

"APPROVED FOR RELEASE: 06/15/2000

CIA-RDP86-00513R001340910017-5

PINCHUK, I. S. and SHUBENKO, V. A.

"Graphic Method of Calculating Transient Phenomena in an Induction Motor,"  
Elektrichestvo, No.2, 1949

APPROVED FOR RELEASE: 06/15/2000

CIA-RDP86-00513R001340910017-5"

SOV 137 57 11 21690

Translation from: Referativnyy zhurnal, Metallurgiya, 1957 Nr. 11 p. 150 (USSR)

AUTHORS: Patskevich, I. R., Kulikov, G. D., Pinchuk, I. S.

TITLE: An Investigation of the Process of Hardfacing by Means of Automatic Vibrating-electrode Arc Welding (Issledovaniye protsessa avtomaticheskoy vibrodugovoy naplavki)

PERIODICAL: V sb.: Vosstanovleniye iznoshennykh detalei avtomaticheskoy naplavkoy. Chelyabinsk, 1956, pp 64-98

ABSTRACT: A study of oscillograms of current and voltage conditions in the course of hardfacing operations performed with the aid of vibrating electrodes demonstrated that this process is essentially an arc process. It differs from standard arc-welding hardfacing procedures only with regard to the employment of vibrating electrodes and a cooling fluid; therefore, it would be more correct to refer to it as a vibrating-electrode arc-welding method (VEAW). Oscillograms indicate that every electrode vibration includes a period of electric arc discharge, an idle period, and a short-circuit period. The greater part of the heat energy (82-94%) is generated during the

Card 1 3

SOV 197 57 11 21690

An Investigation of the Process of Hardfacing (con't)

period of the arc discharge. The idle period has an adverse effect upon the basic characteristics of the electrode and the quality of bonding between the deposited metal and the parent metal. Idle periods may be eliminated by employing a welding generator as a source of power. In order to stabilize the process it is desirable that generators with good "surge-and-dip" characteristics be utilized. Reverse polarity must be employed during VEAW. The vibration of the electrode ensures the stability of the process by providing frequent excitation of the arc discharge (100 per second). In addition, the vibration causes the electrode metal to be transferred in small quantities (at the instant when the electrode contacts the component), thus favorably affecting the formation of beads. The cooling fluid reduces the effects of heat on the component, increases the rate of cooling of the metal, and protects the molten metal from the action of air. The selection of the area on the component to which the coolant is supplied, and the manner in which this is accomplished, are factors of great importance. The process of propagation of heat in the parent metal during VEAW may be schematically described by the action of a rapidly moving point source of heat traveling along the surface of a semi-infinite body. Structural changes occurring during VEAW essentially do not differ from changes taking place in a heat-affected zone during standard arc-welding procedures.

Card 23

SOV 132-57-1 - 21690

An Investigation of the Process of Hardfacing (cont)

Large temperature gradients and high rates of cooling in the process of VEAW favor the formation of hardened structures, which frequently results in cracking of the heat affected zone.

N. K.

Card 33

105-9-6/32

THOR: Pinchuk, I.S., Dotsent and Candidate of Technical Sciences.

LE: Transients in Periodically Loaded Induction Motors. (Perekhod-nyye protsessy v asinkhronnykh dvigatelyakh pri periodicheskoy nagruzke)

PERIODICAL: Elektrichestvo, 1957, Nr 9, pp. 27-30 (USSR)

ABSTRACT: In the case of gratings, vibrators and similar machines the load and the rotor velocity of the induction motor change very often and within wide ranges during one period. For such drives the driving motor must be selected with regard to the electric-magnetic transition processes. A calculation taking account of this circumstance is carried out. The problem of the electric-magnetic transition process is solved analytically with a given rule concerning the change of rotor-velocity and for the case of a lacking effective resistance in the stator circuit. A steady operation with periodic load is investigated restricted to those cases where the mean quadratic value of the motor moment and therefore also the mean sliding value do not exceed the nominal value. The description of the experimental investigation follows. A comparison between experimental and calculated results shows and proves the applicability of the suggested method for the consideration of the electric-magnetic transition process in the case of periodic load. In the end an example is calculated through.

Card 1/2

PINCHUK, I.S., knnd.tekhn.nauk; SHAPOVALOV, A.T., inzh.

Running of machines with crankgears. Mekh. i tek. sots. sel'khoz.  
15 no.2:38-40 '58. (MIRA 11:5)

1. Chelyabinskiy politekhnicheskiy institut (for Pinchuk). 2.  
Chelyabinskiy institut mekhanizatsii i elektrifikatsii sel'skogo  
khozaystva (for Shapovalov).  
(Electric machines)

Vjatka

AUTHOR: Sergeyev, A.V. Project

TITLE: Dissertations (Dissertatsii)

PERIODICAL: Elektricheskie iush. Nr 5. pl. 91-100 USSR

ABSTRACT: For the Degree of Candidate of Technical Sciences  
At the Ural Polytechnic Institute imeni Kirov (Ural'skiy  
politekhnicheskij institut im. Kirova)  
S.D. Levintov on June 27, 1949 "Electromechanic Transition Processes  
in a Synchronous Motor in the Case of Periodic Load (of the Com-  
pressor Type)". Official opponents: N.S. Siunov, Professor, Doctor  
of Technical Sciences; I.D. Urusov, Docent; and A.T. Plavskiy,  
Candidate of Technical Sciences.  
I.S. Pinchuk on June 27, 1949 "Electromechanic Transition Processes  
in Asynchronous Motors". Official opponents: N.S. Siunov, Professor,  
Doctor of Technical Sciences; A.A. Yanko Trinit'skiy Docent; candi-  
date of Technical Sciences and F.M. Chudnovskiy Engineer.  
I.D. Urusov on June 27, 1949 "The Mechanical Strength of the Casing  
of Electric Machines Subjected to the Action of Electromagnetic  
Loads". Official opponents: I.P. Sokolovskiy, Doctor of Technical  
Sciences and M.V. Belyayev, Docent Candidate of Technical Science.

Card 1/4

## Dissertations

CC 6-12/14

- S.P.Sitnikov on March 1, 1950 "Some Problems Connected with the Theory of Arc-Extinguishing Devices". Official opponents: N.S.Siunov, Professor, Doctor of Technical Sciences, V.G.Stepanov, Docent, Candidate of Technical Sciences and V.M.Sitnikov, Docent, Candidate of Technical Sciences.
- D.M.Shakhrai on June 26, 1950 "The Investigation of a Special System for the Electric Equipment of Dredges". Official opponents: I.B.Sokolovskiy, Professor, Doctor of Technical Sciences, M.V. Belyayev, Docent, Candidate of Technical Sciences and A.Ie.Trofimov, Candidate of Technical Sciences.
- G.P.Kropachev on June 30, 1953 "Investigation of an Asynchronous Starter in Synchronous Machines with Salient Poles and Without Starter Cage". Official opponents: N.S.Siunov, Professor, Doctor of Technical Sciences, S.A.Volotkovskiy, Doctor of Technical Sciences and M.A.Pirumyan, Docent.
- V.P.Shasherin on January 18, 1954 "Some Problems of Cathode-Current Lographic Measurements when Testing High-Frequency Apparatus". Official opponents: N.S.Siunov, Professor, Doctor of Technical Sciences and V.G.Stepanov, Candidate of Technical Sciences.
- R.N.Urmanov on June 7, 1954 "Investigation and Calculation of Circuits with a Three Phase Welding Arc". Official opponents: S.A.Volotkovskiy, Professor, Doctor of Technical Sciences and G.P.Mikhaylov, Professor, Doctor of Technical Sciences.

Card 2/4

Dissertations

At the Sverdlovsk Mining Institute imeni Vakhnina (Sverdlovskiy gornyy institut im. Vakhnina):

I.P.Ietrov on February 11, '94 "Electric Locomotives for Polyphase Repulsion Traction Motors for Single Phase Current" (of Normal Frequency," Official opponent: N.I.Simov. Professor. Doctor of Technical Sciences and A.T.Blazhkin. Docent. Candidate of Technical Sciences

At the Gor'kiy Polytechnic Institute imeni Zhdanov (Gor'kiy politekhnicheskiy institut im. Zhdanova):

S.N.Shevchuk on June 4, 1949 "Problems of Insulation against Loss of Heat in Electromotors of Metal Working Machines" Official opponents: D.M.Morozov. Professor. Doctor of Technical Sciences N.V.Shchedrin. Docent. Candidate of Technical Sciences and M.F.Shvakov. Engineer.

At the Tomsk Polytechnic Institute imeni Kirov (Tomskiy politekhnicheskiy institut im. Kirova):

G.P.Pukhova on March 26, '94 "On the Problem of the Automatic Connection of Individual Lines in the Case of Electrical Transmission with Bilateral Feed" Official opponent - V.A.Vlasov. Professor. Doctor of Technical Sciences and I.D.Kutayev. Docent. Candidate of Technical Sciences

Card 3/4

Dissertations

A.N.Zhilin on April 26, 1950 "Transition Processes in Three-Phase  
Circuits in the Case of Non Simultaneous Phase Connection".  
Official opponents: V.K.Shestopalov, Professor, Doctor of Technical Sciences and Yu.Ye.Nebolsynov, Docent, Candidate of Technical Sciences.

V.A.Abakumov on June 30, 1950 "Automation of a Series of Three-Phase  
According to the Leonard Circuit with Shunt Wound Generators".  
Official opponents: I.A.Balashov, Professor, Doctor of Technical Sciences and L.I.Gandzha, Docent, Candidate of Technical Sciences.  
V.U.Kostikov on March 13, 1954 "Methods of Determining Electrical  
Specific Electric Conductivity". Official opponents: V.K.Shestopalov,  
Professor, Doctor of Technical Sciences and V.M.Titov, Doctor,  
Candidate of Technical Sciences.

AVAILABLE: Library of Congress

Scientific report no. 1. Electrical equipment. 117  
1. Electrical engineering. 117

Card 4/4

Vinogradov, I.S.

25(1)

PHASE I BOOK EXPLOITATION

SOV/2280

- Chelyabinsk. Politekhnicheskiy institut

Voprosy svarochnogo proizvodstva (Problems in Welding) Moscow, Mashgiz,  
1959. 92 p. (Series: It's Sbornik, No. 16). 6,000 copies  
printed.

Reviewers: P.I. Boykov, Engineer, A.G. Menzenkampf, I.I. Vinnik, N.A.  
Klykov, N.A. Karpova, N.I. Andrianov, V.M. Solovskoy, L.Ye. Garmash,  
and N.M. Yegorov, Docent; Ed. (Title page): K.A. Yes'kova, Docent;  
Ed. (Inside book): A.G. Kozlov; Tech. Ed.: N.A. Dugina; Exec. Ed.  
(Ural-Siberian Division, Mashgiz): A.V. Kaletina, Engineer.

PURPOSE: This collection of articles is intended for engineers, technicians and scientific workers.

COVERAGE: This is a compilation of articles written by scientific workers of the Department of Welding Processes and Equipment of the Chelyabinsk Polytechnical Institute. The articles deal with little developed or entirely new problems of practice and theory of welding. The articles cover weldment deformation, welding of strips

Card 1/4

Card 2/4

Problems in Welding

SOV/2280

tion of the electrode.

Bakshi, O.A. Candidate of Technical Sciences. The Method of Measuring Electrode Vibration Amplitude in Automatic Vibroarc Surfacing by Welding

45

The author describes the principles of measuring electrode vibration by means of a measuring wedge.

Berezkin, P.N., Docent. Method of Checking Weldability of Thin Carbon Steel Sheet Metal

51

The author discusses the preference of using rimmed, killed, and semi-killed steel for the above purpose.

Patskevich, I.R., and Engineer V.M. Shakhmatov. Investigating Resistance Welding of Cast Iron to Steel

56

The authors discuss results of metallographical investigations, the results of mechanical testing of weld joints, and the possibilities of introducing the method into industry.

Rudakov, A.S., Docent, and Engineer V.M. Shakhmatov. Butt Welding of Resistance Alloys Strips

68

Card 3/4

PINCHUK, I.S., kand.tekhn.nauk; SHAPOVALOV, A.T., inzh.

Drawing up diagrams for gang-saw motors used in lumbering.  
Mekh. i elek.sots.sel'khoz. 17 no. 3: 19-41 '59. (MIRA 12:8)

1. Chelyabinskij institut mekhanizatsii i elektrifikatsii  
sel'skogo khozyaystva.  
(Saws) (Electric motors)

RINCHUK, L.S., kand.tekhn.ranek. dozent

Equivalent circuit of an electric drive with an asynchronous  
motor and varying load. Energ. stor. no.: 15-166 159. (MIA 15:  
(Electric motors, induction)  
(Equivalent circuits)

8(3)

## AUTHORS:

Pinchuk, I.S., Candidate of Technical Sciences. Sov/105-60-1-16/25  
Zykin, V.A., Candidate of Technical Sciences

## TITLE:

Some Methods of Improving the Characteristics of Reactors With  
Direct Current Magnetization 17

## PERIODICAL:

Elektrichestvo, 1960, Nr 1, pp 78-80 (USSR)

## ABSTRACT:

The so-called characteristics of simultaneous magnetization  $B_{\sim} = f(H_{\sim}; H_0)$  are often taken as initial data for the computing of reactors with magnetization (Refs 1,2).  $B_{\sim}$  is the mean value of the amplitude of the alternating component of the magnetic induction.  $H_{\sim}$  is the mean effective value of the alternating component of the core magnetic field.  $H_0$  is the mean value of the constant field strength component of the magnetic field. The results of experimental investigations of the influence of some factors on the form of the characteristics are given here. To utilize the power of a motor at its peak speed as completely as possible, it is necessary to make the voltage in the reactor get smallest. This can be achieved

Card 1/2

Some Methods of Improving the Characteristics of  
Reactors With Direct Current Magnetization

SOV/105-60-1-16/25

by reducing  $B_{\text{av}}$ , at a chosen number of windings of the working winding and core cross section. From this point of view it is desirable to obtain characteristics of simultaneous magnetization, at which there is a smallest possible inclination in their initial stage, depending not only on the type of steel but also on a number of other factors. The characteristics of a reactor with two magnetic conductors (Fig 1) for example, can thus be altered by varying the gap  $\delta$ .<sup>v</sup> By increasing  $\delta$ , the  $B_{\text{av}}$  value can be reduced by 15-20% for the greatest field intensity of the magnetic field. The explanation for this process is given. Based on these statements, the shape of the sheet proposed in the paper (Ref 1) is unsuitable, the air gap being practically nil for this design. A considerable improvement of the reactor characteristics can be obtained by using split working windings (Fig 3). An explanation for this improvement is given. There are 5 figures and 2 Soviet references.

SUBMITTED: June 13, 1959

Card 2/2

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PINCHUK, L.B.

Possibility of using sodium lactate in radiation sickness.  
abstract. Probl. gemit. i perel. krovi 8 no.6-54 Je'63

1. Iz Kiyevskogo nauchno-issledovatel'skogo instituta pereli-  
vaniya krovi i neotlozhnoy khirurgii (dir. - dozent S.S.  
Lavrlik).

ANDREYKO, O.F.; PINCHAK, I.M.

Occurrence of the castade Atrichomelia in the Saitsev, P.A.  
Spassky, 1961 on the territory of the .... Izv. AN Mold.  
SSR no.5:37-40 (63).  
MIRA 17:11

AUTHORS:

I. V. Kuznetsov, E. M. Sov, Z. S. Gulyaeva

TITLE:

On the Content of Lipid Compounds in the Fruits of Oil-  
bearing Plants and their Relation to the Yield of Oil  
and Fatty Acids

PERIODICAL:

Sov. Akad. Nauk. SSSR. Zool. Vol. 120, No. 2, p.  
35-38, 1962

ABSTRACT:

The investigation of the physiology of fruits represents one of the ways to examine the process of oil formation in the seeds of higher plants. In particular the study of the assimilation and transformation character of the substances which are transported from the assimilating organs into the fruits. In the course of their earlier investigations of poppy fruits (Ref. 1, 2) the authors pronounced the assumption that not all compounds which participate in the synthesis of reserves in the seeds were produced in the seeds. The plants, according to the participants in the production of the fruits, were in order to determine the role played by some fruit elements in the synthesis of the reserve substances, the fruits investigated the organs with respect to the influx and the content of compounds which immediately take

Card 1/3

On the Content of Volatile Acids in the Fruit of SCV, 20-120, 120, etc.  
Oil-Poppy

part in the fat production (hydrocarbons, volatile acids). The obtained results (Figs 1,2, Table p. 586) permit to draw the following conclusions:

- 1) Acetic acid represents the main content of volatile acids in the fruits of oil-poppy. Formic acid appears only at certain periods and in small quantities.
- 2) The production and the accumulation of acids in individual parts of the fruit (wall, placenta, seeds, and i., the leaves) modifies in the course of the ontogenesis and exhibits a different character.
- 3) The maximum velocity of the production and the accumulation of acetic acid in the wall and in particular in the placenta coincides with the period of the intensive oil synthesis in the seeds.
- 4) The utilization of acetic acid which is produced in the placenta, by the seeds for the purpose of fat synthesis is possible. There are 2 figures, 1 table, and 11 references, 3 of which are Soviet.

Card 2/5

On the Content of Volatile acids in the Fruit of SOV/ 20-120-3-41/6  
Oil-Poppy

PRESENTED: January 28, 1958, by A. L. Kursanov, Member, Academy  
of Sciences, USSR

SUBMITTED: January 28, 1958

1. Fruits--Physiology 2. Seeds--Physiology 3. Oils--Biosynthesis  
4. Acids--Photosynthesis

Card 3/3

"APPROVED FOR RELEASE: 06/15/2000

CIA-RDP86-00513R001340910017-5

PINCHUK, L.T.

Fifth in series. MURKIN 20121000000000000000  
(MURKIN 20121000000000000000) MURKIN 11141

APPROVED FOR RELEASE: 06/15/2000

CIA-RDP86-00513R001340910017-5"

PINCHUK, L.T.

Under the guise of socialism. Nauka i zhizn' 27 no. 1; 47-51  
Mr '60. (MIRAL 1:6)  
(Socialism and religion)

~~PINCHUK, L.V.~~, OVSYANIKOV, L.P., ORECHKIN, D.B.; KALECHITS, I.V.

Using stationary catalysts for destructive hydrogenation of high-molecular raw materials. Report 2. Deactivation of modern industrial catalysts. Trudy Vost.-Sib.fil. AN SSSR no.4:137-149 '56.  
(Catalysts) (Hydrogenation) (MLRA 9:12)

PINGUIN, L. V.

1483. USE OF STATIONARY CATALYSTS FOR DESTRUCTIVE HYDROGENATION OF HIGH MOLECULAR WEIGHT RAW MATERIALS. 11. CHARACTER OF DEACTIVATION OF CONTEMPORARY INDUSTRIAL CATALYSTS. Pinguin, L.V., Chavaynikov, I.F., Obruchkin, D.B., and Kolechits, I.V. (Trud. Inst. Neftegaz. Nauk SSSR, Ser. Khim. (Proc. E. Sib. Branch Acad. Sci. U.S.S.R., Ser. Chem.), 1956, (4), 137-149; abstr. in Chem. Abstr., 1957, vol. 51, 13357). The deactivating effect is studied of hydrogenation of raw distilled petroleum oils on the catalysts tungsten disulphide and tungsten disulphide-nickel sulphide-alumina (I). A miniature continuous process equipment is used with a hydrogenation chamber of 100 c.c. operating at 300 to 450°. It is established that at 300 atm tungsten disulphide and I are effective for 30-60 hours after which period the oil does not change except for a decrease of resinous residue, I having a slight advantage. Partial activation with hydrogen under pressure is effected. The deactivation of the catalyst is caused not by physical changes of the catalyst, but by the adsorption of high molecular weight compounds. Deactivation of the catalysts is related to the rate of hydrogenation. Increasing the pressure during the hydrogenation from the usual 300 to 600 atm increases the stability of tungsten disulphide and I.

C.A.

P  
Used  
Very

P.D.

I 3C33A-66  
ACC NR APR 1966

REF ID: UFR0115

AUTHOR: Inchuk, L. Ye.

Copy: 100

TITLE: Investigation of magnetic reed relays in a transverse magnetic field

SOURCE: Radio Engng. Electron. Phys., Vol. 11, No. 1, Jan. 1966, 60-63

TYPE: Technical report

ABSTRACT: The author presents experimental results obtained with magnetic reed relays having contacts with a transverse magnetic field. The field is normal rather than parallel to the contacts. Two batches of relays were tested. One batch had ten relays each, all having the same dimensions and characteristics. The other batch had 1.0-mm-diameter reeds while the others had 0.5-mm-diameter reeds. The magnetic material identified only as type



Fig. 1. Reed relay

Card 1/3

L 30333-65  
ACC NR: A16617004

R-47-D5 coil was wound on a core consisting of 1000 turns of 0.35-mm wire wound on a 39 x 4 x 4 mm rectangular core. The coil was energized from a 6-12-v d-c source. The main objective of the tests was to determine the threshold operating characteristic of the relay as a function of actuator-coil position. The movable reed was moved both laterally along the relay envelope and vertically along the center axis.

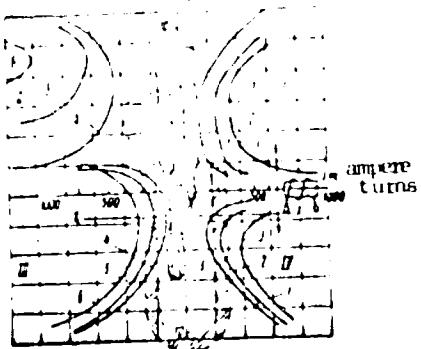


Fig. 2. Threshold operating characteristics

where the graph overlays a cross-section of the relay. The curves represent the threshold ampere-turns required for contact operation at varying distances of the coil from the reed contacts. The graph shows, for example, that maximum sensitivity occurs when the coil is in quadrant III, i.e., nearest to the movable reed, but that

Cord 2/3

L 3033d-66  
ACC NR: AP6019581

a greater tolerance in coil positioning can be had in quadrant I; also, a pronounced dead zone appears between quadrants I and IV. A similar family of curves was obtained for motion of the coil across the envelope, i.e., in the X-X direction of Fig. 2. From their data the authors have derived empirical design formulas for optimum coil positioning. They conclude that the cross-field design is practical and can be realized without unreasonable demands on geometry tolerances. Operating specifications of the tested relays are included. Orig. art. has: 3 figures and 6 formulas.

[SH]

SUB CODE: 09/ SUBM DATE none/ ORIG REF: 002/ OTH REF: 001/ ATD PRESS: 50/6

Cord 3/3 Jb2

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CIA-RDP86-00513R001340910017-5

PINCHUK, Mariya, zvenevay; RUDANOVICH, LASKA LUKANOVICH, zvenevay;  
ZIMBAL', Matrona [Lidora], Matrona

A field crew of close friends. Ref. stat. 37 nov 1984 p 17  
(Minsk)

(Stolin District--Women as farmers)

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PINCHUK, M.

Is it an ordinary village? Rab. 1 sial. 39 no. 2:4-5 P 163.  
(MIRA 16:4)

(Pugachevo(Brest Province)—Tailoring)

PINCHUK, M.A.; KANTOV, Ye.A.

Portable three-phase checking equipment. Igm.tekh. 20 no.1:49-50  
(MIPA 11:12)  
Ja '59.  
(Electric instruments)

PINCHUK, M.D.

School montages and exhibitions. Biol. v shkole no. 1:87-88  
Ja-F '63. (MIRA 16:6)

1. Armanikhinskaya vos'miletnyaya shkola Dal'ne-Konstantinovskogo rayona Gor'kovskoy oblasti.  
(Audio-visual education)

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P. 13017, . . .

3. Name of the Bureau or Department and its location,  
No. 2, S. -

80: Location and name of the Bureau or Department and its location,  
No. 2, S. -

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CIA-RDP86-00513R001340910017-5"

PINCHUK, M. G.

USSR (600)

Acorns

Good way to carry out collection, transportation, and storage of acorns. Lef 1  
step no. 9, 1952.

Monthly List of Russian Accessions, Library of Congress, December 1952. Unclassified.

1. PINCHUK, M. G.
2. USSR (600)
4. Windbreaks, Shelterbelts, Etc.
7. Use nut-bearing varieties more extensively in shelterbelt stands. Les. i step' 14  
No. 11, 1952.

9. Monthly List of Russian Accessions, Library of Congress, February 1953. Unclassified.

PINCHUK, M.G.

Growing gutta-bearing trees in the U.S.S.R. Trudy Inst. lesa 46:  
11-17 '58. (MIRA 11:6)

1. Glavnaya upravleniya lesnogo khozyaystva i polezashchitnogo  
lesorazvedeniya Ministerstva sel'skogo khozyaystva SSSR.  
(Gutta-percha)

PINCHUK, M.G.

Forest drainage in the U.S.S.R. Trudy Inst. lesa 49:5-8 '59.  
(MIRA 13:2)

1. Glavnoye upravleniye lesnogo khozyaystva Ministerstva sel'skogo  
khozyaystva SSSR.  
(Forests and forestry) (Drainage)

PINCHUK, M.G., lyubitel'-sadovod

Fumigation against aphids. Zashch. rast. ot vred. i bol. 2 no.1:  
42 N '63. (MIRA 17:3)

NORDASOV, P.M., kand.veterin.nauk; BITYUKOV, P.A., kand.veterin.nauk;  
INCHUK, M.I.; MALINOVSKIY, I.F.; LOGEYEV, A.M.

Mass prophylaxis of babesiosis in cattle by means of early  
(preventive) chemotherapy. Trudy NIVI 1:100-104 '60.  
(MIRA 15.10)  
(Chemotherapy) (Babesiosis)(Cattle--Diseases and pests)

PINCHUK, N.

~~Where once was "the devil's pasture."~~ Rab. 1 sial. 33 no.11:14 N '57.  
(MLRA 10:11)

1. Kalgas imya Gorkogo, Brestski rayen.  
(Brest District-- Plax)

11  
1231020952  
S/1967/1/000/007/106/013  
DC40/L113

AUTHORS: Medved, S.I., Krasavtsev, G.K., Gurevich, S.M., Chokotile,  
L.V., Lyand, A.S. and Pinchuk, N.I.

TITLE: Some peculiarities of electron-beam welding of austenitic  
steels and alloys

PERIODICAL: Avtomaticheskaya sverka, no. 7, 1961, 79-81

TEXT: In their introductory remarks, the authors state why the electron-beam welding of austenitic steels and alloys in a vacuum is superior to conventional welding. For experimental purposes, specimens of 9A 726 (EI 726) and 9MnMo (EI 946) heat-resistant austenitic steels and a nimonic-type 3K 437B (EI 437B) alloy were welded by the electron-beam method. All these types contain boron and are prone to cracks in the area near the weld and in the weld metal, if the composition of the base metal is reproduced. Welding was carried out with an electron-beam gun designed by the Orlensk Trudcempa (Electric Krasnogor Znameni Institut elektrosvarki im. Ye.O. Patona AS USSR (Electric Welding Institute "Order of the Red Banner of Labor" im. Ye.O. Paton AS UkrSSR) using 120 mA, 20 kw current and a 35 m/hr welding speed. Metal X

Card 1/2

22552

5/18/11/001/007/008/01\*

DOC /2411

Some peculiarities of electron-beam ...

produced by the electron beam is completely sound, except in the case of E17Cr steel where an intermetallic content of 0.61% caused cracks to form in the base metal at the seam and sometimes even in the weld metal. The following conclusions are drawn. The new method of electron-beam welding, in a vacuum, must be used not only for refractory and chemically active metals, but also for heat-resistant austenitic steels and alloys. The electron-beam method gives welds much more resistance to crystallization cracks than other known welding methods. It is to be expected that the use of filler wire will make the electron-beam process applicable to a wider range of austenitic steels and alloys, and that the form and shape of the seam will necessitate no modification of the design of the joints. There are 6 figures. X

ASSOCIATION: Orlensk Trubnoye Krasnogor Znameni Institut elektronvarki im. Ye. O. Patona AN USSR (Electric Welding Institute "Order of the Red Banner of Labor" im. Ye. O. Paton AS UkrSSR)

SUBMITTED: April 17, 1961

Card 2/2

18.111

3/15/68/3007-10/17-5  
K/E/KH.

AUTHORS: Nedevan, B. I., Doctor of Technical Sciences, Cherkashin, I. V.,  
Pinenuk, N. I., Batsyuk-Khudin, V. A., Engineer.

TITLE: Intercrystalline weld-adjacent cracks in welding austenite steels and alloys

PERIODICAL: Svarochnye proizvodstva, no. 4, 1962, p. 31

TEXT: The authors, with the participation of engineer I. I. Lutsyn, present some concepts on the formation of weld-adjacent intercrystalline cracks in flash-welding of austenite steels and alloys. During this process the following types of crack may arise: 1) crystallization cracks extending from the weld, or originating in the weld; 2) cracks along the fusion line at a distance from one to several grains; 3) cracks along the linear eutectics of intermetallic and nonmetallic impurities. An effective means of preventing crystallization cracks in heat-resistant austenite steels, is to raise the carbon content in the weld metal, for the purpose of increasing the quantity of ferrite eutectics, which is able to close-up weld-adjacent cracks. To prevent cracks which run at an equal distance from the fusion line, it is imperative not to

Card 1/2

Intercrystalline weld-adjacent cracks ...

A. S. Kuznetsov

allow superheating of the base metal and slow cooling in the temperature range of least resistance of the gamma-solid solution. Changes in the thermal treatment of the steel or alloy, and, first of all, a reduced carbon content during development of a second phase in the structure, should help to prevent the formation of weld-adjacent cracks of this type. To prevent cracks due to clusters of impurities, it is necessary to use for stressed parts a metal that had been subjected to electric slag remelting in order to raise sharply its micro-homogeneity. Electric slag remelting is simultaneously a reliable means of preventing weld-adjacent crystallization cracks. There are 7 figures and 12 references; 7 Soviet-bloc and 3 non-Soviet-bloc.

ASSOCIATION: Institut elektrosvarki imeni Ye. N. Patona AN UkrSSR (Institute of Electric Welding imeni Ye. N. Paton, AS UkrSSR)

Card 2/2

S/125/62/000/005/003/010  
K40/D1.3

ADDRESS: Todorov, V.V., Latsynuk-Kludin, V.A., Vinograd, N.I.,  
and Puzrin, L.S.

TITLE: *Investigation of heat-resistant austenitic steels, alloys, and welds with*  
*chromium carbide precipitates*

PUBLISHED: Moscow, "Naukova Dumka", 1982, -17

TEXT: The authors review data from their own experiments and from 22 Soviet  
and non-Soviet publications, and show that heat-resistant austenitic metal  
alloyed with 0.3 - 1.5% carbides increases long-term strength and crack  
resistance. It is proved that metal containing boron as an alloying element  
has a two-phase (austenite and carbide) structure, which improves  
the properties of the metal. As revealed by Todorov and Latsynuk-Kludin,  
("Avtomaticheskaya svarka", no. 12, 1981), C.V% = 0.0204 B in steel leads to  
local fusion of the grain boundaries and to the growth of hot cracks which

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2/27/2023 2/27/2023  
A. J. M.

Alloying heat-resistant austenitic steels.....

can subsequently cause embrittlement of the weld metal in the weld zone, measured with an X-ray diffraction technique, and found to be 1.4%.  
According to data presented by P. J. Karr, D. L. Tamm and J. W. Lien, at the  
Institute of Boron Technology, the heat-resistant austenitic welds, with addition  
of 0.4% boron, greatly increased the heat resistance of welds, while addition  
of 0.5% boron greatly reduced the heat resistance of welds almost doubled the strength of  
welds in 10-hour test at 500° under a load of 20-ton/in<sup>2</sup>, increased the pre-  
failure test time ten-fold. Similar results were obtained with X-1-H 3  
failure test time ten-fold. Similar results were obtained with X-1-H 3  
(K. L. 5N75) welds. Hardening of steel with 0.5% boron caused no  
difficulties, but it did not increase the weld cracking danger because  
of lower plasticity and larger ductile phase. It is advised to use pre-  
heat and moderation cooling in welding such steel. Electroslag remelting is  
suggested for improvement of ductility of boron-alloyed steel as stated for  
stainless steel. However, conventional alloying heat-  
resistant austenitic steel and welds with over 0.3 - 0.4% boron greatly in-  
creases the resistance to crystallization cracks, practically eliminates the  
danger of jet cracking occurring at the welds, produces very good welded joints  
in service at high temperature and loads, and considerably improves the heat

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5/125/c2/003/005/003/010

DX57/B113

Alloying heat-resistant austenitic steels....

resistance of the steel. Curve and figures and tables.

ASSOCIATION: Chinese Association of Metallurgical Engineers Institute of Ferrous Materials  
(Academy of Military Sciences, Ministry of Defense, Order of the Red Banner of Labor Unit, Yev. Paton, A.S. Ussr.)

SUBMITTED: January 15, 1982

Card 3/3

MEDOVAR, B.I., kand.tekhn.nauk; PINCHUK, N.I., inzh.; PUZRIN, L.G., inzh.

Effect of phosphorus on the stress-rupture strength of joints in  
welded Kh18N9T steel. Metalloved. i term. obr. met. no.8:24-25  
Ag '62. (MIRA 15:11)

1. Institut elektrosvarki im. Ye.O.Patona AN UkrSSR.  
(Steel alloys—Welding) (Welding—Testing)

MEDOVAR, B.I.; PINCHUK, N.I.

Preventing the embrittlement of 25-20 type austenitic  
welded joints. Avtom.svar. 15 no.10:46-49 O '62.  
(MIRA 15:11)

1. Ordona Trudovogo Krasnogo Znameni Institut  
elektrosvarki im. Ye.O. Patona AN UkrSSR.  
(Steel, Heat-resistant--Welding)  
(Phase rule and equilibrium)

ACCESSION NR: AT4013946

S/2659/63/010/000/0178/0185

AUTHOR: Medovar, B. I.; Chekotilo, L. V.; Lutsyuk-Khudin, V. A.; Pinchuk, N. I.;  
Puzrin, L. G.

TITLE: Boron alloys (over 0.3-0.4%) for high temperature austenite steel and weld seams

SOURCE: AN SSSR. Institut metallurgii. Issledovaniya po zharoprochnym splavam,  
v. 10, 1963, 178-185

TOPIC TAGS: boron, boron containing alloy, austenite steel, high temperature  
steel, weld seam, weld metal

ABSTRACT: Austenite high-temperature steels alloyed with boron consist of two phases (austenite + boron component of eutectic origin) and are characterized by high tensile strength and elasticity. The use of boron alloys (over 0.3-0.4%) for high temperature austenite steel allows one to solve several important problems. The weld metal sharply increases stability against the formation of hot (crystalline) cracks. Hot cracks adjacent to the weld seams are completely eliminated during welding. The reliability of weld seams working under high temperature and loads is increased significantly by the exclusion of the causes of local brittle failure in the seam zone. The heat resistance of austenite steel and

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ACCESSION NR: AT4013946

weld seams is increased to a great extent. Investigations and experimental work at plants should be expanded so as to develop both new high-temperature austenite steel, as well as flow processes for the use of these steels for welding. Orig. art. has: 3 tables and 3 microphotographs.

ASSOCIATION: Institut metallurgii AN SSSR (Metallurgical Institute AN SSSR)

SUBMITTED: 00

DATE ACQ: 27 Feb 84

ENCL: 00

SUB CODE: ML

NO REF SOV: 015

OTHER: 007

Cord 2/2

MEDOVAR, B.I.; PINCHUK, N.I.; CHEKOTILO, L.V.

Increasing the maximum permissible concentrations of  
phosphorus and silicon in stable austenitic welds. Dokl.  
AN SSSR 150 no.3:541-543 My '63. (MIRA 16:6)

1. Institut elektrosvarki im. Ye.O. Patona AN UkrSSR.  
Predstavлено академиком B.Ye. Patonom.  
(Welding)

MEDOVAR, B.I.; PINCHUK, N.I.

Effect of boron on the structure of an austenite joint. Avtom.  
svar. 16 no.6:91-93 Je '63. (MIRA 1 :7)  
(Iron-nickel-chromium alloys--Welding)  
(Boron)

MEDOVAR, B.I., CHEKOTILO, L.V.; LUTSYUK-KHUDIN, V.A.; PINCHUK, N.I.; PUZRIN, L.G.

Addition al oys of boron (more than 0.3 - 0.4%) in austenitic heat-resistant steels and weldments. Issl. po zharoproch. splav. 10:170-125  
'63. (MIRA 17:2)

L 10763-63

EWP(k)/EWP(q)/EWT(m)/BDS--AFFTC/ABD--PI-4--JD/EM

ACCESSION NR: AP3002322

S/0125/63/000/006/0091/0093

60

AUTHOR: Nedovar, B. I.; Pinchuk, N. I.TITLE: Effect of boron on austenitic weld structureSOURCE: Avtomatischeskaya svarka, no. 6, 1963, 91-93

TOPIC TAGS: fully austenitic welds, hot cracking, boron effect, silicon, phosphorus

ABSTRACT: A recent study has shown that the upper limits of the Si and P contents (0.2% Si and 0.02% P) in fully austenitic welds can be considerably increased by the addition of 0.3-0.6% boron to the weld metal. The experiments were conducted with two 18-8-type steel weld metals: 05Kh19N9TBS (0.06-0.07% C, 19.33-21.16% Cr, 9.18-9.61% Ni, 1.51-1.60% V, 1.13-1.26% Nb, 0.0-1.06% B) and 05Kh19N9T (0.4-0.06% C, 17.75-18.91% Cr, 9.36-9.95% Ni, 0.21-0.31% Ti, 0.0-0.50% B). Boron was introduced as an Fe-B master alloy (20.2% B, 1.98% Al, 1.70% Si). Metallographic examination and phase analysis indicate that B acts as a strong austenitizer; it reduces the amount of primary  $\delta$ -ferrite in the metal and is 10 times as effective as Ni in this respect. Thus, the addition of 0.3-0.5% B to the weld is equivalent to increasing the Ni content by 3-5%. The boride eutectic

Card 1/2

I-10763-63

ACCESSION NR: AP3002322

formed in boron-bearing austenitic welds dissolves active ferritizers, such as V, Nb, Si, Ti, and apparently, also P. Such welds, have satisfactory ductility and improved resistance to hot cracking at respective Si and P contents as high as 0.7 and 0.08%. Orig. art. has: 3 figures and 1 table.

ASSOCIATION: none

SUBMITTED: 00

DATE ACQ: 12Jul63

ENCL: 00

SUB CODE: 00

NO REF Sov: 004

OTHER: 002

*Jim D*  
Card 2/2

11000-63

IMP(k)/IMP(q)/IMP(n)/BDS--NFTG/ASD--PZ-4--JD

3/0020/63/130/003/0541/0543

62

61

ACCESSION NR: AF3000749

AUTHOR: Makryuk, D. I.; Pinchuk, N. I.; Chatotille, L. V.TITLE: Increasing the upper limits of phosphorus and silicon in fully austenitic  
welds 27 27

SOURCE: AN SSSR. Doklady, v. 130, no. 3, 1963, 541-543

TOPIC TERM: welding, fully austenitic steel, hot cracks, boron effect, silicon  
effect, phosphorous effect

ABSTRACT: The effect of boron on susceptibility to hot cracking of fully austenitic Cr-Ni steel welds has been studied. Currently the Si content must be kept below 0.25% and the P content below 0.020% to reduce hot cracking. This, however presents serious difficulties in melting these steels. Adding 0.3-0.5% boron to 23-20 and 13-35 type austenitic steels solved the problem and made it possible to weld steels containing 0.53-0.63% Si and 0.028-0.94% P. The addition of boron results in the formation of a complex Fe-Ni-Cr-B eutectic, capable of dissolving Si, P, and other liquating elements. Mechanical tests made on 23-20 and 13-35 austenitic welds (see Table 1 of Enclosure) showed that boron-bearing welds annealed at 1100°C have satisfactory mechanical properties, though somewhat

Cont 1/3

L 11000-63

ACCESSION NO: AP3000749

inferior to those of boron-free welds. At high temperatures, however, the differences become negligible (see Table 2 of Enclosure). The rupture life of welds C, D, and E, at 800°C under a stress of 10 kg/mm<sup>2</sup> (after 10-hr stabilization at 800°C) was 78, 192, and 215 hr.

ASSOCIATION: Institut elektrosvarki im. Ye. O. Patona Akademii nauk SSSR  
(Electric Welding Institute, Academy of Sciences, USSR)

SUBMITTED: OSAver62

DATE ACQ: 21Jun63

ENCL: 01

SUB CODE: ML,MA

NO REF Sov: 004

OTHER: 000

Card 2/3

L 13272-66 EWT(m)/EWA(d)/EWP(v)/T/EWP(t)/EWP(k)/EWP(z)/EWP(b)/EWA(h)/EWA(c)  
ACC NR: AF6002908 JD/EM SOURCE CODE: UR/0286/65/000/024/0073/0073

INVENTOR: Medovar, B. I.; Borzdyka, A. M.; Latyshov, Yu. V.; Pinchuk, N. I.;  
Chekotilo, L. V.; Topilin, V. V.

ORG: none

TITLE: Weldable, heat-resistant steel. Class 40, No. 177079

SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 24, 1965, 73

TOPIC TAGS: steel, heat resistant steel, chromium containing steel, nickel containing  
steel, tungsten containing steel, titanium containing steel, manganese containing  
steel

ABSTRACT: This Author Certificate introduces a weldable, heat-resistant steel with  
increased resistance to local failure of welded parts. The steel contains 0.08%  
max carbon, 0.5% max silicon, 0.5—1.0% manganese, 14.5—16.5% chromium, 23—25%  
nickel, 4.0—5.0% tungsten, 1.5—2.0% titanium, 0.4—0.7% boron, and 0.02% max sulfur.  
[AZ]

SUB CODE: 11/ SUBM DATE: 25Apr64/ ATD PRESS: 4/55

Card 1/1

UDC: 669.14.018.44

L 35825-66 EWP(k)/EWT(m)/T/EWP(v)/EWP(t)/ETI IJ(c) JD/IM

ACC NR: AP6021827

SOURCE CODE: UR/0413/66/000/012/0136/0136

43

B

INVENTOR: Medovar, B. I.; Chakotilo, L. V.; Pinchuk, B. I.

TITLE: Welding wire. Class 49, No. 183042

SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 12, 1966, 136

TOPIC TAGS: welding, steel, austenitic steel, oxidation-resistant steel, welding, welding rod, welding wire, weld

ABSTRACT: This Author Certificate introduces a filler or electrode wire for welding oxidation-resistant, austenitic, silicon-rich steels. The wire contains up to 0.1% carbon, 2.5–3.0% silicon, up to 1.5% manganese, 24–27% chromium, 18–21% nickel, 0.02% max sulfur, 0.03% max phosphorus and 0.45–0.65% boron. Boron increases the weld resistance against carburization, hot cracking, and sigma-phase formation. [ND]

SUB CODE: 1301/ SUBM DATE: 06Aug66/ ATD PRESS: 5036

10  
Card 1/1

UDC: 621.791.042

L 35823-66 EWP(k)/EWT(m)/T/EWP(v)/EWP(t)/ETI IJP(c) JD/HM  
ACC NR: AP6021799 (N) SOURCE CODE: UR/0413/66/000/012/0063/0063

INVENTOR: Madever, B. I.; Stryov, V. S.; Chashko, L. V.; Tarkov,  
N. A.; Pinchuk, N. I.

40  
B

ORG: none

TITLE: Electrode for welding oxidation-resistant steels. Class 21, No.  
182814 [announced by the Electric Welding Institute im. Ye. O. Paton (Institut  
elektrosvarki)]

SOURCE: Izobreteniya, promyshlennyye obraztay, tehnicheskiye snaki,  
no. 12, 1966, 63

TOPIC TAGS: steel, welding, oxidation-resistant steel, welding  
electrode

ABSTRACT: This Author Certificate introduces an electrode for welding  
oxidation-resistant steels. The electrode coating contains 31% marble,  
27% fluorspar, 6.5% manganese, 1.5% aluminum, and 14% ferrosilicon. To  
increase the weld resistance against carburization, hot cracking, and  
oxidation, 12% ferroboron and 8% dolomite are added to the coating com-  
(ND)

SUB CODE: M11,0/SUBM DATE: 26 May 65/ATD PRESS: 5136

Card 1/1

ACC NR: AP6015254

SOURCE CODE: UR/CL/5/66/

AUTHOR: Tabidze, A. I.; Pinchuk, N. I.; Us, V. I.; Yushkevich, Z. V.

ORG: none

TITLE: Stress corrosion cracking resistance of austenite chromium-manganese steels  
and alloys in chloride solutions

SOURCE: Avtomaticheskaya svarka, no. 5, 1966, 76-77

TOPIC TAGS: low nickel steel, stainless steel, chromium steel, manganese steel, cor-  
rosion resistance, chloride / Kh14G30 steel, 1Kh18N10T austenitic steelABSTRACT: Austenitic stainless steels of the 18-8 type are prone to stress corrosion cracking in chloride-containing solutions whereas high-Ni alloys (containing >40-45% Ni) resist corrosion of this kind. In this connection it was of interest to investigate the corrosion resistance of these alloys in chloride solutions on partial replacement of Ni with Mn. Accordingly, the authors investigated alloys of the Kh14G30 types containing from 1 to 23% Ni, which, to enhance their resistance to general corrosion, were additionally alloyed with 2.5-3.35% Mo, 0.23-0.3% Ti, 0.25-0.38% Al and 0.23-0.4% B. Various stressed specimens of these steels were tested for stress corrosion cracking in boiling (+154°C) 42% MgCl<sub>2</sub> solution, on first undergoing heat treatment (1100°C for 1 hr, cooling in air). Specimens of 1Kh18N10T austenitic

UDC: 621.791;620.193;669.15-194

Card 1/2

ACC NR: AP6015254

steel were also investigated for purposes of comparison. Findings: the stress corrosion cracking of 1Kh18NiOT steel in the MgCl<sub>2</sub> solution sets in within the first 24 hr, and the same happens for specimens of Kh14G30 steel containing 8-23% Ni. On the other hand, specimens of Kh14G30 steel containing <8% Ni take more time to corrode; for specimens containing 3.68% Ni the time to corrosion is 143-169 hr, and for specimens with <2% Ni, more than 400 hr (Fig. 1).

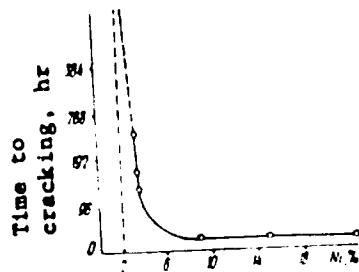


Fig. 1. Effect of Ni on corrosion resistance of Kh14G30-type austenitic Cr-Mn alloys in boiling 42% solution of MgCl<sub>2</sub>

Thus, the replacement of Ni with Mn further contributes to enhancing the resistance of austenitic steels to stress corrosion cracking. Orig. art. has: 4 figures, 1 table.

SUB CODE: 13, 11/ SUBM DATE: none/ ORIG REF: 003/

Card 2/2

ACC NR: AT6034462

(A)

SOURCE CODE: UR/000/66/000/000/025B/0262

AUTHOR: Medovar, B. I.; Pinchuk, N. I.; Us, V. I.

ORG: none

TITLE: Effect of boron on properties of austenitic steels

SOURCE: AN SSSR. Institut metallurgii. Svoystva i primenenie zharoprovchnykh splavor (Properties and application of heat resistant alloys). Moscow, Izd-vo Nauka, 1966, 258-262

TOPIC TAGS: austenitic steel, boron containing alloy, tungsten containing alloy, titanium containing alloy

ABSTRACT: The article reports a study of the effect of boron within the limits of 0.40-0.70% on the properties of austenitic steels Types 18-12 with niobium, and 15-25 with tungsten and titanium. Austenitic boride steels Kh18N12B1, Kh18N12B2R1, and Kh15N24V4T2R1 were compared with analogous steels without boron. The austenitic boride steels were tested after austenizing at 1050-1100°C for 1-3 hours, with cooling in air; the analogous austenitic steels Kh18N12B and Kh15N24V4T were tested after a typical heat treatment: austenizing at 1130°C for 2 hours. Comparison of the mechanical properties showed the following: 1) as a result of alloying austenitic steel hardened with carbides, Type Kh18N12B, with boron within the limits of 0.40-0.70%, the strength

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ACC NR: AT6034462

increased and the plastic properties were lower. The toughness of the steel decreases sharply from 24 to 3-8 kgm/cm<sup>2</sup>; 2) as a result of alloying austenitic steel Kh15N24V4T with intermetallic hardening, with boron in amounts between 0.40-0.70%, the strength properties of the steel decrease, and there is a simultaneous decrease in the plastic properties. The toughness decreases from 10-13 to 4-8 kgm/cm<sup>2</sup>. In conclusion, the following advantages are listed for the alloying of austenitic steels with boron: 1) high resistance to local failure in the neighborhood of welded joints; 2) high resistance to the appearance of hot cracking around welded joints and to crystallization cracking in the metal joint; 3) high stability of structure and properties, attainable with boride hardening; and, 4) high long term ductility and heat resistance, attainable with boride hardening. Orig. art. has: 3 figures and 2 tables.

SUB CODE: 11 / SUBM DATE: 10Jun66 / ORIG REF: 003 / OTH REF: 002

Card 2/2

ACC NR: AP7001930

SOURCE CODE: UR/0125/66/000/0012/0052/0057

AUTHOR: Medovar, B. I.; Pinchuk, N. I.; Chekotilo, L. V.; Pavliychuk, G. A.;  
Us, V. T.; Tabidze, A. I.

ORG: Electric Welding Institute im. Ye. O. Paton, AN UkrSSR (Institut elektrosvarki  
AN UkrSSR)

TITLE: Weldable boron-bearing austenitic steels and alloys

SOURCE: Avtomaticheskaya svarka, no. 12, 1966, 52-57

TOPIC TAGS: <sup>weldability,</sup> chromium nickel boron steel, austenitic steel, weldable austenitic  
steel, niobium containing steel, tungsten containing steel, titanium containing  
steel, Kh18N12B2R1 austenitic steel, Kh615N24V4T2R1 austenitic steel

ABSTRACT: Several new weldable chromium-nickel austenitic steels and alloys con-  
taining up to 0.70% boron have been developed in a joint effort by the  
Electric Welding Institute im. Ye. O. Paton, TsNIITMASH, TsNIIChM, the  
Moscow Experimental Welding Plant, and Orgenergostroy. Heat-resistant  
steels Kh18N12B2R1 or EP531 (0.10% max carbon, 17—19% chromium,  
11—13% nickel, 1.8—2.3% niobium, and 0.40—0.70% boron) and  
Kh15N24V4T2R1, or EP467 (0.08% max carbon, 14.5—16.5% chromium, 23—25%  
nickel, 4—5% tungsten, 1.5—2.2% titanium, and 0.40—0.70% boron) are  
tube materials intended primarily for steam pipelines and superheaters.

Card 1/2

UDC: 621.791.011:669.15-194

ACC NR: AP7001930

Both steels have satisfactory heat resistance (EP467 steel in stress-rupture tests at 650°C under a stress of 28 kg/mm<sup>2</sup> failed after 5909 hr at an elongation of 14.0% and a reduction of area of 19.9%), satisfactory weldability, and low susceptibility to local fractures in the weld-adjacent zone. Boron-bearing nickel-base alloys were developed as cast alloys for parts operating at temperatures up to 200°C. Cast Kh20N77T3YR alloy containing 0.70% boron had at 800°C a tensile strength of 64.5 kg/mm<sup>2</sup>, a yield strength of 64.1 kg/mm<sup>2</sup>, an elongation of 1.76%, a reduction of area of 3.0%, and a notch toughness of 1 mkg/cm<sup>2</sup> compared to 46.0 kg/mm<sup>2</sup>, 39.4 kg/mm<sup>2</sup>, 8.2%, 16.0%, and 20.6 mkg/cm<sup>2</sup> for the same alloy but without boron. In stress-rupture tests at 800°C under a stress of 29 kg/mm<sup>2</sup>, the alloy with 0.70% boron failed after 26 hr compared to 3 hr for alloy without boron. Boron improved significantly the weldability of oxidation-resistant steels Kh25N20S2 and Kh18N35S3 without affecting the oxidation resistance at temperatures up to 1000°C. Kh18N10BR(EP381) and Kh13G30NR1(EP537) steels, intended for operation in chloride solutions, are highly resistant to stress corrosion. Specimens of these steels were removed and amassed after 4150—4300 hr test in a boiling 42% solution of magnesium chloride under a stress of 27.3—27.6 kg/mm<sup>2</sup> (90% of yield strength), while the specimens of standard K18N10T and Kh18N10B steels failed after 8—24 and 2—18 hr, respectively. Orig. art. has: 10 figures and 8 tables.

SUB CODE: 11/ SUBM DATE: 23May66/ ORIG REF: 006/ OTH REF: 001/ ATD PRESS: 5111

Card 2/2

MORACHEVSKIY, Yu.V.; PINCHUK, N.Kh.

Determination of "sulfate" sulfur. Uch.zap.Len. un. 163:28-36 '53.  
(Sulfates) (Sulfides)  
(MLRA 9:6)

PINEHUK, N. KH.

USSR.

✓ Determination of sulfide sulfur. Yu. V. Alenachikhil and N. Kh. Pinehuk. Uchenye Zapiski Leningrad. Gornodob. Univ. im. A. N. Zhidkova No. 103, Ser. Khim. Nauk No. 12, 29-30 (1953).—The det. of S in FeS ores (pyrite and marcasite) often yields high results because of the incidental oxidation of the sulfide S by  $\text{Fe}^{3+}$  usually present. Digestion of 0.3000 g. of  $\text{FeS}_2$  at 100° for 8 hrs. with 0.6, 1.9, and 3 g.  $\text{FeCl}_3$  in 1% HCl resulted in the oxidation of 12, 19, and 21% of the S to  $\text{SO}_4^{2-}$  and free S; the corresponding values in 0.6 and 10% HCl were progressively lower. The presence of phosphoric or tartaric acid reduced the extent of oxidation; hydroxylamine stopped it. The following procedure is recommended: to 0.6-2 g. of the ore, add 1-2 g.  $\text{NH}_4\text{OH}$  in 10% HCl. Heat until the ore is all attacked. Add 100-150 ml. hot  $\text{H}_2\text{O}_2$ , filter, and det.  $\text{SO}_4^{2-}$  as usual.

L. Benowitz

Pinchuk, N. M.

An apparatus for the reduction, storage and titration of salts of tervalent titanium. N. M. Pinchuk. Nauka Byull. Leningrad Univ. 1953, 13(5), 44-51; Ref. Zhar., Khim., 1954, Abstr. No. 63,116.—The apparatus for the production, storage and titration of a soln. of  $Ti^{4+}$  consists of a three-necked flask of capacity 500 to 800 ml, painted black or with paper glued on to it. To the flask is joined a separating funnel of capacity 300 to 500 ml in which are several glass beads, a little glass wool and a layer of metallic Zn or Cd almost to the neck; a flask of capacity 2 to 8 litres; a siphon of 2 to 3 mm diam, and a burette with a side-tap and with a side-arm fused in the top for the exit of gas, with a Bonnser valve closed by a glass tube with a rubberbung, which is removed when reducing  $Ti^{4+}$  and filling the burette. Having assembled the apparatus, pass  $CO_2$  or H for 30 to 40 min. Fill the funnel three-quarters full with a soln. of  $Ti^{4+}$ , then run the reduced soln. into the three-necked flask and determine its concn. The burette is filled by increasing the gas pressure in the three-necked flask (i.e., by raising the flask which contains water). It may be used for the production, storage and titration of solns. of  $Cr^{3+}$ . C. D. KOPKIN

PINCHUK, N.Kh.

Apparatus for reduction, preservation, and titration by using a salt  
of trivalent titanium. Nauch. biul. Len. un. no.33:24-27 '55.  
(MLRA 10:4)

1. Kafedra analiticheskoy khimii.  
(Reduction, Chemical) (Volumetric analysis) (Titanium)

Pinchuk, N. Kh.

18

4E2C

✓3663. Phase analysis of iron minerals. J. Yu. V.  
Morachevskii and N. Kh. Pinchuk. Vestnkh  
Leningr. Univ., 1958, (10), 60-87; Rej. Zhar.,  
Khim., 1959, Abstr. No. 78,596.—Satisfactory con-  
ditions have been found for the separation of  
magnetite from haematite by using their different  
rates of dissolution in  $H_3PO_4$ . Magnetite completely  
dissolves in a soln. of  $H_3PO_4$  and 1% HCl (1:1) by  
shaking on a boiling-water bath, while haematite is  
practically insoluble; in the presence of magnetite  
the solubility of haematite in these conditions is  
much increased, owing to the presence in the soln.  
of  $Fe^{2+}$ ; on adding an oxidant to the  $H_3PO_4$ , the  
solubility of haematite is greatly reduced. The  
optimum conditions for the separation of magnetite  
and haematite are a 90-min. treatment at 40°  
with  $H_3PO_4$  (sp.gr. 1.70) and 1% HCl (1:1 by vol.),  
with the addition of  $KMnO_4$  to a pale-pink colour.  
Under these conditions complete dissolution of the  
magnetite is accompanied by minimum dissolution  
of haematite (on the average  $\approx 1\%$  of the total  
iron in the sample passes into solution).

C. D. KOPPIN

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PINCHUK, N. H.H.

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*Phase analysis of iron ore. II. Selective dissolving of magnetite in the presence of chalcopyrite. Ya. V. Marnichenko and N. Kh. Pinchuk. Vestnik Leningrad. Univ. 11, No. 23, Sov. Nauch.-Tekhn. Kibernetika, No. 4, 170-8 (1956); cf. C.A. 50, 16839a.—To 0.11-0.13 g. powd. ore add 10 ml.  $H_3PO_4$  (sp. gr. 1.70) dilut. 1:1). Heat 5 min. on a boiling water bath with mech. stirring. All of the magnetite dissolves and about 1% of the Fe of the chalcopyrite. Filter and wash the residue. To the filtrate add 25 ml. concd.  $HCl$ , heat nearly to boiling, reduce with  $SnCl_4$ , and titrate with  $K_2Cr_2O_7$  to obtain the Fe content of the magnetite in the sample. Ignite the residue (chalcopyrite), dissolve in "reversed" aqua regia, and det. Cu by a standard method.*  
I. D. Pinche

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PINCHUK, N. Kh.

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V 390. Phase analysis of iron ores. II. Selective solution of magnetite in the presence of chalcopyrite.  
Yu. Y. Morachinskii and N. Kh. Pinchuk. Vestn.  
Leningr. Univ., 1956, (3), 170-175; Zhur.  
Khim., 1957, Abstr. No. 34,742.—A method is  
evolved for the determination of Fe in magnetite  
(I), or in an ore composed of I and chalcopyrite  
(III), based on the selective solution of I in  $H_3PO_4$ ,  
I being practically insoluble in this acid.

C. D. KORNIN

✓ 11

MORACHEVSKIY, Yu.V.; PINCHUK, N.Kh.

Phase analysis of iron ores. Part 2. A selective dissolution of  
magnetite in the presence of chalcopyrite. Vest.Len.un.ll no.22:  
170-175 '56. (MLRA 10:2)

(Magnetite) Chalcopyrite)

ABSTRACT

**FILE** Chemical Properties of the Compound  
III. The Selective Solution **DATE** 10-10-68  
**PUBLICATION** III. Selective Solubility of the Compound  
III. Dissolving of Nitrite in Water

**EXTRICAL.** Author: L. S. J. and co-authors: S. S. K. and  
M. A. (N.Y. 1), 1958, Nr. 4

**ABSTRACT:**

The authors have studied the solubility of the compound III, **dissolving**, in water. In the first experiments it was found that the solubility of nitrite in water decreased with increasing concentration of the compound III. This decrease in solubility was attributed to the formation of a complex between the compound III and the nitrite. It was noted, however, that solubility increased again at a certain concentration of the compound III. The authors also found that penetration of the solute into the nitrite solution decreased from the planar to the spherical configuration of the solute. Increased solubility of the nitrite in water was observed at a low concentration of the nitrite. Thus, it appears that the solubility of the

Card 1,7

Hematite in Iron Oxide  
III. The Selective Solution Dissolution of the  
Presence of Hematite

To reduce the solubility of hematite, to remove the magnetite, it is proposed during the treatment with a phosphoric acid in the presence of a gelatinous zinc oxide. This can be carried out by the addition of the iron in the divalent form by means of ferrocyanide or hydrazine, etc. While reducing, it is also possible by means of complex-forming reagents. In the present paper the authors investigated the dissolution of hematite in the presence of magnetite with an addition of oxidation- and complex-forming media. The results obtained by the investigations showed that by the addition of tartaric acid, citric acid, phosphoric acid during the process of dissolution of the magnetite-hematite mixture its solubility is diminished by the addition of tartaric acid to the phosphoric acid solution the solubility of hematite is diminished and magnetite is practically fully dissolved. Thus, favorable conditions for the selective dissolution of magnetite in the presence of hematite were found in the case of a reduction of magnetite 0 + 20 mesh. There are figures, and a reference list which are Slides.

Card 23

the analysis of iron ore  
III. The Selective Solution of Magnetite in the  
presence of lecitite

S. I. P. D. stated, 1957

Available: Library of Congress

1. Iron-Analysis
2. Ores-Analysis
3. Magnetite-Solubility
4. Hematin-Solubility

AUTHORS:

Firsov, N.P., Kurnikov, Yu.V.

-10-2-8

TITLE:

The Phase Analysis of Iron Ore. IV. Study of the Selective Dissolution of Mineral Ferric Hydroxides in the Presence of Magnetite and Hematite (Fizicheskaya analiza rastvorimosti IV. Izuchenie izbivayushchego rastvorimosti ferriyev vidrodzheniy v prisutstvii magnetita i hematita)

PERIODICAL:

Vestnik Leningradskogo Universiteta, Seriya fiziki i khimii  
1962, Vol. 10, No. 2, pp. 24-37 (USSR)

ABSTRACT:

The authors elaborated a method of selective dissolution of magnetite in the presence of hematite (Ref. 1), and in the presence of calcium pyrite (Ref. 6) in a phosphoric acid solution (Ref. 5). The study of the selective dissolution of ferric hydroxide in a phosphoric acid solution is a continuation of the work concerning phase analysis carried out by the Chair of Analytical Chemistry. For the selective dissolution of iron ore component conditions must be found at which the solubility of hydroxides would be either minimal or complete. In order to reduce the solubility of hydroxides in phosphoric acid, its solubility was studied at 100°, but after complete dissolution of the

Card 1/4

The Phase Analysis of Iron Ores. IV. Study of the  
Selective Dissolution of Mineral Ferric Hydroxide in  
the Presence of Magnetite and Hematite

4-10-8/4

magnetite (table 2). It is shown (table 3) that higher concentration of phosphoric acid reduces the solubility of ferric hydroxides down to 3-4%. In the case of dilution of phosphoric acid 1:1, 3% and at 50°C the hydroxides dissolve only to a small extent. Therefore, conditions were found at which magnetite dissolves completely, whereas ferric hydroxides in the case of separate treatment are hardly dissolved at all. It is shown (fig. 4) that the solubility of ferric hydroxides increases rapidly in the presence of magnetite. Whereas, in the absence of magnetite, only 3% of the ferric hydroxides had been dissolved, 90% were dissolved at the same condition but in the presence of magnetite. These experiments showed that it is not possible, or the strength of the behavior of individual minerals in one or the other solvents, to draw conclusions as to whether they would also be dissolved in the presence of other minerals. In order to clear up the behavior of hematite on the occasion of the dissolution of the entire quantity of magnetite and ferric hydroxides, experiments were carried out with a view of bringing about the total dissolution of the said minerals at conditions similar to those prevailing in the case of previous experiment. At these conditions magnetite is dissolved entirely

Card 2/4

The Phase Analysis of Iron Ores. IV. Study of the  
Selective Dissolution of Mineral Ferric Hydroxides in  
the Presence of Magnetite and Hematite

54-10-2-8/16

and ferric hydroxides on the average are dissolved to the extent of 98.43% (table 5), the remaining 1.57% consequently consist of hematite and a small part of the not dissolved hydroxides. It may be seen (table 6) that in the case of a common dissolution of magnetite, of the hydroxides, and of hematite, magnetite and practically also the hydroxides are fully dissolved, whereas only about 13% of hematite are dissolved. In the presence of tartaric acid the solubility of hematite - conditions remaining the same - is reduced by 4-5%. The data mentioned (tables 8 and 9) lead to the conclusion that for the selective dissolution of the total quantity of magnetite and some ferric hydroxides in the presence of hematite favorable conditions have been found. As is known, the minerals - ferric hydroxides and hematite originating from different deposits differ considerably from each other. For this reason it is not possible to elaborate a method of selective dissolution of the minerals mentioned that would be applicable equally well in the case of minerals originating from different deposits. Therefore, the method worked out can only serve as a basis for the

Card 3/4

The Phase Analysis of Iron Ores. IV. Study of the  
Selective Dissolution of Mineral Ferric Hydroxides in  
the Presence of Magnetite and Hematite

54-10-2-8/16

study of selective dissolution of the aforementioned minerals  
of the deposit concerned. There are 9 tables and 10 refer-  
ences, all of which are Soviet.

SUBMITTED: December 25, 1957

AVAILABLE: Library of Congress

1. Iron ores—Phase studies      2. Ferric hydroxides—Solubility

Card 4/4

1962

2-1-1

PL-1341

5370

ATTACHED

HEDGES, R. J., WYOMING, WYOMING, DEPT. 7

PRINCETON, N. J.

TYPE

Reactions of hexa(alkylbenzene) with alkyl  
ketones

EXPERIMENTAL

Potassium hydroxide was added to a

one liter round-bottom flask containing

hexa(ethylbenzene) and the mixture was heated

under nitrogen until it became saturated with

nitrogen, and sodium was added. The ratio of

alkali to alkylbenzene was 0.15:1.0, and the

reaction mixture was stirred at 100° C. for 4.5

hr. (II), yielding 1.5 g. of product. The

yield in % melting point of 100° C. The

reaction mixture of 3 with 0.15 mole of potassium

hydroxide was proved by infrared analysis that the

Card 17

Reaction of hexylamine with 14

and 15 in acetonitrile at -78°C for 1 hr. at -78°C

with KHMDS (1.0M) and 1.0M LiClO<sub>4</sub>

in THF at -78°C for 1 hr. at -78°C

and 1.0M LiClO<sub>4</sub> in THF at -78°C for 1 hr.

Yield: 1.0 g (40%) of product

mp: 100°C (lit. mp: 100°C)

IR: 3330, 2950, 1650, 1500, 1450, 1350, 1250, 1150, 1050, 950, 850 cm<sup>-1</sup>

MS: m/z 210, 224, 238, 252, 266, 280, 294, 308, 322, 336, 350, 364, 378, 392, 406, 420, 434, 448, 462, 476, 490, 504, 518, 532, 546, 560, 574, 588, 602, 616, 630, 644, 658, 672, 686, 698, 712, 726, 740, 754, 768, 782, 796, 810, 824, 838, 852, 866, 880, 894, 908, 922, 936, 950, 964, 978, 992, 1006, 1020, 1034, 1048, 1062, 1076, 1090, 1104, 1118, 1132, 1146, 1160, 1174, 1188, 1202, 1216, 1230, 1244, 1258, 1272, 1286, 1290, 1304, 1318, 1332, 1346, 1360, 1374, 1388, 1402, 1416, 1430, 1444, 1458, 1472, 1486, 1490, 1504, 1518, 1532, 1546, 1560, 1574, 1588, 1592, 1606, 1620, 1634, 1648, 1662, 1676, 1690, 1704, 1718, 1732, 1746, 1760, 1774, 1788, 1792, 1806, 1820, 1834, 1848, 1862, 1876, 1890, 1904, 1918, 1932, 1946, 1960, 1974, 1988, 1992, 2006, 2020, 2034, 2048, 2062, 2076, 2090, 2104, 2118, 2132, 2146, 2160, 2174, 2188, 2192, 2206, 2220, 2234, 2248, 2262, 2276, 2290, 2304, 2318, 2332, 2346, 2360, 2374, 2388, 2392, 2406, 2420, 2434, 2448, 2462, 2476, 2490, 2504, 2518, 2532, 2546, 2560, 2574, 2588, 2592, 2606, 2620, 2634, 2648, 2662, 2676, 2690, 2704, 2718, 2732, 2746, 2760, 2774, 2788, 2792, 2806, 2820, 2834, 2848, 2862, 2876, 2890, 2904, 2918, 2932, 2946, 2960, 2974, 2988, 2992, 3006, 3020, 3034, 3048, 3062, 3076, 3090, 3104, 3118, 3132, 3146, 3160, 3174, 3188, 3192, 3206, 3220, 3234, 3248, 3262, 3276, 3290, 3304, 3318, 3332, 3346, 3360, 3374, 3388, 3392, 3406, 3420, 3434, 3448, 3462, 3476, 3490, 3504, 3518, 3532, 3546, 3560, 3574, 3588, 3592, 3606, 3620, 3634, 3648, 3662, 3676, 3690, 3704, 3718, 3732, 3746, 3760, 3774, 3788, 3792, 3806, 3820, 3834, 3848, 3862, 3876, 3890, 3904, 3918, 3932, 3946, 3960, 3974, 3988, 3992, 4006, 4020, 4034, 4048, 4062, 4076, 4090, 4104, 4118, 4132, 4146, 4160, 4174, 4188, 4192, 4206, 4220, 4234, 4248, 4262, 4276, 4290, 4304, 4318, 4332, 4346, 4360, 4374, 4388, 4392, 4406, 4420, 4434, 4448, 4462, 4476, 4490, 4504, 4518, 4532, 4546, 4560, 4574, 4588, 4592, 4606, 4620, 4634, 4648, 4662, 4676, 4690, 4704, 4718, 4732, 4746, 4760, 4774, 4788, 4792, 4806, 4820, 4834, 4848, 4862, 4876, 4890, 4904, 4918, 4932, 4946, 4960, 4974, 4988, 4992, 5006, 5020, 5034, 5048, 5062, 5076, 5090, 5104, 5118, 5132, 5146, 5160, 5174, 5188, 5192, 5206, 5220, 5234, 5248, 5262, 5276, 5290, 5304, 5318, 5332, 5346, 5360, 5374, 5388, 5392, 5406, 5420, 5434, 5448, 5462, 5476, 5490, 5504, 5518, 5532, 5546, 5560, 5574, 5588, 5592, 5606, 5620, 5634, 5648, 5662, 5676, 5690, 5704, 5718, 5732, 5746, 5760, 5774, 5788, 5792, 5806, 5820, 5834, 5848, 5862, 5876, 5890, 5904, 5918, 5932, 5946, 5960, 5974, 5988, 5992, 6006, 6020, 6034, 6048, 6062, 6076, 6090, 6104, 6118, 6132, 6146, 6160, 6174, 6188, 6192, 6206, 6220, 6234, 6248, 6262, 6276, 6290, 6304, 6318, 6332, 6346, 6360, 6374, 6388, 6392, 6406, 6420, 6434, 6448, 6462, 6476, 6490, 6504, 6518, 6532, 6546, 6560, 6574, 6588, 6592, 6606, 6620, 6634, 6648, 6662, 6676, 6690, 6704, 6718, 6732, 6746, 6760, 6774, 6788, 6792, 6806, 6820, 6834, 6848, 6862, 6876, 6890, 6904, 6918, 6932, 6946, 6960, 6974, 6988, 6992, 7006, 7020, 7034, 7048, 7062, 7076, 7090, 7104, 7118, 7132, 7146, 7160, 7174, 7188, 7192, 7206, 7220, 7234, 7248, 7262, 7276, 7290, 7304, 7318, 7332, 7346, 7360, 7374, 7388, 7392, 7406, 7420, 7434, 7448, 7462, 7476, 7490, 7504, 7518, 7532, 7546, 7560, 7574, 7588, 7592, 7606, 7620, 7634, 7648, 7662, 7676, 7690, 7704, 7718, 7732, 7746, 7760, 7774, 7788, 7792, 7806, 7820, 7834, 7848, 7862, 7876, 7890, 7904, 7918, 7932, 7946, 7960, 7974, 7988, 7992, 8006, 8020, 8034, 8048, 8062, 8076, 8090, 8104, 8118, 8132, 8146, 8160, 8174, 8188, 8192, 8206, 8220, 8234, 8248, 8262, 8276, 8290, 8304, 8318, 8332, 8346, 8360, 8374, 8388, 8392, 8406, 8420, 8434, 8448, 8462, 8476, 8490, 8504, 8518, 8532, 8546, 8560, 8574, 8588, 8592, 8606, 8620, 8634, 8648, 8662, 8676, 8690, 8704, 8718, 8732, 8746, 8760, 8774, 8788, 8792, 8806, 8820, 8834, 8848, 8862, 8876, 8890, 8904, 8918, 8932, 8946, 8960, 8974, 8988, 8992, 9006, 9020, 9034, 9048, 9062, 9076, 9090, 9104, 9118, 9132, 9146, 9160, 9174, 9188, 9192, 9206, 9220, 9234, 9248, 9262, 9276, 9290, 9304, 9318, 9332, 9346, 9360, 9374, 9388, 9392, 9406, 9420, 9434, 9448, 9462, 9476, 9490, 9504, 9518, 9532, 9546, 9560, 9574, 9588, 9592, 9606, 9620, 9634, 9648, 9662, 9676, 9690, 9704, 9718, 9732, 9746, 9760, 9774, 9788, 9792, 9806, 9820, 9834, 9848, 9862, 9876, 9890, 9904, 9918, 9932, 9946, 9960, 9974, 9988, 9992, 10006, 10020, 10034, 10048, 10062, 10076, 10090, 10104, 10118, 10132, 10146, 10160, 10174, 10188, 10192, 10206, 10220, 10234, 10248, 10262, 10276, 10290, 10304, 10318, 10332, 10346, 10360, 10374, 10388, 10392, 10406, 10420, 10434, 10448, 10462, 10476, 10490, 10504, 10518, 10532, 10546, 10560, 10574, 10588, 10592, 10606, 10620, 10634, 10648, 10662, 10676, 10690, 10704, 10718, 10732, 10746, 10760, 10774, 10788, 10792, 10806, 10820, 10834, 10848, 10862, 10876, 10890, 10904, 10918, 10932, 10946, 10960, 10974, 10988, 10992, 11006, 11020, 11034, 11048, 11062, 11076, 11090, 11104, 11118, 11132, 11146, 11160, 11174, 11188, 11192, 11206, 11220, 11234, 11248, 11262, 11276, 11290, 11304, 11318, 11332, 11346, 11360, 11374, 11388, 11392, 11406, 11420, 11434, 11448, 11462, 11476, 11490, 11504, 11518, 11532, 11546, 11560, 11574, 11588, 11592, 11606, 11620, 11634, 11648, 11662, 11676, 11690, 11704, 11718, 11732, 11746, 11760, 11774, 11788, 11792, 11806, 11820, 11834, 11848, 11862, 11876, 11890, 11904, 11918, 11932, 11946, 11960, 11974, 11988, 11992, 12006, 12020, 12034, 12048, 12062, 12076, 12090, 12104, 12118, 12132, 12146, 12160, 12174, 12188, 12192, 12206, 12220, 12234, 12248, 12262, 12276, 12290, 12304, 12318, 12332, 12346, 12360, 12374, 12388, 12392, 12406, 12420, 12434, 12448, 12462, 12476, 12490, 12504, 12518, 12532, 12546, 12560, 12574, 12588, 12592, 12606, 12620, 12634, 12648, 12662, 12676, 12690, 12704, 12718, 12732, 12746, 12760, 12774, 12788, 12792, 12806, 12820, 12834, 12848, 12862, 12876, 12890, 12904, 12918, 12932, 12946, 12960, 12974, 12988, 12992, 13006, 13020, 13034, 13048, 13062, 13076, 13090, 13104, 13118, 13132, 13146, 13160, 13174, 13188, 13192, 13206, 13220, 13234, 13248, 13262, 13276, 13290, 13304, 13318, 13332, 13346, 13360, 13374, 13388, 13392, 13406, 13420, 13434, 13448, 13462, 13476, 13490, 13504, 13518, 13532, 13546, 13560, 13574, 13588, 13592, 13606, 13620, 13634, 13648, 13662, 13676, 13690, 13704, 13718, 13732, 13746, 13760, 13774, 13788, 13792, 13806, 13820, 13834, 13848, 13862, 13876, 13890, 13904, 13918, 13932, 13946, 13960, 13974, 13988, 13992, 14006, 14020, 14034, 14048, 14062, 14076, 14090, 14104, 14118, 14132, 14146, 14160, 14174, 14188, 14192, 14206, 14220, 14234, 14248, 14262, 14276, 14290, 14304, 14318, 14332, 14346, 14360, 14374, 14388, 14392, 14406, 14420, 14434, 14448, 14462, 14476, 14490, 14504, 14518, 14532, 14546, 14560, 14574, 14588, 14592, 14606, 14620, 14634, 14648, 14662, 14676, 14690, 14704, 14718, 14732, 14746, 14760, 14774, 14788, 14792, 14806, 14820, 14834, 14848, 14862, 14876, 14890, 14904, 14918, 14932, 14946, 14960, 14974, 14988, 14992, 15006, 15020, 15034, 15048, 15062, 15076, 15090, 15104, 15118, 15132, 15146, 15160, 15174, 15188, 15192, 15206, 15220, 15234, 15248, 15262, 15276, 15290, 15304, 15318, 15332, 15346, 15360, 15374, 15388, 15392, 15406, 15420, 15434, 15448, 15462, 15476, 15490, 15504, 15518, 15532, 15546, 15560, 15574, 15588, 15592, 15606, 15620, 15634, 15648, 15662, 15676, 15690, 15704, 15718, 15732, 15746, 15760, 15774, 15788, 15792, 15806, 15820, 15834, 15848, 15862, 15876, 15890, 15904, 15918, 15932, 15946, 15960, 15974, 15988, 15992, 16006, 16020, 16034, 16048, 16062, 16076, 16090, 16104, 16118, 16132, 16146, 16160, 16174, 16188, 16192, 16206, 16220, 16234, 16248, 16262, 16276, 16290, 16304, 16318, 16332, 16346, 16360, 16374, 16388, 16392, 16406, 16420, 16434, 16448, 16462, 16476, 16490, 16504, 16518, 16532, 16546, 16560, 16574, 16588, 16592, 16606, 16620, 16634, 16648, 16662, 16676, 16690, 16704, 16718, 16732, 16746, 16760, 16774, 16788, 16792, 16806, 16820, 16834, 16848, 16862, 16876, 16890, 16904, 16918, 16932, 16946, 16960, 16974, 16988, 16992, 17006, 17020, 17034, 17048, 17062, 17076, 17090, 17104, 17118, 17132, 17146, 17160, 17174, 17188, 17192, 17206, 17220, 17234, 17248, 17262, 17276, 17290, 17304, 17318, 17332, 17346, 17360, 17374, 17388, 17392, 17406, 17420, 17434, 17448, 17462, 17476, 17490, 17504, 17518, 17532, 17546, 17560, 17574, 17588, 17592, 17606, 17620, 17634, 17648, 17662, 17676, 17690, 17704, 17718, 17732, 17746, 17760, 17774, 17788, 17792, 17806, 17820, 17834, 17848, 17862, 17876, 17890, 17904, 17918, 17932, 17946, 17960, 17974, 17988, 17992, 18006, 18020, 18034, 18048, 18062, 18076, 18090, 18104, 18118, 18132, 18146, 18160, 18174, 18188, 18192, 18206, 18220, 18234, 18248, 18262, 18276, 18290, 18304, 18318, 18332, 18346, 18360, 18374, 18388, 18392, 18406, 18420, 18434, 18448, 18462, 18476, 18490, 18504, 18518, 18532, 18546, 18560, 18574, 18588, 18592, 18606, 18620, 18634, 18648, 18662, 18676, 18690, 18704, 18718, 18732, 18746, 18760, 18774, 18788, 18792, 18806, 18820, 18834, 18848, 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PINCHUK, N.P., gornyy inzr.

Using igdanite at Balaklava flux limestone quarries. Vzryv.  
delo no.54/11:322-325 '64. (MIRA 17:9)

1. Balaklavskoye rudoupravleniye imeni A.M. Gor'kogo.

KOVALENKO, I. ., kand.med.nauk; PINCHUK, N.V. (Dnepropetrovsk)

Public help in the work of a hospital. Sov.zdrav. 21 no.7:2C-2. '6..  
(MFA 14:8)

1. Iz 4-y gorodskoy bol'nitsy (glavnyy ~~vveden~~ Ye.N.Fedotov)  
Dnepropetrovsk.  
(DNEPROPETROVSK—HOSPITALS)

KOVALENKO, I.V., kandidat meditsinskikh nauk; PINCHUK, N.V.

Studying the morbidity of the population according to data on the number of visits. Sov. zdrav. 15 no.4:31-35 Jl-Ag '56. (MLRA 9:9)

1. Iz kafedry organizatsii zdravookhraneniya (zav. - prof. B.M. Shklyar) Dnepropetrovskogo meditsinskogo instituta (dir. - dotsent D.P.Chukhriyenko)

(VITAL STATISTICS.  
morbidity calculation (Bus))

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CIA-RDP86-00513R001340910017-5

IMCHUK, C. I.

IMCHUK, C. I. - "BRIEFING ON THE SITUATION IN KOREA" - 20. 1. 1951  
"SITUATION" - 20. 1. 1951

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CIA-RDP86-00513R001340910017-5"

Determination of butyl and higher alcohols in the condensates and butyl fractions by settling out with calcium chloride. V. G. Shaposhnikov and S. I. Puchuk  
Izdatel'stvo Akademii Nauk SSSR, Moscow, 1956.  
B-111 Synthetic Rubber (1956). One hundred  
of the sample units at least 100 ml. Butyl is dried through a  
four-fold dephlegmator. A light fractionate is present.  
The remaining liquid which is composed of Butyl and  
higher alcohols is measured and 4 cc pipetted off and added  
out with 20 cc of  $\text{CaCl}_2$  solution ( $\text{Mg} = 1$  mol) which was  
preliminarily acidified with Butyl. The separation is carried  
out in a glass stoppered bottle. The upper layer contains  
Butyl, higher alcohols and some hydrocarbons. The lower  
are dried by adding excess of  $\text{HgCl}_2$  and reading the weight  
hydrocarbon layers, which must be subtracted from the  
total alkohol and ether layer to obtain the amount of alcohols.  
A. A. Borodulin

UDC 547.55

AUTHORS: Raduyev, G.A., Vjazkikh, G.V., and V. V. Kostylev

TITLE: The Reaction Between n-Alkylbenzene Derivatives and Triethylstannane

PUBLISHER: Izd. Akad. Nauk SSSR po Khimii i Mekhanicheskym Naukam  
Vedenskaya Akademiya Nauk SSSR

TEXT: The authors have investigated the reaction of triethylstannane with certain organic halide derivatives at elevated temperatures. It has been shown in this article for the first time that it is the halogen, bound to the benzene ring, that particularly facilitates the reaction of triethylstannane, when heated to 150°C, with alkyl iodides. In this case, it was found that the rate of reaction increases with increasing temperature of the alkyl derivative. In the next stage, triethylstannane reacts with the iodide formed with triphenylmethyl bromomethane (4 hrs at 150°C) or with phosphorus pentachloride (1 hr at 150°C). In the first case the yield of triethylstannane is 60% and in the second case 70%. The formation of triethylstannane is due to the formation of triphenylmethyl radicals. The presence of the latter was proven by electronic paramagnetic resonance methods.

Card 1/4

T-77

The Reaction between hexaethoxybenzene and triethylbenzyltin chloride (30.9%) and n-tolyltriethylstannylchloride were prepared from the respective chlorides and n-toluenesulfonfchloride. Yield of the second was 77% melt-crystallized in alcohol. The structure of the silicon has been verified by infrared analysis carried out in a medium of anisole at about 150°C. The yield of the product of 44.2% of the theoretical:

$$n\text{-CH}_3\text{C}_6\text{H}_4\text{Si}(\text{Cl})_2\text{SnI}_3 + (\text{C}_2\text{H}_5)_3\text{SiLi} \longrightarrow \text{H}_3\text{Si}(\text{C}_2\text{H}_5)_3\text{SnLi} + \text{C}_6\text{H}_4\text{Si}(\text{Cl})_2\text{SnI}_3$$

Under more severe conditions it occurs at 120°C in the hexaethoxybenzene which reacts with the benzene chloride. This reaction of hexaethoxybenzene with the addition to the triethylbenzyltin chloride yields 70% of the product. After separation of the main product there is found 10% of a by-product with a homologous separation of the main product starting with 100°C. In this type of decomposition of the tin chloride starts first the formation of the reaction with  $\beta$ -bromobenzylbenzene, 1,4-dibromobutane and 1,4-dibromobutene also, taking place at 120°C. In addition to the main product there is found 10% of the addition to the main product of triethylbenzyltin chloride and 10% of the product of 1,4-dibromobutene and 1,4-dibromobutene. The yield of the product of the same two species also: 10%  $\text{C}_6\text{H}_4\text{Si}(\text{Cl})_2\text{SnI}_3 + (\text{C}_2\text{H}_5)_3\text{SiLi} \longrightarrow \text{H}_3\text{Si}(\text{C}_2\text{H}_5)_3\text{SnLi} + \text{C}_6\text{H}_4\text{Si}(\text{Cl})_2\text{SnI}_3$ . It is assumed that reaction is catalyzed by triethylbenzyltin chloride.

Card 2/4

6557  
167/60/500, P-6/10/74  
A-1/2/74

The Reaction Between Hexaethylstannane and Triethylstannane. In the previous reactions discussed here, based on previously made assumptions (not by the author), that reaction (2) is a catalytic one, i.e., as the disproportionation of the hexaethylplumbane is (Ref 1-3) the author). This assumption was confirmed by the thermostatic action of the mixture hexaethylstannane and triethylstannous chloride, at 200-210°C (1. hours molar ratio). It is assumed (2) takes place more energetically in the presence of 3 moles of dichloroethylstannate and 2 moles of hexaethyldistannane (for a period of 1. hour at 200°C). The formed tetraethylstannate reacts with the dichloroethylstannous chloride,  $[(C_2H_5)_2Sn]_2Cl_2 \rightarrow SnCl_2 + Sn$ . (3). It is stressed that equation (3) describes only the final result. The reaction mechanism is thought to be complex from the following indications: during the reaction intensive wine-colored, presumably hexamolecular compounds are formed, decomposing toward the end of the process. Stannous chloride is thought to play an important role in equation (3). It is usually identified when conducting the disproportionation in an excess of dichloroethylstannate. It was established that the  $SnCl_2$  can cause change not only in the hexaethyldistannane, but also in the more stable tetraethylstannane.

Card 3/4

*Recess*3/10/65/RC/1001340910017-5  
ACB/AE26

### The Reaction Between Hexaethylstannane and Organic Halide Derivatives

derivatives of the tin. The following reaction is given as an example of the thermostatic action of equimolar quantities of tetraethylstannate and SnCl<sub>2</sub> (for 10 hours at 230°C):  $2(C_2H_5)_4Sn + 2SnCl_2 \rightarrow (C_2H_5)_3SnCl + C_2H_5Cl + Sn$ . (4) also taking place with the formation of dark-red colored intermediary compounds. Another fact proving the complexity of the reaction is given as being the fact that catalytic quantities of  $(C_2H_5)_3SnCl$  and  $C_2H_5Cl$   $SnCl_2$  (2% of the weight of hexaethylstannane) do not bring about the complete conversion according to equation (4). It is pointed out that the interaction of the hexaethylidiplumbane with an excess of triethyl lead chloride triethyl stannous chloride or dichlorodietylstannate takes place quite differently. In this case the disproportionation reaction is completely suppressed by the complex oxidation-reduction process. In conclusion the authors state that investigations are still being continued in this field. There are no other references.

ASSOCIATION Gor'skiy gosudarstvenny universitet im N.I. Lobačevskogo  
(The Gor'kiy State University im N.I. Lobačevskogo)

Card 4/4

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PINCHUK, N.S.

Conference of veterinary specialists. Veterinaria 3<sup>rd</sup> no.1.  
81 D '90.  
'Kokchetav Province—Veterinary medicine—Congresses)  
(MIRA 1<sup>st</sup>:4)

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CIA-RDP86-00513R001340910017-5"

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Report no. 1. Organization of the State Control over the issue of native and feed antibiotics.

Report no. 2. About the order of reports on the basis of the statements of the National Insurance concerning losses of insured animals.

Veterinariya, Vol. 37, No. 12, p. 71, 80, 81, 1964.

PINCHUK, O.I.

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132-157 '57.  
(Coal geology) (MIRA 11:5)

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(MIRA 18:9)

I. Dnepropetrovskiy gornyy institut imeni Artyoma.

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PINCHUK, P.

Accumulation and use of the undivided fund of collective farms.  
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1.Zaveduyushchiy Voroshilovskim rayfinotdelom Minaska.  
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