

YEL'YASHKEVICH, Samuil Abramovich; PEVZNER, I.M., inzh., retsenzent; BABUK, G.V., inzh., retsenzent; PEVZNER, I.N., red.; ZHITNIKOVA, tekhn. red.

[Elimination of faults in television receivers] Ustranenie neispravnostei v televizore. Izd.3., perer. i dop. Moskva, Gos. energ. izd-vo, 1961. 205 p. (Massovaya radiobiblioteka, no. 387)
(Television—Repairing)

PEVZNER, I.S.

Clinical aspects of cardiac tamponade. Zdrav. Belor. 6 no.4:67-
68 Ap '60. (MIRA 14:5)

1. Minskaya oblastnaya klinicheskaya bol'nitsa (glavnyy vrach
G.A.TSgoyev).
(HEART—DISEASES)

PEVZNER, I.S.

Hardness of abrasive tools. Standartizatsiia 25 no.6:34-60
Je '61. (MIFA 14:6)

(Grinding wheels--Standards)

IVANOV, I.T., kandidat tekhnicheskikh nauk, otvetstvennyy redaktor;
ANTONOV, K.K., redaktor; VOLZHENSKIY, A.V., redaktor; GORNOV, V.N.,
redaktor; KUZNETSOV, G.P., redaktor; ~~PEYZNER~~, I.V., inzhener,
redaktor; ROTERT, P.P.; FRIDBERG, G.V., redaktor; PECHKOVSKAYA,
T.V., tekhnicheskiy redaktor

[Skyscraper designs; experience in design and construction] Konstruk-
tsii vysootnykh zdaniy; iz opyta proektirovaniya i vozvedeniya. Red.
kollegiya I.T.Ivanov, K.K.Antonov, A.V.Volzhenskii i dr. Moskva,
Oos. izd-vo lit-ry po stroitel'stvu i arkhitekture, 1952. 103 p.
[Microfilm] (MLRA 7:10)

1. Chlen-korrespondent Akademii arkhitektury SSSR (for Antonov,
Volzhenskiy, Gornov, Kuznetsov, Rotert) 2. Akademiya arkhitektury
SSSR, Moscow. Institut stroitel'noy tekhniki.
(Skyscrapers)
(Architecture--Designs and plans)

PEVZNER, I.Ya.

Diagnosis of auricular infarct. Terap. arkh. 29 no.7:48-51 J1 '57.
(MIRA 11:4)

1. Iz kliniki propedevtiki vnutrennikh bolezney (zav.-prof. S.V.
Shestakov) Kuybyshevskogo meditsinskogo instituta.
(MYOCARDIAL INFARCT, diagnosis,
auric. (Rus)

PEVZNER, I.Ya. (Chapayevsk)

Rupture of the right ventricle of the heart. Kaz. med. zhur.4:
60 JI-Ag'63 (MIRA 17:2)

PEVZNER, I.Ya. (Kuybyshev)

Nature of various conduction disorders in myocardial infarct. Pat.
fiziol. i eksp.terap. 3 no.6:62 N-D '59. (MIRA 13:3)

1. Iz kliniki propedevtiki vnutrennikh bolezney (zaveduyushchiy -
prof. S.V. Shestakov) Kuybyshevskogo meditsinskogo instituta.
(MYOCARDIAL INFARCT pathology)

ZHEVNOVATYY, A.I.; VOLKOV, V.N.; PEVZNER, I.Z.; Prinimali uchastiye:
KRUK, O.P.; KRUTITSKIY, V.M.; KOL'TSOV, I.M.; TSVETKOV, F.A.

Effect of elastic ultrasonic waves on reducing the speed of
scale formation. TSvet. met. 35 no.3:48-53 Mr '62. (MIRA 15:4)

(Ultrasonic waves--Industrial applications)

ABRAMOV, V.Ya.; PIVNER, I.I.

Analysis of the performance of heavy calcination in the
alumina production. Izvet. nat. SP no. 212. P. 121.
(USSR 18:3

Pevzner, K. S.

27
The determination of niobium in titanium tetrachloride.
K. S. Tramm and K. S. Pevzner. *Zapodskaya Lab.* 22,
1025-7(1956). Two methods are recommended for the
detr. of Nb in $TiCl_4$, where the ratio of concns. may reach
1-25,000. (1) Most of the $TiCl_4$ can be sepd. by volatiliza-
tion at a pressure of 50 mm. (at which pressure $TiCl_4$ boils
at 60°), and Nb is then detd. colorimetrically in an aliquot
of the residue with CNS^- . (2) Nb can be detd. by pptn.
with tannin from a soln. contg. $TiCl_4$. Metallic Cd was
best for reduction. The sensitivity of either method is
around 0.001% Nb, and can be increased by the detr. of Ti
in the Nb residue.
W. M. Sternberg

4
27 1-AE2C

PEVZNER, ~~SS~~ K.S.

000

✓ 2610. Separation of tantalum from titanium by extraction. Yu. A. Chernikhov, R. S. Tramm and K. S. Pevner, *Zapod. Lab.*, 1958, 23 (6), 637-639. Tantalum is separated from Ti by extraction with cyclohexanone from a soln. (15 ml) of 0.4 M HF in 2 M H₂SO₄ containing 1 to 3 mg of Ta₂O₅ and 1-100 mg of TiO₂. The extraction is carried out three times with 5-ml portions of the solvent. The second extract contains > 1 per cent. of the Ta and the third is free from Ta. Re-extraction of the Ta is carried out by 7 ml of a soln. containing 4 g of ammonium oxalate and 4 g of boric acid in 100 ml. The extraction is carried out three times. The third extract contains > 0.06 per cent. of the Ta and the solvent layer then contains > 0.07 per cent. of the Ta. Determination of the Ta is carried out by evaporating an aliquot portion of the separated aq. phase with H₂SO₄ and H₂O₂ to destroy organic matter and applying the colorimetric pyrogallol reaction (cf. Marry, *Anal. Abstr.*, 1936, 2, 2083). The method is also suitable for the separation of Ta from Nb. G. S. SMITH

DM
LFH

5(2)

AUTHORS:

Shervishov, Ya. A., Gram, K. G., Fevzner, K. S. SCV: 52-25-4-4 71

TITLE:

Determination of Tantalum in Niobium (Opredeleniye tantala v niobii)

PERIODICAL:

Doklady Akad. Nauk SSSR, Vol. 25, Nr. 4, pp. 3-4-1967 (USSR)

ABSTRACT:

As the niobium is used for heat-resisting alloys, the content of tantalum in it is strictly limited. A method is described by which tantalum in niobium is determined according to the reaction with pyrogallol in a mixture of sulphuric and oxalic acid on the photocolorimeter PEK-N with a light filter Nr. 2 (413 nm). The tantalum is extracted from the main quantity of the niobium with oxalic acid from a hydrofluoric-sulphuric-acid mixture before the determination (Ref. 1). The present paper is completed in 1957, i.e. before the publication of a similar article (Ref. 2). It was ascertained that at a concentration of 0.4 - 1.2 moles and sulphuric acid, tantalum practically passes completely into the oxalic acid layer (Table 1). The reliability of the described method was examined by the method of analysis of Nb₂O₅ samples (Tables 2, 3).

Cont. 1/2

SOV/32-25-4-4.71

Determination of Tantalum in Niobium

The determination can be carried out with a sensitivity of 0.02% and an accuracy of $\pm 0\%$ which is usual in the analysis of trace elements. It is recommended for analysis of alloys to transfer the niobium into the oxide before analysis. There are 3 tables and 4 references, 3 of which are given.

ASSOCIATION: G. A. Kuznetsov, Nauchno-Issledovatel'skiy institut rezhimov i tekhnologii (State Scientific Research Institute of Regime and Technology)

Card 2, 1

ACCESSION NR: AP4015321

S/0032/64/030/001/0020/0022

AUTHORS: Tramm, R. S.; Pevzner, K. S.

TITLE: Photometric determination of niobium content in ores with the use of acid chromoviolet pigment K

SOURCE: Zavodskaya laboratoriya, v. 30, no. 1, 1964, 20-22

TOPIC TAGS: niobium; niobium ore, chromoviolet pigment, K pigment, Nb detection, B pigment, SF 10 spectrophotometer, FEK N 54 photoelectrocolorimeter

ABSTRACT: The formula for the chromoviolet pigment K is identical to that for the anthracene-chromoviolet die B previously used for photometric determination of Nb in ores. Pigment B (a sodium salt 5-sulfo-2-oxybenzene-azo- β -naphthol) is applicable for detecting Nb in the presence of large quantities of Ti. Both pigments have similar absorption curves, but the specific absorption intensity of K is somewhat lower. The B pigment is soluble in water while K is soluble in the water-acetone solution. The red-violet reaction of Nb with K takes place in hydrochloric acid and is not affected by tartaric acid added to prevent the hydrolysis of Nb. The maximum color intensity is obtained in 40 minutes at room

Card 1/2²

ACCESSION NR: AP4015321

temperature and in 5-10 minutes after warming in hot water to 60-70C. The optical density of the solutions of Nb with the pigment is directly proportional to the Nb concentration. The light-absorption curves of the K solutions and of the K combination with Nb were registered by the SF-10 spectrophotometer. The experiments were performed in the photoelectrocolorimeter FEK-N-54. The results obtained are shown on Fig. 1 of the Enclosure. The minimum Nb quantity detected was 2 micrograms in 10 milliliters. "T. F. Kuznetsova and L. P. Savel'yeva participated in the experimental work." Orig. art. has: 2 tables and 1 figure.

ASSOCIATION: Gosudarstvennyy nauchno-issledovatel'skiy i proyektnyy institut redkometallicheskoj promyshlennosti (State Scientific Research and Design Institute of Rare Metals Industry)

SUBMITTED: 00

DATE ACQ: 03Feb64

ENCL: 01

SUB CODE: MM

NO REF SOV: 004

OTHER: 001

Card 2/2

L 29982-65 EWT(m)/EPF(n)-2/EPR/EWP(t)/EWP(b) Ps-4/Pu-4 IJP(c) JD/WW/JG

ACCESSION NR: AP5005473

S/0032/65/031/002/0163/0163

AUTHORS: Tramm, R. S. Pevsner, K. S.

TITLE: Titrimetric determination of zirconium and aluminum in binary alloys

SOURCE: Zavodskaya laboratoriya, v. 31, no. 2, 1965, 163

TOPIC TAGS: zirconium, aluminum, titrimetry, alloy, hydrochloric acid, thorium compound, chemical reaction, complexone

ABSTRACT: The large difference of the pH values in titrating zirconium and aluminum makes it possible to determine the amounts of these elements consecutively in one solution. The mean quadratic error of the determination is up to 0.7% for zirconium and 1.3% for aluminum. Zirconium is titrated in 2-N hydrochloric acid with xylenol orange indicator; aluminum is determined by reverse titration of the excess complexone III with a thorium solution, using the same indicator. The process consists of melting the alloy with potassium pyrosulfate, treating it with hydrochloric acid, filtering out the sesquioxides and dissolving them in hydrochloric acid. Xylenol orange is then added to the hot solution, and zirconium is titrated with complexone III. After the bright magenta color changes to pink, the solution is heated to boiling, and complexone is added in drops until the color

Card 1/2

L 29982-65

ACCESSION NR: AP5005473

turns yellow. The solution is then cooled, treated with more complexone, and left to stand at room temperature. Next, the solution is neutralized with ammonia, diluted with water, and mixed with monochloroacetic acid, sodium acetate, and xlenol orange. The excess of complexone is then titrated with thorium nitrate until the yellow coloration changes to red. The amount of aluminum present is determined from the amount of complexone used.

ASSOCIATION: Gosudarstvennyy nauchno-issledovatel'skiy i proyektnyy institut redkometallicheskey promyshlennosti (State Scientific Research and Design Institute of the Rare Metal Industry)

SUBMITTED: 00

ENCL: 00

SUB CODE: 1C, Gd

NO REF SOV: 001

OTHER: 000

Card 2/2

SECRET
NO FORN DISSEM
EO 1.4(c)

AUTHORS:

Chernikova, Yu. A. et al. R. S. S. R. Acad. Sci. Div. Chem. Sci. Ser. B, 1974, No. 1, p. 1241

TITLE:

Titration of the rare earth elements with EDTA in the presence of complex-forming agents
Zavodskaya laboratoriya, Leningrad, U.S.S.R.

PERIODICAL:

TEXT: In the present paper the possibility is examined of successively determining thorium and the total content of rare earths by complexometric titration at different pH values without preceding separation. The selectivity of the method is attained at low pH values. Therefore, xylenol orange, alizarin red S, and arsenazo were used as indicators. The composition of the rare earth mixture is such: 5% of CaO converted to Ca_2O_3 , 25% of La_2O_3 , 13% of Nd_2O_3 , 4% of Pr_6O_{11} and 0.5% of Sm_2O_3 . All completely 1% of the yttrium group was present; the average molecular weight of the mixture was 392. First, thorium was titrated with complexon III at a pH less than 3. At a pH = 1.5 - 2.5, a distinct color transition from red to lemon takes place when xylenol orange is used. with alizarin red S red

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APPROVED FOR RELEASE

Successive Complexometric Determination of Thorium and the Totality of the Rare Earths

S/O 10/10/60
R/C 20

changes into green. In the presence of rare earths, the pH of the solution
titration must not exceed 2.2. Not even a ten-fold excess of rare earths
interferes in the thorium determination at a pH of 1.5 - 1.6. Table 1 gives
the effect of some admixtures on the determination of thorium with xylenol
orange. Fe^{3+} interferes with the determination of thorium in the presence of
masked by additions of ascorbic acid. Nitrates and sulfates of rare earths
do not interfere, but phosphates must not be present. In the determination of
thorium against alizarin red S as indicator, the presence of aluminum
interferes even in micromolar amounts. With an addition of 1 mg. of aluminum
the maximum amount of Al must not exceed 1 mg. Mn²⁺ can only be present in
amounts lower than 3 mg. Nickel must not be present. In the determination of
thorium in the presence of ascorbic acid, a color change takes place (with an
1.6, a color transition from violet to pink takes place (with an addition of
rare earths). Rare earths were titrated in the presence of xylenol orange and
of an acetate buffer with pH 1.5 and xylenol orange. The hydrolysis of thorium
Cerium was previously reduced by ascorbic acid. The hydrolysis of thorium
is prevented by an addition of 1 mg. of ascorbic acid. Since the color
transition is not distinct (especially in the presence of rare earths).

Card 2/4

Successive Complex formation of Thorium and the Totality of the Rare Earths

$\text{C}^{\text{I}} = \text{FCO}^{\text{I}}$ $\text{C}^{\text{II}} = \text{FCO}^{\text{II}}$
 $\text{BC} = \text{O}, \text{FC}^{\text{I}}$

Thorium and the Tetravalent Rare Earths

methylene blue is added. Table I gives the effect of concentrations on the titration of the rare earths. To find the concentration amounts of up to 70 mg for 150 ml. Mn has to be removed by a double extraction by chloroform with pH = 5. Aluminium must be removed as insoluble precipitate of sulfosalicylic acid. If aluminum is added in amount of up to 1 mg, rare earths can be titrated without disturbing the color. If aluminum more is used as indicator, not more than 30 mg of Th are allowed to be present. In the titration of rare earths against arsenazo III, color transition only takes place at a pH of 5.5 while in the presence of thorium a color transition was observed. Since in this case arsenazo III forms a complex which is more stable than its complex rare. This explains orange and slightly red S may be used for the determination of thorium and rare earths. The best suited best. Successive titrations of rare earths with arsenazo III are also possible. Approximately 10% of the total amount of rare earths can be determined. Analysis is described in detail. A few examples are given. The results of analysis are mentioned. There are tables and figures. The following countries are mentioned: 2 Czech, 1 Austrian, 1 Swiss, 1 US, and 1 Hungarian.

Card 3/4

Successive Complex metal...
Thorium and the Totality of the...
S...
...PO...

ASSOCIATION: Gosudarstvennyy...
institut' redkometall...
and Planning Scientific Research Institute of the Rare
Metals Industry

Card 4/4

MALYUTIN, T.M.; TRAM, R.S.; PEVZNER, K.S.

Differential spectrophotometric determination of titanium with
diantipyrylmethane. Zav.lab. 31 no.9:1054-1057 '65. (MIRA 18:10)

1. Gosudarstvennyy nauchno-issledovatel'skiy i proyektnyy institut
redkometallicheskoj promyshlennosti.

TRAMM, R.S.; PEVZNER, K.S.

Complexometric determination of zirconium and aluminum in binary alloys. Zav. lab. 31 no.2:163 '65. (MIRA 18:7

1. Gosudarstvennyy nauchno-issledovatel'skiy i proyektnyy institut redkometallicheskey promyshlennosti.

TRAMM, R.S.; PEVZNER, R.S.

Photometric determination of the concentration of
chromophore violet R. Zav. int. 30. 11. 1964. 1964.

1. Gosudarstvennyy nauchno-issledovatskiy tsentr
institut radiofizicheskoy khimii i fiziki.

S/137/62/000/003/178/191
A160/A101

AUTHORS: Chernikov, Yu. A.; Dobkina, B. M.; Tramm, R. S.; Pevzner, K. S.

TITLE: Determining tantalum and niobium in mineral raw materials by colorimetric analysis

PERIODICAL: Referativnyy zhurnal. Metallurgiya, no. 3, 1962, 2 - 3, abstract 3 K5
("Khim., fiz., khim. i spektr. metody issled. rud redk. i rasseyan. elementov", Moscow, Gosgeoltekhizdat, 1961, 108 - 115)

TEXT: Conditions have been developed required for determining Ta in columbite and tantalite concentrates containing Nb $\geq$ 48 % and Ta $\leq$ 50 %. For eliminating the effect of Ti, an appropriate amount of it is introduced into the index solutions. When Ta is analyzed by the photometric means within the visible region of spectrum, Ti is separated-off in advance, by using tannin. The photometric analysis of Ta is carried out at 325 m μ right after the fusion of the assay with K pyrosulfate and leaching of the melt with an (NH₄)₂C₂O₄ solution, without separating it in advance, from other elements. The presence of < 30% Ti does not hinder the determination of Ta. The photometric analysis of Ta is performed on Specker's colorimeter within a concentration range of 0.4 - 0.7 mg/

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62
Transformation in 18:8 (chromium-nickel) austenitic steel. I. Magnetic investigation of the $\gamma \rightarrow \alpha$ transformation. G. AKISOV and L. PAVLOV. II. Investigation of the transformation by thermoelectric method. G. AKISOV and

N. TOMANOV. III. Thermal expansion of cold-worked 18:8 steel. IV. The $\gamma \rightarrow \alpha$ transformation in 18:8 austenitic steel deformed by twisting at different temperatures. G. AKISOV and J. FRENKMAN. V. Thermal analysis of deformed and hardened stainless steel. G. AKISOV and N. TOMANOV (Tech. Phys. U.S.S.R., 1958, 3, 142-148, 149-154, 155-157, 158-164, 165-175).—1. When austenitic 18:8 stainless steel is cold-rolled, transformation of γ into α starts along the grain boundaries and slip planes and reaches 45% after a reduction of the cold-worked metal the subsequent heating of the cold-worked metal the amount of α begins to increase at 250° and the rate of transformation increases with the degree of reduction, a definite relation between α and γ being established for a definite temp. and a definite degree of reduction. At 445° reconversion of α into γ begins.

irrespective of the degree of reduction, but above 475° there is a definite equilibrium between the α and γ for each temp., and this varies with degree of reduction up to about 60%, above which it again becomes independent of degree of reduction, since at this temp. α has practically disappeared.

II. Measurements of the e.m.f. between deformed and undeformed 18:8 steel show a sudden change at 465-700° due to the $\alpha \rightarrow \gamma$ transformation. Increase in degree of reduction from 48 to 71% lowers the temp. at which carbide pptn. occurs from 730° to 705°. The thermoelectric power-temp. curve for deformed steel resembles closely the magnetic saturation-temp. curve above 450°.

III. Dilatometric curves for cold-worked 18:8 steel show that a contraction occurs at 500° due to the $\alpha \rightarrow \gamma$ change which is not affected by degree of reduction and an inflexion at 650° probably due to carbide pptn.

IV. The degree of work-hardening of 18:8 steel produced by twisting varies only slightly between 30° and 470°; as the deformation temp. is raised to 300° the magnetic saturation decreases sharply

and at higher temp. approaches zero asymptotically, indicating that transformation of γ into magnetic α practically ceases at 150°. Twisting at room temp. produces a more fine-grained structure, but tends to rupture the grains, whereas twisting at 450°-470° produces no deformation of the microstructure and no refinement of the grain structure.

V. Thermal analysis of cold-worked 18% steel shows a heat effect due to removal of elastic stress starting at 490° and reaching a max. at 540°, a second effect due to carbide pptn. starting at 635° and reaching a max. at 685°, and a third effect due to the beginning of recrystallization at 700°. On reheating the steel after quenching from 1200° heat effects occur at 435° and 540° due to stress removal and at 700° due to carbide pptn.

A. R. P.

PETROV, G., doktor tekhnicheskikh nauk; ~~PEVZNER, I.~~ kandidat tekhnicheskikh nauk; DOROMENKOV, I., inzhener; YEZERSKIY, A., inzhener.

Facing slabs made of phenolite. Stroimaterialy, izdelani konstruktsiya 2
no.5:33-34 My '56. (MLRA 9:8)

(Floors) (Walls)

IONISH, Yu.I.; ANTSEFER, V.F.G., kand. fiz. nauk, reizenent;
BRANOVSKIY, V.A., kand. tekhn. nauk, red.; BRAIAN VSKIY, V.A.,
red.; BYKHOVSKIY, I.I., inzh., red.; VASIL'YEVA, E.V., inzh.,
red.; KOLITYSSKIY, Ya.I., kand. tekhn. nauk, red.; KUSHUL',
M.Ya., doktor tekhn. nauk, red.; PEVZNER, L.A., inzh., red.;
SHEMELEV, V.A., kand. tekhn. nauk, red.; BYSTRITSKIY, V.V.,
red. izd-va M. A. A. A., A.F., tekhn. red.

[Vibrometry: measurement of vibrations and shocks, general
theory, methods and devices: Vibrometriya; izmerenie vibra-
tsii i udarnykh kolebaniy teorii, metody i pribory. Izd....
perel. s angl. M. A. A. A., 1967. 771 p. (MLA 17:2)

PEVNEVA, L. A.

Absorption spectra of colored beryls and topazes. S. V. Grun-Grebimalla and L. A. Pevneva. *Trudy Inst. Krist., Akad. Nauk S.S.S.R.* 1956, No. 12, 85-92; cf. *C.A.* 42, 7667g. — Beryl crystals from the Ural, and topaz from Volhynia were investigated by spectrophotometric measurements in the range $\lambda = 350$ to 1100 m μ . The comparison of the absorption spectra of beryl and topaz shows a strong displacement of the characteristic peaks towards longer waves for beryl, evidently a structural polarization effect.

W. Rittel

2

GRUM- GRZHIMAYLO, S.V.; PEVNEVA, L.A.

Absorption spectra curves for beryls and topazes of different coloration. Trudy Inst.Krist.no.12:85-92 '56. (MLBA 10:2)
(Topaz crystals) (Beryl crystals) (Absorption spectra)

PEVZNER, L.B.

Work of the rheumatic fever section. Zdravookhranenie 2 no.4:
9-11 JI-Ag '59. (MIRA 14:6)

1. Iz 1-oy detskoy bol'nitsy Kishineva (glavnyy vrach - K.I.
Lokhvinskaya). (RHEUMATIC FEVER)

1ST AND 2ND COPIES		3RD AND 4TH COPIES	
PROCESSING AND PROPERTY INDEX			
THERMO-ELECTRIC METHOD OF CLASSIFYING STEELS. G. V. Akinov and L. E. PAVANER. (Zavodskaya Laboratoriya, 1939. No. 12 pp. 1273-1282). (In Russian). The authors describe some preliminary investigations of the thermo-electric e.m.f. produced with thermocouples made up from a number of standard Russian plain and low-alloy steels. The effects of changes in chemical composition and heat treatment of the steels and of the temperature of the hot junction were observed, the object being to work out, if possible, a method of classifying steels by the e.m.f. produced. They describe two types of instrument which were successfully used for the routine classification of certain steel compositions.			
ASB-11A METALLURGICAL LITERATURE CLASSIFICATION			
1939-1940		1941-1942	
1943-1944		1945-1946	
1947-1948		1949-1950	
1951-1952		1953-1954	
1955-1956		1957-1958	
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1967-1968		1969-1970	
1971-1972		1973-1974	
1975-1976		1977-1978	
1979-1980		1981-1982	
1983-1984		1985-1986	
1987-1988		1989-1990	
1991-1992		1993-1994	
1995-1996		1997-1998	
1999-2000		2001-2002	
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2011-2012		2013-2014	
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2195-2196		2197-2198	
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2207-2208		2209-2210	
2211-2212		2213-2214	
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PEVZNER, L. E.

AKIMOV, G.V. AND L.E. PEVZNER

C.A. Vol. 29, Nov. 10 - Dec. 20, 1935

"The Anisotropy of Sheet Steel". F.V. Akimov and L.E. Pevzner. J. Tech. Phys. (U.S.S.R.) 4, 1935-44, 1945-50(1934).

Data on the anisotropy of various carbon steels are given as detd. by the magnetic method. Carbon steels are given as detd. by the magnetic method. An investigation of the distribution of the δ -phase in 18/8 stainless steel is reported. The phase transformation $\gamma \rightarrow \delta$ as a consequence of deformation proceeds first on the grain boundaries and along the slip planes. Carbide sepn. also occurs first along the grain boundaries.

AKIMOV, G. V. C. A. Vol. 26, Aug. 20, 1932 - Nov. 20, 1932

L.F. PEVNER

The anisotropy of sheet steel. G. V. Akimov and L. b. Pevner. *J. Tech. Phys. (U. S. S. R.)* 6, 1935-44, 1945 (SU1944).—Data on the anisotropy of various carbon steels are given as detd. by the magnetic method. An investigation of the distribution of the α -phase in 18-8 stainless steel is reported. The phase transformation $\gamma \rightarrow \alpha$ as a consequence of deformation proceeds first on the grain boundaries and along the slip planes. Carbide sepa. also occurs first along the grain boundaries. F. H. Rathmann

ASB 514 METALLURGICAL LITERATURE CLASSIFICATION

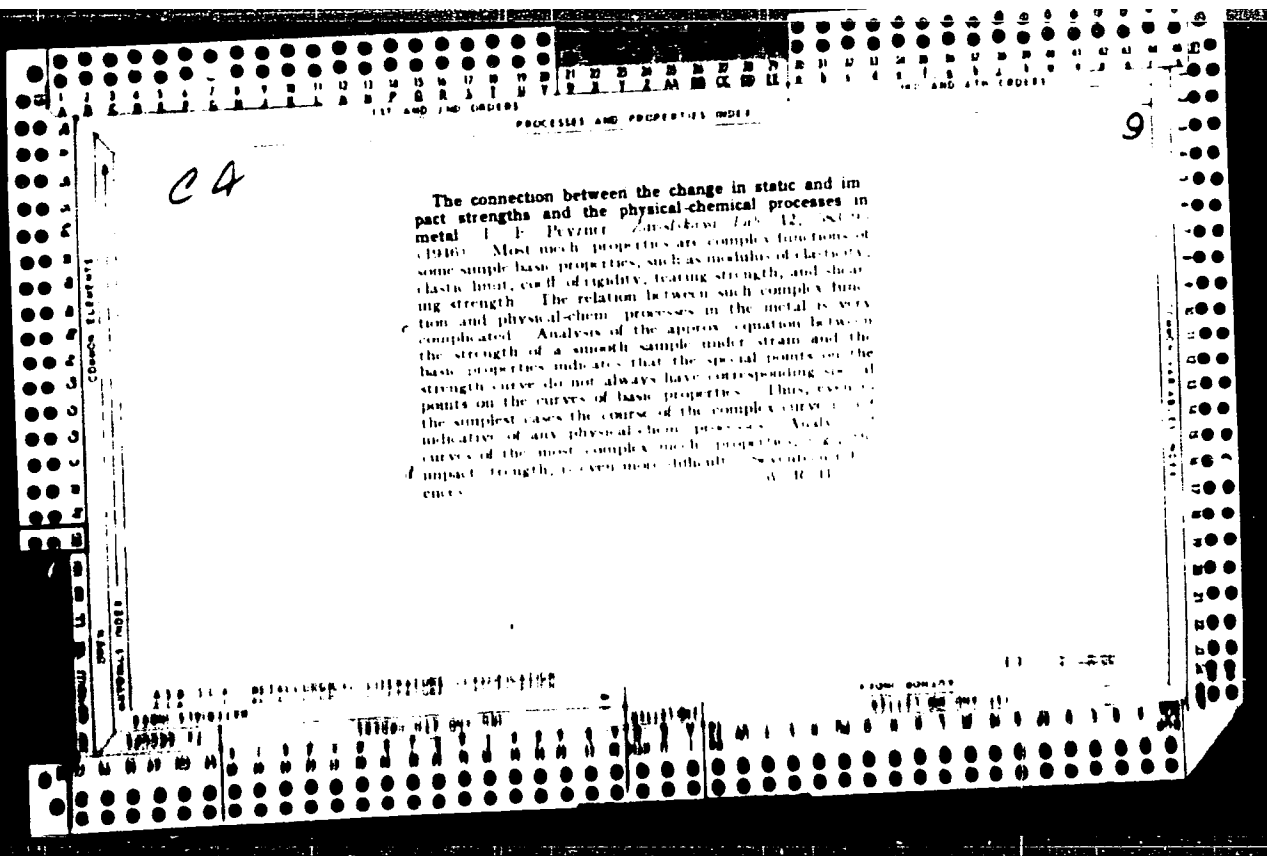
PROCESS AND PROPERTIES INDEX	
Transformation in 18-8 (chromium-nickel) austenitic steel. I. Magnetic investigation of the $\gamma \rightarrow \alpha$ transformation G. V. Akimov and E. Pevzner <i>Tech Phys. U. S. S. R.</i> 3, 142 (1958). When austenitic 18-8 stainless steel is cold-rolled, transformation of γ into α starts along the grain boundaries and slip planes and reaches 45% after a reduction of 80% in thickness. On subsequent heating of the cold-worked metal the rate of α begins to increase at 250° and the rate of transformation increases with the degree of reduction, a definite relation between α and γ being established for a definite temp. and a definite degree of reduction. At 445° reversion of α into γ begins irrespective of the degree of reduction, but above 475° there is a definite equilibrium between the α and γ for each temp., and this varies with degree of reduction up to about 600°, above which it again becomes independent of degree of reduction, since at this temp. α has practically disappeared. II. Investigation of the transformation by thermoelectric method. G. V. Akimov and N. D. Tomashov. <i>Ibid.</i> 149-51. Measurements of the e. m. f. between deformed and undeformed 18-8 steel show a sudden change at 485-700° due to the $\alpha \rightarrow \gamma$ transformation. Increase in degree of reduction from 48 to 71% lowers the temp. at which carbide pptn occurs from 730° to 705°. The thermoelectric power	temp. curve for deformed steel resembles closely the magnetic saturation-temp. curve above 450°. III. Thermal expansion of cold-worked 18-8 steels. G. V. Akimov and Ya. B. Prikman. <i>Ibid.</i> 155-7. Dilatometric curves for cold-worked 18-8 steel show that a contraction occurs at 500° due to the $\alpha \rightarrow \gamma$ change which is not affected by degree of reduction and an inflection at 650° probably due to carbide pptn. IV. $\gamma \rightarrow \alpha$ transformation in 18-8 austenitic steel deformed by twisting at different temperatures. <i>Ibid.</i> 158-64. The degree of work hardening of 18-8 steel produced by twisting varies only slightly between 20° and 470°, as the deformation temp. is raised to 150° the magnetic satn. decreases sharply and at higher temp. approaches zero asymptotically, indicating that transformation of γ into magnetic α practically ceases at 150°. Twisting at room temp. produces a more fine-grained structure, but tends to rupture the grains, whereas twisting at 450-70° produces no deformation of the microstructure and no refinement of the grain structure. V. Thermal analysis of deformed and hardened stainless steel. G. V. Akimov and N. D. Tomashov. <i>Ibid.</i> 165-75. Thermal analysis of cold-worked 18-8 steel shows a heat effect due to removal of elastic stress starting at 490° and reaching a max. at 540°, a second effect due to carbide pptn starting at 650° and reaching a max. at 695°, and a third effect due to the beginning of recrystn. at 800°. On reheating the steel after quenching from 1200° heat effects occur at 435° and 540° due to stress removal and at 700° due to carbide pptn. Also in <i>J. Tech. Phys. U. S. S. R.</i> 6, 94-124 (1958).

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TESTING OF DETAILS BY MEANS OF MAGNETIC POWDERS. A. V. SHIGALOV and L. E. PEVNER (Zavod. Lab., 1936, 5, 182-187).—The application of known methods is discussed. R. T.

AND SEA METALLURGICAL LITERATURE CLASSIFICATION

1936	1937	1938	1939	1940	1941	1942	1943	1944	1945	1946	1947	1948	1949	1950	1951	1952	1953	1954	1955	1956	1957	1958	1959	1960	1961	1962	1963	1964	1965	1966	1967	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100	2101	2102	2103	2104	2105	2106	2107	2108	2109	2110	2111	2112	2113	2114	2115	2116	2117	2118	2119	2120	2121	2122	2123	2124	2125	2126	2127	2128	2129	2130	2131	2132	2133	2134	2135	2136	2137	2138	2139	2140	2141	2142	2143	2144	2145	2146	2147	2148	2149	2150	2151	2152	2153	2154	2155	2156	2157	2158	2159	2160	2161	2162	2163	2164	2165	2166	2167	2168	2169	2170	2171	2172	2173	2174	2175	2176	2177	2178	2179	2180	2181	2182	2183	2184	2185	2186	2187	2188	2189	2190	2191	2192	2193	2194	2195	2196	2197	2198	2199	2200	2201	2202	2203	2204	2205	2206	2207	2208	2209	2210	2211	2212	2213	2214	2215	2216	2217	2218	2219	2220	2221	2222	2223	2224	2225	2226	2227	2228	2229	2230	2231	2232	2233	2234	2235	2236	2237	2238	2239	2240	2241	2242	2243	2244	2245	2246	2247	2248	2249	2250	2251	2252	2253	2254	2255	2256	2257	2258	2259	2260	2261	2262	2263	2264	2265	2266	2267	2268	2269	2270	2271	2272	2273	2274	2275	2276	2277	2278	2279	2280	2281	2282	2283	2284	2285	2286	2287	2288	2289	2290	2291	2292	2293	2294	2295	2296	2297	2298	2299	2300	2301	2302	2303	2304	2305	2306	2307	2308	2309	2310	2311	2312	2313	2314	2315	2316	2317	2318	2319	2320	2321	2322	2323	2324	2325	2326	2327	2328	2329	2330	2331	2332	2333	2334	2335	2336	2337	2338	2339	2340	2341	2342	2343	2344	2345	2346	2347	2348	2349	2350	2351	2352	2353	2354	2355	2356	2357	2358	2359	2360	2361	2362	2363	2364	2365	2366	2367	2368	2369	2370	2371	2372	2373	2374	2375	2376	2377	2378	2379	2380	2381	2382	2383	2384	2385	2386	2387	2388	2389	2390	2391	2392	2393	2394	2395	2396	2397	2398	2399	2400	2401	2402	2403	2404	2405	2406	2407	2408	2409	2410	2411	2412	2413	2414	2415	2416	2417	2418	2419	2420	2421	2422	2423	2424	2425	2426	2427	2428	2429	2430	2431	2432	2433	2434	2435	2436	2437	2438	2439	2440	2441	2442	2443	2444	2445	2446	2447	2448	2449	2450	2451	2452	2453	2454	2455	2456	2457	2458	2459	2460	2461	2462	2463	2464	2465	2466	2467	2468	2469	2470	2471	2472	2473	2474	2475	2476	2477	2478	2479	2480	2481	2482	2483	2484	2485	2486	2487	2488	2489	2490	2491	2492	2493	2494	2495	2496	2497	2498	2499	2500	2501	2502	2503	2504	2505	2506	2507	2508	2509	2510	2511	2512	2513	2514	2515	2516	2517	2518	2519	2520	2521	2522	2523	2524	2525	2526	2527	2528	2529	2530	2531	2532	2533	2534	2535	2536	2537	2538	2539	2540	2541	2542	2543	2544	2545	2546	2547	2548	2549	2550	2551	2552	2553	2554	2555	2556	2557	2558	2559	2560	2561	2562	2563	2564	2565	2566	2567	2568	2569	2570	2571	2572	2573	2574	2575	2576	2577	2578	2579	2580	2581	2582	2583	2584	2585	2586	2587	2588	2589	2590	2591	2592	2593	2594	2595	2596	2597	2598	2599	2600	2601	2602	2603	2604	2605	2606	2607	2608	2609	2610	2611	2612	2613	2614	2615	2616	2617	2618	2619	2620	2621	2622	2623	2624	2625	2626	2627	2628	2629	2630	2631	2632	2633	2634	2635	2636	2637	2638	2639	2640	2641	2642	2643	2644	2645	2646	2647	2648	2649	2650	2651	2652	2653	2654	2655	2656	2657	2658	2659	2660	2661	2662	2663	2664	2665	2666	2667	2668	2669	2670	2671	2672	2673	2674	2675	2676	2677	2678	2679	2680	2681	2682	2683	2684	2685	2686	2687	2688	2689	2690	2691	2692	2693	2694	2695	2696	2697	2698	2699	2700	2701	2702	2703	2704	2705	2706	2707	2708	2709	2710	2711	2712	2713	2714	2715	2716	2717	2718	2719	2720	2721	2722	2723	2724	2725	2726	2727	2728	2729	2730	2731	2732	2733	2734	2735	2736	2737	2738	2739	2740	2741	2742	2743	2744	2745	2746	2747	2748	2749	2750	2751	2752	2753	2754	2755	2756	2757	2758	2759	2760	2761	2762	2763	2764	2765	2766	2767	2768	2769	2770	2771	2772	2773	2774	2775	2776	2777	2778	2779	2780	2781	2782	2783	2784	2785	2786	2787	2788	2789	2790	2791	2792	2793	2794	2795	2796	2797	2798	2799	2800	2801	2802	2803	2804	2805	2806	2807	2808	2809	2810	2811	2812	2813	2814	2815	2816	2817	2818	2819	2820	2821	2822	2823	2824	2825	2826	2827	2828	2829	2830	2831	2832	2833	2834	2835	2836	2837	2838	2839	2840	2841	2842	2843	2844	2845	2846	2847	2848	2849	2850	2851	2852	2853	2854	2855	2856	2857	2858	2859	2860	2861	2862	2863	2864	2865	2866	2867	2868	2869	2870	2871	2872	2873	2874	2875	2876	2877	2878	2879	2880	2881	2882	2883	2884	2885	2886	2887	2888	2889	2890	2891	2892	2893	2894	2895	2896	2897	2898	2899	2900	2901	2902	2903	2904	2905	2906	2907	2908	2909	2910	2911	2912	2913	2914	2915	2916	2917	2918	2919	2920	2921	2922	2923	2924	2925	2926	2927	2928	2929	2930	2931	2932	2933	2934	2935	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9

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Investigation of the residual austenite in hardened structural steels. L. E. Pavlyuk. *Vestnik Mashinostroyeniya*, 1967, 55-3; *Chem. Zvest.* (Russian Zone Ed.) 1969, 1, 820; cf. C.A. 41, 1886b. — Investigations made on 4 Cr-Ni steels indicated that the amt. of residual austenite present in alloyed, subeutectoid steels was practically unchanged by increasing the hardening temp. The notch-impact strength in the range of lower annealing temps. can be changed in various ways by increasing the hardening temp. In ind-

vidual cases it may show a slight increase for fine-grained steels; in coarse-grained steels it is reduced. In no case, however, is such a change a function of the amt. of residual austenite. Detn. of residual austenite by the magnetic method is inaccurate for super-eutectoid steels having large amts. of carbide. Various phases are present in such steels, including martensite with a high magnetic satn. (in the neighborhood of the satn. of Fe), various carbides with essentially slight satn. or paramagnetic carbides, and paramagnetic austenite. The change in the magnetic satn. of the mixt. has previously been regarded as assoc. only with changes in the amt. of residual austenite. Actually, however, the change in austenite is ordinarily accompanied by processes of sepn. or soln. of carbides, which, in turn, affect the magnetic satn. of the mixt. M. G. Moore

MUKHAMEDZHANOV, M.V.; UL'DZHABAYEV, T.U.; MAMEDOV, M.T.; RODICHEV, S.D.;
FIRSOV, B.P. Prinimali uchastiye: PROTASOV, P.V.; POLEVSHCHIKOVA,
V.N.; MAL'TSEV, A.M. PEVZNER, L.I., red.; BONDARENKO, M., red.;
BAKHTIYAROV, A., tekhred.

[On cotton plantations of the U.S.A.] Na khlopkovykh plantatsiyakh
SShA. Tashkent, Gos.izd-vo Uzbekskoi SSR, 1959. 172 p.
(MIRA 13:10)

(United States--Cotton growing)

"APPROVED FOR RELEASE: 06/15/2000

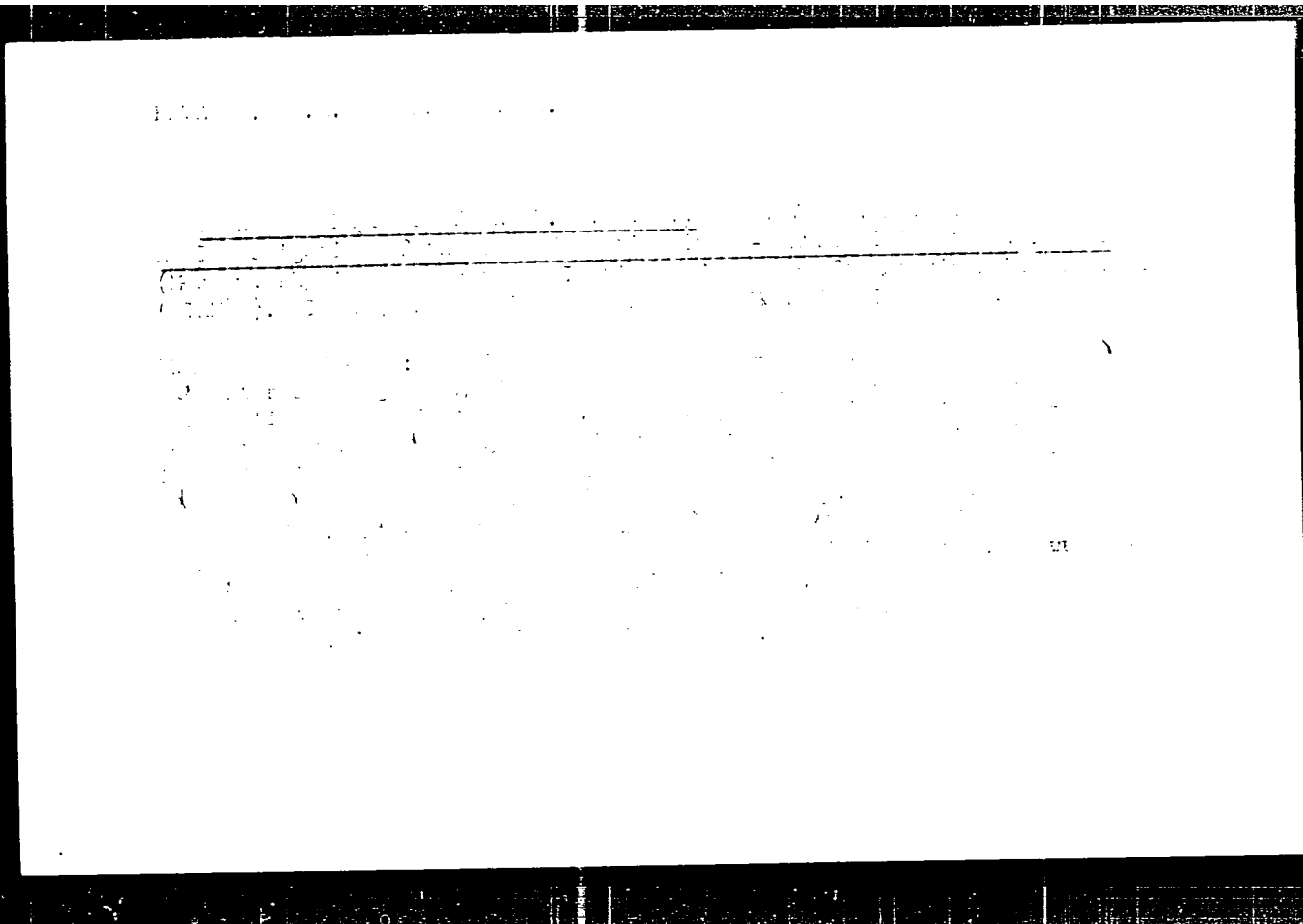
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SECRET, 1950

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PEVZNER, L. M. and AKIMOV, G. V.

Zavodskaya Laboratoriya, 1939, Vol 8, Nr 12, pp 1273-1282, Thermoelectric Method of Sorting Steel (Vsesoyuznyi Institut Aviatsionnykh Materialov).

"The e. m. f. of many thermocouples 'standard steel-steel under examination' is measured up to 500. The differences between various steels are 0.05--1.3 mv., which is sufficient to permit sorting. E.g., steels containing C 0.24, Mn 0.46--0.99, and Si 0.05--0.13% can be recognized from those having C 0.31--0.33, Mn 0.52--0.82, Si 0.25--0.32, Cr 0.65--0.86, Ni 0.07--0.14, and Mo 0.20--0.30%."

[illegible]

THE RELATION OF THE SHAPES OF THE CURVES OF STATIC AND IMPACT STRENGTHS TO
PHYSICO-CHEMICAL PROCESSES IN ALLOYS. L. M. Pyzner (*Izv. Akad. Nauk
S.S.S.R.*, 1948, [Tekhn.], 212-218; *C. Abstr.*, 1948, 63, 2429). — [In Russian].
A discussion of the mechanical properties of alloys in relation to their chemical
composition, conditions of thermal treatment, and effect of cold and hot
deformation.

ASB 31.4 METALLURGICAL LITERATURE CLASSIFICATION

PEVZNER, L. M.

Zaĭodskaya Laboratoriia, 1946, Vol 12, Nr 6, pp 583-595, The Connection Between the Change in Static and Impact Strengths and the Physical-Chemical Processes in Metal (Vsesoiuznyi Institut Aviatsionnykh Materialov).

"Most mech. properties are complex functions of some simple basic properties, such as modulus of elasticity, elastic limit, coeff. of rigidity, tearing strength, and shearing strength. The relation between such complex function and physical-chem. processes in the metal is very complicated. Analysis of the approx. equation between the strength of a smooth sample under strain and the basic properties indicates that the special points on the strength curve do not always have corresponding special points on the curves of basic properties. Thus even in the simplest cases the course of the complex curve is not indicative of any physical-chem. processes. Analysis of curves of the most complex mech. properties, e.g., the impact strength, is even more difficult. Seventeen references."

PEVZNER, L. M.

Vestnik Inzhenerov i Tekhnikov, 1947, Nr 2, pp 55-58, Investigation of the Residual Austenite in Hardened Structural Steels.

"Investigations made on 4 C-Ni steels indicated that the amt. of residual austenite present in alloyed, subeutectoid steels was practically unchanged by increasing the hardening temp. The notch-impact strength in the range of annealing temps. can be **changed** in various ways by increasing the hardening temp. In individual cases it may show a slight increase for fine-grained steels; in coarse-grained steels it is reduced. In no case, however, is such a change a function of the amt. of residual austenite. Detn. of residual austenite by the magnetic method is inaccurate for supereutectoid steels having large amts of carbide. Various phases are present in such steels, including martensite with a high magnetic satn. (in the neighborhood of the satn. of Fe), various carbides with essentially slight satn. or paramagnetic carbides, and paramagnetic austenite. The change in the magnetic satn. of the mixt. has previously been regarded as assocd. only with changes in the amt. of residual austenite. Actually, however, the change in austenite is ordinarily accompanied by processes of sepn. or soln. of carbides, which, in turn, affect the magnetic satn. of the mixt."

9a-7. Method for Evaluation of Plasticity in Notches. (In Russian.) I. M. Levaner. Zavodskaya laboratoriya (Factory Laboratory), v. 13, Sept. 1947, p. 1108-1112.

Relationships between deformation characteristics and impact strengths. A few tests were made on magnesium from -195 to 250° C., but most of the work was done on a Cr-Ni-Mo steel. In general changes in plasticity with temperature are not parallel to those in impact strength. 17 ref.

PEZIK, M.O.

Bin charging device for grinding cylindrical parts like 1.5
to 5 mm. diameter rollers. Mod. metallorezh.stan. no.2:7-9
'58. (MIRA 13:5)
(Grinding machines)

PEZIK, M.S.

Modernizing the drive of the BA-11 type turret lathe made by
the Hasse and Wrede Company. Mod.metallorozn.stan. no.13:3-4
'59. (MIRA 13:5)

(Lathes--Electric driving)

PEZIK, M.O.

Standard plans for the modernization of machine tools developed
by the Central Design Bureau of the Machinery Department of the
Moscow City Economic Council (continued). Mod.metallorozn.stan.
no.10:33-37 '59. (MIRA 13:5)
(Machine tools--Technological innovations)

VECSERNYES, Lajos (Budapest); PRZSGAY, Gyergyi (Budapest)

Spectrochemical analysis of superficial adhesive films of zinc-sulfide microcrystalline layers. In German. Acta chimica Hung. 21 no.2:123-129 '59. (KEAI 9:4)

1. Research Institute for Telecommunication, Budapest.
(Spectrum analysis) (Films) (Zinc sulfide)

EVANS, L. M.

"Methods of Increasing the Constructional Strength of Steel Structures,"
Dok. AN, 56, No. 3, 147

Application of Isothermal Treatment for Increasing the
Strength of Structural Steel. (in Russian) I. M. Pevz.
Zhurnal Tekhnicheskoi Fiziki (Journal of Tech-
nical Physics), v. 19, Apr. 1949, p. 481-491.

Experimental data indicate that isothermal treat-
ment, causing formation of bainite, permits con-
siderable increase in the structural strength of
some steels. Steel with a bainite structure possesses
considerably higher strength than the same steel
with low-annealed martensite or sorbite structure.

AND S. A. METALLURGICAL LITERATURE CLASSIFICATION

Pevzner, L. M.;

PA 169T54

USSR/Metals - Testing

Sep 50

"Influence of the Soft Surface Layers on the Mechanical Properties of Notched Specimens," Ya. B. Fridman, L. A. Pevzner

"Zavod Lab" Vol. XVI, No 9, p. 1074-1077

Reviews and discusses literature on subject and makes conclusions: Distribution of plastic deformations in notched section is nonuniform. Surface layers are deformed more greatly than inner layers. Plasticity in notch may be considerably increased by softening of comparatively thin surface layer. Surface decarburization of 0.1-0.15 mm in depth increases impact strength of steel from 5-6 to 9-10 kg/sq cm.

169T54

FDD

PA 169T54

PA 227T33

PEVZNER, I. M.

USSR/Metallurgy - Steel, 1 Aug 52
Structural Analysis

"Redistribution of Carbon During Transformation
in the Transition Zone," I.M. Pevzner, G.M.
Bovenskiy, T. D. Kubyshkina

"Dok Ak Nauk SSSR" Vol 85, No 4, pp 811-814

Determines C concn in residual austenite in
hypoeutectoid alloy steels after isothermic
decompn in transition zone, particularly in
its lower part. Transformation begins in pro-
grams impoverished with respect to C. In proc-
ess of needle troostite formation enrichment
of residual austenite with C occurs, and its
227T33

concn reaches 1.2 - 1.5%, i.e., 3-4 times av-
C content in investigated steels. High C con-
tent in residual austenite explains its high
stability, which decreases when C concn de-
creases with rising isothermal temp in transi-
tion zones. Submitted by Acad P.A. Rebinder
6 Jun 52.

227T33

PEVZNER, L. M.

Liteinoe Proizvodstvo, 1953, pp 11-13, Production of Bronze Castings by the Vacuum-Suction Method.

"Prodn. of bronze bushes and journal bearings using a watercooled mould into which the molten metal is introduced by suction is described. The castings manufactured by this method have shown superior mech. properties (hardness, yield strength, ductility, and wear resistance) to those obtained by casting in sand."

PEVZNER, L. M.

Liteinoe Proizvodstvo, 1954, Nr 8, pp 31-32, Review of B. M. Kaenofontov's
Book "Casting by the Method of Vacuum Suction."

PEVZNER, L. M.

In Physical Metallurgy and Heat Treatment, State Scientific-Technical
Publishing House for Machine-Construction Literature, Moscow, 1955, 320 pp,
74-106, Structure and Properties of Steel During Tempering.

DEVZNER, L M

✓ Influence of several processes of heat treatment on the tendency to delayed fracture of steels with tensile strengths of 120-140 kg/mm. L. M. Devzner, V. B. Fedovskii, T. K. Zhukov, G. S. Volkov and Ya. M. Potak. *Metalloved. i Obrabotka Metallov* 1956, No. 5, 5-14. An experimental study was made of the effect of stress and H on delayed fracture in steel 20KhGSA (0.24% C, 1.0 Mn, 1.0 Si, 1.0 Cr, 0.4 Ni). Plates 5 x 8 x 10 mm. were heat treated in the elastic or elastoplastic range and were made the cathode in a 5% NaHSO₄ solution for 20 min. The max amt. of bending for which no cracking occurred was tabulated. Hardness in the range 37-40 H was produced by a variety of heat treatments. The surface layer was important in determining the behavior. For specimens that had been given the same hardening treatment, tempering in a nonoxidized salt bath gave a value of more than 8 mm. of bending while tempering in a muffle furnace gave about 2 mm. Fresh salt baths also gave about 2 mm., although well used, decarburized baths gave values comparable to nonoxidized baths. The fresh baths produced a surface layer contg. 0.0271 g. N compared to 0.0014 for used baths. When the fresh bath was used at 410° it gave more than 8 mm. of bend because the nitriding process was almost absent. Heating in a muffle furnace, either for hardening or for tempering, gave a low bend value because of the oxide layer produced. Isothermal quenching in salt baths at 390-410° gave the best results. There was considerable variation among heats of steel. Polishing the surface after heat treatment lowered the bend value in many cases; for isothermal quenching the lowering was from more than 8 mm. down to 2. The above

Pavner, L. M., Sadowski, V. E.

results were confirmed by further tests on pickling and zincification of plates. When zincified bolts were tested, it was found that there was little tendency toward delayed fracture if the bolts were tightened in flat plates. Therefore, plates with an 8° bend were used, and the bolts were tightened in stages, with a period of 2 or 3 days allowed for delayed fracture to occur at each stage. The results were in agreement with those above except that specimens heated in a muffle furnace were satisfactory, probably because the oxide layer was removed by the pickling operation preceding zincification. Microhardness tests of bolts that had failed in previous tests showed that the surface layer to a depth of about 80 μ had a hardness of about 800 kg./sq. mm. compared to a core hardness of 400.

2/2

of JFM

Peuzner, L. M.

✓
Metal
1941* (Russian.) On the Intermediate Transformation of Austenite. O prozhenhutechnom prevratizhenii avstenitsy. L. M. Peuzner, T. D. Kubyshkina, O. M. Rovenski, and A. I. Samoilov. *Metallovedenie i Obrabotka Metallov*, 1956, no. 10, Oct. 1956, p. 2-20.
A study of the re-distribution of C in the process of the intermediate transformation of austenite, and of the kinetics of the ultimate stages of decomposition. The transformation was observable in all alloy steels in special diffusion conditions.

of

2

ACCESSION NR: AP4037065

S/0129/64/000/005/0021/0028

AUTHOR: Drozdovskiy, B. A.; Pevzner, L. M.; Tarantova, A. S.;
Fridman, Ya. B.; Kishkin, S. T.

TITLE: Effect of carbon content on the tensile strength of structural
steel sheets

SOURCE: Metallovedeniye i termicheskaya obrabotka metallov,
no. 5, 1964, 21-28

TOPIC TAGS: high strength steel, superstrength steel, medium alloy
steel, VKS-1 steel, solid fuel rocket, rocket case, rocket case
material, steel notch sensitivity

ABSTRACT: The effects of carbon content, melting conditions, and heat
treatment conditions (primarily tempering temperature) on the strength
and ductility (in conventional tensile tests and under biaxial ten-
sion), and notch sensitivity of two superstrength steels VKS-1 and
[AISI]4137-Co are investigated. Four grades of VKS-1 (0.30, 0.39,
0.45, or 0.53% carbon; 0.89% manganese; 1.2% silicon; 1.87% chromi-
um; 0.72% nickel; 0.49% molybdenum; .05% vanadium; 0.011% sulfur; and 0.008%
Cord 1/4

ACCESSION NR: AP4037065

phosphorus) were melted in an open atmosphere induction furnace. The 4137-Co (0.40% carbon, 0.84% manganese, 1.02% silicon, 1.32% chromium, 0.36% molybdenum, 0.19% vanadium, and 1.1% cobalt) was melted either in an open atmosphere induction furnace or in a consumable electrode vacuum arc furnace. Both steels were rolled into sheets 1 mm (VKS-1) or 15 mm (4137-Co) thick. Special care was taken to prevent surface decarburization. Tests revealed that tensile and yield strength of VKS-1 steel increased steadily with increased carbon content up to 0.45%. Steel with 0.45% carbon tempered at 150C has a tensile strength of 240—245 kg/mm² but low ductility and a high notch sensitivity. When tempered at 220C the steel had a tensile strength of 220—230 kg/mm², yield strength of 180 kg/mm², and elongation 6.5%. Further increase of carbon content brings about premature brittle failures. Elongation remains almost unaffected by increase of carbon content from 0.30 to 0.45% but notch sensitivity increases very sharply. Under conditions of biaxial tension the strength of VKS-1 increased with higher carbon content only up to 0.39%. With 0.30—0.39% carbon the fracture is ductile and the strength is higher than that in uniaxial tension. As the carbon content is increased to 0.45% the fracture becomes brittle, the

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strength drops and goes below the level noted in uniaxial tension. Generally, the maxima on the strength-carbon content or strength-tempering temperature curves for biaxial tension do not coincide with those for uniaxial tension but occur at carbon contents and tempering temperature at which the strength in uniaxial tension amounts to about 200 kg/mm². The behavior of 4137-Co steel followed a similar pattern. It was found, however, that vacuum arc melting improved ductility, especially in biaxial tension, and lowered notch sensitivity. No brittle failures were observed even at tempering temperature as low as 150C. No correlation between the strength in biaxial tension and any characteristics in uniaxial tension was found in either steel. It is concluded that the problem of improvement of structural strength is closely related to the prevention of brittle fracture at higher uniaxial strength. This can be achieved by complex alloying with a minimum segregation of components; improved metallurgical processes ensuring higher purity of metal; control of solidification processes to prevent microsegregation and improve the strength of interdendritic boundaries; and finally by thermomechanical treatment with a maximum grain refinement.

- Card 3/4

ACCESSION NR: AP4037065

ASSOCIATION: none

SUBMITTED: 00

DATE ACQ: 05Jun64

ENCL: 00

SUB CODE: MM

NO REF SOV: 004

OTHER: 004

Card 4/4

18 (7)

AUTHORS:

Tarantova, A. S., Solov'yeva, G. G.,
Pevzner, L. M.

SOV/32-25-9-23/53

TITLE:

Methods for the Metallographic Analysis of Stainless Steels of
the Transition-type

PERIODICAL:

Zavodskaya laboratoriya, 1954, Vol 25, Nr 9, pp 1089-1091 (USSR)

ABSTRACT:

During recent years the transition-type stainless steel of
the austenite-martensite class (BAM) (EI904, EI925 grades and
others) have found wide application. The basic structure of
these steels is austenitic, sometimes with fairly large
quantities of martensite, all steels of this sort (except
EI904) containing 5-20% of δ -ferrite. As these steels differ
from the standard types of austenite steels (such as steel
Kh18N9 etc) in having a lower stability of the austenite,
electropolishing must be employed for obtaining ground-metal
surfaces. Various electrolytes were tried out (Ref 1), and on
the basis of the results obtained a method for the make of
ground sections was developed. The following electrolyte is
recommended: 55 g of citric acid, 5.0 ml of sulphuric acid
(1.84), 25 ml of distilled water. Temperature of the electrolyte:
80-90°, current density: 1.0-2.0 A/cm², duration: 3-5 minutes.

Card 1/2

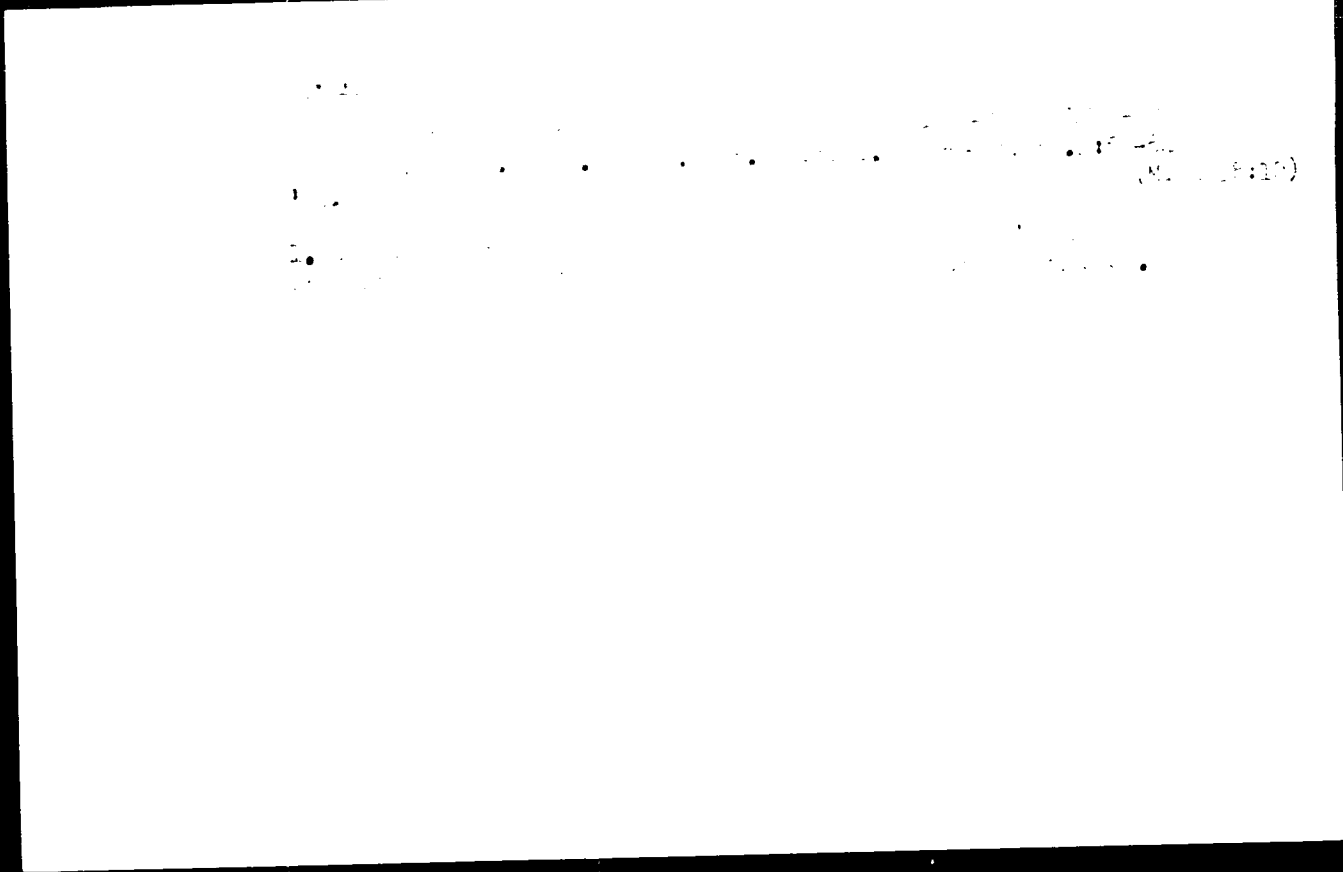
Methods for the Metallographic Analysis of Steels and
Steels of the Transition-type

A layer 0.05 mm thick is removed. Stainless steel Kh18N9T is used as a cathode. The main structure of (BAM)-steels (austenite, martensite, carbides, and δ -ferrite) is made visible by anodic etching in 10% aqueous oxalic acid at room temperature and a current density of 0.5-1.0 A/cm² for a period of 45-120 sec. Some examples of differently treated (BAM)-steels are given with corresponding structure plotting. The occurrence of an increased amount of martensite in the surface layer of the ground-metal sections which could be observed in several cases is explained by the hypothesis of Ya. M. Solovchiner and G. D. Melnikova, i.e., that the energy conditions for the formation of martensite are more favorable on the surface than in the interior of the metal. To make δ -ferrite visible, etching in a hot solution of 10 g KOH + 10 g $K_3Fe(CN)_6$ + 100 ml H₂O for 5-10 min is recommended. To make δ -ferrite visible, the method of magnetic metallography can also be used (Ref 2). There are 4 figures and 3 references, 2 of which are Soviet.

Card 2/2

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CIA-RDP86-00513R001240710018-7



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CIA-RDP86-00513R001240710018-7"

KUZYNETS, N.I., inzh.; FELTZER, L.I., inzh.; SLOVITSKY, M.I.,

[Instructions for the major repair of a diesel engine in
construction] Ukazaniya po kapital'nomu remontu mashin,
zaniatykh v stroitel'stve (U5-02). Moskva, Gosstro-
izdat. No.7. 1963. 72 p. (U.S.A. 1964)

1. Moscow. Nauchno-issledovatel'skiy institut organizatsii, mekhanizatsii i tekhnicheskoy pomoshchi stroitel'stva.

KUVYRKIN, N.I., inzh.; PEVZNER, L.M., inzh.; SLOTSKIY, S.I., inzh.

[Instruction on the overhauling of machinery used in construction (U5-64)] Ukazaniia po kapital'nomu remontu mashin, zashchitnykh i stroitel'stve (U5-64). Moskva, Stroiizdat.
No.11. 1965. 194 p. (MIRA 18:6)

1. Moscow. Nauchno-issledovatel'skiy institut organizatsii i mekhanizatsii i tekhnicheskoy pomoshchi stroitel'stva.

DROZDOVSKIY, B.A.; PEVZNER, L.M.; TALANOVA, A.S.; FELDMAN, Ya.B.;
KISHKIN, S.T.

Effect of carbon content on the strength of structural
sheet steel under the effect of tension. Metalloved. i
term. obr. met. no.5:21-28 My '64. (MIRA 17:7)

Pevzner, L. M.

AID Nr. 9751-2 29 May

AUSFORMING OF STRUCTURAL STEELS (USSR)

Pevzner, L. M., I. N. Roshchina, T. D. Kubysheva, and L. V. Zaslavskaya.
Metallovedeniye i termicheskaya obrabotka metallov, no. 4, Apr 1963, 13-20.

S/129/63/000/004/004/014

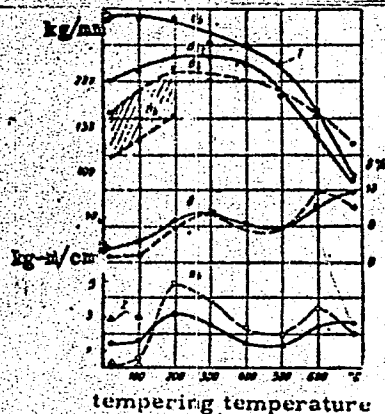
The effect of the low-temperature thermomechanical treatment "ausforming" on the structure, phase composition, and mechanical properties of low-alloy structural steels containing 0.47-0.58% C, 1.67-1.97% Cr, 2.15-2.44% Ni, 0.80-1.12% W, 0.40-0.46% Mo, and 0.9-0.28% V has been studied. Test specimens 90 x 35 x 22 mm, enclosed in 1X18H9T steel [AISI 321] envelopes, were austenitized at

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AID Nr. 979-2 29 May

AUSFORMING OF STRUCTURAL STEELS [Cont'd]

S/129/63/000/004/004/014



1 - 0.58% C; 2 - 0.47% C.

— ausformed

- - - conventionally hardened

1000°C, cooled to 500-530°C in a saltpeter bath, rolled at this temperature in several passes with a total reduction of 90%, oil quenched, and tempered at 100-550°C for 3 hrs or at 600-700°C for 1 hr. The maximum effect of ausforming, compared with conventional hardening, was observed in steels, as quenched or tempered at 100°C. [see illustration]. The optimum combination of strength and ductility was obtained in a steel containing 0.48% C, 1.15% Mn, 1.60% Si, 1.97% Cr, 2.15% Ni, 1.12% W, 0.45% Mo, and 0.28% V, which after tempering at 100°C

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AID Nr. 979-2 29 May

AUSFORMING OF STRUCTURAL STEELS (Cont'd)

S/129/63/000/004/004/014

$a_k = 3 \text{ kg-m/cm}^2$. With an increase in C content to 0.58%, a_k decreased to 1.5-2 kg-m/cm². With tempering at 200 to 600°C, the advantages of austempering over conventional hardening become less pronounced; e.g., the impact strength of ausformed steel drops even below that of conventionally hardened steel. Ausforming brings about considerable anisotropy of mechanical properties and structure: the tensile strength of transverse specimens is considerably higher and the ductility considerably lower than those of longitudinal specimens. Crystals of ausformed martensite shaped like small plates parallel to the sheet plane were found to be oriented in the direction of rolling. X-ray diffraction patterns showed that the substructure, too, becomes anisotropic as a result of ausforming; the martensite blocks of coherent spattering acquire the shape of flakes parallel to the sheet plane and has a thickness only $\sim 1/3$ that of conventional martensite. No difference in phase composition between ausformed and conventionally hardened steels was found. Ausformed martensite at temperatures up to 500-550°C appears to be more stable than martensite of conventionally hardened steel; tempering of the former proceeds at a lower rate than that of the latter. At temperatures over 550°C the opposite is true.

(MS)
Card 3/3

AID Nr. 985-2

7 June

Pevzner L.M.

AUSFORMING OF CHROMIUM STEELS (USSR)

Kubyshkina, T. D., L. M. Pevzner, L. S. Fedotova, and M. F. Alekseyenko.
Metallovedeniye i termicheskaya obrabotka metallov, no. 4, Apr 1963, 32-35.
S/129/63/000/004/008/014

The effect of ausforming on mechanical properties of complex alloyed steels 1X12HBMΦA or 3X196L (0.12% C, 11.3% Cr, 1.77% Ni, 1.60% W, 0.43% Mo, 0.27% V) and BHC-6 (0.25% C, 12.3% Cr, 1.64% Ni, 1.74% W, 1.96% Mo, 0.23% V) was investigated. Steel specimens 90 x 35 x 22 mm were austenitized at 1020°C, furnace-cooled to 550°C, rolled with 90% reduction to a thickness of 2.5 mm, and immediately oil-quenched. The table shows tensile strength σ_b , yield strength $\sigma_{0.2}$, elongation δ , and notch toughness a_k of ausformed and conventionally hardened steels in as-quenched condition and after tempering at 500°C for 2 hrs.

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AID Nr. 985-2 7 June

AUSFORMING OF CHROMIUM STEELS [Cont'd]

S/129/63/000/004/008/014

Steel	Condition	σ_b , kg/mm ²	$\sigma_{0.2}$, kg/mm ²	δ , %	α_k , kg-m/cm ²
1X12HBM0A	Ausformed	180.5	170.0	15.2	6.4
	Ausformed and tempered	173.5	167.0	13.9	8.6
	Quench hardened	147.0	127.5	15.8	
	Quench har- dened and tempered	142.0	131.5	13.2	
	Ausformed	231.5	150.5	10.9	4.1
BHC-6	Ausformed and tempered	220.5	171.0	13.5	6.8
	Quench hardened	191.0	151.5	11.5	4.5
	Quench har- dened and tempered	183.5	150.5	11.5	3.4

Thus, compared to conventional hardening, ausforming increases tensile and yield strength by approximately 20% without lowering ductility. It also makes

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AID Nr. 985-2 7 June

AUSFORMING OF CHROMIUM STEELS [Cont'd]

S/129/63/000/004/008/014

the steel structure more stable; the softening of ausformed steels begins at temperatures well over 500°C. Both steels after conventional hardening are susceptible to temper brittleness; for example, tempering at 400-500°C lowers the notch toughness of BHC-6 steel to 2.5-3.0 kgm/cm². In the ausformed BHC-6 steel, however, notch toughness increases steadily with increasing tempering temperature up to 7 kgm/cm² at 500°C. Another special advantage of ausformed steels is high notch toughness at subzero temperatures; BHC-6 ausformed and tempered at 500°C has an average notch toughness at -70 to -196°C of over 7 and 4.0 kgm/cm², respectively. In conventionally hardened steel, notch toughness dropped to 1-1.5 kgm/cm² at -70°C. [WW]

Card 3/3

PEVZNER, L.M.; Prinimali uchastiye: IVANOVA, A.K.; PALLADIYEVA, M.V.;
RYNDINA, A.A.; BOGOVSEIY, N M , otv. red.; LYSYY, A., otv. za
vypusk; MALEK, Z., tekhn. red.

[Excursions around Moscow, its suburbs and museums]Ekskursii
po Moskva, prigorodam i muzeiam. Moskva, Profizdat, 1947. 103 p.
(MIRA 15:12)

1. Vsesoyuznyy tsentral'nyy sovet professional'nykh soyuzov.
Turistsko-ekskursionnoye upravleniye.
(Moscow—Guidebooks)

POTAK, Ya.M., kand.tekhn.nauk; ORZHEKHOVSKIY, Yu.F., kand.tekhn.nauk;
PEVZNER, L.M., kand.tekhn.nauk; ROSHCINA, I.N., inzh.; YERMAKOV,
V.H., inzh.

Thermal and mechanical treatment of steel for higher strength.
Metalloved. i term. obr. met. no.5:249 My '61. (MIRA 14:5)
(Steel, Structural—Hardening)

POTAK, I. M. [Potak, Ya. M.]; ORJEHOVSKI, I. F. [Orzhekhovskiy, Yu. F.];
PEVZNER, L. M.; ROSCINA, I. N. [Roshchina, I. N.]; ERMAKOV, V. N.
[Yermakov, V. N.]

Thermomechanical treatment of steel for the obtainment of a high
mechanical resistance. Analele metalurgie 15 no.4:114-123 O-D '61.

(Steel—Heat treatment)

22545

06/15/2000 11/11/1961

Trznerkhovskiy, Yu. F., Graduate of Technical School
Levzner, I. M., Candidate of Technical Sciences
Roshchina, I. N., Engineer and
Yermakov, V. N., Engineer.

TITLE: Thermal-mechanical treatment of steel to increase strength

PERIODICAL: Metallovedeniye i termicheskaya obrabotka metallov
1961, No. 5, pp. 2-9

TEXT: The authors point out that recently much attention has been given to combined mechanical and heat treatment, by two possible methods. In one method the steel is rapidly deformed in the austenite-stable temperature range and quenched. While this improves the steel in many ways it fails to increase tensile strength. In the second method the steel is deformed at a temperature between the martensite point M_d and the recrystallization temperature, and quenched. This gives increased strength with satisfactory plasticity. Results of thermal-mechanical
Card 1/8

22545

S/129/61/000/005/001/003
E111/E152

Thermal-mechanical treatment of steel to give high strength treatment are not universally successful, and there are no reliable data on the practical use of the "ausform" or "ausforming" treatment widely advertised in the USA. The object of the present work was the study of thermal-mechanical treatment of alloy structural steels to a high strength and the structure produced by the treatment. The composition of the steels was as shown in Table 1, steels A-Г being melted in induction and Д and E in arc furnaces: the first group were austenitized at 1000, the second at 900 °C. After cooling in a nitrate bath to the deformation temperature the steels were rolled in 4-5 passes (reduction 90%), oil-quenched and tempered. To reduce cooling the work was reheated between passes and other measures taken, e.g. rolls were preheated to 100 °C. A portable magnetic instrument (developed by G Yu. Sila-Novitskiy and T D. Kubyshkina) was used to detect isothermal-decomposition products: if found the specimen was rejected. After treatment specimens had a hardness R_c of 58-64 and mechanical-test pieces were prepared by spark machining and removal by grinding (temperature kept below 100 °C).

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S/129/61/000/005/001/003
E111/E152

Thermal-mechanical treatment of steel to give high strength of a 0.5 mm deep surface layer. Fig.2 shows tensile strength kg/mm² and relative elongation as functions of carbon content for steels A, B, R and E after treatment (90% deformation at 550 °C, 4 hours tempering at 100 °C); for steel A tempering at 100 and 200 °C is shown by points 1 and 2 respectively, steels E and R indicated by point 3. Fig.3 shows for steel A tensile strength and elongation in relation to the 90% deformation temperature (tempering at 100 °C). The effect of variation in austenitization temperature with 90% deformation and tempering at 100 °C of steel A on tensile strength, Rockwell hardness and elongation is shown in Fig.4. Fig.5 shows the effect of tempering temperature on these properties of the normally thermomechanically treated alloys B and R (left- and right-hand graphs respectively). The treatment enabled a tensile strength of 280-300 kg/mm² and elongation of 6% to be obtained for the steels tested, which is better than with ordinary or stepwise hardening followed by low-temperature tempering. As carbon content rises to about 0.5% strength of thermomechanically treated steels rises and falls with higher

Card 3/8

22545
S/129/61/000/005/001/003
E111/E152

Thermal-mechanical treatment of steel to give high strength C content due to semi-brittle or brittle fracture. The best strength/plasticity combination was obtained with tempering at 100 °C. In some experiments on steel the deformation was decreased to 50%. the results were less favourable than with the 90% deformation as regards strength, but gave high plasticity. The advantage of 50% deformation is that it can be effected at relatively high temperatures, even above the recrystallization temperature. Bend tests on 60 x 10 x 2 mm plates of steel heated in various ways were also carried out. Electron-microscopic study of the fine structure of thermomechanically treated steel A showed a pronounced texture and considerable refinement of martensite plates. X-ray diffraction by rotating specimens was also studied (with a JRC-501 (URS-501) ionization apparatus with automatic recording of intensity distribution in Fek_{α} radiation): block size of the thermomechanically treated steel was one half to one quarter that obtained with ordinary hardening. The authors conclude that structure refinement is one factor in the effectiveness of the treatment.

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22545

S/129/61/000/003/001/005
0111/E152

Thermal-mechanical treatment of steel to give high strength

V.V. Chugunov, K.S. Medvedeva, G.G. Solov'yeva, Ye.G. Filippova,
T.D. Kubyshkina, V.V. Bol'shakova and Yu.N. Kabanov participated
in the work.

There are 6 figures, 4 tables and 21 references: 15 Soviet and
6 English. The four latest English language references read:

Ref.8: E.B. Kula, J.M. Dhosi, "TASM", v. 52, 1960.

Ref.11: D.J. Schmatz, V.F. Zackay, "TASM", v. 51, 1959.

Ref.12: D.J. Schmatz, J.C. Shyne, V.F. Zackay, "Metal Progress",
v.76, No.3, 1959.

Ref.13: J.C. Shyne, V.F. Zackay, D.J. Schmatz, "TASM", v.57, 1961.

Card 5/8

KURYSAKINA, T.D., inzh.; PEVZNER, L.M., kand.tekhn.nauk; POTAK, Ya.M., kanl.
tekhn.nauk

Martensite transformation in the austenite-martensite class of
stainless steels. Metall. ved. i term. obr. met. no.8:9-17 Ag '60.
(Steel, Stainless Metallography) (Data 1:9)
(Phase rule and equilibrium)

18 7100

18 1130

81876

S/129/60/000/08/003/009

E073/B135

AUTHORS:

Kubyshkina, T.D. (Engineer); and Pevzner, L.M. and
Potak, Ya.M. (Candidates of Technical Sciences)

TITLE:

Martensitic Transformation in Austenite-Martensite
Class Steels

PERIODICAL: Metallovedeniye i termicheskaya obrabotka metallov,
1960, No 8, pp 9-17

TEXT:

The work described in this paper was devoted to studying the kinetics of the martensitic transformation during cooling and isothermal heating. The investigations were carried out on steel Kh15N9Yu (composition 0.07% C, 15% Cr, 8.5% Ni, 1% Al). The results of this paper relate to heats for which the quantity of martensite after quenching with cooling to room temperature did not exceed 1.4%. The kinetics of martensite transformation were investigated magnetically by means of an improved anisometer. The martensite quantity was determined by measuring the magnetic saturation in strong fields using a ballistic method. In addition to that, a method described by Auerbach and Cohen (Ref 4) was also used for some of the specimens. Furthermore optical, electron metallography studies and separation of the anodic precipitate followed by chemical and X-ray analysis (Ref 6) were also applied. The influence of the

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S/129/60/000/08/003/009

EO73/E135

Martensitic Transformation in Austenite-Martensite Class Steels

heating temperature on the quantity of martensite in the case of quenching to $+20^{\circ}\text{C}$ and to -70°C is plotted in Fig 1. The quantity of martensite was determined after cooling from 1050°C down to room temperature in air (point II) and subsequent soaking at -70°C for 2 hours (point I). After quenching from 1050°C a series of specimens were subjected to reheating at temperatures between 20 and 1050°C for a duration of one hour and then cooled in air down to 20°C and the quantity of martensite was determined (curve 1); following that, cold treatment was applied at -70°C for 2 hours with subsequent heating to room temperature, and the quantity of martensite was measured again (curve 2). It was established that heating to $525-950^{\circ}\text{C}$ after austenisation at 1050°C leads to an appreciable decrease in the austenite stability. Destabilization of the austenite is attributed to the fact that the solid solution combines with chromium and carbon due to rejection of chromium carbide. Long-duration storage at room temperature after austenisation, and also heating to temperatures up to 500°C , lead to stabilization of the austenite

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91876

S/129/60/000/08/003/009

E073/E135

Martensitic Transformation in Austenite-Martensite Class Steels

Martensite transformation after thermal stabilization has the following characteristic features: super-cooling of austenite can be achieved without transformation down to any temperature (down to 196 °C) at relatively low cooling speeds; austenite to martensite transformation proceeds isothermally after a certain incubation period. The dependence of the speed of transformation on the temperature of the isotherm and also on the duration of the isothermal holding can be expressed by a curve which shows a maximum (Fig 3). These relations do not extend to ordinary martensitic transformations of unstabilized austenite. After thermal stabilization relations of the martensitic transformation were detected which indicate that in this case the kinetics of transformation are determined by the thermal oscillations of the atoms. The thermal stabilization is linked with changes in the fine structure of the lattice, the nature of which is not clear. It is possible that there is a relaxation of stress peaks in small sections or that there is an annihilation of particular sections of the lattice which are prepared for transformation. There are 8 figures and 19 references: 10 Soviet, 8 English and 1 German.

Card 3/3

BLINOVSKIY, A.A.; BUSLOVA, N.A.; YEROKHOV, N.F.; IVANOV, K.A.; KITAYEVA,
G.V.; LEYBOSHITS, L.M.; NEDELYAYEV, I.A.; PALLADIYEVA, M.V.;
PEVZNER, L.M.; PETROVA, Ye.D.; ROGOVSKIY, N.M.; RUZHYY, M.M.;
SMIRNOV, B.F.; DENISOVA, I.S., red.; RAKOV, S.I., tekhn.red.

[Through our land; tourist sites and itineraries of the Moscow
Interprovince Tour Administration of the All-Union Central
Council of Trade Unions] Po rodnoi zemle; turistskie bazy i
marshruty Moskovskogo mezhoblastnogo turistsko-ekskursionnogo
upravleniya VTsSPS. Moskva, Izd-vo VTsSPS Profizdat, 1959.
154 p. (MIRA 13:4)

1. Moskovskoye mezhoblastnoye turistsko-ekskursionnoye upravleniye
Vsesoyuznogo tsentral'nogo soveta profsoyuzov (for all, except
Denisova, Rakov).
(Tourism) (Steamboat lines)

TARANTOVA, A.S.; SOLOV'YEVA, G.G.; PEVZNER, L.M.

Methods for the metallographic analysis of stainless steels
of the transition class. Zav.lab. 25 no.9:1089-1091 '59.
(MIRA 13:1)

(Steel, Stainless--Metallography)

PEVZNER, L. M.

10

The influence of a diet containing raw ox-heart on heart disease patients. M. S. Turkeltaub, L. M. Pevzner and V. D. Motrenko. *Leprosy* (Tokyo) 3, No. 1, 128, 1940. The whole heart of the bovine or heart extra were found to have a very beneficial action. This is interpreted as due to the hormone content. P. H. R.

ASB 514 METALLURGICAL LITERATURE CLASSIFICATION

BRITISH

PEVZNER, L.M.
CA

17

Methods of obtaining the greatest quantity of ascorbic acid from the wild rose hips. L. M. Pevzner and T. V. Ibratvina. *Klin. Med.* (U. S. S. R.) 21, No. 10/11, 73-4 (1943). Single water extract is insufficient. Recommended procedure is to use at least 2 extracts with 10 parts water to 1 part of the plant (weight), with the peeled (or hulled) hips being preferred owing to better degree of extract.

G. M. Kondapoff

ASTM-SLA DETALLURGICAL LITERATURE CLASSIFICATION

PEVZNER, L. R.

Pevzner, L. R. "Works of national scientific school on the theory and designing of ship screw propellers," Trudy Vses. nauch. inzh.-tekhn. o-va sudostroyeniya, Vol. V, Issue 4, 1948, pp. 136-144

SO: U-3264, 10 April 53 (Letopis 'Zhurnal 'nykh Statey, No..4, 1949).

L 01008-66 EWT(m)/EPF(c)/EWP(j) RM

ACCESSION NR: AP5019566

UR/0191/65/000/008/0013/0017

678.63—9:678.743.22

AUTHOR: Pevzner, L. V.; Kolodyazhnyy, V. Z.; Karyakina, K. N.; Ravich, G. B.

TITLE: Study of combination products of phenolformaldehyde resins with polyvinyl chloride

SOURCE: Plasticheskiy massy, no. 8, 1965, 13-17

TOPIC TAGS: copolymer, polyvinyl chloride, phenolformaldehyde, resin, polyformaldehyde plastic

ABSTRACT: The purpose of this work was to investigate in detail the interaction of phenolformaldehyde resins with polyvinyl chloride to produce phenolates. The investigation consisted of thermogravimetric and thermomechanical measurements. For thermomechanical measurements specimens were produced by pressing. A polarizing microscope with a heated stage was used for microstructural analysis of specimens. A comparison of thermographic and thermomechanical properties of the starting resins and their combination products indicates that the combination of polyvinyl chloride with phenolformaldehyde resins in the presence of hexamethylenetetramine results in cross linking of phenolformaldehyde resins with polyvinyl chloride by methylene

Card 1/2

L 01008-66

ACCESSION NR: AP5019566

groups. This conclusion is verified by the solubility data and spectroscopic analysis. "The experimental part of this work was conducted with the participation of Ye. A. Dubrovina." Orig. art. has: 10 figures. 5

44,55
ASSOCIATION: none

SUBMITTED: 00

ENCL: 00

SUB CODE: MT

NO REF SOV: 005

OTHER: 000

Card 2/2 *AP*

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