

PODZERKO, V.A.

Further development of technological innovations. Bezop.truda
v prom. 5 no.10:5-6 0 '61. (MIRA 14:10)

1. Predsedatel' Tsentral'nogo komiteta profsoyuza rabochikh
metallurgicheskoy promyshlennosti.
(Metallurgical plants--Technological innovations)

PODZERKO, V.A.

In the land of constant sunshine Metallurg 6 no.4:37-38
Ap '61. (MIRA 14:3)

1. Predsedatel' Tsentral'nogo komiteta profsoyuza rabochikh
metallurgicheskoy promyshlennosti.
(Chile---Description and travel)

PODZERKO, V.A.

Resolutions of the party put into practice. Metallurg ? no.1:
1-2 Ja '62. (MIRA 15:1)

1. Predsedatel' Tsentral'nogo komiteta profsoyuza rabochikh
metallurgicheskoy promyshlennosti.
(Metallurgical plants)

EGDZERSKIY, S.

Cotton Growing

Basic problems of method in the growing of cotton seeds on unirrigated lands.
Khlopkovodstvo no. 11, 1951

Monthly List of Russian Accessions, Library of Congress, August 1952. UNCLASSIFIED

AUTHOR: Podzey, A.G., Loginov, V.E., and Novikov, N.N.

TITLE: Attaching Thermocouple Electrodes in the
Investigating Temperature Fields in Solids.
(Krepleniye elektrodov termopar pri issledovanii
temperaturnogo polya.)

PERIODICAL: Stanki i Instrument, 1957, No. 1. pp.33-34 (U.S.S.R.).

ABSTRACT: The attachment of fine electrodes to bulky components is best accomplished by welding. A butt welding process using a condenser discharge is described. A set of electrolytic condensers of 30 mcf each are charged with a 6.3 kw and 120 V d.c. generator. The total capacity is 3000 mcf. After adjusting the required capacity the electrodes are brought together by hand. Grinding the electrode faces improves the connection joint. A numerical table summarizes the recommended capacity and voltage for each combination of electrode and specimen material.

ASSOCIATION:
Card 1/2

Podzey, A.V.

AID P - 5191

Subject : USSR/Engineering
Card 1/1 Pub. 103 - 13/24
Authors : Loginov, V. Ye., and A. V. Podzey
Title : Adjustment of the amplifier for measuring deformation of loaded mechanisms.
Periodical : Stan. i instr., 7, 36-37, J1 1956
Abstract : The method of adjustment is described and illustrated. Two drawings and 1 graph.
Institution : None
Submitted : No date

PODZEV, A.V., kandidat tekhnicheskikh nauk; YAKIMOV, A.V., inzhener.

Dynamics of gear grinding and its effect on precision in machining gear wheels. Trudy MAI no.70:44-56 '56. (MLBA 9:12)
(Gear cutting)

PODZEY, Anatoliy Vladimirovich; SULIMA, Andrey Mikhaylovich; FIRAGD,
Valentin Petrovich; TSUKANOV, Ivan Semenovich; KUINDZHI, A.A.,
inzhener, retsenzent; STANKEVICH, V.G., inzhener, redaktor;
BELITSKAYA, A.M., redaktor; SHCHERBAKOV, P.V., tekhnicheskiiy redaktor

[Technology of building aviation engines; the processing of
principal parts and units] Tekhnologiya aviadvigatelsestroeniia;
obrabotka osnovnykh detalei i uzlov. Pod red. A.V. Podzeia. Moskva,
Gos. izd-vo obor. promyshl., 1957. 415 p. (MLRA 10:5)
(Airplanes--Engines)

PODZEY, A.V.

AUTHOR: PODZEY, A.V., NOVIKOV, N.N., LOGINOV, V.Ye. 121-8-11/22
TITLE: The Determination of Heat Emitted to the Work Piece During Surface Grinding. (Opredeleniye tepla, vydelyayemogo v detal' pri ploskom shlifovanii.)
PERIODICAL: Stanki i Instrument, 1957, Vol. 28, Nr 8, pp.33-34 (USSR)
ABSTRACT: The emission of heat from the grinding zone to the work piece depends on the thermo-physical parameters of the material: it is more intense in the case of high heat conductivity than in the case of low heat conductivity. In the first case this gives rise to inaccurate measuring and the shape of the worked surface, and in the second case it causes considerable temperature stress and structural changes of the surface layer. For the purpose of the exploration of internal stress and internal heat deformations the determination of the thermal field in the work piece is necessary which, at present, can only be brought about by means of the calorimetric method. Illustrations show such a calorimetric apparatus, which is described in detail and explained; formulae for the calculation of the work-piece are also given. The results of calorimetric experiments are given in a table, and another table shows the quantity of heat emitted to the work piece on the occasion of the grinding-off of 1 mm³ of metal and for various grinding depths.

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The Determination of Heat Emitted to the Work Piece
During Surface Grinding. 121-8-11/22

ASSOCIATION: Not given
PRESENTED BY:
SUBMITTED:
AVAILABLE: Library of Congress

Card 2/2

POVZE Y, A.V.

PODZEY, A.V.; NOVIKOV, N.N.; LOGINOV, V.Ye.

Temperature field in metals subjected to surface grinding. Stan. i
instr. 28 no.10:16-17 0 '57. (MIRA 10:11)
(Grinding and polishing) (Heat transmission)

PODZEY, A.V.; LOGINOV, V.Ye.; NOVIKOV, N.N.

Measuring residual stresses by strain gauges. Stan.i instr. 29
no.6:25-27 Je '58. (MIRA 11:7)
(Strain gauges) (Strains and stresses--Measurement)

PODZEY, A.V.; SEREBRENNIKOV, G.Z.

Determining residual stresses in shafts subjected to sudden
cooling. Stan.1 instr. 29 no.12:18-20 D '58. (MIRA 11:12)
(Thermal stresses) (Shafting)

PODZNY, A.V.; SEREBRENNIKOV, G.Z.

Calculating residual thermal stresses in plain shafts. Nauch.
dokl.vys.shkoly; mash. i prib. no.1:171-181 '59.

(MIRA 12:8)

1. Stat'ya predstavlena kafedroy "Proizvodstvo aviadvigateley"
Moskovskogo aviatsionnogo instituta.
(Thermal stresses)

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S/121/59/000/11/004/005

AUTHOR: Podzey, A.V.

TITLE: Investigating Residual Stresses During Grinding Operations by Way of Thermal Simulation

PERIODICAL: Stanki i Instrument, 1959, No 11, pp 39 - 40

TEXT: The author describes tests which were carried out in order to investigate the formation of residual stresses during grinding operations. The tests were carried out by way of thermal simulation, with the aid of HF-current heating, of the temperature field existing during the grinding process. Formerly it was established [Ref 1] that the temperature field of an article ground without cooling can be expressed by the N.N. Rykalin equation like this:

$$T(y, \tau) = \frac{q}{\sqrt{\pi c \lambda \tau}} e^{\left(\frac{-y^2}{4a \tau}\right)}, \text{ where } T(y, \tau) \text{ is the}$$

temperature at the point of the article with the coordinate y at the moment τ in $^{\circ}\text{C}$; q is the intensity of the heating source in cal/cm^2 ; a is the

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Investigating Residual Stresses During Grinding Operations by Way of Thermal Simulation

coefficient of temperature conductivity of the machined part in cm^2/sec ;
 λ is the coefficient of heat conductivity in $\text{cal}/\text{cm}\cdot\text{sec}\cdot\text{degrees}$; c is the coefficient of thermal capacity in $\text{cal}/\text{g}\cdot\text{degree}$; γ is the specific gravity in g/cm^3 . Based on the data given in the article by A.V. Podzey, N.N. Novikov, V.Ye. Loginov, in the periodical "Stanki i Instrument", No 10, 1957, Figure 6, this equation can be used for the analytical calculation of temperature fields in the ground metal, consequently it can also be applied in the case of thermal simulation. The author states the equation for the magnitude of q for circular external grinding operations, the total amount of heat Q and the component of the cutting force P_z , found on the basis of the formula of Professor Ye.N. Maslov [Ref 4]. He refers to Ref 5 where data on the distribution of heat between the article Q_a , the disk Q_d and the chip Q_{ch} are given, and gives a derivation of the Isayev and Silin Formula [Ref 5] in order to determine the coefficient k . The thermal simulation of the grinding process was effected on an installation of 60kW with a frequency of 250 kc, with ring-shaped specimens and with the

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Investigating Residual Stresses During Grinding Operations by Way of Thermal Simulation

aid of a standard cylindrical inductor. The specimen dimensions were selected as a result of extensive tests and had the following magnitude: $D_{ext} = 85$ mm, $d_{int} = 65$ mm, wall thickness $h = 3 \div 5$ mm. Figure 1 shows the heating device. The temperature variations in the course of time were recorded by a MPO-2 oscillograph. Figure 2 shows the curves of temperature variations during the grinding process and for the HF-current heating of 38KhA grade steel. Moreover, tests were carried out to obtain the curves of temperature variations for the grinding with sodium carbonate water cooling and for repeated cutting operations. An X-ray analysis of the specimen surface after grinding and HF-current heating did not reveal any recrystallization phenomena. In all the cases mentioned, the determination of residual stresses was effected in the surface layer of the metal according to the N.N. Davidenkov method [Refs 8 and 9]. The results of these tests are shown in Figure 3. Figure 4 shows the results of measurements which were carried out in order to study the causes of hardness variations of the surface layer after grinding operations. The author draws the following conclusions: 1) A thermal simulation of a cutting process ✓

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Investigating Residual Stresses During Grinding Operations by Way of Thermal Simulation

can be effected by way of HF-current heating of the metal. 2) The temperature field during the HF-current heating and during the cutting process can be satisfactorily described by an equation for a single thermic cycle. 3) The curves of residual stresses after grinding and after HF-current heating show a fully satisfactory coincidence. This proves that the basic factor in the origination of residual stresses during the grinding of steel is the localized heating.

Four graphs, 9 Soviet references.

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PODZEY, A.V.; LOGINOV, V.Ye; NOVIKOV, N.N.

Measuring cutting forces with strain gauges. Stan.1 instr. 30 no.3:
24-25 Mr '59. (MIRA 12:3)
(Strain gauges) (Metal cutting)

PODZEY, A.V.; LOGINOV, V.Ye.; NOVIKOV, N.N.

Calibration device for strain gauges. Stan.1 instr. 30 no.4:24
Ap '59. (MIRA 12:6)
(Strain gauges) (Calibration)

KISHKIN, S. T., doktor tekhn.nauk; PODZBY, A. V., kand.tekhn.nauk;
KARYAKINA, N. V., kand.tekhn.nauk, NIKOLENKO, V. V., kand.tekhn.
nauk, LOGINOV, V. Ye., inzh., GRIBOVSKI, L., inzh.

Investigating the quality of the surface layer on ramjet, gas-
turbine blades. Trudy MAI no.123:76-89 '60. (MIRA 13:8)

(Airplanes--Ramjet engines)

(Gas turbines--Blades)

(Surface hardening)

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25964

S/535/60/000/129/002/006

EO32/E514

AUTHOR: Podzey, A. V., Candidate of Technical Sciences

TITLE: Determination of the temperature field in components during grinding

PERIODICAL: Moscow. Aviatsionnyy institut. Trudy, No.129, 1960. Issledovaniye fizikomekhanicheskikh i ekspluatatsionnykh svoystv detaley posle obrabotki, pp.42-55

TEXT: In previous papers (Ref.1: Stanki i instrument, 1959, No.11; Ref.2: Izvestiya vysshikh uchebnykh zavedeniy, Mashinostroyeniye, 1959, No.8) the author showed that localised heating during grinding is largely responsible for residual stresses in components. It follows that if the temperature distribution in the material is known, one can calculate the stresses and hence select working conditions which would minimise these stresses. The experimental determination of the temperature field is an exceedingly difficult problem and hence analytical methods are of major interest. Work carried out at the Moskovskiy aviatsionnyy institut (Moscow Aviation Institute) by I. A. Morozov (Ref.3: Trudy MAI, No.70, Oborongiz, 1956), A. I. Isayev and S. S. Silin (Ref.4: Card 1/6

Determination of the temperature ...

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E032/E514

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Vestnik mashinostroyeniya, 1957, No.5) and others has led to a method for calculating the temperature fields in semi-infinite bodies not subjected to cooling. However, in practice it is frequently necessary to deal with thin walled components using lubricating-cooling fluids. From a practical point of view the following three cases are of particular importance: 1) temperature field in thick walled components not subjected to cooling during grinding; 2) temperature field in thick walled components subjected to cooling during grinding; 3) temperature field in thin walled components subjected to cooling, including effects associated with the periodic repetition of the thermal cycles. The present author describes a method whereby these calculations can be carried out. The solutions obtained have been checked experimentally. It is known that the temperature field produced during grinding of thick walled components not subjected to cooling can be described by

$$T(y, \tau) = \frac{q}{\sqrt{\pi \lambda c \gamma \tau}} \exp \left(- \frac{y^2}{4a\tau} \right) \quad (1)$$

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where T - temperature at the point whose coordinate is y ,
 τ - time,
 q - intensity of the heat source,
 λ - conductivity,
 c - specific heat,
 γ - specific weight,
 $a = \lambda/c\gamma$ - the temperature diffusivity.

This expression was derived by N. N. Novikov (p.5 of the present issue), N. N. Rykalin (Ref.6: Calculation of Thermal Processes Occurring During Welding, Mashgiz, 1951) and the present author et al. (Ref.5: Stanki i instrument, 1957, No.10). This formula holds for a semi-infinite body heated by a fast moving linear heat source. Experimental results showed that this equation holds for components thicker than 5-6 mm. A. V. Lykov (Ref.8: "Heat transfer theory", Gostekhizdat, 1952) has shown that the temperature distribution in the case of a semi-infinite body, subjected to cooling at the same surface at which the instantaneous heat source acts, is given by

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$$T(y, \tau) = \frac{b}{\sqrt{\pi}} \left\{ \frac{1}{\sqrt{a\tau}} \exp\left(-\frac{y^2}{4a\tau}\right) - \sqrt{\pi} \frac{\alpha}{\lambda} \exp\left[\frac{\alpha}{\lambda} y + a\tau \left(\frac{\alpha}{\lambda}\right)^2\right] \operatorname{erfc}\left(\frac{y}{2\sqrt{a\tau}} + \frac{\alpha}{\lambda} \sqrt{a\tau}\right) \right\}$$

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where $b = q/c\gamma$, α is the emissivity and $\operatorname{erfc}(u) = 1 - \operatorname{erf} u$. As in the previous case, the quantity q can be determined calorimetrically or by calculation. Finally, in the case of a thin walled component subjected to cooling (thickness less than 5 mm), the solution cannot be found in a closed form and must be expressed as a series. The problem can be reduced to the solution of the Fourier heat transfer equation

$$\frac{\partial T}{\partial \tau} = a \nabla^2 T$$

subject to the following initial and boundary conditions:

1) $\tau = 0, T = 0$; 2) $y = 0, \partial T / \partial y - \alpha T / \lambda = 0$ and 3) $y = \delta, \partial T / \partial y = 0$ (adiabatic boundary). The general solution has been obtained by A. V. Lykov (Ref.8) and is of the form

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$$T_{l,n} = \frac{2b}{l} \sum_{n=1}^{\infty} \frac{\mu_n}{\mu_n + \sin \mu_n \cos \mu_n} \cdot \cos \mu_n \cos\left(\mu_n \frac{l-y}{l}\right) \exp\left(-\mu_n^2 \frac{ax}{l^2}\right).$$

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where

$$b = \frac{q}{c\gamma}, \quad \frac{b}{a} = \frac{q}{\lambda}, \quad \mu_n = f(Bi, n), \quad Bi = \frac{al}{\lambda}.$$

$$\mu_n = Bi \operatorname{ctg} \mu_n$$

It was found that the experimental results can be made to agree with the calculations to within 15-20%. Fig. 8 shows the residual stresses, σ (kg/mm²) in the surface layer of a ground component (ЭИ437А (EI437A)) as a function of depth, h (μ). Curve 1 was obtained without cooling, curve 2 with ordinary cooling and curve 3 with a cooling jet. It follows from these curves that it is essential to apply cooling in order to reduce the depth of penetration of high residual stresses during the grinding process. The more intensive the cooling the smaller the penetration.

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25968

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E073/E535

AUTHOR: Podzey, A.V., Candidate of Technical Sciences

TITLE: Investigation of the residual stresses in components subjected to grinding

PERIODICAL: Moscow. Aviatsionnyy institut. Trudy. No.129, 1960. Issledovaniye fizikomekhanicheskikh i ekspluatatsionnykh svoystv detaley posle obrabotki, pp.112-141

TEXT: Experimental investigation alone does not permit full study of the process of generation of residual stresses and elucidating the value of one or another of the machining parameters. Analytical investigation requires studying the mechanism of formation of residual stresses. L. A. Glikman et al. (Ref.1: Doctor Dissertation, LPI im. Kalinina, 1947; Ref.2: Zhurnal tekhnicheskoy fiziki, Vol.19, No.4, 1949) believe that the predominating factor in the formation of grinding stresses is the thermal process of cutting, i.e., that the stresses arise as a result of localized heating of the surface being machined. The author of this paper fully agrees with this view. However, for analytical investigation it is first necessary to confirm this

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hypothesis and to study the thermal phenomena in the component during the process of grinding. In the first instance it was necessary to solve the problem of the temperature fields which would permit thermal simulation of the process of grinding and then, if the results of this thermal simulation are positive, it is necessary to analyse the stress state. In other work of the author it was shown that, with certain assumptions, the temperature field during grinding without cooling can be described for the case of thin walled components by means of

$$T(y, \tau) = \frac{q}{\sqrt{\pi \lambda c \gamma \tau}} \exp \left[-\frac{y^2}{4a\tau} \right] \quad (1)$$

- where $T(y, \tau)$ - temperature of a point of the component at a depth y at the instant τ ;
- q - intensity of the thermal source, cal/cm^2 ;
 - λ - coefficient of thermal conductivity, $\text{cal/cm}\cdot\text{sec}$;
 - c - specific heat, $\text{cal/g}\cdot\text{deg}$;
 - γ - specific gravity, g/cm^3 ;
 - a - coefficient of thermal diffusivity, $\lambda/c\gamma, \text{cm}^2\text{sec}$.

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This equation was derived by Corresponding Member AS USSR N. N. Rykalin (Ref.5: "Calculation of thermal processes during welding", Mashgiz, 1951). Experimental results published by N. N. Novikov (p.5 of this issue) have shown that the intensity of the heat source during grinding decreases with increasing speed of the component, decreasing depth of cut t and by using oil emulsions and oil as cutting fluids and also by applying soft grinding wheels. The thermal simulation of grinding was by means of high frequency heating and was based on the following idea: if the temperature fields in the ground component and the analogue, heated by high frequency currents, are equal and the epures of the distribution of the residual stresses in these coincide, this can be taken as a valid conclusion that the thermal factor is the dominant one. Numerous experiments carried out with high frequency equipment provided confirmation of this hypothesis and thus enabled elucidating the mechanism of the stress formation. Before carrying out the analysis, the authors were interested to elucidate the difference in the distribution of the residual stresses during grinding and during vibro-contact polishing, still assuming that

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the influence of heat is predominant. During grinding, the temperature gradients are very high and at the surface the temperature approaches the melting point, whilst at a depth of 0.5 to 1 mm it is near to the initial temperature of the component. In polishing, the temperature in the surface layer is not high. First, a qualitative assessment is made of the conditions pertaining to grinding and polishing. Then it is stated that the quantitative aspects of the problem can be elucidated by analytical solution, which can be reduced to determining the thermal stresses on the basis of the real temperature field in the body of the component. The author considers only type I stresses, which equalize in area commensurate with the size of the component. Types II and III stresses and also stresses associated with structural phase transformations are not considered. It is pointed out that the stress state is also affected by the way in which the component is clamped (chucked) during machining. Only two cases are considered, which differ in the way the forces are applied, Figs. 2 and 3. These conditions are extremal of the multitude of conditions encountered in practical work. In addition,
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during analytical solution of the problem, the stress state after machining but before taking the component out of the chuck is considered. In all the solutions considered, it is assumed that the temperature distribution obeys Eq.(1), i.e. the conditions which are valid for a semi-infinite body without intensive heat removal. This enabled simplifying the problem, which is permissible, since the study is limited to analysing the stress state and no attempt is made to present an accurate method of calculation. A concrete problem is considered using basic relations originally published by A. A. Il'yushin in his book "Plasticity", Gostekhizdat, 1948. The problem is formulated as follows: plates of a thickness d are ground on their free surface. Initially, the plate and the clamping device have the same temperature. During the entire process of grinding the plate is prevented from bending. The effect of the grinding wheel is approximated by the effect of an instantaneous source of heat which is equally distributed along the free surface. The thermal properties of the component and of the clamping device will be assumed as being equal and not depending on the temperature. The temperature is reckoned from

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the initial temperature and its distribution as a function of time obeys Eq.(1). On the basis of these assumptions, the free thermal expansion of each layer and the thermoplastic strain are calculated. Depending on the conditions of clamping the component, two cases are distinguished - 1) during heating the component cannot expand in the x and z directions, Fig.2; 2) the deformation of the component being ground is in no way constrained, Fig.3. The author also investigates the conditions pertaining at the edges of thin walled components (for instance, turbine and compressor blades) by analysing the stress conditions during grinding in thin plates of a shape as shown in Fig.16. The analytically arrived at results are compared with experimental data published in an earlier paper of the author and his team (Ref.4: Stanki i instrument, No.8, 1957) and it is stated that the calculated results are in good agreement with the experimental ones. The following conclusions are arrived at:

1. The magnitude and depth of propagation of the residual stresses are directly proportional to the intensity of the heat source q , the coefficient of linear expansion α_p , the modulus of elasticity

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E, and is inversely proportional to the specific heat γ and the yield point $\sigma_{0.2}$ of the material. The technologist can only influence the value of q , which depends on the grinding conditions.

2. The level of the residual stresses can be reduced if grinding is effected at high speeds of the component, applying smaller depths of cut t and using lubricating and cooling cutting fluids which permit better heat removal and reduce friction. Better results could be obtained by using softer grinding wheels with 60 to 80 grain size.

3. The clamping of the component during grinding has a great influence on the distribution of the residual stresses. The second method of clamping (Fig.3 - deformation not constrained) ensures a better distribution of the residual stresses than the first one (Fig.2 - deformation is constrained in the direction x and z). The jig design should be such that it should allow as far as possible thermal expansion in the major directions.

4. Analysis shows that harmful residual stresses cannot be avoided if phase transformations, the influence of surface roughness and

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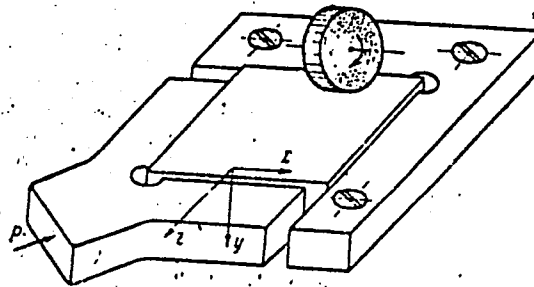
Investigation of the residual ...

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the block mosaics are not taken into consideration. However, residual tensile stresses will occur in all cases. 5. Control of the residual stresses to comply with the requirements of practical operation cannot be attained without introducing additional operations into the manufacturing process. There are 17 figures, 1 table and 13 Soviet references.

Fig.2



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D240/D304

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AUTHORS: Podzey, A.V., and Serebrennikov, G.Z., Candidates
of Technical Sciences

TITLE: Control of residual stresses by heating components with
subsequent quick cooling

SOURCE: Moscow. Aviatsionnyy institut. Trudy, no. 140. Tekh-
nologicheskiye metody povysheniya kachestva detaley i
uzlov aviadvigateley, 1961, 5-15

TEXT: After a review of previous theoretical and experimental results,
the authors consider the problem of the heat regime. It is assumed
that after grinding 1) the radial stresses are negligible, 2) the axial
stresses are nearly equal to the tangential stresses; moreover, 1) the
coefficient of linear expansion remains constant during heating and
cooling, 2) the mean integral value (over the cross section) of the
elasto-plastic components of the axial deformations is equal to 0,
3) elastic incompressibility of the material is assumed. The authors

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Control of residual ...

obtain the following scheme: 1) For given conditions of cooling one finds the heat transfer coefficient in a reference book, 2) the value of Biot's criterion is determined with the aid of the above coefficient, 3) maximum design deformation is found for the required value of Biot's criterion from a graph given by the authors (design deformations are defined as the differences of complete yield deformations and the plastic components of the deformations due to previous stages of loading), 4) maximum intensity of design deformations at the surface is determined from a formula given by the authors, 5) for certain points, the maximum plastic component of design deformation intensity is determined, 6) resultant magnitude of residual stresses is calculated. When the heat transfer coefficient varies, different values of residual stress are obtained. Experimental verification of this method was made on eight specimens; two were only ground, two were ground and heated to 700°C, with quick cooling in a 10% solution of NaCl, two were cooled and then ground and the last two were left in the initial state. A graph of the results is given. There are 5 figures and 7 references, 6 Soviet-bloc and 1 non-Soviet-bloc. The reference to the English-language publication reads as follows: H.R. Letner and A.B. Sauvageot, Metal Progress, 72, no. 3, (1957).

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L 45814-65 EWT(d)/EWT(m)/EWP(w)/EPF(c)/EWP(c)/EWA(d)/EWP(v)/EWP(j)/T/EWP(t)/
 EWP(k)/EPA(bb)-2/EWP(b)/EWP(1)/EWA(h)/EWA(c)/EWP(f)/EPF(n)-2 Pc-4/Pf-4/Pr-4/Peb/
 ACCESSION NR AM5002547 BOOK EXPLOITATION Pu-4 JD/EW/EM/PM S/

YEvstigneyev, M. I. (Docent); Marczov, I. A. (Docent); Podzay, A. V. (Professor,
 Doctor of Technical Sciences); Sulima, A. M. (Docent); TSukanov, I. S.
 (Docent)

Production of basic parts and units of aircraft engines (Izgotovleniya osnovnykh
 detaley i uzlov aviadvigatelye), Moscow, Izd-vo "Mashinostroyeniye", 1964,
 456 p. illus., biblio. Errata slip inserted. 5,200 copies printed. Series
 note: Tekhnologiya aviadvigatelayestroyeniya

TOPIC TAGS: aircraft engine manufacture, turbine blade, engine compressor,
quality control, plastics, nuclear propulsion, aircraft fuel supply, combustion
 chamber

PURPOSE AND COVERAGE: This book is a textbook for students of aviation higher
 educational institutions and departments. It deals with the engineering processes
 of fabricating parts and components of aircraft engines. The book considers
their design features, the technical specification for fabrication and materials,
 the engineering processes, methods of executing the basic processes, and quality
 control. The book will also be useful to engineers and technicians of the
 aviation industry.

Card 1/2

L 45814-65

ACCESSION NR AM5002547

10

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Card 2/3

YEVSTIGNEYEV, M.I., dots.; MOROZOV, I.A., dots.; PODZEY, A.V.,
prof.; SULIMA, A.M., dots.; TSUKANOV, I.S., dots.;
ZHADIN, G.P., dots., retsenzent; KOLOSOV, M.A., inzh.,
red.

[Manufacture of basic parts and units of airplane engine]
Izgotovlenie osnovnykh detalei i uzlov aviadvigatelyei.
[By] M.I.Evstigneev i dr. Moskva, Mashinostroenie, 1964.
456 p. (MIRA 17:9)

RYKALIN, N.N.; PODZEY, A.V., doktor tekhn.nauk, prof.; NOVIKOV, N.N., kand.tekhn.
nauk; LOGINOV, V.Ye., inzh.

Calculation and simulation of the temperature field in a part subjected
to grinding and milling. Vest.mashinostr. 43 no.11:74-80 N '63.
(MIRA 17:2)

1. Chlen-korrespondent AN SSSR (for Rykalin).

S/795/62/000/000/001/007

AUTHOR: Podzey, A. V.

TITLE: Residual stresses during grinding and their control.

SOURCE: Vysokoproizvoditel'noye shlifovaniye. Ed. by Ye. N. Maslov. Kom. po tekhn. mashinostr. In-t mashinoved. AN SSSR, Moscow, Izd-vo AN SSSR, 1962, 57-70.

TEXT: The paper describes the results of an experimental investigation, performed predominantly on specimens made of the alloy ЭМ437А (EI437A), a choice dictated by the desire to eliminate any complications of the T-stress picture by any structural phase transformations within the metal tested. The investigation was intended to determine the degree to which grinding produces residual tensile stresses in the surface layer of a part subjected to grinding, stresses which frequently may exceed the yielding strength of the material. Inasmuch as these stresses are primarily temperature-produced, the present study regards them as thermal stresses evoked by a nonstationary T field. A comparison of theoretical concepts with experimental measurements shows that the stress analysis of parts, including thin-walled parts, is fully valid if the equations of the T field for a semi-infinite body are applied. The magnitude and the depth of propagation of the residual tensile

Card 1/3

Residual stresses during grinding and their control. S/795/62/000/000/001/007

stress, σ_o , are found to be proportional to the intensity of the heat source, q , the linear expansion coefficient, α_{exp} , and Young's modulus of elasticity, E , and inversely proportional to the volumetric heat capacity, c_v , and the yield limit of the material, σ_s . A radical approach to the problem would be to reduce the level of the residual tensile stresses by means of a decrease in the intensity of the heat source, q . This may be achieved practically by increasing the speed of the part, v_p , a reduction in the cutting depth, t , the use of softer grinding disks with a grain size 60-80, and ample cooling by means of liquids with elevated lubricating properties. It is found that the method of attachment of the part to the machine base is of considerable consequence. If the attachment of the part allows a deformation of the part along the principal directions, the tensile stresses and the depth of their propagation are reduced thereby. It is important to bear this consideration in mind in the design of grinding machines and their accessories. The grinding procedure as such cannot eliminate the presence of tensile stresses along the surface of a part. This can only be achieved by the introduction of supplementary control operations, comprising, for example, vibrocontact polishing, anneal, and through heating and subsequent rapid cooling. Of advantage in the design of grinding machines is the development of a kinematic geometry that affords an increase in the time of contact between the tool and the part, a provision which helps to equalize the T in the

Card 2/3

Residual stresses during grinding and their control. S/795/62/000/000/001/007

surface layer and to form compressive stresses within it. The Soviet grinding machine В П Л -2 (VPL-2) for vibrocontact polishing is cited as a prototype of such a machine. The control of residual stresses affords a significant improvement in the fatigue characteristics of the resulting products. There are 6 figures and 6 Russian-language Soviet references.

Card 3/3

PODZEY, L.I.; VINOGRADOVA, V.D.

Results of heterogenic transplantation of a Rous sarcoma in decerebrated and normal pigeons. *Biul. eksp. biol. med.* 42 no.7:54-57
Jl '56. (MLRA 9:9)

1. Iz Gosudarstvennogo onkologicheskogo instituta imeni P.A.Gertsena (dir. - doktor meditsinskikh nauk prof. A.N.Novikov; nauchnyy rukovoditel' - chlen-korrespondent AMN SSSR prof. A.I.Savitskiy) Predstavlena deystvitel'nym chlenom AMN SSSR N.N.Petrovym.

(SARCOMA, transplantation,

Rous sarcoma, in decerebrated & normal pigeons (Rus))

(NEOPLASMS, transplantation,

same)

(BRAIN, physiology,

eff. of decerebration on transplanted Rous sarcoma in pigeons (Rus))

PODZEY, L.K.

Metastasis of Brown-Pierce tumors transplanted into different sections of the stomach, under normal conditions and following the action of carbon tetrachloride on the liver. Biul. eksp. biol. i med. 51 no.6:70-73 Je '61. (MIRA 15:6)

1. Iz patofiziologicheskoy laboratorii (zav. - kand.med.nauk I.P. Tereshchenko) Gosudarstvennogo onkologicheskogo instituta imeni P.A. Gertsena (dir. - prof. A.N. Novikov), Moskva.
(STOMACH--CANCER) (LIVER--CANCER)
(CARBON TETRACHLORIDE--PHYSIOLOGICAL EFFECT)

PODZEY, L.K. (Moskva)

Metastatic spreading of Brown-Pearce tumors in the presence
of functional changes of the liver. Pat. fiziol. i eksp. terap. 6
no.4:76-78 J1-Ag '62. (MIRA 17:8)

1. Iz patofiziologicheskoy laboratorii (zav. -- kand. med.
nauk I.P. Tereshchenko) Gosudarstvennogo onkologicheskogo
instituta imeni P.A. Gertsena (dir. -- prof. A.N. Novikov).

POZNEY, L.K.

Characteristics of the course of the preneoplastic period in male and female mice of the C57bl line under an increased functional stress in the liver. Pat. fiziol. i eksp. terap. 8 no.5:66-68 S-0 '64. (MIRA 18:12)

1. Patofiziologicheskaya laboratoriya (zav. - kand.med.nauk I.P.Tereshchenko) Onkologicheskogo instituta imeni P.A. Gertsena (direktor - prof. A.N.Novikov), Moskva. Submitted February 28, 1963.

PODZEY, L.K.; BOLONINA, N.I.

Pretumorous changes in the liver of C57BL mice induced by
orthoaminoazotoluene. Vop. onk. 11 no. 12:94 '65.

(MIRA 19:1)

1. Iz patofiziologicheskoy laboratorii (zav. - kand. med. nauk
I.P. Tereshchenko) Gosudarstvennogo onkologicheskogo instituta
imeni Gertsena (dir. - prof. A.N. Novikov).

PODZET, L. K.

✓ The effect of the prolonged use of sleep-inducing drugs on the growth and on the process of metastasis of Brown-Pierce sarcoma of rabbits. L. K. Podzetz and V. O. Vinogradova. *Veprasy Onkologii* 1, No. 2, 28-32 (1955).—Expts. were performed with male rabbits of 2 kg. wt. Na amytal (I), chloral hydrate (II) and hexinal (III) were administered to the exptl. rabbits, the first time 30 min. before the cancer transplant was made. One half ml. of a saline suspension of Brown-Pierce sarcoma was then injected intratesticularly, including the controls. Thereafter the narcotizing drugs were administered to the exptl. rabbits daily up to 25-30 days. All animals were then sacrificed. Cancerous developments were divided into (1) extensive, including metastases, (2) medium, (3) slight, and (4) absence of tumors. The prolonged administration of I, II, and III inhibited the functions of the central nervous system which resulted in an augmented growth of the B.-P. sarcomas and rate of the metastatic processes. I and III were more potent than II. B. S. L.

Med 3

State Oncological Inst. im P. A. Gertsin

PODZEY, L.K.

USSR/Medicine - Oncology

FD-2565

Card 1/1 Pub. 17-18/23

Author : Vinogradova, V. D.; Piontkovskiy, I. A.; Podzey, L. K.

Title : Experiments in transplantation of a Brown-Pearce tumor into tongue tissue

Periodical : Byul. eksp. biol. i med. 5, ^{V.39} 65-67, May 1955

Abstract : Discusses and gives results of experimental transplantation of Brown-Pearce tumors into the tongue of rabbits. Photograph. No references.

Institution : Pathophysiology Laboratory (Head - Prof I. A. Piontkovskiy) of the State Oncology Institute imeni P. A. Gertsen (Scientific Director - Prof A. I. Savitskiy, Corresponding Member of the Academy of Medical Sciences USSR; Acting Director - V. V. Gorodilova, Kandidat of Medical Sciences)

Submitted : June 22, 1954 by L. A. Zil'ber, Member of the Academy of Medical Sciences USSR

BOCHAROV, F.; DOBRA, A.; ZAYTSEV, N.; KALUTSKIKH, N.; KOMOGORTSEV, N.;
KOPANITSA, Ya.; MIKHAYLENKO, I.; PLIKHIN, P.; ~~PODZHAROV, P.~~;
RUZOV, M.; SEMENOV, N.; STAKHANDV, A.; USKOV, A.

Foma Evgen'evich Tiurin; an obituary. Mast. ugl. 7 no.11:32 N '58.
(MIRA 11:12)

(Tiurin, Foma Evgen'evich, 1898-1958)

PODZHAROV, P., Geroy Sotsialisticheskogo Truda

Of what consist miners' traditions? Mast. ugl. 8 no.6:18-19
Je '59. (MIRA 12:10)

(Coal miners)

PODZHAROV, V.K., aspirant

Interaction of pine and perennial lupine root systems in joint
growths. Sbor. nauch. trud. BLTI no.11:77-85 '58. (MIRA 15:12)
(Pine) (Lupine)
(Forest ecology)

PODZHAROV, V.K.

USSR/Forestry - Forest Management.

K-3

Abs Jour : Ref Zhur - Biol., No 20, 1958, 91537

Author : Podzharov, V.K.

Inst : Belorussian Forest Technology Institute.

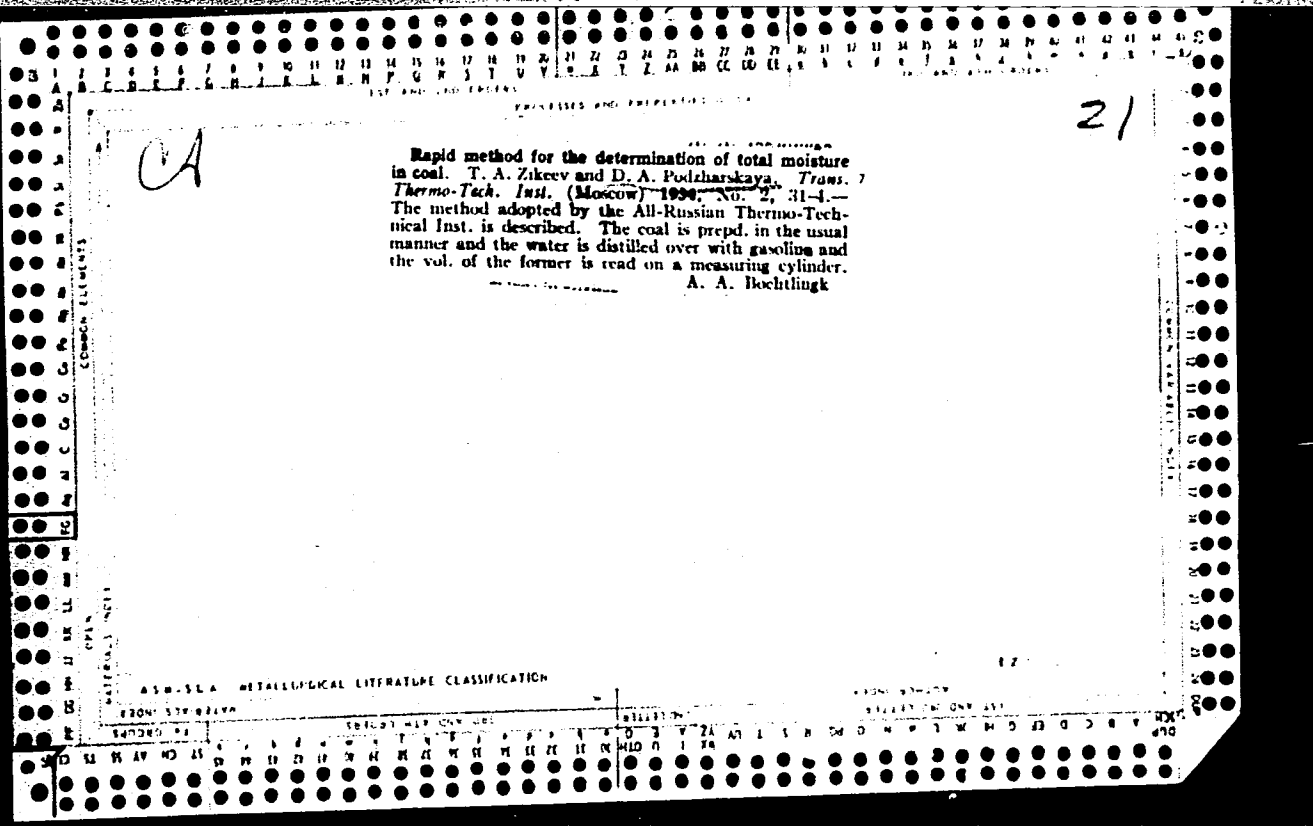
Title : An Increase in the Fertility of Forest Soils by the Cultivation of Perennial Lupine in Pineries with Heath, Cowberry Plus Eagle and Bilberry Plus Eage Fern.

Orig Pub : Sb. nauchn. tr. Belorussk. lesotekhn. in-t, 1957, vyp. 10, 213-232.

Abstract : Experiments with the sowing of perennial lupines in inter-row crops together with the common pine have been carried out at Negorel'skiy Experimental and Training leskhoz (Belorussian SSR); characteristic samples the plots under cultivation are given together with the agrotechny of planting. The development of lupine was especially

Card 1/2

Card
PODZHAROV, V. K.: Master Agric Sci (diss) -- "The effect of inter-row cultivation of perennial lupine (*Lupinus polyphyllus* Linal) on the productivity of pines in the Belorussian SSR". Minsk, 1958. 20 pp (Min Higher Educ, USSR, Beloruss Forestry Engineering Inst im S. M. Kirov), 150 copies (KL, No 4, 1959, 129)

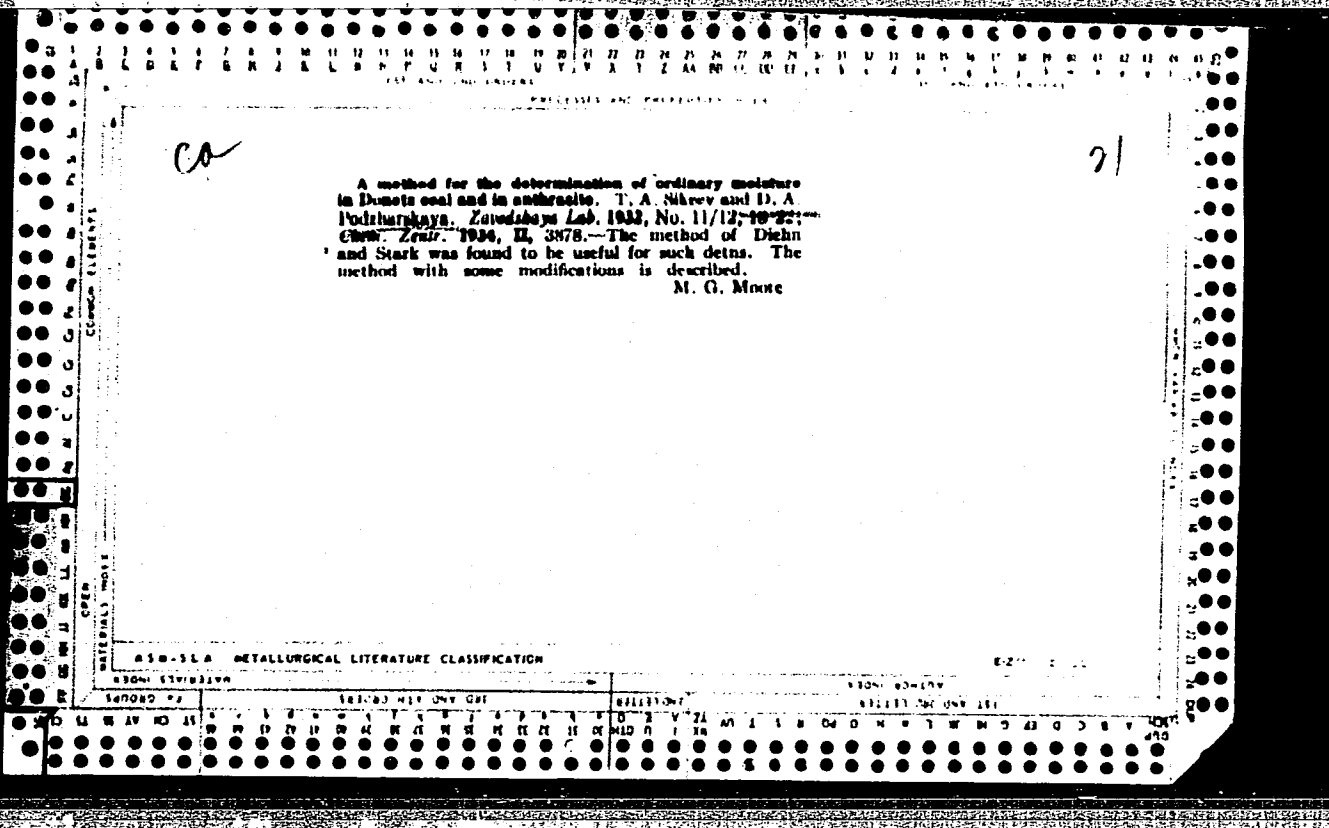


POKHARSKAYA L. A. AND ZIKUYEV, T.A.

Opyt Utochneniya Metodik Analiza Karbonatnykh Slantsev, Goryuchiye Slantsy, 1934, No 2, 44, No 3, 26.

SO:

Goryuchiye Slantsy # 1934-35, TN .871
G .74



U I J K L M N O P Q R S T U V W X Y Z 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50

1ST AND 2ND ORDERS

PROCESSES AND EXPERIMENTAL

Adiabatic calorimeter for exact determination of heat content of fuel. A. P. Pakhino and I. A. Polshchikova. *Zavodskaya Lab.* 4, 304-10 (1935). A modification of the Richardson adiabatic calorimeter by Sventolavskii and Pakovich (C. A. O. 2165) is illustrated and described. The results of the detns. of heat contents of coals are tabulated and discussed. Chas. Blanc

21

AD-156 DETALLURGICAL LITERATURE CLASSIFICATION

TECHNICAL INDEX

TECHNICAL INDEX

U I J K L M N O P Q R S T U V W X Y Z 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50

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PROCESSED AND REPRODUCED FROM THE ORIGINAL SOURCE

ca *21*

Changes in coals on drying. H. A. P. Shakhno and D. A. Podzharskaya. *Khim. Tverdogo Topliva* 6, 909-12 (1969).—*Coal* 20: 7012.—Anthracite and the coals "T" are but little changed on drying at 50-60°. The prepn. of the analytical samples in usual conditions in air without heating and under water with consecutive drying in a stream of N did not change the org. mass of the coal. The dried coals showed a complete dependence of their wt. on the humidity of air. Thus usual criterion of the wt. constancy is not correct without accounting for the air humidity. Details are given. A. A. Podgorov

ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION

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A B C D E F G H I J K L M N O P Q R S T U V W X Y Z AA AB AC AD AE AF AG AH AI AJ AK AL AM AN AO AP AQ AR AS AT AU AV AW AX AY AZ

1ST AND 2ND ORDERS

COLLECTED AND PROPERTIES INDEX

21

Handwritten mark: 21

Mechanization of laboratory coal sampling. A. P. Shakhno and D. A. Podibarskaya. *Zavodskaya Lab.* 5, 431-6(1936).--Best results were obtained by the use of the British device "Cascade." Chas. Blanc

Materials Index

ASS-51A METALLURGICAL LITERATURE CLASSIFICATION

1ST AND 2ND ORDERS

1ST AND 2ND ORDERS

1ST AND 2ND ORDERS

1ST AND 2ND ORDERS

1ST AND 2ND ORDERS										3RD AND 4TH ORDERS									
PROCESSES AND PROPERTIES INDEX																			
ca										21									
<p>Changes in coal on drying. A. P. Shakhno and D. A. Budshanskaya <i>Trudovye Zapiski</i> 6, 370-371 (1955). — A drying temp. of 105° affects the properties of coal, particularly its heating value, which may be lowered by 20 cal. Best results are obtained by drying coal in a stream of dry air heated to 50-65°. Brown coal is changed most and anthracite least. Operations carried out with a great variety of coals are described. A. A. Hochlingk</p>																			
ASD-31A METALLURGICAL LITERATURE CLASSIFICATION										E-2-11-2-11-2-11									
SERIALS										SERIALS									
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21

Effect of laboratory treatment and storage on coal samples. III. A. P. Shakhno and D. A. Podsharnkaya.
Khim. Tverdogo Topliva 6, 813-20(1967); *Ch. C. A. 31*, 1562.
—Coal samples change in wt. as a result of (a) action of atm. moisture, (b) absorption of O, and (c) removal of oxidation products, CO, H₂O, CO₂. There is a change also in such properties as calorific value and caking ability. Five references
A A P

ASB-SLA DETALLURGICAL LITERATURE CLASSIFICATION

MUSA-ZADE, M.M.; PODZHARSKIY, B.I.

Improving the quality of thin-walled pipe. Metallurg 7 no.10:
36-37 0 '62. (MIRA 15:9)

1. Tsentral'naya zavodskaya laboratoriya Azerbaydzhanskogo
truboprokatnogo zavoda.
(Pipe mills—Quality control)

MUSA-ZADE, M.M., inzh.; PODZHARSKIY, B.I., inzh.; ALIYEV, I.P., inzh.

Improving the quality of thin-walled pipe. Stal' 25 no.10:
935 0 '65. (MIRA 18:11)

1. Azerbaydzhanskiy truboprokatnyy zavod.

MIZYUK, L.Ya.; PODZHARYY, V.M.

Change in the parameters of an elliptically polarized field in inductive electric prospecting. Izv. AN SSSR. Ser. geofiz. no.7:1050-1063 J1 '63. (MIRA 16:8)

1. Institut mashinovedeniya i avtomatiki AN UkrSSR.
Predstavleno chlenom redaktsionnoy kollegii Izvestiy AN SSSR,
Seriya geofizicheskaya, B.M. Yanovskim.
(Electric prospecting)

ACC NR: AT6020480

(A)

SOURCE CODE: UR/0000/65/000/000/0111/0119

AUTHOR: Podzharyy, V. M. (L'vov)

ORG: none

TITLE: Determination of a field's components from elliptical polarization constants

SOURCE: AN UkrSSR. Teoriya i elementy sistem otbora geofizicheskoy informatsii (Theory and elements of systems for selecting geophysical information). Kiev, Naukova dumka, 1965, 111-119

TOPIC TAGS: electromagnetic field, prospecting, electric polarization

ABSTRACT: Methods of measuring the components of low frequency electromagnetic fields in prospecting for mineral deposits are discussed. These methods are useful since the measurements are independent of the position in space of the electrodes or measuring units. The object measured is the magnitude of such invariants as the semiaxes of the polarization ellipsoid of the magnetic field. The present paper touches only on the functional relationship between the elliptically polarized field and its components. The amplitudes and phases of the polarized field may be represented on nomograms and the solution can be made graphically. Orig. art. has: 4 figures, 11 formulas.

SUB CODE: 08/ SUBM DATE: 10Nov65/ ORIG REF: 007

Card 1/1

KIRICHENKO, A.N., inzh.; MUSA-ZADE, M.M., inzh.; PODZHATSKIY, B.I.,
inzh.; KAFAROV, S.V., inzh.; ZAYCHENKO, R.V., inzh.

Effect of certain factors in piercing on the formation of double
skins. Stal' 21 no.8:727-730 Ag '61. (MIRA 14:9)

1. Ukrainskiy nauchno-issledovatel'skiy trubnyy institut
i Azerbaydzhanskiy truboprokatnyy zavod.
(Rolling (Metalwork))

ACC NR: AP6021424

SOURCE CODE: UR/0413/66/000/011/0022/0022

INVENTOR: Krasovitskiy, B. M.; Podzhaylo, V. F.; Derevyanko, L. N.

ORG: None

TITLE: A method for producing liquid scintillators. Class 12, No. 182164 [announced by the All-Union Scientific Research Institute of Single Crystals (Vsesoyuzny nauchno-issledovatel'skiy institut monokristallov)]

SOURCE: Izobreneniya, promyshlennyye obraztsy, tovarnyye znaki, no. 11, 1966, 22

TOPIC TAGS: scintillator, luminescent material

ABSTRACT: This Author's Certificate introduces a method for producing liquid scintillators by using a base and activators -- diaryl derivatives of 1,3,4-oxadiazole and 1,3-oxazole. The luminescence yield is increased and a wider selection of liquid scintillators is produced by using dicumylmethane as the base.

SUB CODE: 11, 07, 18/ SUBM DATE: 12Apr65

Card 1/1

UDC; 547.787.2.07

ACC NR: AP6021548

(N)

SOURCE CODE: UR/0198/66/002/006/0092/0098

AUTHOR: Marchenko, V. P. (Odessa); Podzhio, V. M. (Odessa)

ORG: Odessa State University (Odesskiy gosudarstvennyy universitet)

TITLE: Motion of a body of variable mass in a resistant medium

350

SOURCE: Prikladnaya mekhanika, v. 2, no. 6, 1966, 92-98

TOPIC TAGS: Euler equation, motion equation, motion mechanics

ABSTRACT: Certain particular cases of the integration of Euler equations of motion of a body having a variable mass about a fixed point with consideration of the resistance of the medium are examined in this article. It was found in the four cases examined that it is possible to integrate the dynamic equations of the Euler type, i. e., the equations of motion of a body of variable mass with one fixed point in a resistant medium when p , q , and r are defined as explicit functions of time. It is pointed out that for a complete investigation of this motion it is necessary to integrate the kinematic equations derived, which is impossible without additional limitations on the character of motion since, if they are taken in the Poisson form, one ultimately arrives at the integration of the Riccati equation with complex coefficients. If the kinematic equations are taken in the Euler form difficulties arise in integration of the integro-

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ACC NR: AP6021548

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differential equation. The condition of the periodicity of the functions $p(t)$, $q(t)$, $r(t)$ permit solving the stated formula to the end in quadratures. Orig.-art.-has: 17 formulas.

SUB CODE: 12,20/ SUBM DATE: 21Mar66/ ORIG REF: 003

Card 2/2 hs

NOVIKOV, V.N.; TOLSTOV, L.K.; SEREBRYAKOVA, Ye.K.; SOKOLOV, B.M.; Prini-
mal uchastiye: Melent'yev, Yu.I.; KAPGER, V.S.; ZORCHENKO, I.P.;
KARPCV, K.F.; Kushnarenko, V.S.; SHEVCHENKO, L.I.; TRIFONOVA, N.
I.; PODZHUNAS, V.A.; MASLITSKAYA, M.P.

Obtaining industrial naphthalene from the centrifugal naphthalene
of the Gubakha Coke and Coal Chemicals Plant. Koks i khim. no.8:
35-38 '62. (MIRA 17:2)

1. Vostochnyy uglekhimicheskiy institut (for Novikov, Tolstov,
Serebryakova). 2. Gubakhinskiy koksokhimicheskiy zavod (for Soko-
lov).

PODZHUTSKI, Ch.; VOYTASIK, Ya.

Cupola furnace melting with briquetted and pitch coke. Lit.
proizv. no. 12: ~~14~~ D '61. (MIRA 14:12)
(Cupola furnaces) (Coke)

BRASYUNAS, V.B., PODZHYUNAS, A.S. [PODŽIUNAS, A.S.]

Production of l-hydroxyphthalazine. Med.prom. 12 no.7:47-50 J1 '58
(MIRA 11:8)

1. Kaunasskiy gosudarstvennyy meditsinskiy institut.
(PHTHALAZINE)

BRASYUNAS, V.B.; PODZHYUNAS, A.S. [Podziūnas, A.S.]

Synthesis of l-chlorphthalasine. Med.prom. 13 no.1:38-40
Ja '59. (MIRA 12:10)

(PHTHALASINE)

BRASUNAS, V.B.; PODZHYUNAS, A.S.

Synthesis of 1-mercaptophthalazine. Med. prom. 13 no.8:53-56 Ag
'59. (MIRA 13:8)

1. Kaunasskiy meditsinskiy institut.
(PHTHALAZINE)

BRASYUNAS, V.B.; PODZHYUNAS, A.S.

Synthesis of apressin. Med.prom. 13 no.12:20-22 D '59. (MIRA 13:4)

1. Kumasskiy meditsinskiy institut.
(PHTHALAZINE)

KRAL, Ludvik, Dr.; PODZIMEK, Ales, Dr.

Surgical therapy of bronchial asthma. Ces. lek. cesk. 93 no.51-52:
1413-1419 24 Dec 54.

1. Z chir. oddeleni, prim. Dr. V.Kreisingera UNZ-ONV Praha 3
a s II chirurg. kliniky K.U. prof Dr. J.Divise
(ASTHMA, surgery)

JOHANOVSKA, Kveta, MUDr.; PODZIMEK, Ales, MUDr.; SOVA, Jos., Doc., MUDr.

Therapy of bronchial asthma with infiltration of the cervical
vago-sympathetic nerve according to Visnevsky. Cas. lek. cesk.
44 no.36:979-980 2 Sept 55.

1. II. interni klinika prof. dr. Ant. Vancury a II. chirurg.
klinika akademika J. Divise.

(ASTHMA, therapy
vago-sympathetic nerve infiltration, Visnevsky's
method.)

(NERVES VAGUS,
infiltration in ther. of asthma, Visnevsky's method.)

PODZIMEK, Ales.; LHOTKA, Jaroslav.

Pathological arteriovenous communication of peripheral blood vessels.
Rozhl. chir. 35 no.5:329-334 May 56.

1. Z II. chirurgicke kliniky Fakulty vseobecneho lekarstvi KU v Praze.
Prednosta akademik Jiri Divis.

(FISTULA, ARTERIOVENOUS, surg.
(Cz))

(ANEURYSM, surg.
racemose (Cz))

LHOTKA, Jaroslav; BOREK, Zoltan; ~~PODZIMEK, Ales~~

Modern concepts in diagnosis and therapy of breast cancer. Cas.
lek. cesk. 95 no.23-24:612-618 15 June 56.

1. Z II. chirurgicke kliniky Fakulty vseobecneho lekar. KU v
Prase: predn. akad. Jiri Divis, J.L.,P. VII., Malirska 1.
(BREAST, neoplasms,
diag. & ther. (Cz))

PODZIMEK, ALES

JOHANOVSKA, Kveta; PODZIMEK, Ales; SOVA, Josef

Further results on the use of Wisniewsky infiltration of cervical
vagosympathetics in bronchial asthma. Cas. lek. cesk. 97 no.25:779-782
20 June 58.

1. II. inter. klinika, prednosta prof. Dr. Fr. Herles a II. chirurg.
klinika, prednosta akademik J. Divis.

(ASTHMA, ther.

Wisniewsky infiltration of cervical vagosympathetics, technic
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