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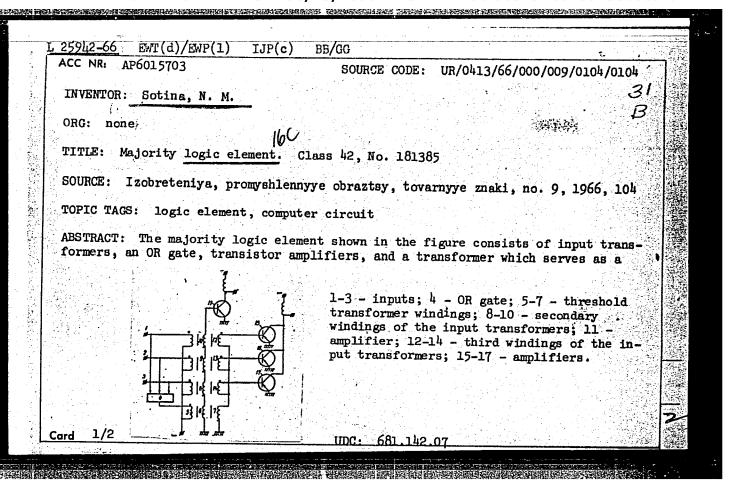
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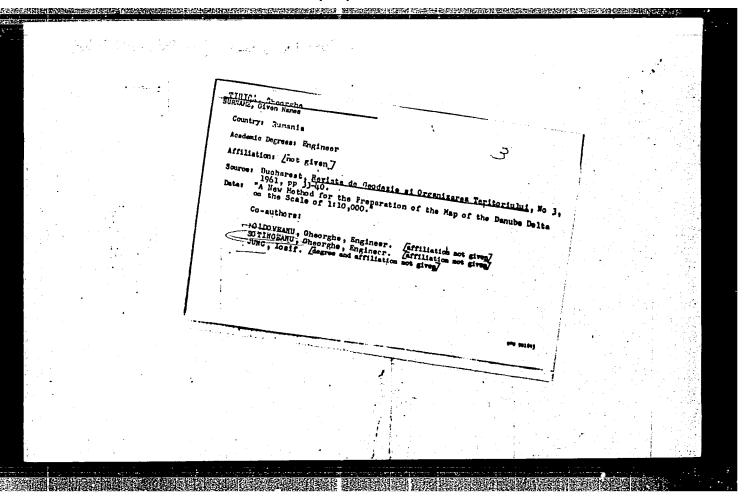
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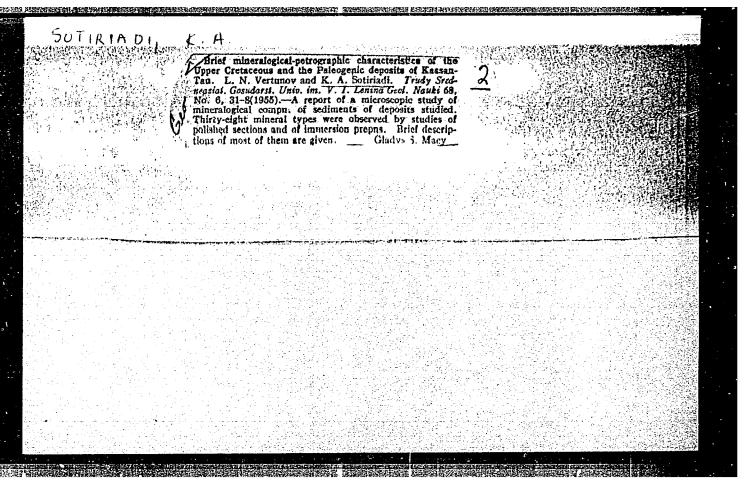
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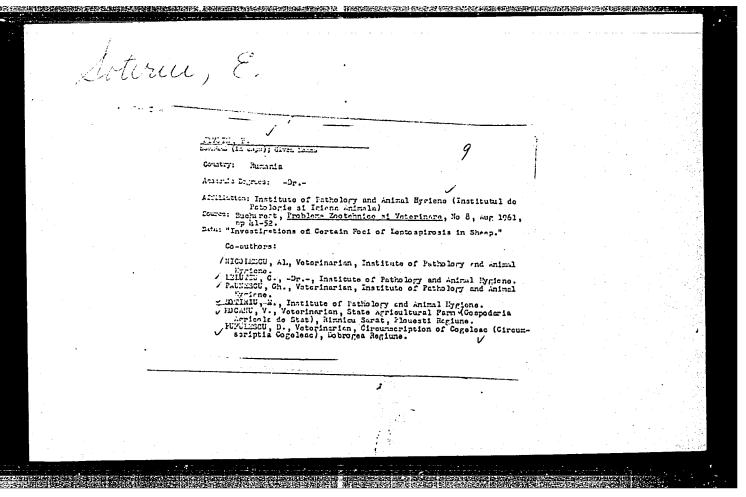
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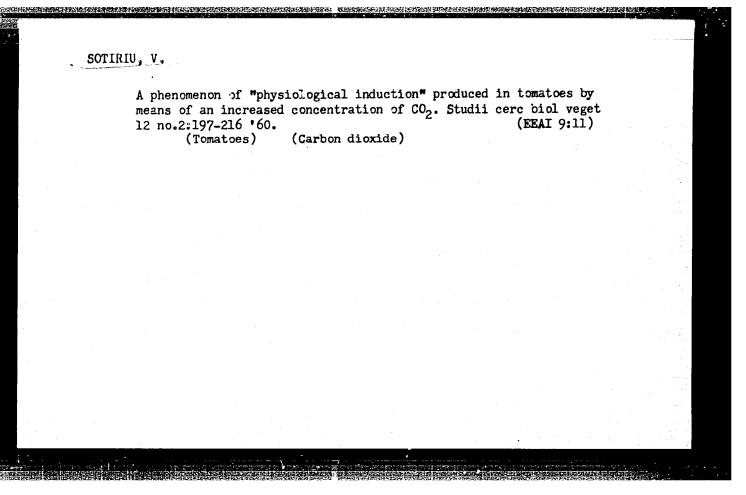
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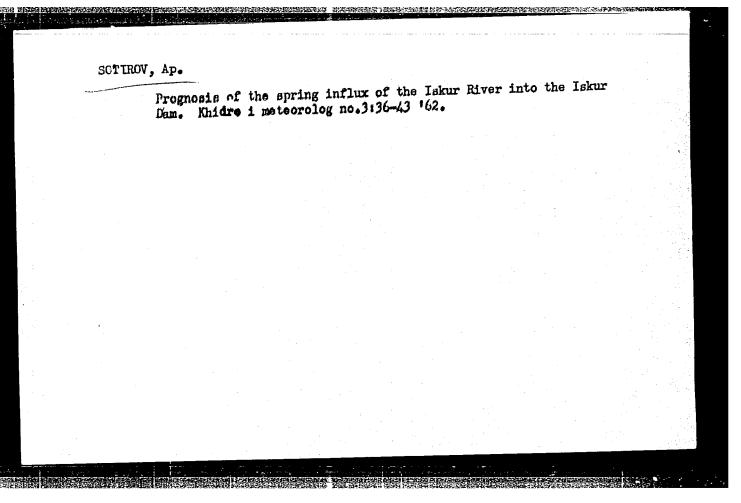
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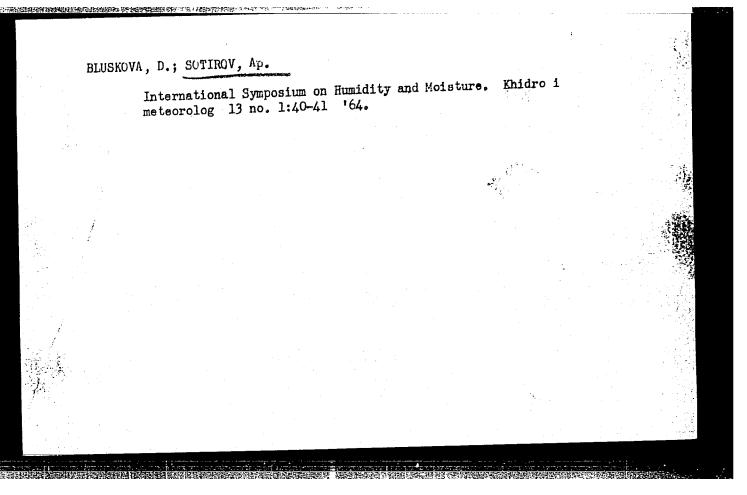
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为这种情况,我们就是这种的人,我们就是这种的人,我们就是这种的人,我们就是这种的人,我们就是这种的,我们就是这种的人,也是这种,我们就是这种的人,我们就是这种的

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ORG: none TITLE: Coaxial shf switch. Class 21, No. 179804 SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 6, 1966, 38 TOPIC TAGS: electronic switch, switching circuit, high power switch, SHF ABSTRACT: An Author Certificate has been issued for a coaxial shf switch. To increase the decoupling between the channels, the switch is provided with a rotating metal shield in the form of an open cylinder. The shield screens the side channels and is shield in the form of an open cylinder. The shield is spring mounted, and its external actuated by a \(\Gamma \)-shaped conductor. The shield is spring mounted, and its external actuated by a line of the shield is spring mounted, and its external surface is polished and coated with a highly wear-resistant metal, e.g., palladium. SUB CODE: 09/ SUBM DATE: 13Jul64/ ATD PRESS: 4234		INVENTOR: Vaulin, A. M.; Kholodilov, N. N.; Sotkov, V. Ya.; Putchkov, Ye. V.
SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 6, 1900, 30 TOPIC TAGS: electronic switch, switching circuit, high power switch, SHF ABSTRACT: An Author Certificate has been issued for a coaxial shf switch. To increase the decoupling between the channels, the switch is provided with a rotating metal shield in the form of an open cylinder. The shield screens the side channels and is shield in the form of an open cylinder. The shield is spring mounted, and its external actuated by a \(\Gamma\)-shaped conductor. The shield is spring mounted, and its external surface is polished and coated with a highly wear-resistant metal, e.g., palladium. SUB CODE: 09/ SUBM DATE: 13Jul64/ ATD PRESS: 4234	-	ORG: none
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ABSTRACT: An Author Certificate has been issued for a coaxial shf switch. To the switch is provided with a rotating metal the decoupling between the channels, the switch is provided with a rotating metal shield in the form of an open cylinder. The shield screens the side channels and is shield in the form of an open cylinder. The shield is spring mounted, and its external actuated by a \(\Gamma\)-shaped conductor. The shield is spring mounted, and its external surface is polished and coated with a highly wear-resistant metal, e.g., palladium. [KM] Orig. art. has: 1 figure. SUB CODE: 09/ SUBM DATE: 13Jul64/ ATD PRESS: 4234		monte mace: electronic switch, switching circuit, high power switch, Shr
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cz/0057/65/000/008/0315/0319 IJP(c) WE/JD SOURCE CODE: T/EWP(t)/ETI L 34918-66 AUTHOR: Sotkovsky, Hilan (Engineer); Kapicova, Svatava (Engineer); Tatak, Vaclav & ACC NR: AP6026580 ORG: Kapicova Kotallurgical Project, Ostrava (Hutni projekt); Tatak VZKG, Ostrava TITLE: Use of various kinds of additive fuels in blast furnaces SOURCE: Hutnik, no. 8, 1965, 315-319 TOPIC TAGS: fuel oil, coal, fuel additive, blast furnace, coke, industrial APSTRACT: Fuels introduced with blast air into the furnace allow management, gas fuel savings of coke which is in short supply. The authors studied the use of fuel oil, coal, oil and oxygen, and coal and oxygen in quantities of 20 - 60 kg of oil per ton of pig iron, 60 to 100 of oil with oxygen, 50 to 250 of coal, and 100 to 250 of coal with oxygen. The best results were obtained with ho kg of oil with oxygen. The best results were obtained with 40 kg of oil and with 145 kg of coal. The price structure was that applying in Gzechoslovakia in 1964. (Oil at 0.30 Kcs/kg, coal 0.2833 Kcs per kg). Changes in the price structure would cause changes in the found optimum quantities. Orig. art. has: 8 figures and 2 tables. [JPRS] SUB CODE: 21, 13, 05 / SUBM DATE: none / ORIG REF: 001 / OTH REF: 006 227

PRAVDIC, Velimir; SOTMAN, S.

在大学的大学的大学的主义,在1915年,在1915年,在1915年,1915年,1915年,1915年,1915年,1915年,1915年,1915年,1915年,1915年,1915年,1915年,1915年,1915年

Electrokinetic studies in disperse systems. Pt.8. Croat chem acta 35 no.3:247-254 '63.

1. Institute "Ruder Boskovic", Zagreb, Croatia, Yugoslavia.

sov/180-59-3-27/43

Osipov, K.A. and Sotnichenko, A.L. (Moscow)

Values of the Activation Energy of Creep and Fracture AUTHORS:

for Aluminium During Tension TITLE:

的主题的**对任何性体,不能会到的种种的对比与全国性的**是更为1960的思想的思想的思想的对比较级的思想。但是他们的对于这种的对比较级的对比较级的对比较级的。

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Metallurgiya i toplivo, 1959, Nr 3, pp 139-141(USSR)

Previous work is briefly discussed. The present work was carried out on 99.99% Al after rolling at room temperature. Testing took place in vacuo (10-4 mm Hg) ABSTRACT: and at temperatures of up to 550°C. The specimen was 80 mm long with a gauge length of 22 mm and diameter 3 mm. The results confirm the relationship:

 $\tau = \tau_0 \exp(\Delta H_1/RT)$

where τ is time to fracture, τ_0 is a constant, AH1 is the activation energy of the process, and R and T have the usual meanings. Fig 1 shows the straight line graphs obtained for log time against inverse temperature for different stresses. Fig 2 shows the relationship between ΔH_1 and the applied stress. The curve is not linear and AH1 approaches a limiting value, believed to be 7.2 k cal/g atom (the theoretically

Card 1/2

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SOV/180-59-3-27/43

Values of the Activation Energy of Creep and Fracture for Aluminium During Tension

calculated value). The facts support the theories of Osipov (Ref 9 to 12). There are 2 figures and 13 references, 6 of which are Soviet, 6 English and 1 German.

ASSOCIATION: Institut metallurgii AN SSSR (Metallurgical Institute, Academy of Sciences, USSR)

SUBMITTED: December 4, 1958

Card 2/2

Multiple specimen vacuum apparatus for testing metals for creep and durability. Issl.po zharopr.splav. 4:367-371 '59. (MIRA 13:5)		
(MetalsTesting)	(Vacuum apparatus)	
	•	

86062

1418, 1045, 1454 18.8200

S/180/60/000/005/003/033 E111/E135

199210

(Moscow) Sotnichenko, A.L.

AUTHOR: TITLE:

Testing Metals for Creep and Long-Time Strength in a

Vacuum at Constant Stress Vo

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh

nauk, Metallurgiya i toplivo, 1960, No. 5, pp.47-51

The author recalls that the atmosphere in which creep and long-time strength tests are carried out can affect the results, and also that such tests are more fruitful if constant stress, rather than constant load, is applied. He describes his new machine, type Fig-12 (VPN-S2) (Fig. 1), with a vacuum of 10-4 mm Hg in the working chamber. Each of six specimens is loaded separately and is automatically kept at constant stress by a mechanical device (Ref. 4) which suitably reduces the load as mechanical device (Ref. 4) which survably reduces the load as elongation proceeds. Fig. 2 shows elongation as a function of time for 99.96% Fe iron, type y8 (U8) steel and 99.97% Ti titanium (middle, bottom and top graphs! respectively). The titanium (middle, bottom and top graphs! respectively), The respective temperatures are 580, 700 and 600 °C, and stresses 10, 8 and 6 kg/mm². Curves 1 relate to tests with constant load in air, 2 in vacuum, and 3 in vacuum and with constant stress. Card 1/2

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S/180/60/000/005/003/033 E111/E135

Testing Metals for Creep and Long-Time Strength in a Vacuum at Constant Stress

The great creep-increasing influence of atmosphere is further illustrated in curves 1 and 3 (air and vacuum, respectively) of Fig. 3 for titanium at 600 °C and constant stress of 10 kg/mm²; curve 2 is for a stress of 6 kg/mm². In all the experiments only vacuum results show a well-developed region of stable creep. The work was carried out under the direction of $\underline{K.A.}$ Osipov.

There are 3 figures and 4 Soviet references.

SUBMITTED: April 5, 1960

Card 2/2

APPROVED FOR RELEASE: 08/23/2000 CIA-RDP86-00513R001652530009-0"

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S/180/60/000/005/016/033 E193/E183

18-8300

1467, 1045

AUTHORS:

(Moscow)

Osipov, K.A., and Sotnichenko, A.L. The Stress-Dependence of the Activation Energy for

TITLE:

Creep of a-Titanium 17

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh

nauk, Metallurgiya i toplivo, 1960, No.5, pp.146-148

Activation energy for creep appears in all basic equations describing the kinetics of this process. However, these equations could be used only if the activation energy within a given temperature interval were independent of other parameters, or if the laws governing its variation were known. stress is one of the factors which may affect the magnitude of the activation energy for creep, and since contradictory conclusions have been reached by various workers regarding the relationship between these two variables, the present investigation was undertaken to obtain more experimental evidence. Creep curves were constructed for α -titanium (99.97% purity), tested in vacuum at various temperatures between 18 and 600 °C, under the applied stress in the 10-35 kg/mm² range. The test pieces Card 1/3

86075 S/180/60/000/005/016/033 E193/E183

The Stress-Dependence of the Activation Energy for Creep of α -Titanium

(gauge length 22 mm, diameter 3 mm), prepared from cast and forged material, were subjected to preliminary vacuum annealing at 800 °C for 100 h. Tests, in which the applied stress of 20-35 kg/mm² had been used, were carried out in a narrow temperature range had been used, were carried out in a narrow temperature range (18-190 °C) so as to minimize the risk of the activation energy (18-190 °C) so as to minimize the risk of the activation energy being affected by temperature. From the experimental creep being affected by temperature and curves the rate, ε (%/min) of steady creep was determined and curves determined and curves det

86075 S/180/60/000/005/016/033 E193/E183

The Stress-Dependence of the Activation Energy for Creep of $\alpha\text{-Titanium}$

applied stresses used in the present investigation, was calculated from the slope of the ln ε versus 1/T graphs. With σ increasing from 10 to 25 kg/mm², Δ H decreased at a gradually diminishing rate and reached constant value of 11.55 kcal/g-atom at the stress of 25 kg/mm². Acknowledgements are made to V.A. Tverezovskiy, who participated in this work.

There are 3 figures, 1 table and 5 Soviet references.

SUBMITTED:

April 5, 1960

Card 3/3

5/032/60/026/06/30/044 B010/B016

18.8200

AUTHOR:

Sotnichenko, A. L.

TITLE:

Device for Testing the Creep Strength of Metals in Vacuo

PERIODICAL:

Zavodskaya laboratoriya, 1960, Vol. 26, No. 6, pp. 760-762

TEXT: A device of the BNH-C2 (VPN-S2) type is described which permits the testing of the creep strength in vacuo (10-5 torr), or inert gas atmosphere up to 1600°C simultaneously on 6 samples. The tests can be performed with constant load and with tension automatically kept constant at the cross-sectional area of the sample. Experiments on the device described were carried out under the supervision of K. A. Osipov, Doctor of Technical Sciences. The samples are vertically fixed in the holders of the device (Fig. 1) and may be loaded one by one. The maximum load is 600 kg. The deformation of the sample is automatically recorded. It may be seen from the circuit diagram (Fig. 2) that an electronic $\Im\Pi\Lambda$ (EPD)-12-22 potentiometer is provided to maintain the voltage for heating the sample, a PBH (RVN)-20 rotary pump for the water cooling, a $\amalg BM$ (TsVL)-100

Card 1/2

OBIPOV, K.A.; SOTNICHENKO, A.L.

Limiting activation energy values of the steady creep of c.Fe and c.Ti under tensile stress in vacu. Dokl.AN SSSR 134 no.2:
333-336 S '60.

1. Institut metallurgii im. A.A. Baykova Akademii nauk SSSR.
Predstavleno akad. C.V. Kurdyumovym.
(Creep of metals) (Iron) (Titanium)

30902 S/180/61/000/005/012/018

10.7300

1418

E193/E383

AUTHORS:

Osipov, K.A. and Sotnichenko, A.L. (Moscow)

TITLE:

Creep of iodide zirconium in vacuum under a constant

stress

PERIODICAL:

Akademiya nauk SSSR. Izvestiya. Otdeleniye tekhnicheskikh nauk. Metallurgiya i toplivo.

no. 5, 1961, pp. 83 -85

TEXT: In continuation of their earlier work (Ref. 1 - DAN SSSR, 1960, v. 134, no. 2; Ref. 2 - Filial VINITI AN SSSR - Peredovoy proizvodstvennyy i nauchno-tekhnicheskiy opyt, 1959, No. P-59-68/6 and Ref. 3 - Problems of the theory of high-temperature strength of metals and alloys. Pub. by AN SSSR, 1960) the present authors studied creep of zirconium tested in

vacuum (10^{-5} mm Hg) at temperatures between 18 and 500 $^{\circ}$ C (i.e. in the α -Zr range) under a constant stress ranging from

10 - 30 kg/mm². Typical creep curves are shown in Fig. 1, where the strain (ϵ , %) is plotted against time (τ , hours), graphs a, ϵ , B and ϵ relating, respectively, to tests carried out Card 1/8

30902 S/180/61/000/005/012/018 E193/E383

Creep of iodide zirconium

under a stress of 10, 20, 30 and 25 kg/mm², the test temperature being indicated by each curve. The rate, &, of steady-state creep was calculated from these curves and it was found that the In & versus 1/T relationship was linear for any stress within the range employed in the present investigation and that, contrary to some published reports, extrapolated (n & versus 1/T graphs did not intersect at one point. In Fig. 3, fn & is plotted against the applied stress (o, kg/mm²), Curves 1 (circles) and 2(triangles) relating to tests at 100 and 500 °C, respectively. Finally, in Fig. 4, the activation energy (Δ H, kcal/g.atom) for steady-state creep of iodide zirconium is plotted against the applied stress (or, kg/mm²), the broken line indicating the calculated limiting value of ΔH . It will be seen that, starting from $\sigma' = 25 \text{ kg/mm}^2$, ΔH remains constant at a level almost identical with the theoretical value obtained in the previous work (Ref. 3). The close agreement between the experimental and theoretical magnitude of $\Delta\,H\,$ was taken to Card 2/5 3

30902 S/180/61/000/005/012/018 E193/E383

Creep of iodide zirconium

indicate that the structure of Zr is changed during plastic deformation from close-packed hexagonal to a body-centered cubic. It was postulated also that this transformation might be preceded by the formation of stacking faults in the hexagonal lattice, which changes first to face-centered cubic and becomes body-centered cubic during the subsequent shear. There are 4 figures and 4 references: 3 Soviet-bloc and 1 non-Soviet-bloc. The English-language reference mentioned is: Ref. 4 - E.J. Rapperport - Acta metallurgica, 1959, 7, no. 4, p. 254.

SUBMITTED: March 5, 1961

Card 3/# 3

s/180/61/000/006/016/020 E193/E383

10.1300

1413

Ivanov, V.I., Osipov, K.A. and Sotnichenko, A.L.

(Moscow)

TITLE:

AUTHORS:

A study of the kinetics of the process of creep and

recovery

PERIODICAL: Akademiya nauk SSSR. Izvestiya. Otdeleniye

tekhnicheskikh nauk. Metallurgiya i toplivo, no.6,

1961, 137-143

The object of the present investigation was to study the relationship between the activation energy for creep of TEXT: α-iron and the applied stress as well as the relationship between the activation energy for recovery of this metal and the degree of plastic deformation. Technical purity (99.76%) iron, preliminarily annealed in vacuum (10 hours at 700°C followed by 50 hours at 450°C), was used in creep tests carried out in vacuum (10⁻⁴ mm Hg) at 250 - 500°C under a constant stress ranging from 10-35 kg/mm². The ln E versus 1/T relationship, where & is the rate of creep and T temperature, was linear over the entire range of the applied

Card 1/40

A study of the kinetics ...

S/180/61/000/006/016/020 E193/E383

stresses studied. The variation of the activation energy for steady creep (Δ H) is demonstrated in Fig.2, where Δ H (kcal/g atom) is plotted against the applied stress It will be seen that the limiting value of σ (kg/mm²). $\Delta H = 20 \text{ kcal/g} \cdot \text{atom was attained at } \sigma > 30 \text{ kg/mm}^2$. At fracture of the specimens took place in a very σ > 35 kg/mm² short time. The process of recovery was studied on both technical and high-purity iron (99.67 and 99.99%, respectively). The experimental wire specimens, 0.6 and 1.5 mm in diameter, preliminarily annealed in vacuum (3 hours at 800°C) were deformed plastically at room temperature to 80, 84, 94 and 98% reduction in area. The kinetics of recovery were studied by measurements of the thermo-emf of plasticallydeformed against annealed material, which were taken immediately after deformation and during subsequent isothermal treatment The value of (1 - e/e), where at various temperatures. e denote the specific thermo-emf $(\mu V/^{8}C)$

Card 2/30 7

S/180/61/000/006/016/020 E193/E383

A study of the kinetics

before and after isothermal annealing, respectively, was taken as the measure of the degree of recovery attained. The results obtained for high-purity specimens, deformed to 94% reduction, are reproduced in Fig. 3, where $(1 - e/e_0)$ is

plotted against time (τ , sec) at temperatures indicated by each curve. This relationship can be described by

$$1 - \frac{e}{-} = a + b \ln \tau$$

where a and b are temperature-dependent constants. In the next series of experiments the temperature dependence of $(1-e/e_0)$ was determined. The results are reproduced in Fig. 4, where $(1-e/e_0)$ is plotted against temperature (°C) of the isothermal treatment of technical and high-purity iron (graphs a and f, respectively); Curves 1-4 in graphs a relate to specimens held at the temperature for Card 3/20

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33182 S/180/61/000/006/016/020 E193/E383

A study of the kinetics

1 800, 180, 30 and 2.5 sec, respectively, Curves 1 = 5 in graphs 5 relating to a holding time of 3 600, 900, 180, 60 and 30 sec, respectively. These data were used to determine the activation energy for recovery of the metals studied. To this end, the temperatures T at which various degrees of recovery could be attained after various times \mathcal{T} were determined from curves in Fig. 4. These were used to construct curves reproduced in Fig. 5, where $\ln \mathcal{T}$ (\mathcal{T} , sec) is plotted against $\frac{1}{T} = 10^4$, the numbers given by each curve indicating the value of $(1 - e/e_0)$, graphs a and $\frac{1}{T}$ relating to technical and high-purity specimens, respectively. Since all the curves reproduced in Fig. 5 were straight lines, it was possible to calculate the activation energy, ΔH , for recovery, from:

 $\ln \tau = A \exp \left[\Delta H / RT \right] \tag{2}$

Card 4/30 7

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A study of the kinetics

where R is the gas constant, and T is the temperature of the isothermal treatment (${}^{o}K$). The results are reproduced in Fig. 6, where \triangle H (kcal/g.atom) is plotted against (1 - e/e_o), the circles (1) and triangles (2) relating, respectively, to high-purity and technical-grade iron. It will be seen that the activation energy for recovery is at its minimum at low values of $(1 - e/e_0)$, remaining practically constant up to $(1 - e/e_0) = 0.3$ and then increasing rapidly to reach $\Delta H = 47.6$ kcal/g.atom at (1 - e/e) = 0.8. Similar results were obtained for material deformed to 98% reduction, which indicated that $\triangle H$ would not decrease even for more heavily deformed material. In the last series of experiments the effect of elastic deformation on the kinetics of recovery was studied. To this end (1 - e/e) was determined for high-purity specimens deformed to 94% reduction, which were stressed in the elastic range during the isothermal annealing. The results are reproduced in Fig. 7, Card 5/

S/180/61/000/006/016/020 E193/E383

A study of the kinetics

where $(1 - e/e_0)$ is plotted against the duration of treatment (mg , sec) at temperatures indicated by each curve. Comparison of isotherms reproduced in Figs. 2 and 7 shows that the elastic strain superimposed on plastic deformation brings about a significant increase in the rate of recovery only when $(1 - e/e_0)$ exceeds 0.3. The results of calculation showed that for $(1 - e/e_0) = 0.2$, 0.3 or 0.4, the value of $\triangle H$ was 12.3, 14.0 and 18.2 kcal/g.atom, respectively, the corresponding value for specimens not stressed elastically being 12.2, 14.7 and 22.8 keal/geatom. This indicates that elastic deformation does not affect the limiting (minimum) value of AH . It was inferred from the results obtained that the activation energy for recovery is a function of several states of the crystal lattice, which vary not only with the degree of preliminary deformation but also with the degree of recovery attained. The dependence of the activation energy on the degree of recovery can be attributed to the following factors;

Card 6/60 7

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大型的形式的现在分词 的现在分词 医克里特氏征 "我们是他们的人们的一个人们的人们的人们的人们的人们的人们的人们的人们的人们们是一个人们的人们们们们的人们们们们

A study of the kinetics

1) the presence in a deformed metal of volumes with different density of defects of various types;

2) variation of the density and distribution of defects during isothermal treatment;

3) different stability of different types of defects;

4) dependence of the activation energy for recovery on the nature of the defects and their density in elemental volumes in which they migrate. There are 7 figures, 1 table and 11 references: 7 Soviet-bloc and 4 non-Soviet-bloc. The two English-language references quoted are: Ref. 3: H. Bross and A. Seeger - The Physics and Chemistry of Solids, 1958, v.4, no. 3, 161; Ref. 8: Silcock, J.M., Acta metallurgica, 1959, v.7, no. 5.

January 10, 1961 SUBMITTED:

Card 7/

34517 s/659/61/007/000/004/044 D217/D303

AUTHORS:

Osipov, K.A., and Sotnichenko, A.L.

TITLE:

Investigating the dependence of the energy of activa-

tion of creep of α-Fe on stress

SOURCE:

Akademiya nauk SSSR. Institut metallurgii. Issledova-

niya po zharorpchnym splavam, v. 7, 1961, 29 - 33

TEXT: Using K.A. Osipov's hypothesis (Ref. 3: AN SSSR, 121, no. 4, 1958) on the limiting and alternating values of energy of activation, two limiting values were calculated for α -Fe: $q_{\alpha,\gamma} = 11.7$

kcal/g atom and q = 22.2 kcal/g atom. The value of q corresponds to the limiting value of the energy of activation of slip in the crystal lattice which will be locally melted at those points where this energy value is reached. It can also be shown that q corresponds on the corresponding to the corresponding t ponds to a slip stress of approximately 0.5 μ , i.e. to a stress the value of which is of the same order as Frenkel's theoretical value. Tests were carried out in a BNH-C2 (VPN-S2) machine in which the creep and long-term strength could be studied in vacuo under a con-

Card 1/3

S/659/61/007/000/004/044 D217/D303

Investigating the dependence of ...

stant stress. Specimens of cast and forged iron (99.6 %) were given a preliminary anneal in vacuo (1.10-4 mm Hg) for 10 hours at 700°C; the temperature was then lowered to 450°C and the specimens were soaked there for 50 hours. The investigations were carried out in the temperature range 250-500°C, in which the modulus of normal the temperature range very little, whereas at temperatures above 500°C elasticity changes very little, whereas at temperatures above 500°C elasticity changes very little, whereas at temperatures above 500°C elasticity changes very little, whereas at temperatures above 500°C elasticity changes very little, whereas at temperatures above 500°C elasticity changes very little, whereas at temperatures above 500°C elasticity changes very little, whereas at temperatures above 70°C mm, a trall length of 60 mm, a trall servery length of 500°C mm, a diameter of the working porworking portion of 22 mm and a diameter of the working porworking portion of 3 mm. It was found that on increasing the stress from 10 to 100°C mm. It was found that on increasing the stress from 30 to 35 kg/mm, the energy of activation creasing the stress from 30 to 35 kg/mm, the energy of activation sobtained. At stresses of above 35 kg/mm², the specimens rupture on stressing. The constant value obtained for the energy of activation is on the average 20.3 kcal/g atom, and is considerably greater than the theoretical value of $q_{\alpha,\gamma}$, this being in good agreement with the second theoretical value of q. The great divergence between the theoretical value of q. and the experimental value of 20.3 kcal/g card 2/3

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Investigating the dependence of ...

atom indicates the possibility that the body-centered cubic lattice may transform into a face-centered cubic lattice during plastic tensile deformation. The calculated value of q/atom is close to that of the energy of vacancy formation and has the same order of value as the nuclear energy of dislocations per atomic plane. There are 7 the nuclear energy of dislocations per atomic plane. There are 7 figures, 1 table and 7 references: 5 Soviet-bloc and 2 non-Soviet-figures, 1 table are to the English-language publication reads as follows: J.M. Silcox, Acta metallurgica, 7, 5, 1959.

card 3/3

S/279/63/000/001/020/023 E040/E451

AUTHORS:

Osipov, K.A., Sotnichenko, A.L. (Moscow)

TTTE .

Effect of oxidizing atmosphere and of stress variation on the creep and long-time strength of iron, titanium

and carbon steel

PERIODICAL: Akademiya nauk SSSR. Izvestiya. Otdeleniye

tekhnicheskikh nauk. Metallurgiya i gornoye delo.

no.1, 1963, 181-186

TEXT: The creep and long-time strength of technically pure iron (99.97%), α-Ti (99.97%) and y-8 (U-8) grade carbon steel were investigated under vacuum and in air under various loading conditions. Before tests, the iron and steel specimens were first annealed under a vacuum of 1 x 10⁻⁴ mm Hg for 10 hours at 800°C. Titanium specimens were similarly annealed for 240 hours. An analysis of the creep curves of the specimens tested at 600°C under a stress of 10 kg/mm² showed that the time-to-rupture of the titanium specimens tested in vacuum was reduced by about 2.5 times, that of the iron specimens was reduced by nearly 1.5 times and that of the U-8 steel was reduced by nearly 3 times compared with Card 1/2

S/279/63/000/001/020/023 E040/E451

Effect of oxidizing ..

the corresponding values obtained in tests in air. Tests were also carried out at various temperatures between 430 and 515°C and the creep curves plotted at several test temperatures under vacuum and in air. A graph is also given of the logarithm of the steadystate creep of all the test specimens. Calculations were made of the creep activation energy under various test conditions employed. An oxidizing atmosphere lowers the steady-state creep activation energy of the U-8 carbon steel by 22 kcal/mol and a further reduction of the creep activation energy by 25 kcal/mol results from an increase of the stress and a decrease of the specimen cross-section area during tests. In the case of the iron specimens the effect of both these factors reduces the steady-state creep activation energy by 26 kcal/mol. On the other hand, an oxidizing atmosphere reduces the creep rate of titanium at temperatures below 600°C and increases it at temperatures There are 4 figures and 3 tables. exceeding 600°C.

SUBMITTED: September 13, 1962

Card 2/2

EWP(q)/EWT(m)/BDS--AFFTC/ASD--JD s/0279/63/000/002/0146/0152 ACCESSION NR: AP3000917 AUTHOR: Osipov, K. A. (Moscow); Miroshkina, Ye. M. (Moscow); Sotnichenko, (Moscow) TITLE: Investigation of the creep of a- and a-modifications of Ti-Zr alloys SOURCE: AN SSSR. Izv. otd. tekh. nauk. Metallurgiya i gornoye delo, no. 2, 1963 146-152 TOPIC TAGS: titanium-zirconium alloys, a-alloys, a-alloys, creep, activation energy, creep mechanism ABSTRACT: The creep behavior of α - and β -modifications of polycrystalline Ti-Zr alloys in a vacuum of about 1 x 10⁻⁴ mm Hg under a constant tensile stress has been studied in an effort to determine the mechanism of steady-stage creep. The alloys (25.15, 50.01, and 75.50 at% Zr, 0.006% max N, 0.03% max C and 02, and 0.03% max Fe) were vacuum-arc melted, forged into rods, annealed for 24 hr at 800C and for 168 hr at 450C (alloy with 50 at% Zr) or at 550C (alloys with 25 and 76 at. % Zr). The a-modification alloys were tested at temperatures from Card 1/2

L 11291-63 ACCESSION NR: AP3000917

20 to 200C under a stress of 30 to 70 kg/mm². The activation energy Δ H of the steady-stage creep, determined from ln ϵ -1/T curves (ϵ , rate of the steady-stage creep; T, absolute temperature), was found to be constant at stresses higher than 40-50 kg/mm² (depending on alloy compositions) and equal to 8100, 6900, and 8000 cal/mol for Zr contents of 25, 50, and 75 at%, respectively. These values are very close to the limiting values of activation energy calculated under the assumption that in α -Ti-Zr alloys the creep-induced activated state of atoms or ions corresponds to that of a local allotropic transformation. This leads to the conclusion that the creep of α -Ti-Zr alloys under high stresses is affected by a mechanism directly associated with a local allotropic transformation. Creep tests of the β -modification of Ti-Zr alloys were carried out under a constant tensile strength of 0.5 kg/mm². Analysis of the data obtained shows that the steady-stage creep of the β -modification of Ti-Zr alloys occurs through a mechanism directly associated with melting. Orig. art. has: 2 formulas, 6 figures, and 4 tables.

ASSOCIATION: Institut metallurgii im. A. A. Baykova (Institute of Metallurgy)

SUBMITTED: 29Nov62

DATE ACQ: 12Jun63

ENCL: 00

SUB CODE: ML

Cord 2/2 40 1

NO REF SOV: 012

OTHER: 002

APPROVED FOR RELEASE: 08/23/2000 CIA-RDP86-00513R001652530009-0"

S/2659/63/010/000/0027/0031

ACCESSION NR: AT4013923

AUTHOR: Osipov, K. A.; Sotnichenko, A. L.

TITLE: Investigation of the limiting values of creep activation energy for titanium-zirconium alloys

SOURCE: AN SSSR. Institut metallurgii. Issledovaniya po zharoprochny*m splavam, v. 10, 1963, 27-31

TOPIC TAGS: creep, creep activation, creep activation energy, titanium, zirconium, titanium zirconium alloy

ABSTRACT: The author previously proved that for set creep at high loads the activation energies of a titanium and a zirconium approach a constant limiting value. The present paper includes information on creep of polycrystalline alloys of the titanium-zirconium type. The samples were tested for creep at 25-200C and loads 08 30-70 kg/mm² on a VPN-S2 machine after being hardened in a vacuum arc furnace. The set creep rate (% deformation/min.) was calculated from the curves obtained. The logarithm of the set creep rate was found to be inversely proportional to the temperature for all values of stress (see Fig. 1 in the Enclosure). Analysis of the results showed that in alloys of the titanium-zirconium type in the 4-modification, the nature of the activated state during creep at high

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ACCESSION NR: AT4013923

loads corresponds to a state of "local polymorphic variation." Orig. art. has: 3 figures and 2 tables.

ASSOCIATION: Institut metallurgii AN SSSR (Institute of Metallurgy AN SSSR)

SUBMITTED: 00

DATE ACQ: 27Feb64

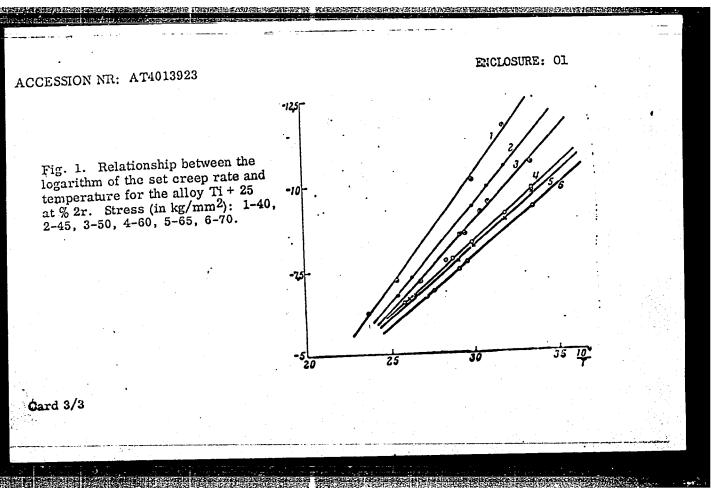
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ACCESSION NR: AT4013935

AUTHOR: Osipov, K. A.; Miroshkina, Ye. M.; Sotnichenko, A. L.

TITLE: An investigation of the set creep of the A-modification of titanium-zirconium alloys

SOURCE: AN SSSR. Institut metallurgii. Issledovaniya po zharoprochny*m splavam, v. 10, 1963, 105-109

TOPIC TACS: titanium, zirconium, creep, A-modification, set creep, titanium zirconium altoy

ABSTRACT: The paper investigates the set creep of A-modifications of titanium-zirconium alloys. These alloys are very interesting theoretically. In the same ways as the A-modifications, they form a continuous row of solid solutions. The chemical composition of the alloys investigated was as follo s: nitrogen 0.006%, carbon 0.03%, oxygen 0.03% and iron up to 0.03%. The tests were performed on a machine described by Berlizov. The samples were 20 mm long, having a working part and a diameter of 14 and 2.5 mm, respectively, and were annealed in a vacuum before testing at 1000C for 24 hours. The tensile stress was constant at

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0.5 kg/mm². Data are given on the creep rate for various titanium-zirconium alloys. Fig. 1 of the Enclosure shows the creep curves for an alloy of titanium with 25 at.% zirconium at various temperatures. Results of the investigation of the set creep rate showed that, in titanium-zirconium alloys of the A-modification the essence of the activated state corresponds to local fusion. Orig. art. has: 4 figures and 6 tables.

ASSOCIATION: Institut metallurgii AN SSSR (Institute of Metallurgy AN SSSR)

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DATE ACQ: 27Feb64

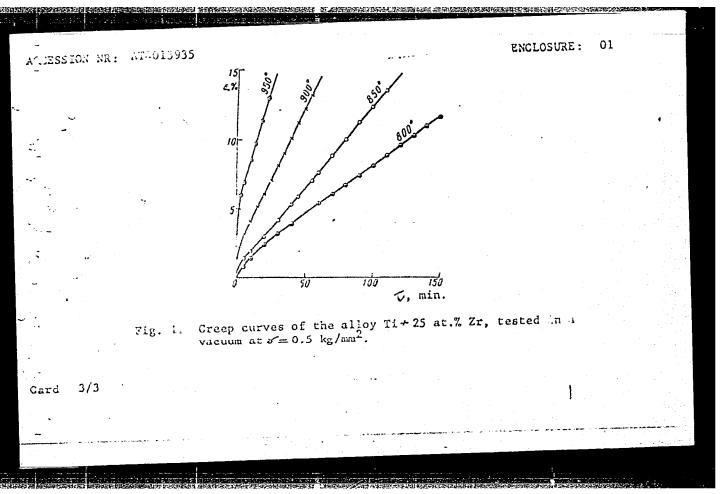
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S/0279/64/000/003/0161/0162 ACCESSION NR: AP4040991 AUTHOR: Osipov, K. A. (Moscow); Sotnichenko, A. L. (Moscow) TITLE: On the duration of tests for creep and rupture strength of metals and alloys SOURCE: AN SSSR. Izvestiya. Metallurgiya i gornoye delo, no. 3, 1964, 161-162 TOPIC TAGS: zirconium creep test, aluminum creeptest, titanium zirconium alloy, alloy creep test, creep test duration, creep test, stress rupture test duration, stress rupture test, zirconium, alumi-ABSTRACT: The effect of the duration of creep tests on the relationship between the rate of secondary stage creep & and rupture life t and the time reciprocal 1/T has been studied in the cases of zirconium iodide vacuum melted alloys of titanium with 50 and 76 at Zr. and 99.99%-pure aluminum. All tests were conducted in a vacuum of 1.10-4 mmHg under constant stress with a test time from 10 to 1500 hr. The test time for iodide zirconium vacuum annealed at 8000 Card : 1 / 2