

НАЗАРЕНКО, И. Д.

KATARSKIY, I.S.; NAZARENKO, N.D.

Investigating the hydration of the magnesite mixture and its effect on sintering during the burning process. Ogosupory 22 no.9:392-398 (MIRA 10:11) '57..

1. Khar'kovskiy politekhnicheskii institut im. V.I. Lenina. (Refractory materials) (Magnesite)

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R001136220

APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R001136220

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R001136220

APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R001136220

SIION NR: AP5002891

RECEIVED: 00

ENCL: 00

SUB CODE: NY, MA

ATTN: 000

ATL PRESS: 3172

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R001136220

APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R001136220

ACC NR: AP6021572

(A)

SOURCE CODE: UR/0131/66/000/003/0059/006

AUTHOR: Nazarenko, N. D.; Vlasko, N. L.; Tikush, V. L.; Skryabinskaya, L. V.

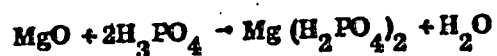
ORG: Institute of Materials Research, AN UkrSSR (Institut Problem Materialovedeniya, AN SSSR)

TITLE: Superduty nonfired refractories with magnesium phosphate used as the binder

SOURCE: Ogneupory, no. 3, 1966, 59-61

TOPIC TAGS: refractory, magnesium compound, phosphate, nonclay refractory product

ABSTRACT: Superduty concretes were experimentally produced on using fused-magnesite wastes of electric-heater production and monosubstituted magnesium phosphate. The phosphate was obtained by adding small portions of active MgO to preheated phosphoric acid:



and evaporating the solution until a dry residue remained. This residue, dry monosubstituted magnesium phosphate, was added as the binder to the charge. Specimens of the resulting material were immediately pressed in semi-dry form in a hydraulic press and dried, first in

Card 1/2

UDC: 666.856

ACC NR: AP6021572

air and then at 100-110°C (when the final setting of the phosphate binder additionally enhanced the strength of the material). The dry specimens were heated to 900°C in a muffle furnace and to 1700°C in a Kryptol furnace. Findings indicate that the minimum spalling resistance of the specimens after heating at 900°C is sufficiently high, and that it increases markedly when they are heated at 1200-1500°C. The material thus developed may be primarily recommended for the production of rammed refractory linings and accessories (including flame tubes) for high-temperature furnaces of the laboratory type. Orig. art. has: 6 tables.

SUB CODE: 11 ✓ SUBM DATE: none / OTH REF: 002

Card 2/2

AMBARTSUMYAN, TS.L.; BASALOVA, G.I.; GORZHEVSKAYA, S.A.; NAZARENKO, N.G.;
KHODZHAYEVA, R.P.; PCHELINTSEVA, G.M., red.; MAZEL', Ye.I., tekhn.
red.

[Thermal investigation of uranium and uranium-containing minerals]
Termicheskie issledovaniia uranovykh i uransoderzhashchikh minera-
lov. Moskva, Gos. izd-vo lit-ry v oblasti atomnoi nauki i tekhniki,
1961. 146 p. (MIRA 14:11)

(Uranium—Analysis)

GERTSEVA, R.V.; TSYBUL'SKAYA, M.S.; AMBARTSUMYAN, TS.L.; NAZARENKO, N.G.;
POLUARSHINOV, G.P.; KHODZHAYEVA, R.P.

New data on hydrous pitchblende and urtite. Zap.Vses.min.ob-va
90 no.5:549-556 '61. (MIRA 14:10)
(Urtite) (Pitchblende)

DYMKOV, Yu.M.; NAZARENKO, N.G.

Coffinite and the nature of pitchblend^e pseudocrystals. *Geokhimiia*
no.4:304-312 '62. (MIRA 16:7)
(Coffinite) (Uraninite)

DYMKOV, Yu.M.; SOLOV'IEVA, F.I.; NAZARENKO, N.G.

Pseudospherulites of uraninite. Zap.Vses.mfn.ob-va. 92 no.2:
242-247 '63. (MIRA 16:5)

(Uraninite)

ABSTRACT X ray and thermogravimetric analyses of uranyl nitrates (with 0.5g/l uranium) showed that as 20°C and arsenic-uranium near stoichiometric the precipi-

and di- and trivalent iron and aluminum arsenates as functions of uranium (0.250g/

SINEYDER, Viktor Aleksandrovich; MANUYLOV, Yu.G., nauchn. red.;
NAZARENKO, M.I., red.

[Scrapers, bulldozers, and graders] Skrepery, bul'dozery,
greidery. Izd.2., ispr. i dop. Moskva, Vysshaya shkola,
1964. 269 p. (MIRA 18:3)

NAZARENKO, N. V.

"Certain Peculiarities of Polyneuritis of Dysenteric Etiology,"
by N. V. Nazarenko, Trudy Instituta Nevrologii i Fizicheskikh
Metodov Lecheniya Ministerstva Zdravookhraneniya Turkmenskoy
SSR (Works of the Institute of Neurology and Physical Methods
of Therapy, Ministry of Health Turkmen SSR), Vol 3, 1955, pp
55-62 (from Sovetskoye Meditsinskoye Referativnoye Obozreniye,
No 15, 1956, p 26, abstract by D. Aniskovich)

"The problem of affection of the nervous system in dysentery has been considered comparatively seldom in neurological literature, but it has always been acknowledged that any part of the nervous system and most frequently the cells and fibers of the peripheral columnae can be affected in dysentery. In this article, a detailed history of disease in five patients suffering from polyneuritis of dysenteric etiology are presented. Three of the patients had severe motor disturbances and two had pain sensations in the hands and feet with a background of polyhypovitaminosis. The increase in motor disturbances developed rather rapidly, but was restored considerably more slowly than that of sensory disturbances. Physical and medicinal methods are the most effective complex therapy. The prophylactic administration of vitamins, especially B complex, into the organism is important." (U)

Serial 1341

SOV/109-4-8-4/35

AUTHORS: Kucherenko, Ye.T. and Nazarenko, O.K.

TITLE: Properties of a Discharge with Electron Oscillations
in a Magnetic Field

PERIODICAL: Radiotekhnika i elektronika, 1959, Vol 4, Nr 8,
pp 1253 - 1256 (USSR)

ABSTRACT: The effect investigated in this work was observed earlier by one of the authors (Refs 1 and 2). The experimental tube employed is illustrated in Figure 1. This consists of a cylindrical anode A, a heated cathode K and two reflectors R_1 and R_2 ; a known longitudinal field is applied to the system. Two different types of discharge can be produced in the system. The first operating regime occurs at pressures $p < 2 \times 10^{-3}$ mm Hg and is dependent on the form of the cathode; this is referred to as the "difficult regime". The cathodes in the tube were made of tungsten and were in the form of a long cylindrical helix, a short helix, a flat helix or a flat oxide cathode. The characteristics

Card 1/4
3

SOV/109-4-8-4/35
Properties of a Discharge with Electron Oscillations in a Magnetic Field

of a difficult discharge in which the cathode was in the form of a cylindrical helix (length 20 mm, diameter 5 mm, spacing 2 mm) are illustrated in Figure 2a. This shows a change of the discharge current I_a , the ion current I_t extracted from the system by means of the Pierce device, and the discharge voltage U_a as a function of the magnitude of the magnetic field H . Figure 2b shows similar curves for a discharge with a flat helix oriented perpendicularly to the direction of the field. The discharge voltage U_a as a function of the magnetic field H is illustrated in Figure 3; the curve was taken with a flat helix, having a diameter of 10 mm, in hydrogen. As the gas pressure is increased, the supply-source voltage being constant, the ion current increases considerably in the region of the peaks (Figure 4a). A further increase in the pressure, above 2×10^{-3} mm Hg, for hydrogen, results in a very

Card 2/4
3

SOV/109-4-8-4/35
Properties of a Discharge with Electron Oscillations in a Magnetic Field

intense discharge, which is characterised by a low voltage drop; this is illustrated in Figure 45. A similar critical pressure is also observed in argon, the pressure being about 5×10^{-4} mm Hg. The discharge above the critical pressure is referred to as the "arc discharge". From Figures 5, it is seen that the increase in the supply voltage, in the case of an arc discharge, leads to an increase of the discharge and ion currents and to the broadening of the "existence" limits of the discharge (towards higher magnetic fields). The authors make acknowledgment to Professor N.D. Morgulis for discussion and his interest in this work. There are 5 figures and 6 references, of which 1 is French, 1 German and 4 Soviet. ✓

Card 3/6

Asat: Kiev State Univ in T.G. Shevchenko

NAZARENKO, O.K.

69782
 SOV/004-52573
 Gromovskiy, V.I., Lukyanov, S.Ye., Spivak, G.V. and
 Al'tsherman, I.G.
 Report on the Second All-Union Conference on Gas
 Electronics
 PERIODICAL: Radiotekhnika i elektronika, 1959, Vol 4, Nr 8,
 pp 1359 - 1358 (USSR)
 ABSTRACT: The conference was organized by the Ac.-Sc. USSR, the
 Ministry of Higher Education and Moscow State University.
 A.A. Litvak - "Measurement of the Gas Density During
 the Dynamic Operation of a Discharge" (see p 1366 of
 the journal). A.V. Sedashev - "The Nature of a Striated
 Positive Column".
 V.K. Fokal' and Yu.M. Lagan - "The Theory of Probes for
 Arbitrary Pressures".
 Yu.M. Kagan et al. - "The Positive Column of a Discharge
 in a Diffusion Regime".
 A.A. Litvak - "Influence of the Processes of the
 Diffusion of the Negative Ions on Their Concentration
 in the Column".
 M.D. Gerasimov and L.I. Paschuk - "Anomalous Scattering,
 Excitation of Plasma Oscillations and Plasma Resonance".
 Yu.L. Klementovich - "Energy Lost by Charged Particles for
 the Excitation of the Oscillations in Plasma (the Langmuir
 paradox)" and "The Theory of Non-linear Plasma Oscillations".
 I.G. Martynov and I.G. Nehrashovich - "Dependence of
 the Temperature in the Near-electrode Region of a Pulse
 Discharge on the Material of the Electrodes".
 S.A. Korovin and S.V. Klyuzhal'a - "Formation of Light
 Spots on the Anode of a Gas Discharge (see p 1361 of
 the journal).
 M.A. Kuznetsov - "Distribution of Binary Mixtures of Inert
 Gases in a Gas Discharge".
 V.G. Stepanov and V.P. Babitskiy - "Some Phenomena
 in Modified Plasma".
 V.G. Stepanov and V.A. Balal' - "The Possibility of
 Obtaining Highly Concentrated Plasmas".
 G.V. Smirnitkaya and S.M. Rukhovich - "Some Character-
 istic Features of the Discharge in an Ion Pump and in a Magnetic
 Isolation Vacuum Gauge".
 Ye.F. Kuznetsov and O.K. Nagornaya - "Properties of
 a Discharge with Slowly Oscillations in a Magnetic
 Field" (see p 1355 of the journal).
 The paper by L.B. Abramov and S.A. Veklenko considered
 the approximate methods for determining the concentration
 of atoms at the cathode level.
 V.I. Fokhtman and K.A. Yarmukhina read a paper on
 "Spectral Binary Theory" of the Stark Broadening of the
 Spectral Lines of Plasma.
 M.A. Nazarenko and S. Mandel'shtam - "The Broadening
 and the Shift of Spectral Lines in a Gas-discharge Plasma".
 A. Gant (England) - "The Kinetics of Electron Collisions
 Leading to the Excitation of the Molecular Hydrogen in
 a Hydrogen Discharge".
 V.A. Kolesnikov et al. - "Some Properties of the Arc
 Discharge in an Atmosphere of Inert Gases".
 A.A. Rik and M.F. Kozlov - "Production of High
 Temperatures by Means of Spark Discharges".

1.2310

2708.2802.1373

S/125/60/000/009/008/017
A161/A130

AUTHORS: Gurevich, S.M., Nazarenko, O.K., Timchenko, V.A.

TITLE: Electron-Beam Welding Unit for Refractory and Chemically Active Metals

PERIODICAL: Avtomaticheskaya svarka, 1960,¹³ No. 9, pp. 48-53

TEXT: Detailed description is given of an electron-beam welding unit for straight and annular seams on cylindrical work up to 700 mm in diameter and 1200 mm length (Fig. 1), developed at the Electric Welding Institute im. Ye.O. Paton. The chamber of 1200 mm length and 1020 mm diameter is made of killed low-carbon steel 12 mm thick; the chamber inside is ground and all parts chrome-plated. The front end opens for placing work, and two shafts are passed into the chamber through the rear end cover (Fig. 2); one has a screw thread for moving the carriage with work in the chamber, and the other bears a pinion to rotate work. The electron gun is installed on the flange (see Fig. 1). Two inspection windows with lead glass are provided in the

Card 1/8

3/125/60/000/009/008/017
A:61/A:50

J

Electron-Beam Welding Unit for Refractory and Chemically Active Metals

chamber wall. The vacuum system has a fore vacuum pump 8H-1 (VN-1), a high-vacuum BA-5-4 (VA-5-4) unit (converted H-5T (N-5T) steam oil pump), two fore-vacuum valves with 90 mm diameter aperture, and a ДУ-380 (DU-380) vacuum gate. The vacuum system produces rarefaction up to $7 \cdot 10^{-6}$ mm Hg. It takes 50-60 min to replace the work and produce a vacuum. The electron gun gives a sharp-focused beam of over 500 ma and up to 20 kv. No special biological protection is necessary. The combination focusing system has a primary electrostatic lens and a secondary electromagnetic lens producing a beam of 1 mm diameter at the weld, with up to 10 kva power. The gun is lowered into the chamber through the mentioned flange; insert rings are used for varying the distance to the work. The gun is illustrated in diagram (Fig. 5). The electric system of the unit consists of two parts: feed circuit of the electron gun (Fig. 6) and auxiliary control circuits. The gun feed system includes a 50 kva transformer with secondary voltage of 22 kv; a 25 kva potential regulator smoothly adjusting the primary transformer

Card ~~2/8~~

S/125/60/000/009/008/017
A161/A:30

Electron-Beam Welding Unit for Refractory and Chemically Active Metals

voltage between 20 and 400 volt; a Larionov kenotron rectifier with B1-0,1/40 (V1-0.1/40) kenotrons; YMN-1 (UIP-1) rectifiers feeding the gun cathode heater and the electromagnetic focusing lens, adjusting output voltage in the 20-600 volt range at a maximum current of 600 ma (one rectifier is connected to a 220 volt network through a 1:1 transformer with insulation between windings, designed for rated 30 kv tension); a heating transformer for heating the flat tungsten spiral of the cathode group (220/20 volt, 100 amp); a smoothing LC filter consisting of a 3 microfarad capacitor and a 25 henry 1 amp choke instruments (milliamperimeters, an amperemeter, a voltmeter, and a kw-meter). The control system includes magnetic starters, intermediate relays and contactors, autotransformers etc., all placed in a separate instrument box and in the operator's control board. The welding process is watched on instruments in a central instrument cabinet including auxiliary electronic equipment (the UIP-1 sources, the heating transformer, the cathode heating unit, etc.). Welding of molybdenum and

Card ~~3/8~~

S/125/60/000/009/008/017
A161/A130

Electron-Beam Welding Unit for Refractory and Chemically Active Metals ✓

other chemically active metals has been tried with success. There are 6 figures and 3 references, 2 of which are Soviet and 1 English.

ASSOCIATION: Ordena Trudovogo Krasnogo Znameni Institut elektrosvarki iz. Ye.O. Patona AN USSR (Electric Welding Institute "Order of the Red Banner of Labor" of the Academy of Sciences of the UkrSSR)

SUBMITTED: April 29, 1960

Card 4/6

1.2310 9.3130

22940
S/125/61/000/006/004/010
D040/D112AUTHOR: Nazarenko, O. K.

TITLE: Electron-beam welding guns

PERIODICAL: Avtomaticheskaya svarka⁴ no. 6, 1961, 31-36

TEXT: Information is given on two new electron-beam welding gun systems developed in the USSR: 1) A spherical-type gun producing a sharply focussed electron beam at 20 kv and 100 m-amps current, giving a 0.5 mm diameter focus spot on the workpiece being welded, and 2) a gun with $\sim 1.1 \cdot 10^{-2}$ amp/kv^{3/2} conductance, forming an up to 20 kva electron beam at 20kv, and giving 6-8 kva/mm² specific power in the welding plane. The two systems, both working with an accelerating voltage of 20-22 kw, are a development of electron guns described in two non-Soviet publications (Ref. 1: E. B. Bas, G. Cremosnik, Schweissen im Hochvakuum mit Elektronenstrahlen, "Vakuum Technik", No. 7, 1959; W. J. Greene, R. R. Banks, R. M. Niedzielski, A New Electron-Beam Welding Unit, "Welding Journal", 39, No. 8, 1960). The design with cathode and anode representing portions of concentric spheres is adopted from radio engineering (Ref. 2: Dzh. R. Pirs [Russian spelling], Teoriya i raschet elektronnykh puchkov [Theory and calculation of electron

Card 1/6

22940

S/125/61/000/006/004/010
D040/D112

Electron-beam welding guns

beams], "Sovetskoye radio", M., 1956). [Abstracter's note: The obviously English name, probably J. R. Pears, suggests translation from English]. The Poisson equation for the stream of electrons between spheres is taken from calculations by I. Langmuir and K. Blodgett (Ref. 3: Currents Limited by Space Charge Between Concentric Spheres, "Phys. Rev.", 24, pp 49-54, 1924). The design is illustrated in two diagrams and two photographs (Fig. 1, 3, 4, 5). The electromagnetic lens of the described gun is a screened coil without pole ends; the nonmagnetic gap is adjusted by replaceable bushings from armco iron. The ampere-turns number, close to that determined empirically, is determined by the formula

$$IN = k \sqrt{\frac{R_{\text{mean}} v_a}{f}}, \quad (9)$$

where f is the focal length of the lens; R_{mean} - mean coil radius ; k - the lens parameter (for the given design $k = 7$); v_a - accelerating voltage . The toroidal lens is placed in a vacuum-tight casing. As can be seen from the formula (9), the focal length of lens depends considerably on the accelerating voltage, and it is evident that pulsation of rectified voltage

Card 2/6

22940

S/125/61/000/006/004/010
D040/D112

Electron-beam welding guns

increases the effective focal spot; this means increased width of the welding seam and a wider zone of heat effect. Larionov rectifiers with LC-filters are used in the gun feed units to eliminate these phenomena, and the rectified voltage pulsates not more than 0.1-0.3%. [Abstracter's note: No information on the Larionov rectifier is included.] The space between the lens and the welded workpiece is 70-100 mm. The cathodes are made from lanthanum hexaboride and developed by the Institut metallokeramiki i spetssplyavov AN USSR (Institute of Powder Metallurgy and Special Alloys AS UkrSSR). They give considerable emission density at comparatively low temperature (10 amp/cm² at 1600°C), and their service life is dozens of hours. Information on these electrodes has been given by Ye. T. Kucherenko (Ref.5: "Radiotekhnika i elektronika", No. 9, 1960). There are 5 figures and 5 references: 3 Soviet-bloc and 2 non-Soviet-bloc. The two references to English-language publications read as follows: W. J. Greene, R. R. Banks, R. M. Niedzielski, A New Electron-Beam Welding Unit, "Welding Journal", 39, No. 8, 1960; I. Langmuir, K. Blodgett, Currents Limited by Space Charge Between Concentric Spheres, "Phys. Rev.", 24, pp 49-54, 1924. X

Card 3/6

22940

X

Electron-beam welding guns

S/125/61/000/006/004/010
D040/D112

ASSOCIATION: Ordena Trudovogo Krasnogo Znameni Institut elektrosvarki im. Ye. O. Patona AN USSR (Electric Welding Institute "Order of the Red Banner of Labor" im. Ye. O. Paton, of the AS UkrSSR)

SUBMITTED: December 15, 1960

Card 4/6

1.2310

22952
S/125/61/000/007/008/013
D040/D113

AUTHORS: Medovar, B.I.; Nazarenko, O.K.; Gurevich, S.M.; Chekotilo,
L.V.; Povod, A.G.; and Pinchuk, N.I.

TITLE: Some peculiarities of electron-beam welding of austenitic
steels and alloys

PERIODICAL: Avtomaticheskaya svarka, ¹⁴no. 7, 1961, 79-81

TEXT: In their introductory remarks, the authors state why the electron-beam welding of austenitic steels and alloys in a vacuum is superior to conventional welding. For experimental purposes, specimens of 3M 726 (EI 726) and 9M696 (EI 696) heat-resistant austenitic steels and a nimonic-type 3M 437B (EI437B) alloy were welded by the electron-beam method. All these types contain boron and are prone to cracks in the area near the weld and in the weld metal, if the composition of the base metal is reproduced. Welding was carried out with an electron-beam gun designed by the Ordena Trudovogo Krasnogo Znameni Institut elektrosvarki im. Ye.O. Patona AN USSR (Electric Welding Institute "Order of the Red Banner of Labor" im. Ye.O. Paton AS UkrSSR) using 120 mA, 20 kw current and a 35 m/hr welding speed. Metal

Card 1/2

22952

S/125/61/000/007/008/013
D040/D115

Some peculiarities of electron-beam ...

produced by the electron beam was completely sound, except in the case of EI726 steel where an increased boron content of 0.025% caused cracks to form in the base metal at the seam and sometimes even in the weld metal. The following conclusions are drawn: The new method of electron-beam welding in a vacuum must be used not only for refractory and chemically active metals but also for heat-resistant austenitic steels and alloys. The electron-beam method gives welds much more resistance to crystallization cracks than other known welding methods. It is to be expected that the use of filler wire will make the electron-beam process applicable to a wider range of austenitic steels and alloys, and that the dagger shape of the seam will necessitate some modification of the design of the joints. There are 6 figures. X

ASSOCIATION: Ordena Trudovogo Krasnogo Znameni Institut elektrosvarki im. Ye. O. Patona AN USSR (Electric Welding Institute "Order of the Red Banner of Labor" im. Ye. O. Paton AS UkrSSR)

SUBMITTED: April 17, 1961

Card 2/2

1 2310 1140 1138 2708 1573

26482
8/125/61/000/003/006/C14
D040/D113

AUTHORS: Nazarenko, O. K.; Povod, A. G.

TITLE: Experimental study of a welding electron gun with a spherical-type projector of long focal length

PERIODICAL: Avtomaticheskaya svarka, ¹⁴no.9, 1961, 33-37

TEXT: A new welding electron gun is described. Its combination focusing system (Fig.1) produces a beam of up to 120 ma and up to 5 kw/mm² energy in the focus spot. Welded joints with weld shape factor below 1.5 have been obtained in experiments with this gun without raising the accelerating voltage over 20 kv. This disproves the opinion that it is impossible to produce welds with a shape factor below 3:1 with the use of low-voltage welding guns (Ref.1: G.Burton, R.L.Matchett, Electrons shot from guns make high-purity welds, "American Machinist", v. 103, no.4, 1959). The gun (Fig.2) primary electrostatic system has a cathod unit (1) cathode electrode (2) and an accelerating electrode (anode) (3) with aperture for the beam. Current is supplied through two high-voltage and two low-voltage leads (4). The electron beam passes through the anode electrode and aperture diaphragm (5) and is

Card 1/4

26482

Experimental study of a welding electron

S/125/61/000/009, 006/014
D040/D115

+

finally focused by an armored electromagnetic lens (9). The gun is attached to the flange (10) of the vacuum chamber by sockets by which the distance between the chamber axis and the electromagnetic lens can be varied. The cathode and anode are shaped like parts of concentric spheres with a radius ratio $\frac{r_{\text{cath}}}{r_{\text{an}}} = 2.5$. The calculation of the projector is given in another

work. (Ref.2: O.K.Nazarenko, "Avtomaticheskaya svarka", no.6, 1961). The cathode material is lanthanum hexaboride (LaB_6). Cathodes of this material have a high emission density ($j = 10 \text{ amp/cm}^2$ at 1600°C), stability against ion bombardment and require no activation after contact with air. The article includes a general view photograph of the gun and two macro-photographs of two welds produced in stainless steel and molybdenum. There are 6 figures and 2 references: 1 Soviet and 1 non-Soviet bloc. The one reference to English language publication reads: G.Burton, R.L.Matchett, Electrons shot from guns make high-purity welds, "American Machinist", v. 105, no.4, 1959.

Card 2/4

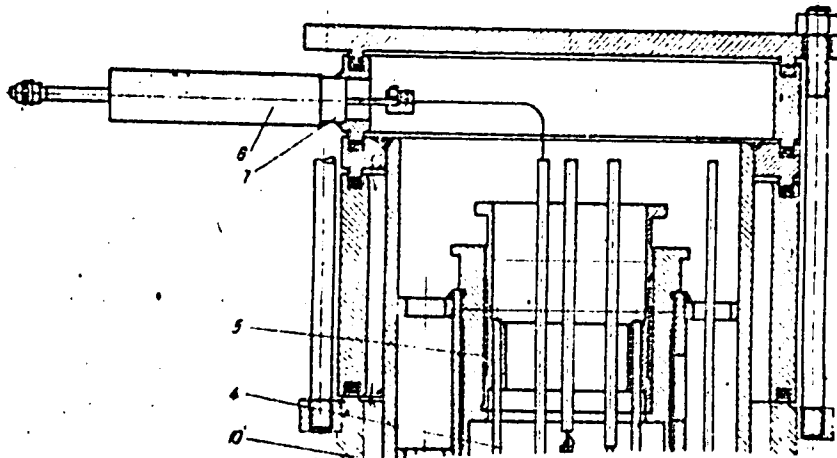
26482

Experimental study of a welding electron

S/125/61/000/009/006/014
D040/D113

ASSOCIATION: Ordena Trudovogo Krasnogo Znameni Institut elektrosvarki im.
Ye.O.Patona AN USSR (Electric Welding Institute "Order of the
Red Banner of Labor" im. Ye.O.Paton, AS UkrSSR)

SUBMITTED: March 18, 1961



Card 3/4

1.2310

21399
S/029/61/000/009/006/006
D037/D113

AUTHOR: Nazarenko, O., Engineer
TITLE: An electron beam in the role of a welder
PERIODICAL: Tekhnika molodezhi, ²⁹no. 9, 1961, 28

TEXT: The author describes the advantages of the electron beam welding method. He stresses in particular the 1.5 - 2 times higher productivity than in argon-arc welding and the possibility of focussing an electron beam with high accuracy on a sharply defined small spot on the surface of the metal. Steel maintains its structure and necessary features. The parts are not deformed or distorted. As welding is carried out in a vacuum the level of impurities is extremely low. The method gives especially good results in fine welding of parts made of tungsten, molybdenum and tantalum. The installation for electron beam welding has been developed at the Institut elektrosvarki imeni Ye.O.Patona (Electric Welding Institute imeni Ye.O.Paton). With this installation it is possible to weld workpieces up

Card 1/3

27399

S/029/61/000/009/006/006
D037/D113

An electron beam in the role of a welder

to 1 m long, up to 0.7 m in diameter and 4-5 mm thick. The electron beam welding process is shown in a diagram (Fig.2). There are 2 figures.

+

Card 2/3

38826

S/125/62/000/007/009/012
D040/D113

1.2300

AUTHORS: Kuzhel', A.V. ; Nazarenko, O.K. ; Povod, A.G ; Strekal', L.P.

TITLE: A universal welding electron gun with up to 50 kv acceleration voltage

PERIODICAL: Avtomaticheskaya svarka,¹⁵ no. 7, 1962, 88-91

TEXT: The described electron gun (Fig. 5) of the Institut elektrosvarki im. Ye.O. Patona (Electric Welding Institute im. Ye.O. Paton) is used in Y-3 (U-3) electron beam welding machines, and permits the accelerating voltage to be adjusted in the 15-25 kv and 25-50 kv ranges. It can be used for welding various metals of different thickness such as thin sheet molybdenum or tungsten and thick aluminum or stainless steel. The gun has a 3-electrode projector with a lanthanum boride cathode, and a one-stage electromagnetic focusing lens of 2,000 amp-t in a screen of armco iron. The long current supply system of the cathode reduces the heat transfer to the vacuum, which seals off the armored high-voltage insulator. A metal bellows joint permits the projector to be displaced along the gun axis during operation, and also allows the space between the focusing electrode and the

Card 1/2

S/125/62/000/007/009/012
D040/D113

A universal welding

anode to be adjusted without disturbing the vacuum in the gun. The entire gun can be tilted 15° from the vertical axis to adjust the focal spot to the work edges. An electromagnetic deflecting system placed under the focusing lens deflects the beam by $5-10^{\circ}$ along the seam; this protects the cathode from metallization and ion bombardment. There are 6 figures.

ASSOCIATION: Ordena Trudovogo Krasnogo Znameni Institut elektrosvarki im. Ye.O. Patona AN USSR (Electric Welding Institute "Order of the Red Banner of the Labor" im. Ye.O. Paton, AS UkrSSR)

SUBMITTED: November 4, 1961

Card 2/8 2

L 15647-63

ENP(k)/ENP(q)/ENP(m)/BDS AFFTC/ASD Pf-4 ID/BM

ACCESSION NR: AP3000840

S/6286/63/000/002/0026/0027

63

AUTHOR: Litvinshuk, M. D.; Vlasenko, P. I.; Nazarenko, O. K.; Timchenko, V. A.; Prosvirov, A. N.

TITLE: Installation for electron-beam welding of tubes with tube panels.
Class H 05b; 21h, 30 sub 10, No. 152714

14

SOURCE: Byul. izobretaniy i tovarnykh znakov, no. 2, 1963, 26-27

TOPIC TAGS: electron-beam welding, automatic program control, welding

ABSTRACT: Installation for electron-beam welding of pipe with pipe panels, containing an electron-beam welding gun with magnetic deflection system, a rotating table for fastening and rotating the work piece during the welding process, and an automatic control system for sequential operation of individual mechanisms; its distinguishing feature is that in order to automate the welding process, the table is provided with two lead screws with a drive system for moving the article in two mutually-perpendicular directions when it comes time

Card 1/3 ✓

L 15647-63

ACCESSION NR: AP3000840

to weld the next tube, and the control system contains a program unit with relay elements for automatic control in accordance with a program recorded on a punched tape or some other program carrier. Orig. art. has: 1 figure (see Enclosure 1) Abstractor's note: complete translation. 7

ASSOCIATION: none

SUBMITTED: 11 Sept 61

DATE ACQ: 28 May 63

ENCL: 01

SUB CODE: MD, MI.

NO REF SOV: 000

OTHER: 000

Card 2/2

S/125/63/000/004/002/011
D040/D112

AUTHORS: Strekal', L.P., and Nazarenko, O.K.

TITLE: Graphical and analytical plotting of electron trajectories in projectors, and investigation of the magnetic lenses of electron welding guns

PERIODICAL: Avtomaticheskaya svarka, no. 4, 1963, 7-11

TEXT: The described graphical and analytical method of plotting electron trajectories takes the space charge in the beam into account and permits accurate determination of optimum electrode configuration and inter-electrode spaces. The fields of a three-electrode gun projector were simulated in an electrolytic bath and the magnetic focusing lenses of welding guns were investigated. A universal relation for obtaining maximum magnetic induction on the lens axis was found. The detailed description is illustrated by graphs. There are 5 figures.

ASSOCIATION: Institut elektrosvarki im. Ye.O. Patona AN USSR (Electric Welding Institute im. Ye.O. Paton, AS UkrSSR)

SUBMITTED: April 23, 1962
Card 1/1

NAZARENKO, O.K., kand.tekhn.nauk; LEONT'YEV, M.N., inzh.

Electron-beam welding in industry. Mashinostroenie no.6:48-52
N-D '63. (MIRA 16:12)

NAZARENKO, O. K.; POVOD, A. G.; LEONT'YEV, N. N.

Experiments on electron beam welding in vacuum $1 \cdot 10^{-1} + 1 \cdot 10^{-2}$ mm rt. st. Avtom. svar. 16 no.3:88-89 Mr '63.
(MIRA 16:4)

(Electric welding—Equipment and supplies)
(Electron beams) (Vacuum technology)

NAZARENKO, O. K.; OLSHANSKIY, N. A.;

"Present Day Status of Electron Beam Welding in the USSR"

Report to be submitted for the First International Conference on Electron and Ion Beam Science and Technology, sponsored by the Electrothermics and Metallurgy Division of The Electrochemical Society and The Metallurgical Society of The American Institute of Mechanical Engineers (AIME), 3-7 Mar 64, Toronto, Canada.

OL'SHANSKIY, N. A. (Dr. Tech. Sci.); NAZARENKO, O. K. (Cand. Tech. Sci.)

"Contemporary Status of Electron Beam Welding in the USSR."

Report to be submitted for the International Conference on Electron and Ion Beam Science and Technology in Toronto, Canada, 3-7 May 1964

ACCESSION NR: AP4020103

S/0125/64/000/003/0044/0049

AUTHOR: Nazarenko, O. K. (Candidate of technical sciences); Povod, A. G. (Engineer); Shnyakin, N. S. (Engineer, Moscow); Artamonov, N. N. (Engineer, Moscow); Panov, Yu. P. (Engineer, Moscow); Kedman, A. B. (Engineer, Moscow)

TITLE: Equipment and techniques of electron-beam welding of large pieces

SOURCE: Avtomaticheskaya svarka, no. 3, 1964, 44-49

TOPIC TAGS: electron beam welding, welding, electron beam welding equipment, electron beam welding method, U86, electron beam welder, dagger shaped fusion

ABSTRACT: An experimental outfit for electron-beam (circular) welding of large-size pieces is described which can be mounted on a "telescopic" carriage with a headstock and tailstock and introduced into a cylindrical (4-m length, 2-m diameter) vacuum chamber; 20-mm-thick stainless steel was used for building

Card 1/2

ACCESSION NR: AP4020103

the chamber. A d-c motor mounted on the carriage ensures an adjustable welding rate within 5-100 m/hr. A VN-6 fore-vacuum pump, an N-20T oil-vapor fine-vacuum pump, and a BN-3 oil-vapor booster pump, with a combined output of 10,000 lit/sec, exhaust the chamber down to 10^{-4} - 10^{-5} torr. Three electron guns are used with these parameters: accelerating voltage, 10-25 kv; test voltage, 50 kv; beam current, 0-500 ma; specific energy in the focal beam spot with optimum lens distance, 5-10 kw/mm². Some details of welding procedures are given. "A. M. Svyat*skiy was the leading designer. Engineers A. A. Mikhaylovskiy, V. I. Khoroshilov, A. L. Loginov, and V. F. Illarionov took part in designing the outfit. V. M. Shiyan was the leading designer of the electron gun." Orig. art. has: 5 figures and 1 table.

ASSOCIATION: Institut elektrosvarki im. Ye. O. Patona AN UkrSSR (Institute of Electric Welding, AN UkrSSR)

SUBMITTED: 21Dec63

DATE ACQ: 31Mar64

ENCL: 00

SUB CODE: ML

NO REF SOV: 000

OTHER: 000

Card 2/2

APPROVED FOR RELEASE: Monday, July 31, 2000
CIA-RDP86-00513R001136220
Doc ID: A6412

AUTHOR: Nazarenko, O. K. (candidate of technical sciences)

TITLE: Universal experimental set for industrial electron beam welding

SOURCE: Avtomaticheskaya svarka, no. 10, 1964, 85-86

TOPIC TAGS: welding, electron beam welding, electron gun, thin sheet, plate

ABSTRACT: The Electric Welding Institute im. Ye. O. Paton and the Sumy Electron Microscope and Electric Automation Plant have developed and built an SP-30 experimental set for industrial electron-beam welding. The set, which includes an electron gun and a standard separate power feed source, is designed for automatic and semiautomatic thin-sheet metals and for one pass welding of thicker plates. It welds stainless steel 20 mm thick. The welding process can be carried out in a vacuum. The set is designed for the production of spot and seam welds. The set is also suitable for the local-spot

1 14409-05

ACCESSION NR: AP4047232

The SP-10 welding set has been series-produced at Gamy Elec-
Microscope and Electric Automation plant since 1954. Orig. art.
figure.

ASSOCIATION: none

SUBMITTED: 00

ENCL: 00

SUB CODE: IE, EE

REF SOV: 000

OTHER: 000

ADDRESS: 3140

Card 2/2

ACCESSION NR: AP4041033

S/0120/64/000/003/0126/0128

AUTHOR: Nazarenko, O. K., Zozulya, S. I., Baranov, G. V.

TITLE: Cathodes for sharp-focused electron guns for electron-beam welding

SOURCE: Pribery* i tekhnika eksperimenta, ⁹⁻no. 3, 1964, 126-128

TOPIC TAGS: electron beam welding, electron gun cathode, cathode emitter, lanthanum hexaboride emitter, tungsten emitter

ABSTRACT: The Electric Welding Institute, AN USSR, has developed two types of electron-gun cathodes for electron-beam welders. Both cathodes have indirectly heated emitters. The emitter of the first cathode is a lanthanum hexaboride pellet held in a molybdenum cup positioned with a molybdenum rod. In tests, the pellet operated at a temperature higher than 1700C, ensuring a thermionic current density of about 20 amp/cm². The contamination of the emitter surface can be prevented by decreasing the solid angle at which the vapors of welded metal can reach the emitter. or by shifting the beam focal spot relative to the anode aperture axis. The second cathode has a tungsten

Card 1/2

ACCESSION NR: AP4041033

rod emitter, 2 mm in diameter. With this cathode at an accelerating voltage of 20 kv, a specific energy of 1 kw/mm² is developed at the focus spot, which is 120 mm distant from the anode. In general, cathodes of both types perform equally well, producing electron beams with a specific energy of 10 kw/mm² with a beam current of several hundred milliamperes at an accelerating voltage of about 30 kv. Orig. art. has: 3 figures.

ASSOCIATION: Institut elektrosvarki AN UkrSSR (Electric Welding Institute, AN UkrSSR)

SUBMITTED: 02Jul62

ATD PRESS: 3048

ENCL: 00

SUB CODE: EC, MM

NO REF SOV: 002

OTHER: 001

Card 2/2

NAZARENKO, O.F.; POVOD, A.G.; SHNYAKIN, N.S. (Moskva); ARTAMONOV, N.N. (Moskva);
PANOV, Yu.P. (Moskva); KEDMAN, A.B. (Moskva)

Instruments and equipment for electron beam welding of large-size
articles. Avtom. svar. 17 no.3:44-49 Mr '64. (MIRA 17:11)

1. Institut elektrosvariki im. Ye.O. Patona AN UkrSSR (for Nazarenko,
Poved).

ACC NR: AH5025629

Monograph

UR/

Nazaranko, Oleg Kur'mich

Electron beam welding (Elektronno-luchevaya svarka) Kiev, Naukova dumka, 1965. 127 p. illus., biblio. (At head of title: Akademiya nauk Ukrainskoy SSR. Ordena trudovogo krasnogo znameni institut elektrosvarki im. Ye. O. Patona) 2000 copies printed.

TOPIC TAGS: welding, electron beam, electron beam welding, electron beam welding technology, electron beam welding apparatus

PURPOSE AND COVERAGE: This booklet is intended for engineering personnel and scientific workers dealing with welding. It may also be useful to students specializing in welding. The booklet reviews the basic physical principles of electron-beam welding, gives information on electron-beam guns with various accelerating voltages, describes the basic components of electron-beam welders, such as vacuum systems, and electric-power sources, and reviews the types of the best industrial equipment.

TABLE OF CONTENTS:

Introduction -- 3

Card 1/4

ACC NR: AH5025629

- Ch. I. Physical principles and technology of electron-beam welding -- 6
- Specific features in the utilization of an electron beam as a welding heat source
 - Transfer of energy to a solid body by a beam of accelerated electrons
 - Heat balance in a welding bath -- 8
 - Pressure on a welding bath during electron-beam welding -- 10
 - Formation of dagger-shaped welds in electron-beam welding -- 12
 - Effect of parameters of electron-beam welding on the pattern of penetration -- 14
- Ch. II. Electron-beam welding equipment ¹⁴ -- 23
- Generation and shaping of intensive electron beams in welding electron guns
 - Cathodes of welding electron guns
 - Emission system of electron welding guns -- 32
 - Design of projectors of welding electron guns -- 39
 - Focusing systems of welding electron guns -- 51
 - Aberrations in electron-optic systems of welding electron guns -- 59
 - The effect of acceleration voltage on the power density in beams of welding electron guns
 - Measuring the beam focal point -- 64

Card 2/4

ACC NR: AM5025629

Vacuum system for electron-beam welders -- 69
Power sources of electron-beam welders -- 72
Power sources of welding guns
Electric drive systems of electron-beam welders -- 78

Ch. III. Industrial applications for electron-beam welding -- 79
Industrial welding electron-beam guns
Classification of welding electron-beam guns
Low-voltage guns -- 81
Guns with accelerating voltage of 40--60 kv -- 92
High-voltage welding and machining guns
Prototypes and industrial electron-beam welders -- 94
Universal welder for electron-beam welding of small articles
Equipment for precision electron-beam welding and
machining -- 101
Specialized equipment for electron-beam welding of large
parts -- 101
Equipment for electron welding in an atmosphere of inert
gases or in air -- 106
Welding in portable and transportable chambers -- 109
Examples of the uses of electron-beam welding -- 110
Protection of personnel from roentgen radiation -- 123

Card 3/4

ACC NR: AK5025629

Problems and directions in development of electron-beam
welding -- 124

References -- 126

SUB CODE: 13/ SUBM DATE: 11Mar65/ ORIG REF: 034/ OTH REF: 015

Card 4/4

ACC NO: AP6002894

SOURCE CODE: 13/12/86/05/000/024/0050/0059

INVENTOR: Strekal', L. P.; Dudko, D. A.; Nazarenko, O. F.

ORG: none

TITLE: Method of automatic following the joint in electron beam welding. *ib*
No. 177006

SOURCE: Byulleten' Izobreteniy i tovarnykh znakov, no. 20, 1967, 50

TOPIC TAGS: electron beam welding, secondary electron emission, automatic control, *equipment*
electron interaction, metal joining, *electron beam*

ABSTRACT: 1. The method of automatic following of the joint in electron beam welding with the application of an electromagnetic deflection system that shifts the electron beam with regard to the workpiece, is characterized by the fact that in order to eliminate the effect of the material and of the workpiece shape on the tracking accuracy, use is made of the secondary electron emission, occurring during the reaction of the electron beam with the surface of the workpiece, in controlling the deflection system.

2. The method, described in paragraph 1, is characterized by the fact that in order to improve the tracking accuracy, use is made of the secondary electron emission, occurring during the reaction of the auxiliary sharply focused electron beam of low intensity with the surface of the workpiece, in controlling the deflection system.

Card 1/2

UDC: 621.791.72.08

L 39642-66

ACC NR: AP6002894

3. The method, described in paragraphs 1 and 2, is characterized by the fact that in order to simplify the apparatus for shifting the main and auxiliary electron beams use is made of a common electromagnetic deflection system to shift the beams in a lateral direction with respect to the edges of the workpiece.

SUB CODE: 13,20/SUBM DATE: 03Nov62/

Card 2/2

L 15212-66 EWT(d)/EWT(m)/EWP(v)/T/EWP(t)/EWP(k)/EWP(h)/EWP(b)/EWP(l)/EWA(h) JD/HM
ACC NR: AF6002968 SOURCE CODE: UR/0286/65/000/024/0136/0136

INVENTOR: Zhivaga, L. I.; Nazarenko, O. K.; Chvertko, A. I. 50
B

ORG: none

TITLE: Welding electron gun Class 49, No. 177261 [announced by the Electrical
Welding Institute im. Ye. O. Paton, AN UkrSSR (Institut elektrosvarki AN UkrSSR)]

SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 24, 1965, 136

TOPIC TAGS: welding, electron beam welding, electron gun, gun cathode

ABSTRACT: This Author Certificate introduces a welding electron gun equipped with an anode and a cathode, the latter heated by electron bombardment. To improve the efficiency and service life of the gun, the disk-shaped tantalum cathode with a concave emitting surface is tightly fitted in a round thin-wall housing whose convex bottom faces the anode. [ND]

SUB CODE: 13/ SUBM DATE: 15Dec64/ ATD PRESS: 419

TS
Card 1/1

UDC: 621.791.72.03

L 27059-66 EWT(m)/ETC(f)/EWG(m)/ENP(v)/T/SWP(t)/ETI/EWP(k) LJP(c)

ACC NR: AP6007843 DS/JD/HM

SOURCE CODE: UR/0J20/66/COO/001/0209/0210

AUTHOR: Zinchenko, G. N.; Zinchenko, N. S.; Kuzhel', A. V.; Nazarenko, O. K. 49

ORG: Institute of Radio Physics and Electronics, AN UkrSSR (Institut radiofiziki i elektroniki AN UkrSSR); Institute of Electric Welding, AN UkrSSR, Kiev (Institut elektrosvarki AN UkrSSR)

TITLE: Hermetic sealing of tungsten-barium cathodes with the aid of electron-beam welding

SOURCE: Pribory i tekhnika eksperimenta, no. 1, 1966, 209-210

TOPIC TAGS: cathode, electron beam welding, hermetic seal, seam welding

ABSTRACT: The authors describe experiments on sealing tungsten-barium cathodes of various geometry, to prevent leakage of the activating BaCO₃ to the outside of the cathode structure. The tests were made with a specially designed laboratory setup in which electron-beam welding could be carried out in vacuum up to 5×10^{-5} Torr (Fig. 1). The welding electron gun operated at 40 kv accelerating voltage and was fed from a source of power up to 2.5 kw. Special welding joints had to be designed to produce a hermetically-tight welded seam. The construction of the optimal cathode and of the proper welding joint are briefly described. Tests have shown the new cathode construction to be immune to leaks resulting from repeated heating and cooling. Orig. art. has: 3 figures.

CLASS REF: 001

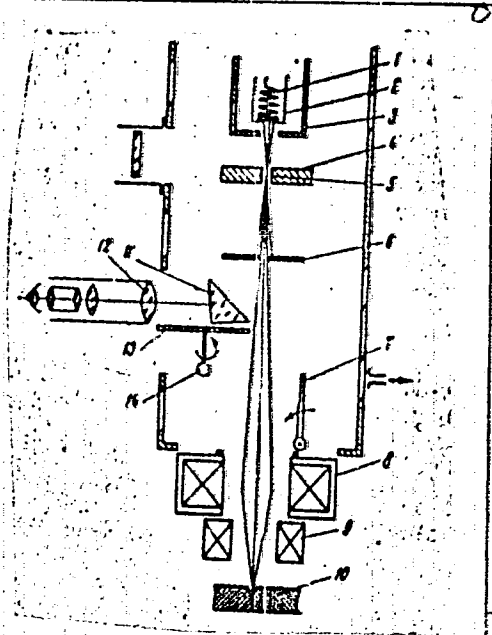
Card 1/2

UDC: 621.385.735

L 27059-66

ACC NR: AP6007843

Fig. 1. Diagram of electron-beam welding gun.
1 - Heater, 2 - cathode, 3 - focusing electrode,
4 - anode, 5 - electron beam, 6 - aperture dia-
phragm, 7 - beam shutter, 8 - focusing lens,
9 - defelecting system, 10 - welded article,
11 - prism, 12 - optical system, 13 - shielding
glass, 14 - glass rotating mechanism.



SUB CODE: 09, 11, 13/ SUBM DATE: 25Dec64/
ORIG REF: 001

Card 2/2

NAZARENKO, O.M.; SHAKH, TS.I.; KAGAN, F.Yu. [Kahan, F.IU.]

Improving the skill of analytical chemists. *Farmatsev. zhar.* 16
no.3:78-80 '61. (MIRA 14:6)

1. Kiyevskiy institut usovershenstvovaniya vrachey.
(PHARMACY--STUDY AND TEACHING)

NAZARENKO, O.V.; BELITSKAYA, S.G.

Data on the induced polarization of potential electrodes obtained
in resistivity prospecting. Trudy AzNII DN no.4:223-229 '56.
(MIRA 14:4)

(Electric prospecting)

(Polarization)

NAZARENKO, O.V.

Effect of spacing between potential and current electrodes on prospecting results obtained by the use of dipole axial installations. Trudy AzNII DN no.4:230-243 '56. (MIRA 14:4)
(Electrodes)

NAZARETO, O.Y.

Effect on results of errors in determining true distances when
using the AMNB symmetrical apparatus. Azerb.neft.khoz.35 no.11:6-
9 N '56. (MLRA 10:4)

(Prospecting--Geophysical methods)

NAZARENKO, O.V.

Method for continuous marine electrical prospecting. Geol. nefi
1 no.8:40-46 Ag '57. (MIRA 10:12)
(Prospecting--Geophysical methods)

HAZARENKO, O.V.

Using differential apparatus in offshore electric prospecting
on the Makarov shoal. Geol.nefti i gaza 3 no.10:44-47
0 '59. (MIRA 12:12)

1. Azerbaydzhanskiy nauchno-issledovatel'skiy institut po
dobyche nefi.
(Baku archipelago--Electric prospecting--Equipment and supplies)

HAZARENEO, O.V.

The ERSK-57 station for electric prospecting at sea. Reserved.
prom.geofis. no.31:45-74 '59. (MIRA 13:4)
(Electric prospecting)

NAZARENKO, O. V., Cand Tech Sci -- (diss) "Development of ocean electrical exploration with direct current." Moscow, 1960. 15 pp; (Ministry of Geology and Conservation of Mineral Resources USSR, All-Union Scientific Research Inst of Geophysical Methods of Exploration, VNIIGeophysics); 150 copies; free; (KL, 25-60, 133)

S/169/62/C00/009/055/120
D228/D307

AUTHORS: Andreyev, L. I., Bayramov, P. S., Nazarenko, O. V.
and Sarkisov, G. A.

TITLE: Marine electric prospecting (Discourse theses)

PERIODICAL: Referativnyy zhurnal, Geofizika, no. 9, 1962, 41, ab-
stract 9A273 (In collection: Sostoyaniye i perspekti-
vy razvitiya geofiz. metodov poiskov i razvedki pol-
ezn. iskopayemykh, M., Gostoptekhizdat, 1961, 379-380)

TEXT: The method of executing various modifications of marine
electric prospecting is described. The perfecting of developed ty-
pes of equipment led in 1957 to the creation of an ЭPCM-57 (ERSM-
57) marine electric prospecting station. Results, which correspond ✓
well with seismic surveying and drilling data and were obtained by
the method of continuous axial dipole sounding (CADS) and map pro-
filing, are mentioned. At present, marine electric prospecting
can be employed: 1) for reconnaissance surveys in order to seek
anticlinal structures (continuous axial profiling and CADS); and

Card 1/2

Marine electric prospecting ...

S/169/62/000/009/055/120
D228/D307

2) to solve some problems connected with the study of the arched parts of anticlinal folds (CADS and map profiling). [Abstracter's note: Complete translation.]

Card 2/2

ACC NR: AP7001396

(N)

SOURCE CODE: UR/0413/66/000/021/0072/0072

INVENTOR: Nazarenko, O. V.

ORG: none

TITLE: A device for electrical exploration for mineral deposits. Class 21, No.187893

SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 21, 1966, 72

TOPIC TAGS: prospecting, mineral, magnetic dipole, dipole, ferromagnetic material, magnetic induction

ABSTRACT: This Author Certificate presents a device for electrical prospecting for mineral resources by means of magnetic profiling. The device contains a magnetic induction meter and a grounded receiving dipole. To simplify the process under the condition of oceanographic investigations and to improve the work efficiency, the magnetic induction meter is combined with the receiving dipole in such a way that one strand of the receiving dipole cable made of a ferromagnetic material serves as a core of the induction meter.

SUB CODE: 08/ SUBM DATE: 12Mar63

Card 1/1

UDC: 550.837(204.1)

KOROTKOV, A.G.; HAZARENKO, P.V.

Tasks in expanding the production of forging machines and presses.
Sel'khoz mashina no.5:22-25 My '57. (MLRA 10:5)
(Forging machinery)

IL86C-65
ACCESSION NR: AP4049132

the hypothesis that the friction force is connected with the dislocation structure occurring on the friction surface. As evidence they

the experimental results show that the friction force is proportional to the area of the friction surface.

It is shown that the friction force is proportional to the area of the friction surface and not to the length of the friction surface.

The results of the experiment show that the friction force is proportional to the area of the friction surface and not to the length of the friction surface.

The results of the experiment show that the friction force is proportional to the area of the friction surface and not to the length of the friction surface.

The results of the experiment show that the friction force is proportional to the area of the friction surface and not to the length of the friction surface.

The results of the experiment show that the friction force is proportional to the area of the friction surface and not to the length of the friction surface.

The results of the experiment show that the friction force is proportional to the area of the friction surface and not to the length of the friction surface.

The results of the experiment show that the friction force is proportional to the area of the friction surface and not to the length of the friction surface.

L 11860-65

ACCESSION NR: AP4049132

Approximation friction law. This report was prepared by the Institute of Civil Aviation, Kiev, USSR. LRS: 2 figures.

ASSOCIATION: Kiyevskiy institut grazhdanskogo vozdušnogo flota
(Kiev Institute of Civil Aviation)

SUBMITTED: 03Apr64

ENCL: 00

REF CODE: ME. 55

NR REF N. 1

STRUCK: 001

Card 3/3

SECRET

040305-65

REF ID: A15009285

ASSOCIATION: KIGA, Kiev

CONNECTED: 1584-184

001 COVER R, 55

ACCESSION NR: AP5004198

AUTHORS: Kostelski, J. I.; Nazarenko, P. V.

26
22
B

TITLE: Interaction of surfaces during external dislocation

SOURCE: AN SSSR. Doklady. v. 160, no. 1, 1968, pp. 1-3, 115-116

TOPIC TAGS: friction, dislocation motion, dislocation interaction

ABSTRACT: The purpose of the investigation was to study the relation between the surface states and the internal structures of bodies in friction. The authors investigated the interaction of dislocations with surface irregularities and the effect of surface roughness on the friction coefficient. It is shown that the interaction of dislocations with surface irregularities leads to a decrease in the friction coefficient. The authors also investigated the effect of surface roughness on the friction coefficient. It is shown that the interaction of dislocations with surface irregularities leads to a decrease in the friction coefficient.

1/3

ACCESSION NR: AP5004198

3

structure in the substance was investigated by means of the etch
 pits corresponding to the emergence of dislocations on the surface
 and by studying the slip bands. It is deduced that the jogs result-
 ing from deformation of the metal give rise to the formation of sub-
 structures. The surface was investigated by means of a scanning electron
 microscope. The plates were then deformed by tension and the friction
 surfaces were measured. The results show that the surface roughness
 increases with the amount of deformation. The roughness is measured
 for stainless steel, aluminum, and alpha brass, respectively.
 The micro-geometry of the surface of the plates remained
 practically unchanged. It is concluded therefore that in external
 friction of crystalline bodies a unique submicrorelief appears on
 the friction surfaces as a result of the external forces, and is the
 consequence of motion and interaction of dislocations. The
 roughness of the surface of the plates was measured by scanning electron

4265
ACCESSION NR: AP5004198

ASSOCIATION: Kiyevskiy institut grazhdanskogo vordushuogo flota
(Kiev Institute of Civil Air Fleet)

SUBMITTED: 03Apr64

ENCL: 00

SUB CODE: SS, ME

NR REF SOV: 004

OTHER: 002

Card

3/3

ACC NR: AF7004184

SOURCE CODE: UR/0369/66/002/006/0664/0667

AUTHOR: Nazarenko, P. V.; Zaytsev, O. V.; Kostetskiy, B. I.

ORG: Kiev Institute of Engineers of Civil Aviation (Kiyevskiy institut inzhenerov grazhdanskoj aviatsii)

TITLE: Effect of initial dislocation density on external friction force and the ratio between elastic and plastic deformations

SOURCE: Fiziko-khimicheskaya mekhanika materialov, v. 2, no. 6, 1966, 664-667

TOPIC TAGS: crystal dislocation, elastic deformation, plastic deformation, friction

ABSTRACT: The process of external friction between solids is chiefly represented by elasto-plastic deformation. In this connection, the deformation of NaCl monocrystals (which have a simple cubic lattice that clearly reveals dislocation and are sufficiently photoactive for examining their deformation in polarized light) was estimated with the aid of a specially designed machine which makes it possible to determine the elastic and plastic components of deformation according to the illumination intensity of double-refraction bands directly in the process of friction under both static and dynamic loads. Dislocation density was determined according to etching pits. Findings: the initial dislocation density of the materials in friction markedly affects the relationship between the plastic and elastic deformations arising in the process

Card 1/2

ACC NR: AP7004184

of friction. When the dislocation density is at a minimum or at a maximum, the elastic component accounts for the greater part of the total deformation. When the dislocation density is medium, the plastic component accounts for the greater part of the total deformation. The friction coefficient is higher in the materials which during friction are subject to considerable plastic deformation. The initial dislocation density influences the formation of the friction force inasmuch as it influences the magnitude of and ratio between the elastic and plastic components of the deformation arising during friction, with the magnitude of the plastic deformation being the principal factor. Orig. art. has: 4 fig.

SUB CODE: 13, 11/ SUBM DATE: 29Jul66/ ORIG REF: 003

Card 2/2

USSR/Forestry - Forest Plants.

K-5

Abs Jour : Ref Zhur - Biol., No 2, 1958, 5933

Author : Nazarenko, S.I.

Inst :

Title : Autumn and Winter Horse Chestnut Sowings in the South of the UkSSR.

Orig Pub : Lesn. kh-vo, 1957, No 6, 83.

Abstract : No abstract.

Card 1/1

NAZARENKO, S.I.

Experience in cultivation of dog rose with high vitamin content
in the southern Ukraine. Apt. delo li no.4:26-29 JI-Ag 162.
(HIRA 17:11)

1. Botanicheskiy sad Odesskogo gosudarstvennogo universiteta
imeni Mechnikova.

NAZARENKO, S.I. (Kiyov)

Excretion of estrogen fractions in otosclerosis. Zhur. ush., nos.
i gor. bol. 24 no.2:12-14 Mr-Apr '64 (NIRA 18:1)

1. Iz laboratorii biokhimii i surdologicheskogo otdela Nauchno
issledovatel'skogo instituta otolaringologii Ministerstva zdravc-
okhraneniya UkrSSR (direktor i nauchnyy rukovoditel' - zaslužen-
nyy deyatel' nauki prof. A.I. Kolomyichenko).

1. NAZARENKO, S. K.
2. USSR (600)
4. Incubators
7. Letter to the editor. Pittsevodstvo no. 10, 1952.

9. Monthly List of Russian Accessions, Library of Congress, February 1953. Unclassified.

TSUKERMAN, R.V., kand.tekhn.nauk; NAZARENKO, S.S., inzh.

Cost indices of high-capacity steam boiler manufacture.
Energomashinostroenie 7 no.10:33-36 0 '61. (MIRA 14:10)
(Boiler-making industry)

TSUKERMAN, R.V., kand. tekhn. nauk; BULANOV, N.G., kand. ekon. nauk;
SHIFRIN, I.B., inzh.; BRIL', A.R., inzh.; NAZARENKO, S.S.,
inzh.; BIZINA, N.S., inzh.

Auxiliary equipment of steam turbine electric power plants.
Energomashinostroenie 11 no.9:40-42 S '65. (MIRA 18:10)

3201H

S/140/62/000/004/007/009
C111/C333AUTHOR: Nazarenko, T. I.

TITLE: The numerical solution of the Cauchy problem for a class of linear integro-differential equations

PERIODICAL: Vysshiyе uchebnyye zavedeniya. Izvestiya. Matematika, no. 4, 1962, 110-117

TEXT: Considered is the numerical solution of the Cauchy problem ✓

$$z^{(1)}(x) + \sum_{i=1}^l a_i(x) z^{(l-i)}(x) + \lambda \int_a^b \sum_{i=0}^s K_i(x,y) z^{(s-i)}(y) dy = f(x) \quad (1)$$

$$z^{(i)}(c) = z_p^{(i)} \quad (i=0, 1, \dots, l-1), \quad c \in [a, b], \quad (2)$$

where $a_i(x)$ and $f(x)$ are continuous on $[a, b]$; $K_i(x, y)$ together with its sufficiently high derivatives being continuous in $a \leq x, y \leq b$. At first one investigates the case $s = 0$ and substitutes the corresponding equation by a difference equation. Thereby one chooses the step-length

Card 1/4

S/140/62/000/004/007/009
C111/C333

The numerical solution of the ...

$h = \frac{b-a}{n}$. The values of the derivatives of Z in the points $x = x_i$ are expressed by the values of Z itself in points which are lying symmetrical with respect to $x = x_i$ according to formulas out of Ref. 2 (Ref. 2: Sh. Ye. Mikeladze, Chislennyye metody matematicheskogo analiza [Numerical methods of the mathematical analysis] GITTL, M., 1953) e. g.

$$Z_i^{(2m-1)} = \frac{\sum_{q=1}^m \binom{m}{q} (Z_{i+q} - Z_{i-q})}{2h^{2m-1}} + R_i^{(2m-1)} \quad (4)$$

where the remainder is estimated. The integral is calculated according to the trapeze formula. If $l = 2m-1$, then (1) is written down with $s = 0$ as a difference equation in the points $x = x_i$ ($i=m, m+1, \dots, n-m$). The so obtained system is completed to a complete system by aid of the initial conditions. Similarly one handles the case $l = 2m$. Approximative values Z_i of $Z(x_i)$ are determined out of the obtained complete system of difference equations by neglecting the remainders in the formulas (4) and in others. The error $\epsilon_i = Z_0 - \tilde{Z}_i$ is estimated.

Card 2/4

S/140/62/000/004/007/009
 C111/C333

The numerical solution of the . . .

Adjoining one considers the case $s \neq 0$. There the equation (1) is brought into the shape

$$Z^{(l)}(x) + \sum_{i=1}^l a_i(x) Z^{(l-i)}(x) + \lambda \left[\sum_{i=1}^l B_{i-1}(x, b) Z^{(s-i)}(b) - \sum_{i=1}^l B_{i-1}(x, a) Z^{(s-i)}(a) \right] + \lambda \int_a^b K(x, y) Z(y) dy = f(x), \quad (30)$$

where $B_i(x, y) = \sum_{j=0}^i (-1)^j \frac{\partial^j K_{l-j}(x, y)}{\partial y^j}$, $K(x, y) = B_s(x, y)$.

by termwise partial integration. Hints concerning the choice of the step h are given in the cases $l \geq s$ and $l < s$.

Card 3/4

The numerical solution of the . . . S/140/62/000/004/007/009
C111/C333
ASSOCIATION: Irkutskiy gosudarstvennyy universitet im. A. A. Zhdanova
(Irkutsk State University im. A. A. Zhdanov)
SUBMITTED: July 20, 1959

Card 4/4

S/199/63/004/002/005/013
B112/B 234

AUTHOR: Nazarenko, T. I.

TITLE: Numerical solution of Cauchy's problem for a class of linear integro-differential equations of the Volterra type

PERIODICAL: Sibirskiy matematicheskiy zhurnal, v. 4, no. 2, 1963, 303 - 308

TEXT: The integro-differential equation

$$z^{(n)}(x) + \sum_{i=1}^n a_i(x) z^{(n-i)}(x) + \int_{x_0}^x K(x,y) z(y) dy = f(x) \quad (1) \text{ with the}$$

initial conditions $z^{(i)}(x_0) = z_0^{(i)} \quad (i = 0, 1, \dots, n-1) \quad (2)$ is replaced by the difference system

$$\sum_{k=0}^{i-(m+1)} E_{ik} z_k + \sum_{k=i-m}^{i+m-1} E_{ik} z_k + z_{i+m} = 2h^{m-1} f_i \quad (7)$$

$E_{ik} = 2h^{m-1} \lambda_{ik} K_{ik}$

Card 1/3

S/199/63/004/002/005/013
B112/B E34

Numerical solution of Cauchy's ...

$$E_{i(i-q)} = 2h^{2m} \lambda d_{i(i-q)} K_{i(i-q)} + 2 \sum_{j=1}^{m-q} h^{2j-1} a_{(i-j)} \beta_q^{(m-1)} - \sum_{j=1}^{m+1-q} h^{2j-1} a_{(i-j)} \alpha_q^{(m+1-l)} \quad (q=0, 1, \dots, m), \quad (8)$$

$$E_{i(i+q)} = 2 \sum_{j=1}^{m-q} h^{2j-1} a_{(i-j)} \beta_q^{(m-1)} + \sum_{j=1}^{m+1-q} h^{2j-1} a_{(i-j)} \alpha_q^{(m+1-l)} \quad (q=1, 2, \dots, m-1), \quad z_0 = z_q, \quad (9)$$

$$[1 - (-1)^p] \sum_{q=0}^{p+1} \gamma_q^{(p+1)} z_q + [1 + (-1)^p] \sum_{q=0}^{p+1} \delta_q^{(p+1)} z_q =$$

$$= [1 - (-1)^p] 2h^p z_0^{(p)} + [1 + (-1)^p] h^p z_0^{(p)} \quad (p=1, 2, \dots, 2m-2).$$

for $n = 2m - 1$, and by

$$\sum_{k=0}^{l-(m+1)} A_{lk} z_k + \sum_{k=l-m}^{l+m-1} F_{lk} z_k + G_l z_{l+m} = 2h^{2m} f_l \quad (10)$$

Card 2/3

S/199/63/004/002/005/013
B112/B234

Numerical solution of Cauchy's ...

for $n = 2m$. Conditions for the stability of the system (7) - (10) are derived. There are 2 tables.

SUBMITTED: August 21, 1961

Card 3/3

HAZARENKO, T.N.

Effect of conditioned reflex bonds on daily variations in
intraocular pressure. Vest.oft. 34 no.5:8-13 S-O '55
(MLRA 8:11)

1. Iz glaznoy kliniki (dir.-prof. N.M.Pavlov) Stravropol'skogo
meditsinskogo instituta.

(REFLEX, CONDITIONED,

conditioned variations daily rhythm of intra-ocular
pressure)

(EYE,

tension, conditioned variations of daily rhythm)

NAZARENKO U.P.

Subject : USSR/Electricity

AID P - 1165

Card 1/1 Pub. 29 - 18/31

Author : Nazarenko, U. P., Eng.

Title : Determination of the amount of leak of compressed air from air ducts

Periodical : Energetik, 11, 26-29, N 1954

Abstract : The author finds that the power consumed for air compression used in the mechanization of various industrial processes amounts to from 20 up to 30 per cent of the total electric power consumption. It is therefore of utmost importance to reduce losses of energy caused by air leaks. He finds a method of measuring those leaks and of determining the productivity of compressors. Six diagrams and 4 tables.

Institution : None

Submitted : No date

NAZARENKO, U.P.; AKULOV, Ye.F., red.; KIREYEV, M.I., red.; NOVIKOV, V.K.,
red.; SAVEL'YEV, V.I., red.; CHUMAKOV, N.M., red.; AFANAS'YEV, N.A.,
red.; BORUNOV, N.I., tekhn. red.

[Economy in the use of electricity in compressor plants] *Ekonomiia
elektroenergii v kompressornykh ustanovkakh.* Moskva, Gos. energ.
izd-vo, 1961. 79 p. (MIRA 14:8)

(Electric power)