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S/136/61/000/011/007/007 E082/E135

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AUTHOR:Shapiro, V.Ya.TITLE:Experimental determination of the movement of
self-aligning plugs, when drawing tubesPERIODICAL:Tsvetnyye metally, no.11, 1961, 70-77

There are two opinions about the behaviour of self-TEXT aligning (floating) plugs during the drawing process: a) that unavoidable variations of the mechanical properties of the tube, coefficient of friction, etc. set up continually changing stresses. These alter the balance of forces which positions the plug, and cause the plug to move, within the zone of deformation. b) that a stable process is possible, only over a strictly defined length of the cylindrical part of the plug, and that in stable conditions the plug is immobile. Neither theory has been confirmed experimentally. To examine the behaviour of the plug, the author has measured, simultaneously, the axial displacement of the plug, its frequency of oscillation, and the drawing force exerted. This was done on a 3-ton drawbench, at a tube speed of 32 m/min. A special linear transducer was used to measure displacement and Card 1/ 1

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Experimental determination of the

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strain-gauge load cells to measure the drawing force. A twochannel oscillograph, connected in a bridge circuit, recorded the results. Nine special plugs were made, all of the form shown in Fig. 3 and having the following dimensions; dia 12 mm, length 40 mm, $\alpha = 6^{\circ}$ 20' to 11° 45', D = 12,98 to 15.49 mm, $\ell_2 = 4$ to 14 mm. Surface finish, class 9, 10 and 11-12. Each plug had a long stem which was located in a guide bush to prevent transverse movement. The transducer was coupled to this stem. 400 sets of recordings were made. The first series of tests was made with different values of plug cone angle, and the second series with different values of die cone angle. The following displacements of the plug were recorded: 0.18 mm when the difference between plug and die angles equalled 1º 20'; 0.23 mm when the difference equalled 3° 45; 0.5 mm when the difference equalled 5° 30'. When the difference between cone angles was increased to 6° 30° , drawing conditions became unstable. These results confirmed the conclusions of earlier workers, that the plug cone angle must be 1º to 3º less than die cone angle. Even under these conditions, drawing is unstable if the die angle is small. This is shown in Card 2/ 🕇 😨

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Fig.4 where die angle 9° 40' gives stable drawing conditions. The pattern of oscillations shown in Fig. 56 shows that, even with optimum working parameters, heavy drawing loads cause instability and narrow the interval of stability of drawing. Parameters must therefore be more closely maintained when loads are heavy, especially when drawing ferrous materials. The effect of surface finish, and hence of friction, is shown in Fig.6. Using plugs with class 9 finish (usual in Soviet factories), tearing of the metal occurred; this made recording difficult, and drawing was impossible (Fig.6a). Flugs with class 10 finish gave better results. With 11-12 class finish, the process was stable. These trials were repeated using different lubricants, and gave analogous results. Alternate dull and bright rings occur on some tubes drawn with floating plugs. There are, respectively, thin and thick parts of the tube wall. The variations of thickness are 0.05 to 0.12 mm. Comparison of the frequency of operation of the plug, the distance between the rings, and the speed of the tube, confirmed that rings are caused by the tube alternately wedging between die and plug, then becoming free again, during the drawing The author concludes that: operation. Card 3/7

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Experimental determination of the ... S/136/61/000/011/007/007 E082/E135

1) When optimum parameters are used, the plug floats from one stable position to another, thus preserving the balance of forces. 2) If the parameters differ from optimum, the plug oscillates, tearing the metal, and forming rings on the drawn tube, i.e. the balance of forces is not maintained. There are 6 figures, 3 tables and 11 Soviet-bloc references.



Fig.3 Sketch of plug Card 4/7

APPROVED FOR RELEASE: 08/09/2001

PERLIN, I.L.; SHAPIRO, V.Ya. Comparative analysis of power conditions in pipe drawing with floating and fixed cylindrical mandrels. Sbor. nauch. trud. (MIRA 15:3) GINTSVETMET no.33:299-304 '60. (Drawing (Metalwork)) Ξ.

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SHAPIRO, V. Ya.

Experimental determination of the throughput of capillary tubes made of L-96 alloy. Priborostroenie no.10:28 0 '62. (MIRA 15:10)

(Capillaries-Testing)

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SHAPIRO, V. Ya.

And Personal and the second states of the

"Basis of theory of process of drawing tube on self-aligning mandrels". Questions were considered in detail on geometric center of deformation, magnitude of various elements of self-adjusting mandrels, power conditions of the process and their analytic determination. Great interest was invoked by an explanation of the decrease of effort of drawing through use of a lubricating wedge.

Report presented at the branch seminar on drawing of tube and aluminum alloys on self-aligning mandrels, Metallurgical Factory im V. I. Lenin, Kuybyshe \checkmark , 24-28 June 1963

(Tsvet. Metally, No. 10, 1963 pp 84-85, author Starostin, Yu. S. JPRS 24,651 19 May 1964

APPROVED FOR RELEASE: 08/09/2001

AUTHOR: Shapiro, V. Ya.; Shkol'nikov, Ye, L. TITLE: Analytical determination of the conditions for the appearance of liquid friction during wire drawing SOURCE: Fizkhim. zakonomernosti deystviya smazok pri obrabotke metallov davleniyem. Moscow, Izd-vo AN SSSR, 1963, 55-61 TOPIC TAGS: friction, wire drawing, hydralic pressure, lubricant, viscosity, fluid mechanics, liquid friction ABSTRACT: The predominantly liquid friction which arises in the process of wire- drawing is caused by the hydraulic action of the lubricating wedge. This friction appears between the surface of the tool and the surface of the material in the zone preceding the location of the deformation. In the present paper, an analytical expression is derived for the determination of the maximal hydraulic pressure in the lubricant. $P_{max} = -\frac{6\mu u}{(T_{x} - T_{on}) \Delta} \left[1 - \frac{z_{\theta}}{t}\right]^{\theta}.$ (1)	ACCESSION NR: AT4014060 S/3072/63/000/00055/0061	•
$P_{\max} = -\frac{\sigma_{\max}}{(T_{\tau} - T_{on})\Delta} \left[\frac{1 - \frac{1}{\tau}}{t} \right].$	 TITLE: Analytical determination of the conditions for the appearance of reparative of reparative during wire drawing SOURCE: Fizkhim. zakonomernosti deystviya smazok pri obrabotke metallov davleniyem. Moscow, Izd-vo AN SSSR, 1963, 55-61 TOPIC TAGS: friction, wire drawing, hydralic pressure, lubricant, viscosity, fluid mechanics, liquid friction ABSTRACT: The predominantly liquid friction which arises in the process of wire-drawing is caused by the hydraulic action of the lubricating wedge. This friction appears drawing is caused by the tool and the surface of the material in the zone preceding the between the surface of the tool and the surface of the material in the zone preceding the location of the deformation. In the present paper, an analytical expression is derived for the determination of the maximal hydraulic pressure in the lubricant. 	
	$P_{\text{max}} = -\frac{6\mu u}{(T_{\tau} - T_{\text{on}}) \Delta} \left[1 - \frac{2}{i}\right]^{2}.$ (1) Cord 1/2	

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ACCESSION NR: AT401	4060		
As shown by the formula the geometry of deforma viscosity of the lubrican angle becomes smaller surface of the material drawing apparatus will i	a, this pressure depends on the visco ation. The hydraulic pressure increa t and the rate of wire-drawing. It als and when the distance between the sur is reduced. Application of these cal ncrease its stability, decrease the dr metal to the surfaces of the instrume	ses with an increase in the so increases when the wedg cface of the tool and the culations to the design of wir rawing pressure required	e
ASSOCIATION: None			
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ENT(m)/EWA(d)/EPR/EWP(t)/EWP(k)/EWP(b) Pf-4/Ps-4 IJP(c) L 21204-65 S/0136/64/000/012/0075/0079 ACCESSION NR: AP5000945 MJW/JD/HW AUTHOR: Shapiro, V. Ya., Patseruk, A.P. DETE-COURT P TITLE: Drawing large-diameter thin-walled tubes from aluminum and its alloys on self-21 adjusting mandrels 37. SOURCE: Tsvetnyy metally, ho. 12, 1964, 75-79 TOPIC TAGS: large diameter tube, thin-walled tube, aluminum drawing, aluminum alloy drawing, self adjusting mandrel/alloy AMG-6 :4 ABSTRACT: Self-adjusting mandrels were designed to draw tubes 150-350 mm in diameter with a wall thickness of 2-2.5 mm from aluminum and its alloys. The angle of taper of the mandrel was 10-11°, being 1-3° less than the die angle. The mandrels were hollow, made of steel U9-U12, and had a Rockwell hardness of 57-62. To reduce friction in drawing, the surface of the mandrels was chrome plated and polished. The dies were made of the same steel and had a Rockwell hardness of 60-63. Tubes 250 mm in diam. were drawn at a speed of 7-12 m/min and tubes 250-350 mm in diam at 1.5-2.0 m/min. The wall thickness of the punched tube workpiece was 3-5.5 mm. During the drawing process the forces arising, the geometric dimensions, surface quality, and mechanical properties of the tube before and after drawing were recorded. Particular interest was Cord 1/2

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shown in the high-alloy, high-strength alloy AMG-6 which could not been drawn over the usual mandrel owing to adhesion but could be drawn on the self-adjusting mandrel. This new type of mandrel greatly reduced the variation in wall thickness. As a result of the study, industrial lots of tubes with diameters up to 335 mm and wall thickness of 2.2 mm have been produced. Ovalization of the trailing end of the tubes was characteristic when drawing the large-diameter, thin-walled tubes owing to uneven wall thickness. The curvature of the middle of the tube was about 1-2 mm/m. Orig. art. has: 3 tables and 3 figures.

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AUTHOR: <u>Tityunik, G.N.; Shapiro, V. Ya.</u> TITLE: <u>Mechanical properties of aluminum-alloy tubes</u> as a function of the degree of deformation during drawing \mathcal{N} SOURCE: Tsvetnyye metally, no. 5, 1965, 76-78 TOPIC TAGS: drawing stress, deformation resistance, aluminum alloy <u>tube</u> , tube drawing mandrel, yield point ABSTRACT: In analytic determinations of the drawing stress deformation re- sistance is the most important quantity. For the drawing of aluminum-alloy tubes the yield point $\sigma_{0.2}$ can be taken as the deformation resistance. Since, however, the available information pertains only to mandrel-less Since, however, the available information pertains only to mandrel-less	53967 <u>-65</u> EWT(m)/EWA(d)/EPR/EWP()/WW/HW CESSION NR: AP5013603	(t)/EWP(k)/EWP(b)/EWA(c) Pf-4/Ps-4 IJP(c UR/0136/65/000/005/0076/0078 669.71-462:539.5	$\frac{1}{4}$
drawing mandrel, yield point ABSTRACT: In analytic determinations of the drawing stress deformation re- sistance is the most important quantity. For the drawing of aluminum-alloy tubes the yield point $\sigma_{0,2}$ can be taken as the deformation resistance. tubes the yield point $\sigma_{0,2}$ can be taken as the deformation resistance. Since, however, the available information pertains only to mandrel-less Since, however, the available information pertains only to mandrel-less since, however, the available information pertains only to mandrel-less since, however, the available information pertains only to mandrel-less	THOR: <u>Tityunik, G.N.; Shapiro,</u> ITLE: <u>Mechanical properties of a</u> egree of deformation during drawi OURCE: Tsvetnyye metally, no. 5,	V. Ya. aluminum-alloy tubes as a function of the $\frac{\log_{\zeta}}{100}$ / / / / / / / / / / / / / / / / / / /	B
drawing of tubes, the authors public during their drawing particularly mechanical properties of these tubes during their drawing particularly respect to the newly developed method of drawing. Longitudinally notched which assures extremely high degrees of drawing.	rawing mandrel, yield point BSTRACT: In analytic determinat distance is the most important qu cubes the yield point $\sigma_{0,2}$ can be Since, however, the available inf irawing of tubes, the authors per	ions of the drawing stress deformation re- nantity. For the drawing of aluminum-alloy taken as the deformation resistance. Formation pertains only to mandrel-less rformed their own investigation of the ubes during their drawing, particularly with	

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L 53967-65 ACCESSION NR: AP5013603 Ospecimens of these tubes (diameter 110x105mm) were tested in a laboratory tensile testing machine with tensile stresses of 1-5 tons. The test results were used as the basis for plotting curves of mechanical properties of the tubes as a function of the integral deformation index In-µ. Beginning with $ln\mu = 0.6$ the yield point was found to differ by 7 tons/m² (0.7 kg/mm²) from the ultimate strength; as the degree of drawing was further increased, this quantity became practically constant and amounted to 4%, which demonstrates the validity of using in analytic calculations the quantity σ_d in place of $\sigma_{0,2}$ when information on the latter is absent. The investigated relations are analogous to those specified in the literature for sheets and wire. The somewhat greater scatter of the obtained values may be explained by the inevitable lack of uniformity in tube-wall thickness, which, by contrast with sheets and wire, makes it impossible to determine the true deformation. The authors' findings can be utilized in scheduling the drawing process as well as in the analytic calculation of the drawing stresses. Orig. art. has: 4 figures, 1 table. ASSOCIATION: none 2/1 2 Card

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$\frac{L 23314-66}{L 23314-66} = \frac{E'T(m)/T/EWP(t)/E'P(k)}{L 1P(c)} = \frac{10/EW/DJ}{D/EW/DJ}$	/002/0063/0	063	
ACC NR: AP6006340 AUTHOR: Kuz'menkov, V. A.; Nikolayeva, M. R.; Shapiro, V. Ya.;		-// 1	1000 - 10000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1
CRG: none TITLE: <u>Lubricant for cold working of metals</u> . Class 23, No. 178 SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki,	006 no. 2, 196	6,63	
TOPIC TAGS: metalworking, cold working, lubricant ABSTRACT: This Author Certificate describes a lubricant for col	d working c orked and re	of metals.	
To reduce the coke residue formed on the suitate of the motion the annealing temperature, polyisobutylene with a molecular weig 100,000 is added to the composition.	t of 20,00	[LD]	
SUB CODE: 13/ SUBM DATE: 11Feb65/ ORIG REF: none/	OTH REF:	none/	
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Card 1/1000 UDC: 621.892.6:621.7.016.3			





SAGAYDAK, I.I.; NEKRASOV, V.G.; KOPYRIN, I.A.; BORTS, Yu.M.; BRATCHENKO, V.F.; RYSYUKOV, N.Ye.; KAKUSHA, N.P.; SHAPIRO, V.Z.

> Operation of a large capacity blast furnace with natural gas. Metallurg 10 no.7:16-19 Jl '65. (MIRA 18:7)

1. Orsko-Khalilovskiy metallurgicheskiy kombinat i Chelyabinskiy nauchno-issledovatel'skiy institut metallurgii.

APPROVED FOR RELEASE: 08/09/2001

LOUISAR







SHAPIRO, Ya.; TEMIROV, T.

Piemann spaces with a reducible isotropy group, Dokl. AN SSSR 157 no.3:539-541 J1 '54. (MIRA 17:7)

1. Gor'kovskiy gosudarstvennyy universitet imeni Lobachevskogo. Predstavleno akademikom A.N. Kolmogorovym.

APPROVED FOR RELEASE: 08/09/2001

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 CIA-RDP86-00513R001548320019-8

sov/88-58-97-7/7 Shapiro, Ya. G., Candidate of Technical Sciences AUTHOR: Experimental Study of a Liquid Ejector (Eksperimental'noye issledovaniye zhidkostnogo ezhektora) TITLE : Trudy Moskovskogo aviatsionnogo Instituta, 1958, Nr 97; Addition of a Supplementary Volume in Jet Apparatus (Prisoyeaineniye PERIODICAL: dopolnitel'noy massy v struynykh apparatakh), pp 191-236 (USSR) The author states that phenomena which occur in the liquid ejector chamber, such as energy losses and the distribution of these losses, ABSTRACI : are not yet sufficiently known. Theoretical determination of the optimum parameters of these processes is rather inexast. The mixing process of the two flows in a water ejector was investigated by measuring the fields of velocities, pressures and pulsations of the full pressure heads and by characteristics of work of the ejector. The analysis of the obtained experimental data made possible a more precise design of the water ejector, providing the basis for selecting the mixing chamber length, for establishing ejector characteristics, and for conducting power analysis of various sectors of the mixing chamber. As a result of this analysis of the available experimental material the following conclusions, applicable to slow Card 1/2

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Experimental Study of a Liquid Ejector

κ,

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velocity ejectors, were made by the author: 1. The mixing of jets in an ejector represents a complex process associated with the transformation of velocity and pressure profiles with a turbulent exchange of impulse among particles. The presence of steep velocity gradients leads to considerable pulsations of velocities at every point of the mixing zone, which result in internal energy losses and in friction losses along the walls. Direct measurements of such velocity fields with a pitot tube are impossible without considerable errors. Measurements are distorted in proportion to the pulsation component of the velocity. 2. Actual losses due to friction with the walls of the ejector's mixing chamber are 2-3 times larger than losses ordinarily allowed for in computation. In the proposed empirical formula they are determined by the so-salled "friction velocity," and not by the average velocity of the mixture. 3. At the beginning of the mixing there is a pressure drop, which depends on the characteristics of the ejector. An empirical formula is given for determining the velocity drop, which attains 7 percent of the velocity head of the working medium. 4. The field of velocities is equalized at a distance of 3-4 times the diameter of the mixing chamber. Equalization is practically completed at 7 times the diameter of the chamber. The length of the mixing chamber of an ejector working with a diffusor should be limited to 7 times the diameter. 5. The performance of the ejector depends mainly on the ratio of speeds of the primary and secondary flow (W1, W2). The efficiency of the ejector decreases sharply, when the velocity coefficient deviates from its optimum value. The bibliography consists of 10 references, 6 of them Soviet, 2 German, and 2 English.

APPROVED FOR RELEASE: 08/09/2001

AKHVERDOV, I., doktor tekhn. nauk; SHAPIRO, Ya., kand. tekhn. nauk; RUDITSER, R., inzh.

Manufacturing three-dimensional prefabricated room units by a method of concreting on a horizontal stand. Zhil. stroi. no.l: 7-10 '64. (MIRA 18:11)

1. Chlen-korrespondent AN BSSR (for Akhverdov).

APPROVED FOR RELEASE: 08/09/2001

CIA-RDP86-00513R001548320019-8

RO Ya T Sapiro, Ya. L. <u>Geodesic fields</u> of directions and pro-<u>jective systems</u> of paths. Mat. Sb. N.S. 36(78), 125-(5) 148 (1955). (Russian) Let us consider a holonomic field of *m*-dimensional I-F/7 directions formed by *m* vectors V^{*} ($\alpha, \beta = 1, \dots, n+m$; $a, b=n+1, \dots, n+m$) in an affinely connected space of n+m dimensional subspaces V_{*} in A_{n+m} . A holonomic field of *m*-dimensional directions is called "geodesic", if the totality of the subspaces V_{*} passing through every point of any geodesic line which is not contained in any V_{*} is a totally geodesic subspace of m+1 dimensions in A_{n+m} . A necessary condition that the field of *m*-di-0000 mensional directions formed by \tilde{V}^* be geodesic is given by mensional directions formed by V be geodesic is given by expressions in terms of the vectors V^a , and it is shown that if such a geodesic field exists in A_{n+m} , the coef-icients of connection of A_{n+m} can be reduced to $\Gamma^i_{ad} = \Pi^i_{ad}(x^a) + \psi_{(a}\delta^i_{\beta)}, \Pi^i_{ad} = 0$ ($i=1, \cdots, n$), and converse ly. All such A_{n+m} form a class contained in the general one. A special one of this class is V. F. Kagan's subprojective space of n dimensions [Trudy Sem. Vektor. Tenzor. Anal, 1, 12-101 (1933)], which contains a linear line system of an (n-1)-dimensional euclidean space. If a system of paths in lover

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A. C. 0.00 an n-dimensional manifold can be supplemented by others an *n*-dimensional manifold can be supplemented by others so that it defines with the given system a complete system of geodesic lines in an affinely connected (n+m)-dimen-sional space, then the system of paths is said to be "imbedded" (projectively). Making use of the concept "imbedding", it is also proved that the above stated necessary condition is sufficient. Then the obtained results are applied to a Riemannian space containing a geodesic field of directions. At the end, there are some appendices where it is shown that the results can be applied readily to metric and generalized subprojective spaces, the gener-alized projective geometry of H. Weyl [Raum Zeit alized projective geometry of H. Weyl [Raum, Zeit, Materic, 4. Aufl., Springer, Berlin, 1921], and the rela-tivistic theory of a central-symmetric gravitational field. A. Kawaguchi (Sapporo).

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SHAFIRC, Ya. L.

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O proizvol'nykh komponentakh tenzora vtorogo ranga. Matem, sb., 17 (59),(1945), 65-84.

SO: Mathematics in the USSR, 1917-1947 edited by Kurosh, A.G., Markushevich, A.I., Rashevskiy, P.K. Moscow-Leningrad, 1948

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APPROVED FOR RELEASE: 08/09/2001

AUTHOR: TITLE; PERIODICAL ABSTRACT:	Shapiro, Ya.L. (Gor'kiy) Sov/39-45-4-7/7 On Linear Manifolds of Geodesic Directional Fields in the Space of Affine Connection (O lineynykh mnogoobraziyakh geodezicheskikh poley napravleniy v prostranstve affinnoy svyaznosti) Matematicheskiy sbornik, 1958, Vol 45, Nr 4, pp 5i1-528 (USSR) The present paper contains a continuation of the investigations carried out by the author in an earlier paper [Ref 4]. The principal result consists in the assertion that systems of paths which are imbedded into an A_{n+1} , are isomorphic to the set of curves which is obtained by projecting the geodesics of the A_{n+1}
SUBNITTED:	There are 5 references, 3 of which are Soviet, 1 Japanese, and 1 Dutch. Karch 20, 1957
Card 1/1	1. Topology 2. Geodesics - Applications
an the second	

TITLE:	Geodesic Direction Fields and Homothety Groups in Space Affinitive Connection (Geodezicheskiye polya napravleni gruppy gomotetiy v prostranstvakh affinnoy svyaznosti)	s of y i
PERIODICAL:	Doklady Akademii nauk SSSR, 1958, Vol 120.Nr 3, pp481-48	4(USSR)
ABSTRACT:	Let A_n be an n-dimensional space of affine connection.	In
	A $(n \geq 2)$ with coordinates x^{n} let a direction field	be
	defined by the vector field $A^{\checkmark}(\mathbf{x}^{\beta})$, \checkmark , $\beta=0,1,\ldots,n$. T	he
	trajectories ("A-lines") of $A^{\mathcal{A}}$, which intersect a geod curve of A_{n+1} are assumed to generate a two-dimension	esic al sur-
	face S. If S is completely geodesic for every geodesic	curve.
	then the field defined by $A^{\alpha \prime}$ is called a geodesic direction field. Let A_{m+n} contain m geodesic direction fields m	rhich
	are assumed to be defined by the vectors \mathbb{A}^{ω} . There exi- ordinate systems (class \mathbb{Z} ') for which the trajectories	st co- of the
	vector fields Å are the u ^a - coordinate lines. In thes coordinates it holds	1e
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Geodesic Direction Pieus and Homothety Groups in Spaces of /20-120-3-11/67 Affinitive Connection $\begin{aligned} & \Gamma_{\alpha,B}^{\sigma} \in \Pi_{\alpha,B}^{\sigma'}(u^{1}) + \Psi(\alpha, \delta_{\beta}^{\sigma'}) \\ \begin{pmatrix} 1 \end{pmatrix} & \Gamma_{\alpha,0}^{b} \in \Pi_{\alpha,0}^{b}(u^{b}, u^{1}) + \Pi_{\alpha,0}^{1} = \Pi_{\alpha,0}^{1}(u^{b}) \\ & \Pi_{\alpha,0}^{b} = \Pi_{\alpha,0}^{b}(u^{b}, u^{1}) + \Pi_{\alpha,0}^{1} = \Pi_{\alpha,0}^{1}(u^{b}) \\ & \Pi_{\alpha,0}^{b} = \Pi_{\alpha,0}^{b}(u^{b}, u^{1}) + \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{1}(u^{b}) \\ & \Pi_{\alpha,0}^{b} = \Pi_{\alpha,0}^{b}(u^{b}, u^{1}) + \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{1}(u^{b}) \\ & \Pi_{\alpha,0}^{b} = \Pi_{\alpha,0}^{b}(u^{b}, u^{1}) + \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{1}(u^{b}) \\ & \Pi_{\alpha,0}^{b} = \Pi_{\alpha,0}^{b}(u^{b}, u^{1}) + \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{1}(u^{b}) \\ & \Pi_{\alpha,0}^{b} = \Pi_{\alpha,0}^{c}(u^{b}, u^{1}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{b} = \Pi_{\alpha,0}^{c}(u^{b}, u^{1}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{b} = \Pi_{\alpha,0}^{c}(u^{b}, u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{c}(u^{b}, u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{c}(u^{b}, u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c} = \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) + \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c}(u^{b}, u^{b}) \\ & \Pi_{\alpha,0}^{c$

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SOV/20-120-3-11/67

Geodesic Direction Fields and Homothety Groups in Spaces of Affinitive Connection

defines a geodesic direction field, where no linear relation with the constant coefficients exists between the $\frac{A^2}{A^2}$. The set The set of the geodesic direction fields defined by the various $\sum A_n \tilde{\mathbf{1}}^2$ is called the linear manifold of the $(\underline{n-1})$ dimensional geodesic direction fields. Vector fields $\tilde{\mathbf{A}}^2$ normalized in the described way are dimoted as \mathbf{I} - normalized. The author gives necessary and sufficient conditions that the $\frac{A^2}{A^2}$ are \mathbf{L} - normalized and that the geodesic direction fields defined by the $\frac{A^2}{A^2}$ belong to a linear manifold in the sense mentioned above. Let $\frac{A^2}{A_n^2} \frac{2!}{2\pi^2}$ be the operators of the group (of order m) of the automorphic transformations of \mathbf{A}_{n+m} . If the direction field defined by the vector $\sum_{\mathbf{A}} \lambda_n^{\mathbf{A}-2}$ of an ar-

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Geodesis Direction Fields and Homothety Groups in SOV/20-120-3-11/67 Spaces of Affinitive Connection bitrary one-parameter subgroup is geodesic, then the transformations of the group are denoted as homotheties of the space A_{m+n} . The homothety group of order m of the space A_{m+n} is locally isomorphic to the homothety group of the (m-1)-dimensional affinitive space. Some further results are given, and 9 theorems. There are 4 references; 2 of which are Soviet, 1 Dutch, and † Japanese. ASCOCIATION: Gortheyskiy gosudarstvennyy universitet imeni N.I.Lobachevskogo (Gor kly State University imeni N.I. Lobache skiy) PRESENTED: December 13, 1957, by P.S.Aleksandrov, Academiciar 12.12111月2日 - 1944年1月11日 1945年1月11日 ¹ Groduations Available - A. Operatora (Mathematics³ - 3. Praneformations (Natheratica)

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Vneshniala ballistika. Utvershdeno v kachestve uchebnika dlia akaderdi : KAKA i vtuzov obor. promyshl. Koskva, Oborongiz, 1939. 2 v., illus., diagrs., tables.

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EXIEN'KIY, Il'ya Markovich; SHAPIRO, YAkov Moiseyevich; YAKOVLEV, Boris Mikhaylovich; MOZZHUKHIN, H.A., red.; VYSOTSKAYA, R.S., red.; GOLUBKOVA, L.A., tekhn.red.

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Discusses characteristics of hemoptysis and pulmonary hemorrhage. Suggests morphine injections as therapeutic remedy, roentgenological observations for accurate diagnosis of diseases, and appropriate treatment.
28/49173

	FA 34/49T9
USSR/Medicine - Pneumonia, Diagnosis Nov 44 Medicine - Pneumonia, Therapy	8
"Croupous Pneumonia and Its Treatment," Ya. E. Shapiro, Dr Med Sci, 5 pp	
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(HEART-INFARCTION)

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V.A., prof.; VOGRALIK, V.G., prof.; DEMIDOVA, A.V., kand. mod.
nauk; DUL'TSIN, M.S., prof.; ZAKRZHEVSKIY, Ye.B., prof.;
KONCHALOVSKAYA, N.M., prof.; KASSIRSKIY, I.A., prof.; KOST,
Ye.A., prof.; LOGINOV, A.S., kand. med. nauk; NESTEROV, V.S.,
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Suggested, created, introduced. Izobr.i rats. no.6:38-40 Je '60. (FIFA 14:2)

1. Byuro sodeystviya ratsionalizatsii i i izobretatel'stvu Gosudarstvennogo soyuznego konstruktorsko-tekhnologicheskogo byuro po proyektirovaniyu schetnykh mashin, g.Leningrad (for Sulin). 2. Sotrudnik gazety "Stroitel", g.Baku (for Shapiro). (Technological innovations)

APPROVED FOR RELEASE: 08/09/2001

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SEIH ⇒LÌ FIZ. MET. I METALL, VOL. 1, N. 1, 1955 nG-Vibrational endurance tests on electrotechnical steels by E. A. Shapiro (p. 176-179) - Fatigue tests on a number of Russian transformer steels-are reported. Specimen strips were cut parallel and at right angles to the direction of rolling and vibrated with the aid of an electromagnet with one end clamped. Results of a few fatigue bend tests are also given.

APPROVED FOR RELEASE: 08/09/2001

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AUTHOR: Shapiro, Ye.A., Engineer.

110-4-8/25

TITLE: The Operation of Coil Springs at Stresses above the Yield Point (Rabota vintovykh pruzhin pri napryazheniyakh vyshe predela tekuchesti)

PERIODICAL: Vestnik Elektropromyshlennosti, 1958, No. 4, pp. 26 - 28 (USSR)

ABSTRACT: High-voltage apparatus contains a large number of springs operating in tension or compression. Most of these are made of carbon spring wire to standard COCT-5047-49 up to 8 mm diameter. The springs should be stable and should not break. Using tension springs made of carbon steel grade B as specimens, residual strain measurements were made after various numbers of cycles up to 50 000 cycles and thereafter every 2 000 - 5 000 cycles until visible cracks appeared and the spring failed. The table gives results of residual stress determinations on three specimens. The tests show that after the appearance of cracks, the springs may continue to operate for 600 - 4 500 cycles. The relationship between the number of cycles and the stress

was tested on springs made of wire grade Π . The ultimate strength of the wire in tension was 130 kg/mm² and the springs Cardl/3perated with maximum tangential stresses ranging from

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110-4-8/25 The Operation of Coil Springs at Stresses above the Yield Point ·

> 55 - 84.5 kg/mm². The relationship between this stress and the number of cycles is plotted. The results are represented by an empirical formula which may be used to determine the stress at which a spring can operate without failure for a given number of cycles.

Investigations were made of the length of time that pieces of a spring can go on operating after the first failure. For example, if the first failure takes place after some 300 cycles at stresses of 50 kg/mm², a second failure occurs 5 - 15 000 cycles later. The test results show that considerable overstresses cause fatigue cracks to develop in several places simultaneously; a sample was observed with three deep cracks. In actual service in high-voltage equipment, springs are maintained under static load for a long time. The influence of prolonged static loading was therefore investigated by three kinds of tests. Static loads up to a tangential stress of

68 kg/mm² were maintained for up to 75 000 hours at room temperature. None of the springs failed. Then, static loads, applied for periods up to 1 000 hours, were followed by dynamic fatigue tests. The static load did not affect the results. Next, static load was applied after dynamic loading and Card2/2

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110-4-8/25 The Operation of Coil Springs at Stresses above the Yield Point maintained for 6 000 hours. All the springs withstood this test, including two which already had deep fatigue cracks. It is concluded that coil springs made of carbon spring wire, grades Π and B, of 5 -6 mm diameter can operate with mean tangenuial stresses of up to 70 kg/mm⁻ for 50 000 - 200 000 working cycles. With dynamic loading, failure occurs after 50 000 cycles; a definite relationship exists between the stress and the number of cycles. Static tests did not cause failure even when stresses up to 68 kg/mm² were applied for 75 000 hours. Alternation of static and dynamic test conditions had no important influence on either the static or the dynamic fatigue strength of the springs. There are 1 figure, and 1 table. ASSOCIATION: Uralelektroapparat Works (Zavod"Uralelektroapparat") SUBMITTED: March 14, 1957 AVAILABLE: Library of Congress vard 3/3

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