fig.3 shows the change in the surface hardness of one of the alloys as a function of the duration of the process at various temperatures between 900 and 1050°C. Results of preliminary wear tests on one of the tested alloys are given in Table 1, which show that treatment at 930°C for six hours increases the wear resistance by 37 times as compared to equal non-treated specimens. Results of wear tests of another of the tested alloys are given in Table 2, p.56, and these also show appreciable increases in the wear resistance of treated specimens. Numerous micro-structure photos are included and spectral analysis revealed presence in the surface layer of 12 to 20% B.

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129-12-8/11

Surface hardening of titanium by treatment in molten borax.

The results are also given of tests of borating a titanium alloy containing 5% Cr in metallic boron powder in vacuum. The micro-photo, Fig.7, shows that the diffusion layer consists of three clearly pronounced zones, two of which are bright; the outside non-etched one is separated by a line of division from the inside, slightly etched, zone. The graphs, Fig.8, give the results of experiments of treating titanium in a mixture of 60% borax and 4% B_4C as recommended by N. P. Besedin and M. Ye. Blanter. On the basis of the obtained results, the following conclusions are arrived at: treatment in molten borax applying electric protection is an effective method of surface hardening of titanium and brings about an increase in hardness from $H_{V5} = 250-300$ to

$H_{V5} = 700-950$; the wear resistance of thus oxidized titanium is comparable with that of case hardened or nitrided steel. Treatment of titanium in molten borax reduces the strength and, particularly, the plasticity and toughness, which is attributed to an intensive grain growth in the process of long duration heating and also with surface hardening.

Card 3/5 Titanium can be treated in molten borax at 900 to 930°C

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Surface hardening of titanium by treatment in molten borax.

for three hours with a current density of about 0.1 A/cm^2 . Treatment at higher temperatures and of longer durations involves a sharp increase of the brittleness of the layer and also a reduction of the mechanical properties of the titanium. Treatment of titanium in molten borax brings about mainly oxidation, whilst boration is very slight or even does not occur at all. Bright surface acicules of the diffusion layer forming during such a treatment consist of a solid solution of oxygen and titanium. Hardening from the saturation temperature does not change the acicular character of the micro-structure of the diffusion layer. When treating titanium with molten borax at an elevated temperature (1000 to 1050°C) and high current densities (1.5 to 2.5 A/cm^2) a thin and very hard (2500 H_v) non-etching layer forms at the titanium surface; however, application of such treatment brings about intensive damage of the specimen surface. In the case of borating of a titanium specimen containing $5\% \text{ Cr}$ in boron powder in vacuum at 1000 to 1050°C a diffusion layer forms at the surface containing a thin non-etching surface zone of a high hardness ($\text{H}_v = 1000$ to 1150 , micro-hardness exceeding 2200). The type of the

Card 4/5

Surface hardening of titanium by treatment in molten borax. 129-12-8/11

lattice and the parameters of the surface zone of this layer correspond to the boride TiB ; the disadvantage of this method is the high temperature required for the process. Hardening of the titanium can be effected at $800^{\circ}C$ for durations of 6 to 9 hours in a bath containing borax and boron carbide; however, this method is suitable only for small components and, in addition, the surface hardness increases only by $H_{V5} = 200$ to 250 and by

300 to $500 H_{\mu}$.

D. Barkaya, L. Zaitseva, I. Kokonina and M. Linchevskaya participated in the experiments.
There are 8 figures and 3 tables.

AVAILABLE: Library of Congress.

Card 5/5

MINKOVICH, A.N.

ARISTOV, N.P., kand. tekhn. nauk.; BLAGOSKLONSKIY, T.I., kand. khim. nauk.;
 VESELOVSKIY, V.S., prof., doktor tekhn. nauk.; VLADISLAVLEV, V.S.,
 prof., [deceased]; GOSTENINA, V.M., inzh.; GRINBERG, B.G., kand.
 tekhn. nauk.; KATTS, N.V., kand. tekhn. nauk.; KESTNER, O.Ye., kand.
 tekhn. nauk.; KIDIN, I.N., prof., doktor tekhn. nauk.; KIRSHENSHTEYN,
 Ye.L., inzh.; KITAYGORODSKIY, I.I., prof., doktor tekhn. nauk.;
 KOLOBNEV, I.F., kand. tekhn. nauk.; KRYLOV, V.V., kand. tekhn. nauk.;
 LAKHTIN, Yu.M., prof., doktor tekhn. nauk.; LEVI, L.I., kand. tekhn.
 nauk.; LEPETOV, V.A., kand. tekhn. nauk.; LUNEV, A.A., kand. tekhn.
 nauk.; LUNEV, F.A., kand. tekhn. nauk., [deceased]; LOTSMANOV, S.N.,
 kand. tekhn. nauk.; MAURAKH, M.A., kand. tekhn. nauk.; MINKOVICH,
 A.N., kand. tekhn. nauk.; OCHKIN, A.V., inzh.; POPOV, V.A., kand.
 tekhn. nauk.; RAKOVSKIY, V.S., kand. tekhn. nauk.; SHESTOPAL,
 V.M., kand. tekhn. nauk.; ACHERKAN, N.S., prof., doktor tekhn.
 nauk., glavnyy red.; MALOV, A.N., red.; POZDNYAKOV, S.N., red.;
 ROSTOVYKH, A.Ya., red.; STOLBIN, G.B., red.; CHERMAVSKIY, S.A., red.;
 KRYLOV, V.I., inzh., red.; KARGANOV, V.G., inzh., red. graficheskikh
 rabot.; SOKOLOVA, T.F., tekhn. red.

[Metal worker's handbook in five volumes] Spravochnik metallista v
 piati tomakh. Moskva, Gos. nauchno-tekhn. izd-vo mashinostroit.
 lit-ry. Vol. 3. Book 1. 1958. 560 p. (MIRA 11:11)
 (Metals--Handbooks, manuals, etc.)

SOV/129-59-4-10/17

AUTHORS: Minkevich, A.N. (Candidate of Technical Sciences) and
Ulybin, G.N. (Engineer)

TITLE: Chromating and Borating of Steel, Applying High Frequency
Heating (Khromirovaniye i borirovaniye stali pri
nagreve t.v.ch.)

PERIODICAL: Metallovedeniye i Termicheskaya Obrabotka Metallov,
1959, Nr 4, pp 48-51 (USSR)

ABSTRACT: The authors investigated processes of chromating and
borating steel by means of chromium and boron-containing
pastes and high-frequency heating. The experiments were
carried out with 12 mm diameter specimens of the steels
20, 45 and U 10. The heating was effected with current
supplied by a 60 kW, 350 kc/sec tube oscillator. The
constancy of the temperature was ensured by means of a
photo-electric pyrometer; the distance between the single
turn inductor and the surface of the paste was about
1 - 2.5 mm. The paste consisted of a chromium or boron-
containing powder and a fluxing medium. The following
conclusions are arrived at: 1) For chromating by means
of high frequency heating for a duration of 2 - 3 minutes
at 1050 - 1200°C a paste consisting of 75% chromium powder
or ferro-chromium and 25% cryolite with a hydrolized

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Chromating and Borating of Steel, Applying High Frequency Heating ethyl-silicate as a binder, is suitable. A chromated layer 0.10 mm deep will be obtained by means of this method for steel 20, heated to 1200°C for 2 minutes, as compared to 8 - 10 hours' heating to 1050°C required in the case of the current method of chromating. However, the surface of the specimens is not always as good for this new method of chromating as it is for the ordinary method. 2) For borating of steels by high frequency heating at 1200°C for 2 - 3 minutes, a paste is suitable consisting of 50% boron carbide and 50% cryolite with hydrolised ethyl-silicate as a binder. Borating by means of this method of steels 45 and U-10 brings about the formation of a layer up to 0.12 mm thick with a hardness of about 1000 Hv₁₀. In the surface zone of the borated layer, borides of iron and boron carbide were detected by X-ray analysis. A layer of an equal depth (of a slightly different structure and of a slightly greater hardness) can be obtained by means of electrolysis at 950°C for 2 hours. Borating by means of the here-described method can be applied for

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SOV/129-59-4-10/17

- . Chromating and Borating of Steel, Applying High Frequency Heating
improving wear resistance of components.
3) The here-described method can also be used for other
processes of chemical - heat treatment of steels and
alloys.
There are 3 figures, 2 tables and 9 references, 5 of
which are Soviet, 2 English and 2 Polish.

Card 3/3

MINKEVICH, A. N.

27
PHASE I BOOK EXPLOITATION SOV/5457

Nauchno-tekhnicheskoye obshchestvo mashinostroitel'noy promyshlennosti. Sektsiya metallovedeniya i tekhnicheskoy obrabotki metallov.

Metallovedeniye i tekhnicheskaya obrabotka metallov; trudy Sektsii metallovedeniya i tekhnicheskoy obrabotki metallov (Physical Metallurgy and Heat Treatment of Metals; Transactions of the Section of Physical Metallurgy and Heat Treatment of Metals) no. 2, Moscow, Mashgiz, 1960. 282 p. 6,000 copies printed.

Sponsoring Agency: Nauchno-tekhnicheskoye obshchestvo mashinostroitel'noy promyshlennosti. Tsentral'noye pravleniye.

Editorial Board: G. I. Pogodin-Alekseyev, Yu. A. Geller, A. G. Rakhshadt, and G. K. Shreyber; Ed. of Publishing House: I. I. Lashchenko; Tech. Ed.: B. I. Model'; Managing Ed. for Literature on Metalworking and Machine-Tool Making: V. I. Mitin.

Purpose: This collection of articles is intended for metallurgists, mechanical engineers, and scientific research workers.

Contents: The collection contains articles describing results of research conducted by members of VVO (Scientific Technical Society) of the machine-building industry in the field of physical metallurgy, and in the heat treatment of steel, cast iron, and nonferrous metals and alloys. No personalities are mentioned. Most of articles are accompanied by Soviet and non-Soviet references and contain conclusions drawn from investigations.

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Barabatsky, M. L., Candidate of Technical Sciences, and L. V. Polyanskaya, Engineer. Effect of Cold Working on the Structure and Properties of the VT2 Titanium Alloy	18
Kudin, I. N., Doctor of Technical Sciences, Professor. On the Reasons for the Improvement of Iron-Alloy Properties After High-Frequency Quench Hardening	25
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AVAILABLE: Library of Congress (TN672.N34)	

MINKEVICH, A. N.

"Boriding of Molybdenum, Tungsten, Columbium, and other Metals."
(In the borided layer a microhardness of 2900-3200 Hv and more was
obtained).

Paper presented at the All-Union Conference on Heat Treatment and Metal
Science held in May 1960, Odessa.

MINKEVICH, A.N., kand.tekhn.nauk; KOTOV, A.N., inzh.

Thermochemical treatment of copper and brass for an increase in
surface hardness and scale resistance. Trudy Sek.metalloved.i term.
obr.met.NTO mash.prom. no.2:106-117 '60. (MIRA 14:4)
(Diffusion coating) (Copper--Corrosion)
(Surface hardening)

S/148/60/000/002/008/008

187520

AUTHORS: Minkevich, A.N., Gvozdev, A.G.

TITLE: Titanizing of Steel in a Molten Salt Bath

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy, Chernaya metallurgiya,
1960, Nr 2, pp 151 - 156

TEXT: Information is given on results of experiments on titanizing of 08 and 50 grade steels in a molten salt bath. Titanizing was successfully performed at 950° and 1,100°C during 0.5 - 2 hours in a bath containing 80 - 90% molten sodium chloride and 10 - 20% fine granulated TiO_x alloy (containing about 10% (at.) O_2). Melting and utilization of the bath was conducted under an argon shield. It is desirable in further experiments to investigate the possible utilization of the bath without a shielding gas. It is also recommended to check the possibility of replacing the powder of a specially molten titanium alloy with oxygen by titanium powder contaminated with oxygen to about the required concentration. Without the indicated experiments the recommendation of an extended use of the aforementioned bath will be premature. The titanized layer formed on 08 steel in the bath consists of a

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Titanizing of Steel in a Molten Salt Bath

S/148/60/000/002/008/008

thick layer of columnar grains separated from the core by a boundary line, and of a thin harder external zone. The columnar grains are solid solutions of titanium in α -iron. In a part of this zone, adjacent to the external thin zone, sometimes the separation of excessive titanides, precipitating during slow cooling, was observed. Data of spectral analysis, carried out under the supervision of V.G. Koritskiy, show that the external zone contains about 30% titanium. According to data from X-ray analysis, the external zone of the layer on O8 grade steel is FeTi_2 titanide; on 50 grade steel it is titanium carbide, TiC . The titanized layer formed on the steel in the investigated bath has high corrosion and acid resistance. There are: 4 graphs, 2 sets of microphotos, 1 table and 7 references, 2 of which are Soviet and 5 English.

ASSOCIATION: Moskovskiy institut stali (Moscow Steel Institute)

SUBMITTED: October 6, 1958

Card 2/2

83293

2308/only 18.7500
2208/only

S/148/60/000/007/014/015
A161/A029

AUTHORS: Minkevich, A.N.; Rastorguyev, L.N.; Andryushechkin, V.I.

TITLE: Diffusion Boride Layers on Metals

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Chernaya metallur-
giya, 1960, Nr 7, pp 171-179

TEXT: Boride layer formation by diffusion on Mo, W, Nb, Zr and Ta was
experimentally investigated. Three different boron-containing media were
used: a molten borax bath (60% borax and 40% B₂C), powdered boron carbide
and powdered boron metal. References are made to previous investigations,
data of which were used /Ref 1-8/. The molten bath was used with a
temperature of 1,100-1,300°C; boration in powder was carried out in vacuum
with 1,300-1,500°C. The microstructures of boride layers are shown (Figure
4) in photographs, viz. microstructures after bath boration in the upper
row, after boration in powder in the bottom row. The boride layers were
0.20 to 0.45 mm deep and had 1,300-2,000 Vickers hardness (with 5 kg load),
and microhardness of 2,300-2,900 and higher. The most effective means

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83293

S/148/60/000/007/014/015
A161/A029

Diffusion Boride Layers on Metals

proved to be boron metal; borax bath with 40% boron carbide had somewhat lesser effect, and boron carbide powder the least. Formation of phases was observed which are absent in the equilibrium state (TA_2B_5). Boration raised the acid resistance of molybdenum in nitrohydrochloric acid 15 times and of zirconium 12 times (in 21 hours at $20^{\circ}C$). The resistance to scale formation increased 21 times for Zr, 31 times for Ta and 14 times for Ti. The wear resistance of borated metals was dozens of times higher than that of non-borated ones and exceeded the wear resistance of case-hardened and quenched steel. The friction coefficient was reduced 1.5-2.0 times. There are 5 figures, 4 tables and 8 references: 4 are Soviet and 4 English. X

ASSOCIATION: Moskovskiy institut stali (Moscow Steel Institute)

SUBMITTED: January 15, 1960

Card 2/2

11800

26569
S/129/61/000/008/002/015
E197/E335

AUTHOR: Minkevich, A.N., Candidate of Technical Sciences

TITLE: Diffusion-formed Boride Layers on Metals

PERIODICAL: Metallovedeniye i termicheskaya obrabotka metallov,
1961, No. 8, pp. 9 - 15 - 1 plate

TEXT: Growing interest in borides as engineering materials can be attributed to their outstanding wear-resistance, coupled with hardness higher and brittleness somewhat lower than that of carbides, nitrides and silicides. The object of the present investigation was to study the properties of boride layers formed on various materials in relation to the conditions which exist during their formation. Sintered Mo, W and Nb, cast and forged Ta, Re and Fe, and electrolytic Ni were used in the preparation of the experimental specimens. The surface boride layers were formed on these metals by four different methods:
1) by heating in a bath of molten borax containing approx. 40% boron carbide; 2) by heating in vacuum (5×10^{-4} mm Hg) in contact with boron carbide; 3) as in method (2) but with boron

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Diffusion-formed

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S/129/61/000/006/002/015
L192/E335

powder used as the boriding medium, 4) by electrolysis in molten borax. The temperature of the process was chosen to be below the minimum solidus temperature of any particular metal-boron system. X-ray diffraction analysis of the boride layers formed on Co and Fe showed that the kinetics of the process was the same in both cases. Needle-like crystals of Fe_2B and Co_2B were formed first; they had a tetragonal lattice and approx. the same (8.8 and 8.9%, respectively) boron content. As the concentration of boron in the surface layer increased, needles of FeB or CoB (containing 16.0 and 15.5% B, respectively) were formed. FeB and CoB had microhardness values of 2 000 and 1 850 kg/mm^2 , the corresponding figures for Fe_2B and Co_2B being 1 850 and 1 550 kg/mm^2 . In Fig. 3 the microhardness (kg/mm^2) of the surface boride layers, formed on Co at 950 °C, is plotted against the distance (mm) from the surface; diagrams (a) and (b) relate to specimens with boride layers formed respectively by 3 and 6 hours treatment in a molten borax-boron carbide mixture (Curves K) and by electrolysis in molten borax (Curves J). It will be seen from Fig. 3 that the electrolytic method is more

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S/129/61/000/008/002/015

E193/E335

Diffusion-formed

efficient since in 3 h it produced a boride layer containing both Co_2B and CoB , whereas only Co_2B was formed by 6 h diffusion from the borax/boron carbide mixture. In Fig. 5 the thickness (mm, top diagram) of the boride layer formed on various metals (indicated by each curve), Brinell hardness (kg/mm^2 , middle diagram) and microhardness (kg/mm^2 , bottom diagram) are plotted against the duration of the process (hours at 1400°C , lefthand-side diagrams) and against its temperature ($^\circ\text{C}$, righthand-side diagrams). the duration of the process in the latter case being 2 h. Fig. 6 shows how the microhardness (kg/mm^2) of boride layers formed on the surface of various metals (as indicated by each curve) varied with the distance (mm) from the surface. In this case, the boride layers were formed by vacuum treatment in boron carbide. the three graphs (from left to right) relating to specimens obtained, respectively, by 2, 4 and 6 h treatment. The following conclusions were reached from the results shown in Figs. 5 and 6. (1) Irrespective of the conditions during the boriding treatment, the thickest boride layer is obtained on Mo, much thinner on W and Nb and thinnest

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Diffusion-formed

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0193/E335

on Zr, Ta and Re. 2) boride layer formed on Ta is the hardest (Brinell hardness of 2 000 - 2 200 kg/mm², microhardness of 3 000 - 3 200 kg/mm²). 3) In most cases, the surface hardness of boride layers increases with increasing duration and temperature of the boriding treatment. X-ray diffraction analysis of boride layers formed by vacuum diffusion from boron carbide (1 h at 1 400 °C) showed them as having the following constitution: Mo₂B₅ and Mo₂B (weak lines) on Mo; W₂B₅ (weak lines), and WB (very weak lines) on W; NbB₄ and Nb₂B₄ (weak lines) on Nb; ZrB₂ and Zr₂B (weak lines) on Zr; Ta₂B on Ta; ReB on Re. The constitution of boride layers, formed in a molten borax/boron carbide mixture, was similar except that the X-ray lines of the boron-rich constituents were stronger. Comparison of the microstructure of boride layers, formed on

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S/129/61/000/008/002/015
E193/E335

various metals, showed that the needle-like crystals are formed on Fe, Co and Ni only; in all other cases, the diffused boride layers have a monolithic structure. The wear resistance of the materials studied was measured on an Amsler machine under a load of 50 kg. The experiments consisted of rotating ring-shaped specimens of hardened steel Y10 (U10) (Rockwell hardness - 62 C), pressed against similar specimens of borided metals or carburized steel 30X11 (30KhGT) (Rockwell hardness - 62 to 64 C) and measuring the weight loss after 2 h testing (without lubrication). The wear-resistance of borided metals was found to be considerably higher than that of other materials. the weight losses (g/m²) of specimens tested being: 0.046 on carburized steel 30 KhGT; 0.024 on borided steel U10; 0.0175 on borided tungsten; 0.0148 on borided molybdenum; 0.012 on borided niobium. Heat-resistance of borided metals was studied by examining the surface condition and measuring the changes in weight of specimens, held for 24 h at 950 °C. Although borided metals showed considerable improvement in comparison with untreated specimens, it was found that boriding offers no

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Diffusion-formed

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S/129/61/000/008/002/015
E193/E335

effective protection against oxidation at elevated temperatures. The results of the next series of tests in which borided and untreated specimens were held for 21 h in a HCl/HNO_3 mixture at 20°C showed that the resistance of Mo and Zr to the corrosive action of this medium was increased after the boriding treatment by a factor of 15 and 12, respectively. Finally, the hot hardness of some borided metals was measured. The results are reproduced in Fig. 8, where Vickers hardness (kg/mm^2) of borided Mo and Nb is plotted against the test temperature ($^\circ\text{C}$) side-by-side with similar curves, constructed for cemented carbides T5K10, T15K6, BK3 (VK3) and BK6 (VK6), and a high-speed cutting steel $\phi 18$ (R18). V.I. Andryushechkin, Ye.V. Akulinichev, N.F. Shur and L.N. Rastorguyev participated in this work. There are 8 figures and 15 references: 1 Soviet and 4 non-Soviet. The three English-language references quoted in the text are: Ref. 7 - A.B. Laubengauer, D.H. Hard, A.E. Neweira - J. Am. Chem. Soc., No. 63, 1943; Ref. 8 - I. Kompbell, C. Powell, D. Novick, B. Conser - J. Electrochem. Soc., v. 96, 1959; Ref. 9 - W. Beck - Metal Industry, v. 86, 1955.

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Diffusion-formed

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S/129/61/000/008/002/015
E193/E335

ASSOCIATION: Moskovskiy institut stali (Moscow Steel Institute)

Fig. 3:



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MINKEVICH, Anatoliy N.

"The enrichment in boron of cobalt and cobalt alloys"
Report to be submitted for the Ninth International Discussion on
Heat Treating, Lausanne, Switzerland, 28-30 May 1962

Institute of Steel, Moscow

MINKEVICH, A. N.

AID Nr. 985-9 7 June

D. K. CHERNOV, AND N. A. MINKEVICH PRIZES FOR 1962 (USSR)

Golovin, A. F., and A. N. Minkevich. Metallovedeniye i termicheskaya obrabotka metallov, no. 4, Apr 1963, 63-65. S/129/63/000/004/014/014

The Scientific and Technical Society of the Machine-Building Industry has announced the results of the All-Union Competition for the Chernov and Minkevich prizes for 1962. The first Chernov prize was awarded to Yu. A. Bagaryatskiy, G. I. Nosova, and T. V. Tyagunova for studies in the x-ray diffraction analysis of the phase transformation in titanium alloys and the structural mechanism of alloy aging. The authors discovered previously

Card 1/2

AID Nr. 985-9 7 June

D. K. CHERNOV. AND N. A. MINKEVICH (Cont.)

8/129/63/000/004/014/014

unknown α " and ω phases which have a significant effect on the mechanical properties of titanium alloys. The second Minkevich prize [a first prize was not awarded for 1962] was awarded to N. I. Korneyev, V. F. Kalugin, Yu. N. Kabanov, S. B. Pevzner, and I. G. Skugarev for their work "Development of the thermomechanical processes of steel strengthening by rolling and pressing." The authors determined the optimum conditions of thermomechanical treatment for structural steels and suggested and tested a low-temperature thermomechanical treatment (ausforming) by rolling in envelopes. They also studied the effect of the number of passes in rolling on the work hardening of supercooled austenite. Ausforming has been introduced into industrial practice. [AZ]

Card 2/2

L 11199-63

ACCESSION NR: AP3001380

EWP(q)/EWT(m)/BDS--AFFTC/ASD--JD

S/0148/63/000/005/0162/0167

AUTHOR: Minkevich, A. N.

TITLE: Structure of boride layers

SOURCE: IVUZ. Chernaya metallurgiya, no. 5, 1963, 162-167

TOPIC TAGS: boride layers, iron, carbon steel, surface treatment, martempering

ABSTRACT: The structure and properties of boride layers forming on iron and carbon steel were studied. From determination of stresses formed, it was found that boride bath layers do not decrease surface stresses after hardening. Rather, the degree of distension which develops is a function of gage of steel and other factors. Surface treatment or martempering of boride bathed steel is recommended in order to decrease stresses. Orig. art. has: 6 figures.

ASSOCIATION: Moskovskiy institut stali i splavov (Moscow Institute of Steel and Alloys)

SUBMITTED: 10Aug62

DATE ACQD: 01Jul63

ENCL: 00

SUB CODE: 00

NO REF SOV: 004

OTHER: 002

Card 1/1 18/117/1

DUBININ, G.N.; BOKSHEYN, S.Z., doktor tekhn. nauk, prof., retsenzent;
GRIBOYEDOV, Yu.N., kand. tekhn. nauk, retsenzent; MINKEVICH,
A.N., kand. tekhn. nauk, red.

[Diffusion chromizing of alloys] Diffuzionnoe khromirovanie
splavov. Moskva, Mashinostroenie, 1964. 450 p.
(MIRA 17:11)

L 24889-65 EWT(m)/EWA(d)/T/ENP(t)/ENP(b) IJP(c) JD/JG/WB/MLK

ACCESSION NR: AT5002787

S/0000/64/000/000/0221/0225

23

AUTHOR: Minkevich, A. N.; Tylkina, M. A. (Candidate of technical sciences);
Rastorguyev, L. N.; Rodionova, G. P.

B+1

TITLE: Thermochemical treatment of rhenum, 1

SOURCE: Vsesoyuznoye soveshchaniye po problema reniya. 2d, Moscow, 1962. Reniy (Rhenium); trudy soveshchaniya. Moscow, Izd-vo Nauka, 1964, 221-225

TOPIC TAGS: rhenum, rhenum diffusion coating, rhenum coating, rhenum chromiz-
ing, rhenum boronizing, rhenum aluminizing, rhenum siliconizing, diffusion coat-
ing property, rhenum oxidation, 6

ABSTRACT: Certain properties and structures of diffusion layers formed by impregna-
tion of rhenum with chromium, boron, aluminum, and silicon have been investigated.
Aluminizing, chromizing, and siliconizing of rhenum were done by pack cementation
at 1000, 1100, and 1200C in a mixture of 40 parts chamotte powder, 60 parts of the
respective metal powder, and 3 parts ammonia chloride. Boronizing was done at 1000
and 1200C in a fused-salt bath consisting of 70% sodium tetraborate and 30% boron-
carbide powder, or by pack cementation at 1400C in boron-carbide powder in a vacuum

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L 24889-65

ACCESSION NR: AT5002787

furnace, Diffusion layers with clearly visible boundary lines were formed in all media tested. Boronized case was 0.06—0.14 mm thick and consisted of two layers, Re_7B_3 compound inside and ReB_3 compound outside. The highest hardness, $H_v = 1200 \text{ kg/mm}^2$, was obtained by pack cementation at 1400C. Siliconized case contained ReSi_2 and ReSi silicides. Its hardness was $927 = 1400 \text{ kg/mm}^2$. Chromizing yielded an α -phase case of rhenium solid solution in chromium. A diffusion layer containing Al_2Re_3 and Al_2Re compounds was formed by aluminizing. Oxidation-resistance tests carried out at 800C for 10 hr showed that chromized rhenium has the highest resistance (see Fig. 1 of the Enclosure). Orig. art. has: 3 figures and 2 tables. [ND]

ASSOCIATION: none

SUBMITTED: 05Aug64

ENCL: 01

SUB CODE: 1C, MM

NO REF SOV: 003

OTHER: 001

ATD PRESS: 3181

Card 2/3

MINKEVICH, A.N.

Trends in the development of thermochemical processes for the
treatment of metals and alloys. Metalloved. i term. obr. met.
no.3:4-9 Mr '64. (MIRA 17:4)

E-11305-65 ENT(m)/EWA(d)/ENP(t)/ENP(b) MJW/JD

ACCESSION NR: AT4043506

S/3107/64/000/003/0030/0041

AUTHOR: Minkavich, A. N. (Candidate of technical sciences, Docent);
Shur, N. P. (Engineer); Trekalo, A. S. (Engineer)

TITLE: Boriding of cobalt and cobalt-base alloys (2)

SOURCE: Nauchno-tekhnicheskoye obshchestvo mashinostroitel'noy
promyshlennosti. Sektsiya metallovedeniya i termicheskoy obrabotki.
Metallovedeniya i termicheskaya obrabotka, no. 3, 1964, 30-41

TOPIC TAGS: cobalt boriding, cobalt alloy boriding, boriding layer
composition, boriding layer structure, boriding layer hardness,
boriding layer corrosion resistance, boriding layer wear resistance

ABSTRACT: The possibility of increasing the hardness of cobalt and
cobalt-base K40KhM, K40Kh20, and 36KhTiYu alloys by boriding has
been studied. Boriding was done by electrolysis in molten borax at
930-1100C;

been studied. In molten borax with 30-40 wt% boron carbide at 950-1000, the boriding process lasted up to 6 hr. It was found that boriding of Co by the second method took about twice as long as the first method, but it produced a clean surface. The borided layer, 0.24 mm

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L 11305-65

ACCESSION NR: AT4043506

3

thick after 3-hr boriding at 1000C, consisted of an outer layer of CoB boride with 15.51% boron; it had a rhombic lattice and a microhardness of H_{100} 1800. An inner layer of Co_2B boride with 8.41% B, located at a depth of 0.07 mm below the surface, had a tetragonal lattice and a microhardness of H_{100} 1550. Boriding of Co-base alloys proceeds at a slower rate than boriding of Co, e.g., boriding at 1000C for 3 hr produced a borided layer 0.03 mm thick on K40NKHM alloy and 0.05 mm thick on K40Kh20 alloy. The borided layers on these alloys had approximately the same microhardness, H_{100} 2300. The thickness of the borided layer and the magnetic susceptibility of the alloys increased with increased boriding time. Boriding also increased the wear resistance of cobalt and its alloys. For example, a 6-hr boriding at 1000C increased the wear resistance of Co 48 times, of K40KhNM alloy, 70 times, and of K40Kh20 alloy, more than 100 times. However, the corrosion resistance of borided alloys under tropical conditions is noticeably lower than that of unborided alloys. Orig. art. has: 8 figures and 6 tables.

APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R001134420009-7"

ASSOCIATION: Nauchno-tekhnicheskoye obshchestvo mashinostroitel'noy promyshlennosti (Scientific Technological Society of Machine Construction Industry)

promy*shlennosti (Scientific Technological Society of Machine Construction
Industry)
Card 2/3

L 11305-65

ACCESSION NR: AT4043506-05

SUBMITTED: 00

ATD PRESS: 3108 ENCL: 00

SUB CODE: HM

NO REF SOV: 005 OTHER: 000

L 26095-65 EWT(m)/EPF(n)-2/T/ENP(t)/ENP(b) Fu-4 IJP(c) JD/JG

ACCESSION NR: AP4049075

S/0148/64/000/011/0185/0188

AUTHOR: Shcherbedinskaya, A.V.; Minkevich, A.N.

TITLE: Diffusional saturation of molybdenum with carbon ✓

SOURCE: IVUZ. Chernaya metallurgiya, no. 11, 1964, 185-188

TOPIC TAGS: molybdenum saturation, carbon diffusion, diffusional saturation, molybdenum carbide, molybdenum diffusion ✓

ABSTRACT: The article reports the results of a study of the diffusion of carbon in molybdenum carbide. The diffusional saturation of the latter was carried out with C14-labeled BaCO₃. Subsequent radiometric layer analysis yielded the concentration curves of the distribution of carbon in molybdenum carbide. The diffusion coefficients varied in the range 900-1600°C. They formed a straight line in the

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B

curves of the distribution of carbon in molybdenum carbide. The diffusion coefficients of carbon were determined in the range 900-1600C. They formed a straight line in the coordinates $\log D - 1/T$; from the slope of this curve, the activation energy was found to be 67000 ± 5400 cal/g-at. To elucidate the mechanism of carbide formation, the authors also studied the diffusion of radioactive molybdenum Mo^{99} in molybdenum carbide, and concluded that when the latter is formed in the carbon - molybdenum system, the predominant diffusion is that of carbon. Orig. art. has: 3 figures, 1 table, and 2 formulas.

Card 1/2

L 26095-65

ACCESSION NR: AP4049075

ASSOCIATION: Moskovskiy institut stali i splavov (Moscow Steel and Alloys Institute)

SUBMITTED: 21Jul64

ENCL: 00

SUB CODE: MM

NO REF SOV: 001

OTHER: 001

Card 2/2

L 23223-66 EWT(m)/T/EWP(t) LJP(c) JD/HW

ACC NR: AP6013599

SOURCE CODE: UR/0148/65/000/001/0095/0098

AUTHOR: Shovensin, A. V.; Minkevich, A. N.; Shcherbedinskiy, G. V. 49
13

ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov)

TITLE: Diffusion of carbon into cobalt and nickel

SOURCE: ^{44.55, 18} ²⁷ ^{44.55, 27} ^{44.55, 27} Izvestiya vysshikh uchebnykh zavedeniy. Chernaya metallurgiya, no. 1, 1965, 95-98

TOPIC TAGS: cobalt, nickel, austenite, carbon, radioisotope, metal diffusion, radioactivity measurement

ABSTRACT: In connection with the influence of alloying elements on the diffusion of carbon into austenite, the authors studied the diffusion of carbon into alloying elements cobalt and nickel in the range of 700-1000°C. Radioactive carbon C14 was used, and the distribution of concentration per depth was measured. The conditions of homogenizing, to which the samples of cobalt and nickel were subjected, and the corresponding diffusion coefficients are tabulated. These data were used to plot the temperature dependence of the diffusion coefficients of carbon in cobalt and nickel. The values of the free energy Q and pre-exponential coefficient D₀ obtained from these plots differ from those given in the literature, and the authors defend their results by pointing out the improvements involved in their approach to the problem. Orig. art. has: 4 figures, 3 formulas, and 1 table. [JPRS]

SUB CODE: 11, 18 / SUBM DATE: 16Dec63 / ORIG REF: 003 / OTH REF: 002

Card 1/1 ⁴⁴

UDC: 669.24: 669.25

L 9639-66 EWT(m)/EWA(d)/T/EWP(t)/EWP(z)/EWP(b)/EWA(c)		MJW/JD
ACC NR: AP5027710		SOURCE CODE: UR/0129/65/00/011/0037/0038
AUTHOR: <u>Semenova, G. A.</u> ; <u>Minkevich, A. N.</u> ; <u>Panchenko, Ye. V.</u> ; <u>Maslenkov, S. B.</u>		
ORG: <u>Moscow Institute of Steel and Alloys</u> (Moskovskiy institut stali i splavov)		
TITLE: <u>Titanium carbide coatings deposited on steel</u>		
SOURCE: <u>Metellovedeniye i termicheskaya obrabotka metallov</u> , no. 11, 1965, 37-38, and top half of insert facing p. 41		
TOPIC TAGS: metal coating, carbide, titanium compound, metal bonding, <u>metal diffusion</u> , steel, annealing		
<p>ABSTRACT: A study of the deposition of TiC coatings on steel is presented. Specimens of 08 kp¹ steel were coated with TiC in a current of H₂, vapors of TiCl₄ and benzene, in a tubular furnace, at 1100°C for 0.5 hr. To improve the adhesion of the coating to the steel, the specimens were subsequently diffusion-annealed in H₂ atmosphere for 6 hr. After this, measurements of microhardness and micro-thermo-e.m.f. as well as laminar X-ray spectral chemical analysis were carried out. Findings: Fe was discovered in the TiC layer in the amount of 12% at the depth of 3 μ from the coating-base metal boundary and in the amount of 0.8% at 6 μ depth. Ti, on the other hand, penetrated into steel to a depth of more than 5 μ from the interface. Some limited decrease in microhardness of the coating with depth was detected. Since, intermediate coatings of</p>		
Card 1/2	UDC: 621.357.76:669.14.018	

L 9639-66

ACC NR: AP5027710

galvanically deposited metals greatly affect the bonding of deposited coating to the base metal, corresponding experiments also were performed. In this case it was found that the hardness of TiC does not vary with depth. This may be attributed to the formation of TiCr at the TiC-Cr boundary. Below that line hardness gradually decreases owing to the change in the solid-solution concentration of Cr in Fe. The visible interface corresponds to the boundary between the α - and γ -phases at annealing temperature (1000°C in this case). Thus, the deposition of TiC on steel and subsequent diffusion annealing result in a redistribution of elements in the boundary regions, which contributes to a stronger bonding of coating to base. The micro-thermo-e.m.f. method is a good complement to the regular methods of investigating diffusion processes. Orig. art. has: 2 figures.

SUB CODE: 11, 13/ SUM DATE: none/ ORIG REF: 001/ OTH REF: 000

Card

9c
2/2

L 13531-66 EWT(m)/EPF(n)-2/T/EP(t)/EP(b)/EWA(c) IJP(c) JD/JG

ACC NR: AP5028980

SOURCE CODE: UR/0149/65/000/004/0123/0125

AUTHOR: Shcherbedinskaya, A. V.; Minkevich, A. N.

ORG: Moscow Institute of Steel and Alloys, Metal Science of Steel and High Strength Alloys Dept (Moskovskiy institut stali i splavov, Kafedra metallovedeniya stali i vysokoprochnykh splavov)

TITLE: Diffusion of ²⁷carbon in the carbides of ²⁷niobium and ²⁷titanium ^{27,44,55}

SOURCE: IVUZ. Tsvetnaya metallurgiya, no. 4, 1965, 123-125

TOPIC TAGS: thermal diffusion, carbon, titanium, niobium, periodic system, activation energy

ABSTRACT: A comparison of the ¹⁶diffusion parameters of nonmetals in refractory metals as a function of their position in the periodic table is of interest. In this connection, the article presents the results of an investigation of the diffusion of C in ²⁷elements located in different groups of the periodic table: Ti (IV), Nb (V) and ²⁷Mo (VI). The findings on the diffusion of C in Mo are presented in another study (A. V. Shcherbedinskaya, A. N. Minkevich, Izv. VUZ, Chernaya metallurgiya, no. 11, 1964). The diffusion coating of Nb and Ti with C was performed at 900-1500°C in a mixture of acti-

Card 1/2

UDC: 669.293+669+295

L 13531-66

ACC NR: AP5028980

vated carbon and BaCO_3 containing the radioactive isotope C^{14} , with subsequent radio-metric analysis of the obtained carbide coatings and plotting of the concentration curves for C throughout the diffusion zone. After this, the diffusion coefficients were calculated from the concentration curves. It is established that the activation energy for the diffusion of C in the carbide of Ti (element of group IV) is higher ($E = 83,000$ cal/g-atom) than in the carbides of Nb ($E = 64,500$ cal/g-atom) and Mo (groups V and VI, respectively), which is in qualitative agreement with Dempsey's (Philos. Mag., 8, no. 86, 1963) theory of the electron structure of transition metals which claims that the maximum melting point is inherent in the compounds for which the number of d-electrons per atom is ≈ 6 and that formation of solid compounds with elements of group IV results in the increase in the number of d-electrons per atom to its optimal value (≈ 6) and hence also in a corresponding sharp increase in melting point. For elements of group VI, which have the optimal number of electrons per atom, the formation of chemical compounds is associated with the increase in this number and decrease in their melting points. Orig. art. has:

SUB CODE: 07, 11, 20/ SUBM DATE: 10Apr64/ ORIG REF: 003/ OTH REF: 002

Card 2/2

L 12077-66 EWP(e)/EWT(m)/EWA(d)/EWP(t)/EWP(z)/EWP(b) MJW/JD/WH
ACC NR: AP6000177 UR/0148/65/000/009/0168/0170

AUTHOR: Semenova, G. A.; Minkevich, A. N.

ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov)

TITLE: Deposition of titanium carbide from gaseous phase onto the surface of steel

SOURCE: IVUZ. Chernaya metallurgiya, no. 9, 1965, 168-170

TOPIC TAGS: metal deposition, titanium carbide, hydrogen, benzene, metal coating, tool steel, titanium compound / Kh12 tool steel

ABSTRACT: In view of the great difference in the thermal expansion coefficients of TiC and various steels ($\alpha_{TiC} = 7.74 \cdot 10^{-6}$ 1/deg against $\alpha = 10 \cdot 10^{-6}$ or $20 \cdot 10^{-6}$ 1/deg), the steel chosen as the substrate for the deposition of TiC was Kh12/tool steel with an expansion coefficient extremely close to that of TiC ($\alpha_{Kh12} = 10 \cdot 10^{-6}$ 1/deg). TiC was obtained from the following source reagents: $TiCl_4$, H_2 and C_6H_6 . The deposition was carried out in a quartz tube of 22 mm diameter placed in a continuous furnace with silic heaters. H_2 was dried with P_2O_5 . Reagent vapors were admitted to the reaction tube by passing H_2 through $TiCl_4$ and C_6H_6 . The deposition of TiC on the steel specimens was carried out for 30 min at $1100^\circ C$, with subsequent measurements of the thickness and microhardness of the coating. Based on the experimental findings, the optimal regime of TiC deposition corresponds to a H_2 feed rate of $v_{H_2} = 0.8$ liter/min.

Card 1/3 UDC: 669.14-16

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ACC NR: AF6000177

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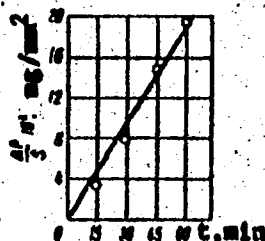


Fig. 1. Weight gain of specimens as a function of duration of the process of TiC deposition (temperature 1100°C)

Card 2/3

L 12077-66

ACC NR: AP6000177

and a partial pressure of reagent vapors amounting to $P_{TiCl_4} = 2.5 \cdot 10^{-2}$ atm and

$P_{C_2H_6} = 1.5 \cdot 10^{-2}$ atm. The shape of the curve of the time dependence of the weight gain of specimens (Fig. 1) indicates that formation of the carbide coating occurs owing to its accretion from the gaseous phase without participation of the substrate material. The coating may be one micron to several millimeters thick depending on duration of the process. Thin carbide films (of the order of 10μ) do not crack regardless of the cooling rate, while thicker films are crackproof only if the cooling rate is very slow. The deposited TIC represents a compact layer that satisfactorily adheres to the metal surface and has a microhardness of 3500 kg/mm^2 . Orig. art. has: 4 figures.

SUB CODE: 11, 13/ SUM DATE: 20Nov64/ ORIG REF: 001/ OTH REF: 002

Card

3/3

L 28513-66 EWT(m)/T/EMP(t)/ETI LJP(c) JD/WB

ACC NR: AP6016593 (A,N)

SOURCE CODE: UR/0129/66/000/005/0049/0052

AUTHORS: Sorokin, Yu. V.; Minkevich, A. N.

ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov)

TITLE: Nitriding steel in a mixture of nitrogen and ammonia

SOURCE: Metallovedeniye i termicheskaya obrabotka metallov, no. 5, 1966, 49-52

TOPIC TAGS: alloy steel, metallurgic process, nitrification, nitridation, corrosion resistance/ 4Kh14N14V2M alloy steel, 25Kh18N8V2 alloy steel, Kh17G9AN4 alloy steel, 38KhMYuA alloy steel, 35KhMYuA alloy steel

ABSTRACT: The effect of nitriding the alloy steels 4Kh14N14V2M, 25Kh18N8V2, Kh17G9AN4, 38KhMYuA, and 35KhMYuA in a mixture of 20--30% ammonia and 80--70% nitrogen on the hardness, brittleness, depth, and corrosion stability of the nitride layer was investigated. The microstructure of the surface layer was also studied. The experimental results are presented in graphs and tables (see Fig. 1). Dilution of ammonia with nitrogen (up to 80% nitrogen) had no effect on the hardness or depth of the nitride layers and slightly increased the corrosion stability and fatigue limit. The results of corrosion experiments are in good agreement with the results of A. G. Andreyeva and L. Ya. Gurevich (MITOM, 1959, No. 4). It is concluded that the best nitriding results are obtained with a mixture of 20--30% ammonia and 80--70% nitrogen.

Card 1/2

UDC: 621.785.53:546.17:546.171.1

L 28513-66

ACC NR: AP6016593

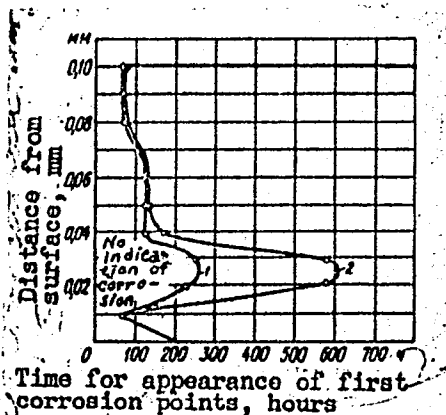


Fig. 1. Change in the corrosion stability along the depth of the nitride layer in steel 4Kh14N14V2M exposed to sea water.
1 - nitriding in ammonia (depth of layer 0.1 mm);
2 - in mixture of 70% N₂ + 30% NH₃.

Orig. art. has: 1 table and 3 figures.

SUB CODE: 11, 07/ SUBM DATE: none/ ORIG REF: 002/ OTH REF: 001

Card 2/2 C ✓

L 44396-66 EWT(m)/T/EWP(t)/ETI IJP(c) JD

ACC NR: AP6024529

SOURCE CODE: UR/0148/66/000/007/0143/0146

AUTHOR: Rastorguyev, L. N.; Kovalev, A. I.; Minkevich, A. N.

ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov)

TITLE: Structure of the diffusion layer in carboantimonized steel

SOURCE: IVUZ. Chernaya metallurgiya, no. 7, 1966, 143-146

TOPIC TAGS: antimonide, surface hardening, metallographic examination, microhardening, x ray diffraction analysis, crystal orientation, thermal emf

ABSTRACT: Carboantimonizing of type 20 steel and Armco iron was studied and compared with the more typical cementizing process. All samples were treated in a Bandyuzhskiy carbonizer at 950°C for 6 hrs. A mixture of 10% Na₂CO₃ and 0.75% Sb₂O₃ was added for carboantimonizing; 10% Na₂CO₃ was added for cementizing. Microstructures showed a light-etching layer in the carboantimonized samples which was harder and thinner than the cementized layer. The microthermal emf method developed at the Moscow Institute of Steel and Alloys was used to study the diffusion layers. Antimony decreased the electronegativity of microthermal emf and above 2.7% Sb, the microthermal emf became more positive ($E=0.7$ v/°C at 3.25% Sb). Changes in microthermal emf are given as functions of layer thicknesses for cementing and carboantimonizing, the latter with 0.75% and 2.5% Sb₂O₃ added to the carbonizer. The Sb content of the layer was greater for 2.5%

UDC: 669.18.046.56:669.75:621.785.53

Card 1/2

L 44396-66

ACC NR: AP6024529

Sb₂O₃ additions. The drop in microthermal emf from the periphery to the center indicated a decrease in Sb and C content; this was confirmed by microprobe analysis. The Fe distribution rose from 10% at the surface to 100% at 120 μ. After water quenching from 850°C, the carboantimonized surface layers reached a Shore hardness of 1000 Hv, which was 100-200 Hv higher than for cemented layers. This was attributed to the presence of FeSb and FeSb₂ phases, confirmed by x-ray powder analysis. Calculated cell volumes of both phases were 7-10% lower than the equilibrium values, due to the supersaturation of Sb in the phases formed by diffusion. No preferred orientation was found in the diffusion surfaces since no preferential diffusion path existed for Sb. Microthermal emf experiments were carried out in consultation with Ye. V. Panchenko, microprobe analysis was done at TsNIICHM by S. B. Maslenkin. Orig. art. has: 3 figures, 1 table.

SUB CODE: 11,20 /

SUBM DATE: 11Apr64/

ORIG REF: 005/

OTH REF: 001

Card 2/2 *ech*

L 09133-67 EWT(m)/EWP(t)/ETI IJP(o) JD/HW/JG
 ACC NR: AP6032055 (N) SOURCE CODE: UR/0148/66/000/009/0158/0161
 AUTHOR: Yusfina, L. I.; Minkevich, A. N.; Rastorguyev, L. N.; Sidokhina, N. B. 34
 ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov) 33
 TITLE: Producing nickel boride and cobalt boride layers on iron
 SOURCE: IVUZ. Chernaya metallurgiya, no. 9, 1966, 158-161
 TOPIC TAGS: nickel compound, cobalt compound, x ray diffraction analysis, micro-hardening, boride
 ABSTRACT: The authors plated the surfaces of Armco iron specimens with a 70-100 μ thick layer of nickel and cobalt. These specimens were tested for 1-6 hours at 950°C in a bath composed of 60% molten borax and 40% carbide or in a melt of borax using electrolysis. A thick boride layer was formed on all specimens which went through the first bath under all processing conditions. The thickness of the boride layer increases with time of treatment. After holding from 1 to 3 hours, the nickel boride layer still consists of one zone. After 4 hours of holding, two zones appear in the layer. X-ray diffraction analysis shows that these zones correspond to Ni_3B_2 and Ni_2B . This process is much quicker in the case of electrolytic plating. The intermediate layer cannot be observed after 3 hours of holding. A figure is given showing the microhardness of all the phases formed in the surface layers. A study of the boride layer shows an acicular microstructure. The length of the boride needles.
 Card 2/2 UDC: 669.18:621.785:53

L.09133-67

ACC NR: AP6032055

varies, and in some places they pierce both the cobalt layer and the iron. X-ray diffraction analysis shows that the cobalt content at the surface is 91-92% in those places where the boride needles do not penetrate the iron. Cobalt concentration approaches 100% at a given distance from the surface and then decreases sharply. This shows that cobalt penetrates iron to a depth of 10 μ which cannot be observed in studying microstructure or microhardness. A completely different picture is seen where the needles penetrate the entire cobalt layer. The microhardness of these needles varies along their entire length. At the surface their microhardness is from 1250-1580 kg/mm² and 1680-2050 kg/mm² at their ends. Iron content at the ends of the needles reaches 92-88%. At the same time, cobalt content in these places is only 10-2%. As can be seen, the boride needles which penetrate the iron mainly represent boride with admixtures of cobalt and iron. Iron content diminishes in the boride toward the surface, the needles consisting basically of Co₂B. On the other hand, Fe₂B is found in the specimens in the center layer. Orig. art. has: 5 figures.

SUB CODE: 11/ SUBM DATE: 15Feb66/ ORIG REF: 005/ OTH REF: 001

Card 2/2 net

ACC NR: AM6014726

Monograph

UR

Minkevich, A. N.

Chemical and thermal treatment of metals and alloys (Khimiko-termicheskaya obrabotka metallov i splavov) 2d ed., rev. Moscow, Izd-vo "Mashinostroyeniye", 1965. 490 p. illus., biblio. Errata slip inserted. 6500 copies printed.

TOPIC TAGS: metal surface impregnation, thermochemistry, metal diffusion, refractory metal, cyanidation, nitridation

PURPOSE AND COVERAGE: This book is intended for engineering personnel and scientific workers specializing in the field of thermochemical treatment. It may also be useful to students of schools of higher education, who study the thermal treatment of metals. The book briefly outlines general laws governing diffusion processes and methods of obtaining diffusion layers in metals. It reviews processes of carburizing, nitrocarburizing, cyanidation, nitriding, aluminizing, chromizing, boronizing and zinc plating of steel as well as processes of impregnation of steel surface with beryllium, silicon, titanium, vanadium, molybdenum, tungsten, niobium, manganese, sulfur and some

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UDC: 621.78.794

ACC NR: AM6014726

other elements. Processes of thermochemical treatment of titanium, molybdenum, niobium, tungsten, tantalum, zirconium, nickel, copper, cobalt and their alloys are discussed. Brief outlines of processes of thermochemical treatment of sintered alloys, electroplating and semiconductor materials are given and conditions of depositing carbides, borides, nitrides and silicides on the metal surface are reviewed. For each type of treatment the methods of impregnation, chemical aspects of impregnation, effect of various factors on the impregnation as well as the structure and properties of metals and alloys resulting from treatment are indicated.

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SUB CODE: 11/ SUBM DATE: 5Nov65/ ORIG REF: 396/ OTH REF: 202/

Card 8/8

ACC NR: AP6036899 (4) SOURCE CODE: UR/0226/66/000/011/0046/0051

AUTHOR: Shovensin, A. V.; Shcherbedinskiy, G. V.; Minkevich, A. N.

ORG: Central Scientific Research Institute of Ferrous Metallurgy (Tsentral'nyy nauchno-issledovatel'skiy institut chernoy metallurgii)

TITLE: Characteristics of carbon diffusion in molybdenum carbide

SOURCE: Poroshkovaya metallurgiya, no. 11, 1966, 46-51

TOPIC TAGS: molybdenum carbide, carbon diffusion, thermal diffusion, diffusion, diffusion saturation

ABSTRACT: Temperature relationships are determined for the self-diffusion and heterodiffusion coefficients of carbon in molybdenum carbide, expressed by the ratio $D = 0.3 \exp(-67,000 RT) \text{ cm}^2/\text{sec}$ and $D = 3 \cdot 17 \cdot 10^3 \exp(-78,000 RT) \text{ cm}^2/\text{sec}$, respectively. The heterodiffusion coefficients, at temperatures investigated, exceed the self-diffusion coefficients by approximately two orders of magnitude. The difference in diffusion coefficients can be explained by a strong dependence of the thermodynamic activity on the concentration of carbon in molybdenum carbide. Orig. art. has: 6 formulas and 4 figures. [Based on authors' abstract] [NT]

SUB CODE: 11/SUBM DATE: 20Dec65/ORIG REF: 003/

Card 1/1

14(10)

SOV/112-59-3-4685

Translation from: Referativnyy zhurnal. Elektrotekhnika, 1959, Nr 3, p 55 (USSR)

AUTHOR: Minkevich, B. I.

TITLE: Setting Conditions of Mortar Placed on a Concrete Surface (Usloviya tverdeniya tsementnogo rastvora, pomeshchennogo na betonnuyu poverkhnost')

PERIODICAL: Tr. Sredneaz. n.-i. in-ta irrigatsii, 1957, Nr 90, pp 105-107

ABSTRACT: A thin coating of mortar on a concrete surface quickly loses water; this fact impairs the normal course of cement hydration. To determine the effect of quantitative water losses on concrete strength, a number of experiments, 12 times each, were stages. Plastic mortar of 1:3 composition (by weight) was placed as a 2-cm layer on the grade-200 concrete. It was found that evaporation alone causes the mortar to lose 68% of the mix water over the first 24 hours; capillary suction alone causes the loss of 35%; both causes, 70%. To attain the normal humid setting of mortar, it is recommended that insulating films be combined with quick-setting mortar of high-water retaining ability.

Card 1/2

SOV/112-59-3-4685

14(10)

Setting Conditions of Mortar Placed on a Concrete Surface

Experiments with the Khilok Plant cements established the effectiveness of introducing 8% of CaCl_2 . Strength of mortar samples without CaCl_2 , after 29 days without moistening, was found to be 9.5 kg/cm^2 ; the same with CaCl_2 added, 18.6 kg/cm^2 .

A.P.T.

Card 2/2

MINKEVICH, B., inzh.

~~Gypsum retarders.~~ Stroitel' no.10:26 0 '58.
(Gypsum)

(MIRA 11:11)

MINKEVICH, B.I.

Effect of vibration and different filling materials on the quality
of plastic concrete made with monomeric furfurole-acetone resin.
Vop. gidr. no.3:118-123 '61. (MIRA 15:4)
(Concrete)

MINKEVICH, B.I. (g.Tashkent); FEDYAY, V.N. (g.Tashkent)

Placing plastic concrete made with the "FA" monomer to protect
hydraulic structures from destruction. Gidr.i mel. 13 no.7:35-39
'61. (MIRA 14:7)

(Concrete construction) (Uzbekistan--Dams)

MINKEVICH, B.I.; MUKHAMEDAMINOV, R.A.

Polyacrylamide retards the hardening of structural gypsum. Sbor.nauch.
trud.fashNIIS no.5:116-118 '63. (MIRA 18:1)

MINKEVICH, B.M.; DAVIDCHEVSKIY, Yu.I.

Concerning the synthesis of an antenna with a circular aperture.
Radiotekh. i elektron 6 no.8:1395-1396 Aug '61. (MIRA 14:7)
(Antennas (Electronics))

MINKEVICH, D.I.

95(1) PHASE I BOOK EXPLOITATION NOV/2098

Moscow. Vysshaya tekhnicheskoye uchilishche imeni M.E. Maumana
Metodye novyye voprosy ahtampovki tochnykh detalей, (abornik
statей) (Some New Problems in Stamping Precision Parts, Col-
lection of Articles) Moscow, Oborongiz, 1959. 110 p. (Series:
Ita: [Trudy] 85) Krata elip inserted. 4,700 copies printed.

Ed.: E.A. Sateyn, Honored Worker in Science and Technology,
Doctor of Technical Sciences, Professor, Ed. of Publishing
House: P.B. Morozova; Tech. Ed.: E.A. Pukhltova; Managing Ed.:
A.S. Zaymevskaya, Engineer.

PURPOSE: This collection of articles is intended for industrial
workers in precision stamping and for teachers and students in
this or related fields.

CONTENTS: The collection covers problems of stamping thin-walled
and low-rigidity sheet products, obtaining rigid recrystallized
joints, forming square and cylindrical blanks in closed dies,

and accuracy and finish in cold extruding. Problems of ultra-
sonic marking of cast alloy materials are also discussed.
The articles represent some of the studies carried out in re-
sult of work at the Department of Technology of the MVTU (Moscow
Higher Technical School) imeni Maumana on methods of stamping
precision machine parts. No personalities are mentioned. Some
of the articles are followed by references.

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Minkevich, D.I., Candidate of Technical Sciences. Investigation of
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square blanks into cylindrical shape is presented and experi-
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The author discusses methods of determining the accuracy of
nearfield rings as well as the shape of the deformed rings
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examples of means of compensating deviations of shape result-
ing during manufacture.

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During 12 - 14 Mar 52, in Moscow, the Hydro-technics and Amelioration Sec of the All-Union Acad of Agri Sci imeni Lenn held a plenum, with participation of agricultural and hydrological administrators, directors, and main agronomists of MTS (machine-tractor stations),

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besides presidents of kolkhozs in irrigated districts of Kuybyshev and Saratov Oblasts. Discussed were problems of utilizing irrigated lands under conditions met beyond the Volga and in other new regions being irrigated. Reports were heard from 22 lecturers: I.A. Minkovich, substitute for Minister of Agri USSR; Prof V.A. Shaumyan, substitute for the director of scientific part of All-Union Sci Res Inst of Hydrotechnics and Amelioration; I.P. Kurylev, head, Kuybyshev Oblast Water Econ; I.A. Isakov, Chief Agronomist, Georgiyev MTS; Dorokhin, Pres, "Krasnaya Znamya" Kolkhoz; Kharitonov, Chief Agronomist, Saratov Oblast Land Admin; Prokhorov, Chief Agronomist, Saratov Oblast MTS; Pekomov, pres "Komsomolets"

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Kolkhoz; Yershov, Pres, Kuybyshev Oblast Exec Committee; Ye.G. Petrov, Cand Agr Sci, All-Union Sci Res Inst of Hydrotechnics and Amelioration; Yegorshilov, Engr; N.P. Samsonov, Sr Sci Assoc, All-Union Sci Res Inst of Hydrotechnics, and Amelioration; Nesterov, Pres, "Zarya" Kolkhoz; V.G. Kornev, Ostovskiy, Sr Sci Assoc of Ukrainian Exptl Sta; etc.

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