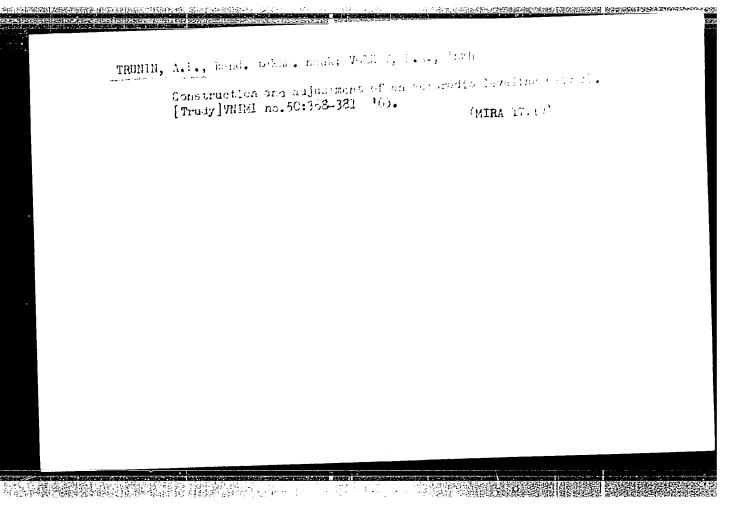
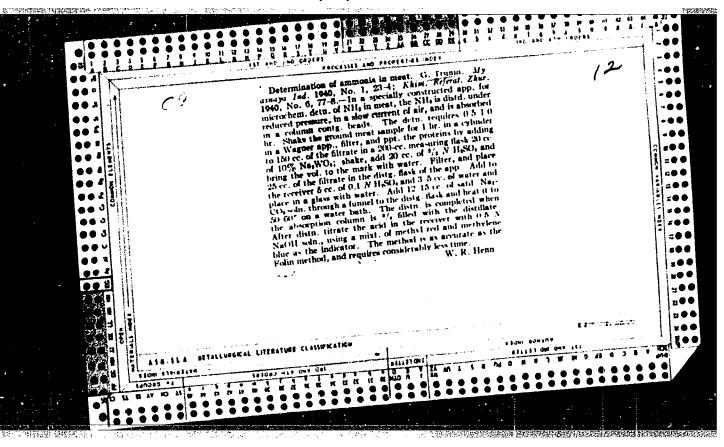
TRUNIN, A.P.; FINAREVSKIY, I.I.; CHISTYAKOV, S.V.; PETUKHOVA, V.A., tekhn. red.

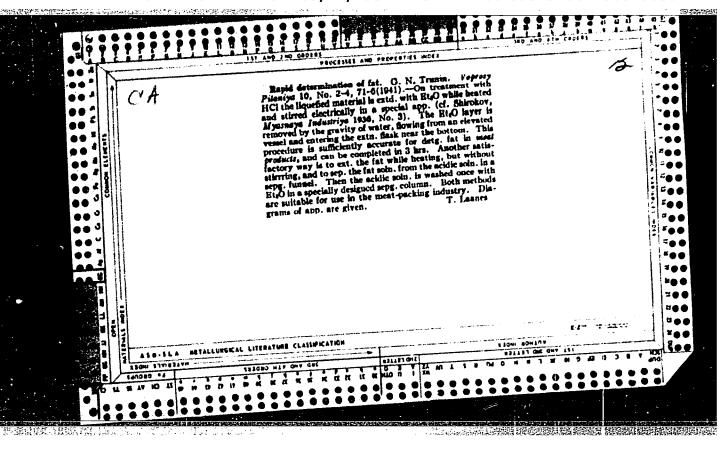
[Practical handbook on large scale phototheodolite surveying]
Fototeodolithaia s"emka v krupnykh masshtabakh; prakticheskoe
rukovodstvo. Leningrad, 1960. 240 p. (MIRA 16:6)

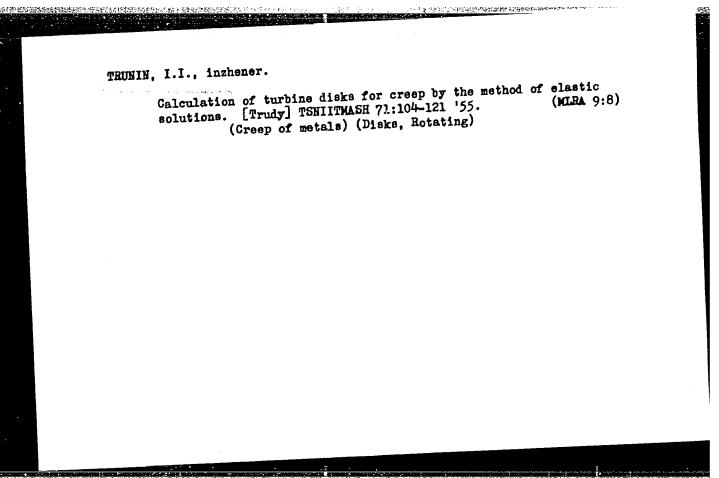
l. Leningrad. Vsesoyuznyy nauchno-issledovatel skiy marksheyderskiy institut. (Photographic surveying) (Theodolites)

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"









SOV/137-57-11-22337

Translation from: Referativnyy zhurnal, Metallurgiya, 1957, Nr 11, p 242 (USSR)

Mirkin, I.L., Trunin, I.I. AUTHORS:

An Investigation Into Creep and the Destruction of Steel in the TITLE:

Zone of Stress Concentration (Issledovaniye polzuchesti i raz-

rusheniya stali v zone kontsentratsii napryazheniy)

V sb.: Prochnost' metallov. Moscow, AN SSSR, 1956, pp PERIODICAL:

117-132

An analysis is provided of the stressed and deformed states ABSTRACT:

of metal and of the process of failure in the creep testing of cylindrical specimens (S) of various degrees of rigidity with annular notches (N). Steels EI-10 and EI-257 are the objects of investigation. Two identical annular N, 40 mm apart, are made on each S to eliminate the mutual influence of unevenly stressed states arising in cross sections of these N. Rigidity is estimated by the stress concentration at the apex of the N and the degree to which the stressed state becomes threedimensional to a point at which this is a real factor. An approx-

imate estimate of the value of the plastic deformation (D) in

each portion of the cross section is made in terms of the Card 1/2

CIA-RDP86-00513R001756820008-4" **APPROVED FOR RELEASE: 03/14/2001**

SOV/137-57-11-22337

An Investigation Into Creep and the Destruction of Steel (cont.)

increase in microhardness relative to its value at the center of the smallest cross section of the S. It is found that at various degrees of stress concentration, various durations and temperatures of testing, a pronounced unevenness in distribution of stresses and of pastic D in the metal beneath the N remains, as does the three-dimensional nature of the stressed state observed during standard tensile testing of notch S at room temperature. Maximum plastic deformation occurs in the layers of metal close to the surface at the bottom of the N. D drops rapidly with distance from the N and radially toward the deeper layers of metal in the direction of the center of the smallest cross section of the S, and a boundary is found between the region of large plastic and small elastic-plastic D. In this zone, at a depth of 0.2-0.4 mm from the bottom of the N, primary loci of failure are found and normal axial stresses attain a peak. Failure always arises and begins to spread from the grain boundaries and is of the nature of cleavage of crystal particles away from each other along their boundaries. L.G.

Card 2/2

加温的探测的现代形式 54.1%。\$14.25%。500

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

O MONTH OF THE PROPERTY OF THE

MIRKIN, I.L., professor, doktor; TRUNIN, I.I., inshener.

"Methods for hot mechanical testing of metals". A.M.Borzdyka.
Beviewed by I.L.Mirkin, I.I.Trunin. Zav.lab.22 no.2:253-255
(MIRA 9:6)

I 156.

(Metals--Testing) (Borzdyka, Anatolli Matveevich)

CIA-RDP86-00513R001756820008-4 'APPROVED FOR RELEASE: 03/14/2001

TRUNIN, I.I.

124-11-13571

Translation from: Referativnyy Zhurnal, Mekhanika, 1957, Nr 11, p 173 (USSR)

Mirkin, I. L., and Trunin, I. I. AUTHORS:

Investigation of the Creep and Failure of Steel in the Stress-Concen-TITLE:

(Issledovani ^{ye}polzychesti i razrusheniya stali v zone tration Zone

kontsentratsii napryazheniy)

V sb.: Ispytaniya i svoystva zharoprochn. materialov, PERIODICAL:

Moscow, Mashgiz, 1957, pp 25-45

The paper describes tests on the creep and continued strength of cylindrical samples with circular notches made of heat-treated steel ABSTRACT:

EI257 or EI10 throughout a temperature range of 550° to 650° C. Having determined the increment of micro-hardness at various points of a longitudinal grind, the Authors have found, with approximation, the zone of maximal plastic deformation. The failure process was analyzed with the aid of microscopic structural analysis of strata-wise grinds. A number of properties established at room temperature remained unchanged under test conditions, namely: a pronounced nonuniformity of the stress distribution and plastic deformation of the

Card 1/2

124-11-13571

Investigation of the Creep and Failure of Steel in the Stress-Concentration Zone . (Continued)

metal underneath the notch; a deformation peak within the nearsurface layers of the metal directly below the furrow of the notch.
The deformation rate drops steeply from the surface layer to the
center of the sample. Inception of failure occurs at a depth of 0.2 to
0.4 mm from the bottom of the notch. The peak of axial stresses lies
near the bottom of the notch and close to the location of incipient
failure. It is deduced therefrom that the normal stress is the determining stress during failure. Through relaxation the peak stresses
diminish somewhat with the passing of time. Failure always occurred
along the grain perimeter.

Bibliography: 8 references.

(V. S. Namestnikov)

Card 2/2

CIA-RDP86-00513R001756820008-4 "APPROVED FOR RELEASE: 03/14/2001

tate Physics - Mechanical Properties of Crystals

E-9

and Poly-Crystalline Compounds

Abs Jour

: Ref Zhur - Fizika, No 1, 1958, 1111

Author

: Mirkin, I.L., Trunin, I.I.

[Central]

: General Scientific Research Institute for Technology and

Machine Building

Title

Inst

: Investigation of the Failure Zone in Creep

Orig Pub

: Metallovedeniye i obrabotka metallov, 1957, No 6, 2-7

Abstract

: It was established experimentally that there is a reduction in the microhardness of the metal near the cracks that occur during creep. This is explained by the crumbling of the material, due to accumulation of vacant sites of the crystalline lattice in places that are located near the visible damage centers. In an investigation of the EIIO steel, the reduction in the hardness, due to

Card 1/2

USSR/Solid State Physics - Mechanical Properties of Crystals E-9

and Poly-Crystalline Compounds

Abs Jour : Ref Zhur - Fizika, No 1, 1958, 1111

crumbling, is observed in a band approximately 100 micron wide. The greatest reduction in the microhardness (the maximum crumbling) reaches 12 -- 14%.

Card 2/2

	TAUN TO THE
	MIRKIN, I.L.; TRUNIN, I.I.
	Statistical method for investigating the destruction zone of metals by measuring microhardness. Zav.lab. 23 no.2:229-235 '57. (MIRA 10:3) 1.TSentral myy nauchne-issledovatel skiy institut tekhnologii 1
	mashinostroyeniya. (Motals-Testing)
)
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TRUMIN, I. I. Cand Tech Sci -- (diss) "Study of the process of disintegration dwynd of steel in dreepage." Mos. 1958. 18 pp (Glavniiproyekt under Gosplan USSR. Central Sci Res Inst of Technology and Machine building TsWIITmash), 150 copies (KL, 36-58, 113)

-43-

AUTHORS: Gel'man, A. S., Griboyedo.a, T. S., Ye. A. Davidovskaya,

Lazare, B. I., Lyubavskiy, K. V., Slepak, E. S., Trunin,

I. I. and Fedortsov-Lutikov, G. F.

TITLE: Investigation of the Steel IXluH12T as TubeMaterial for

Power-generation Equipment (Issledovaniye stali 1Kh18N12T

v kachestve trubnogo materiala dlya energoustanovok)

PERIODICAL: Metallovedeniye i Obrabotka Metallov, 1958, No. 3, pp. 16 - 24 (USSR)

ABSTRACT: For producing tubes operating at super-critical steam parameters, it is necessary to have available a cheap, strong and ductile material which has a stable structure and stable properties at 550 to 650 °C, is not inclined to develop intercrystallite corrosion and possesses good technological properties. The work carried out in 1952 and 1953 by TsNIITMASh jointly with the imeni Ordzhonikidze Works (Ref.1) proved that it was possible to utilize cheap steel of the type IX18H9T for operation at high temperatures. Later, complex investigations were carried out with this steel as a material for tubes of super-critical parameter power-generation equipment. The steel IX18H9T may contain large quantities of ferrite and, after long duration annealing at 600 to 700 °C, it embrittles due to the formation of a 6-phase. Increase in the nickel content

Card 1/4

generation Equipment

to 11-13% brought about an appreciable increase in the stability of the austenite without affecting the high strength. This steel, designated as 1X18H12T steel, does not show any α - or o'-phase separation during ageing at 700 °C for 10 000 hours and at 750 °C for 3 000 hours; only slight quantities of carbides were found to separate out. Thereby, the impact strenght is maintained at 22-24 kg/cm² for this steel, whilst in the case of the steel 1X18H9T, it drops to 9-18 kg/cm^2 . The investigations described in this paper were carried out on commercial tubes, rods and also on laboratory produced steels with compositions as given in Rable 1, p. 16. The results are entered in tables and plotted in graphs. It is concluded that the steel 1X18H12T, containing 0. 08-0.2% C, max. 75% Si, 1-2% Mn, 17-18.5% Cr, 11-13% Ni, max. 0.20% S and max. 0.035%P, is suitable for operation at high temperatures; the Ti content or the steel is thereby determined by means of the formula 5(C-0.02). The best combination of mechanical properties was obtained after annealing at 1 050 to 1 100 °C for 30 min. and cooling in air, and this regime is recommended for tubes as well as for bends. Wled joints should be annealed at 1 000 to 1 050 °C for 1 hour and then cooled in air. The mechanical properties of steels Card 2/4

Investigation of the Steel IX18H12T as Tube Material for Fowergeneration Equipment

> heat-treated in accordance with these recommendations are entered in Table 6, p. 24, for test temperatures of 20, 600, 650 and 700 °C. Practically no embrittlement takes place for this steel after ageing at 600 and 750 °C for durations of 3 000 to 10 000 hours; no o-phase formation could be detected after such ageing for steel containing 12% Ni, whilst under similar conditions, d-phase formation can occur in steel containing 10 % Ni. Preliminary, non-uniform work-hardening influences the ultimate strength of the steel, but does not influence appreciably the ductility in the case of longduration loading. In the case of contact-welding of tubes of superheaters, the strength of non-heat-treated weld joints is not lower than that of the base metal. Steam at 600 °C and long-duration tests for up to 3 000 hours do not affect appreciably the long-duration strength of the steel and of welded joints. The steels 1X18H12T and 1X18H9T are less inclined to develop thermal fatigue than the steel 1X14H14B2M, and the authors recommend using the steel 1X18H12T for tubes of powergenerating equipment, operating with steam of super-critical parameters. There are 5 figures, 6 tables and 8 references, 5 of which are Russian, and 3 English.

Card 3/4

Investigation of the Steel 1X18H12T as Tube Material for Powergeneration Equipment

ASSOCIATION:

TsMIITMASh

AVAILABLE:

Library of Congress

Card 4/4

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

SOV/129-58-11-4/13

AUTHORS: Trunin, I. I., Engineer, and Mirkin, I.L, Doctor of

Technical Sciences Professor.

Investigation of the Creep Failure of Steel TITIE:

(Issledovaniye razrusheniya stali pri polzuchesti)

PERIODICAL: Metallovedeniye i Obrabotka Metallov, 1958, Nr 11,

pp 25-32 (USSR)

記憶/**建設/建設**/建設/基本/基度/表示。

ABSTRACT: The authors studied the failure in the stress concentration zone for three-dimensional tensile forces under creep conditions. In earlier work (Ref 1) the method of static micro-hardness measurements on cuts prepared from the failure zone of notched specimens after long duration strength tests was applied, a method described in another paper of the authors (Ref 2). On the basis of investigating the pearlitic steel EI10 it was shown that the formation of micro and macro-cracks is preceded by a loosening of the metal which is evidenced by a reduced resistance to squeezing inside a radius of 100µ around For verifying earlier obtained the visible failure spot. results, the authors investigated smooth specimens of the steel EI10 and notched specimens of the steels EI257 and 1Kh18N12T. For ferromagnetic materials, the magneto-Card 1/3 metallographic analysis was also used. The measured

Investigation of the Creep Failure of Steel SOV/129-58-11-4/13

micro-hardness values in the zone of influence of the For elucidating entire notch are entered in Table 1. the nature of settling of magnetic particles around visible failure spots, a cut with a visible crack and only small failure foci was magnetised; the magnetic particles settled intensively along the crack and filled up the entire surface of the failure area, see Fig.1. The magneto-metallographic investigations also enabled establishing the existence of a loosening of the material which precedes the formation of visible failure spots. If the defects in the loosened zone are such that heating can heal them, an appropriate heat treatment should bring about an increase of the relative resistance to squeezing

and local disturbances of the magnetic field should To verify this assumption experiments were carried out, the results of which are entered in Table 2; heating to 650°C brings about an increase in the micro-hardness of the metal near to the edge of the crack, whilst the resistance to pressing in of the "healthy" metal remains almost unchanged. On the basis of the results obtained

Card 2/3 by the authors of this paper and comparison of these with

Investigation of the Creep Failure of Steel SOV/129-58-11-4/13

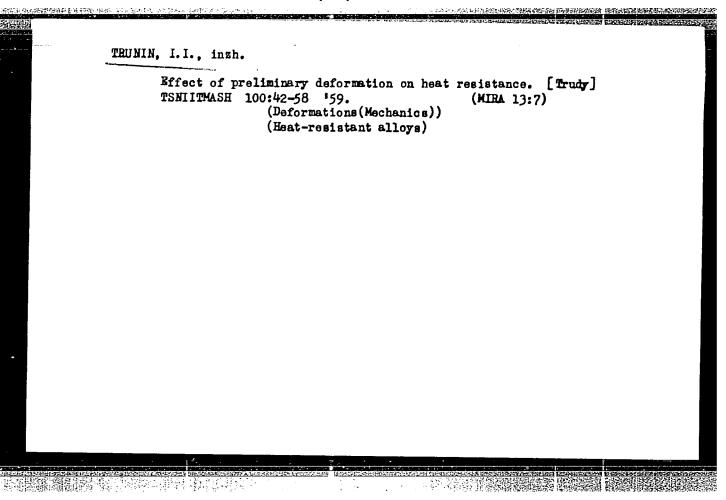
results of experimental and theoretical work of other authors, the following conclusions are arrived at: long duration failure at elevated temperatures is preceded by the formation of a loosened zone with an increased concentration of accumulations of vacancies in the crystal lattice; this process leads to a weakening of the interatomic bond forces in the highest stressed volumes of the metal which brings about favourable conditions for forming nuclei of micro and macro-cracks. There are 4 figures, 2 tables and 14 references, ll of which are Soviet, 3 English.

ASSOCIATION: TENIITMASh

1. Steel--Creep 2. Steel--Failure 3. Steel--Mechanical properties 4. Steel--Test results

Card 3/3

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S/137/61/000/010/031/056 A006/A101

AUTHOR:

Trunin, I.I.

TITLE:

The effect of cold hardening conditions on the durability of steel

PERIODICAL:

Referativnyy zhurnal. Metallurgiya, no.10, 1961, 53, abstract 10Zh338 (V.sb. "Metallovedeniye i term. obrabotka metallov" [Tr. Sektsii metalloved. i term. obrabotki metallov. Tsentr. pravl. Nauchno-tekhn. o-va mashinostroit. prom-sti, no. 2], Moscow, 1960, 12 - 17)

TEXT: The author studied the effect of preliminary deformation by tension, torsion or bending on the durability of cylindrical 1X 18 H12T (1Kh18N12T) steel specimens at 610°C. It is noted that cold hardening resulting from tension increases durability by 10%. Cold hardening by non-uniform tension raises durability by about 20%; cold hardening by torsion by 30% causes a reduction of reference durability limits by about 20%. Cold hardeness by torsion and bending by 15% does not affect noticeably changes in durability at 1,000 - 1,500 hours testing time. The effect of cold hardening on heat resistance of the steel is explained by two factors: 1) mechanical strengthening during cold hardening, connected

Card 1/2

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The effect of cold hardening conditions ...

8/137/61/000/010/031/056 A006/A101

with distortions of the crystal lattice which causes higher durability; 2) activation of diffusion processes, which is connected with an increase in the gradient of stress in the metal and entails the lowering of reference limits of durability.

P. Zubarev

[Abstracter's note: Complete translation]

Card 2/2

S/032/61/027/001/017/037 B017/B054

AUTHORS:

Trunin, I. I., Tseytlin, V. Z., and Zeytman, G. I.

TITLE:

多的發展的關係的特別的特別的

Effect of Interruptions on Stress-rupture Tests

PERIODICAL:

Zavodskaya laboratoriya, 1961, Vol. 27, No. 1, pp. 66-71

TEXT: The authors tested the effect of periodic interruptions on stress-rupture tests of the following steels and alloys: IX18M9T (IKh18N9T), 3M723 (EI 723) (0.22-0.33% C, 2.1-2.5% Cr, 0.90 - 1.10% Mo, 0.3-0.5% V), 3M765 (EI 765) (0.09% C, 14.5% Cr, 1.3% Ti, 5.2% W, 4.2% Mo, 1.94% Al, 0.08%. B, balance Ni), and nickel-chromium alloys in a highly plastic state. Interruption of the stress-rupture endurance test during which the specimen was cooled to room temperature, and then held at this temperature for 24 hrs, had little effect on the course of the curves. A significant effect, however, was produced on specimens that had not been cooled before. IX18M9T (IKh 18N9T) and 3M765 (EI 765) steel specimens were destroyed at the grain boundaries. Most of the materials which had been cooled previously withstood up to 14 interruptions. Only EI 723, which possesses a very high ductility in continuous tests (average reduction of area of 55.8%), showed Card 1/2

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Effect of Interruptions on Stress-rupture Tests

S/032/61/027/001/017/037 B017/B054

lower ductility in interrupted tests. A considerable effect of interruptions on rupture life can be expected in cases where total elongation in continuous tests does not exceed 1%, and when sudden shocklike load removal occurs. Engineer T. A. Bugrov and Senior Technician M. F. Lesnykh (TSNIITMASh = Central Scientific Research Institute of Technology and Machine Building) assisted in the tests. There are 6 figures, 1 table, and 4 references: 3 Soviet and 1 German.

ASSOCIATION: Tsentral'nyy nauchno-issledovatel'skiy institut tekhnologii i mashinostroyeniya (Central Scientific Research Institute of Technology and Machine Building), Taganrogskiy zavod "Krasnyy kotel'shchik" (Taganrog "Krasnyy kotel'shchik"

Plant)

Card 2/2

S/207/62/000/005/010/012 B125/B102

AUTHOR:

Trunin, I. I. (Moscow)

TITLE:

お原理論 選挙令 湯じこと

Creep of heat-resistant steel under a complex state of stress

PERIODICAL:

Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki, no. 5,

1962, 159-162

TEXT: The regularities of creep for complex states of stress where the increase in deformation is constant are studied. Sufficiently reliable values of the constant creep rate were sought for each stress. Most of the tests lasted 2000 hrs. Their results are given in Table 1. The stress intensity σ_i is taken as a measure of the state of stress. Creep is more intense in tension than in torsion. An additional twisting moment slightly reduces the axial rate V of creep in the case of axial normal stress. Under torsion an additional tensile force raises angular velocity of creep. Determining the intensity of plastic deformation intensity of creep. Determining the intensity of plastic deformation intensity affords only a qualitative picture of the process. The creep criterion $V_i = A\sigma_i^n(\tau_{max})^m$ (1) is in good agreement with the experimental results.

S/207/62/000/005/010/012 B125/B102

Creep of heat-resistant steel ...

E.g., this criterion gives the correct rate of creep for 1X18H9T (1Kh16N9T) steel. Despite the lack of sufficient experimental data this criterion is suitable for many substances. Yu. N. Rabotnov and V. S. Nemestnikov are thanked for advice.

SUBMITTED:

February 5, 1962

Table 1. 15X1M1 Φ (15Kh1M1F) steel. Results of test for creep t = 570°C, n = 13.0353, m = -11.4440, logA = -8.8898, stresses in kg/mm², rates in % per hour, values V_{i1} - from measurements, V_{i2} - from the formula (1).

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Card 2/2

s/590/62/105/000/004/015 1031/1242

AUTHORS: Trunin, I.I., Candidate of Technical Sciences,

and Shaban, G.A., Technician

TITLE: Tensile strength of heat-resistant steels under

complex stress conditions

SOURCE: Moscow. Tsentral'nyy nauchno-issledovatel'skiy

institut tekhnologii i mashinostroyeniya. Trudy,

v.105, 1962, 42-56

TELT: There is no reliable method for designing power-plants for service at elevated temperatures. Tensile

strength of steam superheater pipes made of perlitic steel 15 X 1M1Q (15 Kh 1M1F) and austeuitic steel 1X18H12T(1 kh18N12T) was investi-

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\$/590/62/105/000/004/015 1031/1242

Tensile strength of heat-resistant ...

gated under combined tensile and torsional loads. Three sets of specimens were cut from pipes and heat-treated. Each set was tested under different stress conditions: simple tension, simple torsion and a combination of the two. During the rupture test, longitudinal and angular deformation were determined and plotted against time of rupture. The stresses were plotted against time of rupture on a log-log scale. Metallographic inspection revealed intergranular types of fracture, regardless of the kind of stress. If complex stresses are expressed by the half-sum of the total stress plus the greatest principal stress, the creep behavior in combined loading may be determined by a unidirectional tensile test. This conclusion is based on test results which follow the equation:

Card 2/3

祖親基準 公台門 清节

S/590/62/105/000/004/015 I031/1242

Tensile strength of heat-resistant... $\Theta_{k} = A\left(\frac{\sigma_{k} + \sigma_{k}}{2}\right)^{-m}$

where: θ_k = time to rupture; σ_1 = greatest principal stress; σ_1 = total stress. [Abstracter's note: A and m not defined]. Propagation of fracture under oreep conditions in complex state of stresses is faster than under a unidirectional tension load. There are 7 figures and 5 tables.

Card 3/3

S/590/62/105/000/011/015 IQ31/I242

AUTHORS: Trunin, I.I., Candidate of Technical Sciences

and Shaban, G.A., Technician

TITLE: Effect of preliminary deformation on the heat-

resistance of pipe steel

SOURCE: Moscow. Tsentral'nyy nauchno-issledovatel'skiy

institut tekhnologii i mashinostroyeniya. Trudy.

v.105, 1962, 144-164

TEXT: The effect of cold work on creep is determined by the mechanical strenthening resulting from cold plastic deformation and the residual stresses induced during preliminary deformation. This investigation was intended to evaluate the effect

Card 1/2

S/590/62/105/000/011/015 1031/1242

Effect of preliminary deformation...

of non-uniform cold plastic deformation on the creep resistance of perlitic steel 15x 1M 10 (15Kh 1M 1F) and austebitic steels: 94 694 (EI 694), 94 695 (EI 695), and 97 17 (EP17) used in pipe manufacture. The experiments were carried out with untreated specimens; specimens deformed by 15% twisting; specimens deformed by 50% twisting; followed by heat-aging for 3000 hrs at 610°C (EI 694) or 660°C (EI 695). As a result of preliminary deformation both austeuitic and perlitic steels became brittle under long-term stresses. Deformation of 10% and above, at 20°C, had detrimental effect on heat-resistant properties of both steels. In order to recover the initial properties, heat treatment of the parts subjected to cold deformation is recommended. There are 5 figures and 6 tables.

Card 2/2

5/207/63/000/001/014/028 E200/E441

Trunin, I.I. (Moscow)

The many of the colored was subject.

Estimation of creep rupture and some characteristics AUTHOR:

of deformations under complex stress system TITLE:

PERIODICAL: Zhurnal prikladnoy mekhaniki i tekhnicheskoy fiziki,

no.1, 1963, 110-114

The author aims at developing a method which would predict creep for complex stress systems from behavior under uniaxial It is found from tests on tubular specimens that log applied stress oi/log period to fracture curves differ from log first principal stress o1/log period to fracture curves for tensile, torsional and combined loadings. Log $[(\sigma_1 + \sigma_1)/2]/\log$ period to fracture curves for those three loadings compare well and allow one to determine creep rupture under tensile-torsional loading from tensile load rupture curves with inaccuracy not The author confined himself to tests on two steels: pearlite (C = 0.09%, Cr = 1.1%, Mo = 0.9%, V = 0.2%) at 570°C and austenite (C = 0.12%, Cr = 17.5%, Ni - 12%, Ti = 0.7%) The author concludes that time to creep rupture can at 610°C. be obtained from Card 1/2

CONTRACTOR STREET, BEAUTION BEAUTIONS

S/207/63/000/001/014/028 E200/E441

Estimation of creep rupture ...

$$\theta_{\text{hours}} = A \left(\frac{\sigma_1 + \sigma_1}{2} \right)^{\eta}$$

where A and η - constants obtained from uniaxial stress experiments for a given material. He also states that extrapolation is permissible only for intercrystalline fracture. There are 3 figures and 1 table.

SUBMITTED: August 5, 1962

Card 2/2

TRUMIN, I.I.

Evaluation of stress-rupture strength of materials by parametric methods. Zav.lab. 29 no.3:344-352 '63. (MIRA 16:2) (Strength of materials) (Refractory materials)

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

S/032/63/029/003/015/020 B101/B186

AUTHOR:

Trunin, I. I.

TITLE:

A method for determining the plasticity of heat resistant

materials under creep conditions

PERIODICAL:

Zavodskaya laboratoriya, v. 29, no. 3, 1963, 357-363

TEXT: To achieve greater accuracy in estimating deformations in the single creep periods it is suggested to adopt for the primary curves the relation log time versus log relative deformation. This represents the single creep periods by straight lines, so that comparison with the curves log time versus log relative deformation makes it possible to determine the end of the first creep period, the beginning of the intensive destruction and the end of the section with minimum creep rate. Experiments with chromium-nickel-austenitic steel proved a linear relation for all three creep periods in the system log time versus log stress. Similar relations are also valid for log stress versus log deformation rate. It is shown that experimental data offer a basis for finding a desired limit of the long-life strength and of the stress where no

Card 1/2

S/032/63/029/003/015/020 B101/B186

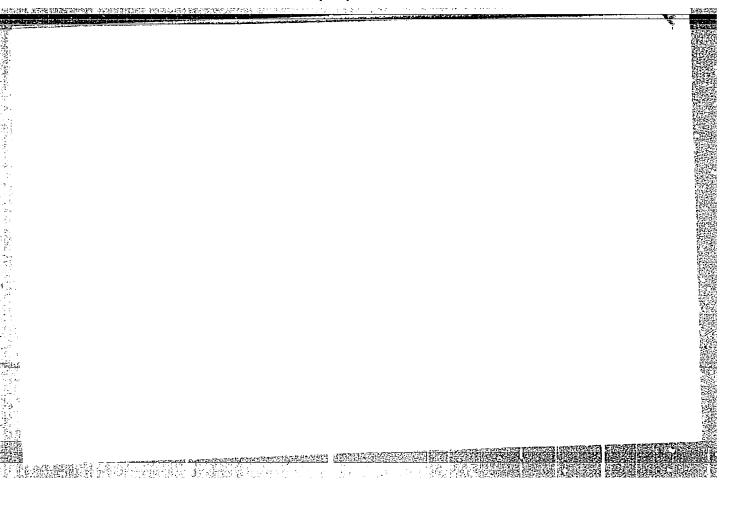
A method for determining the ...

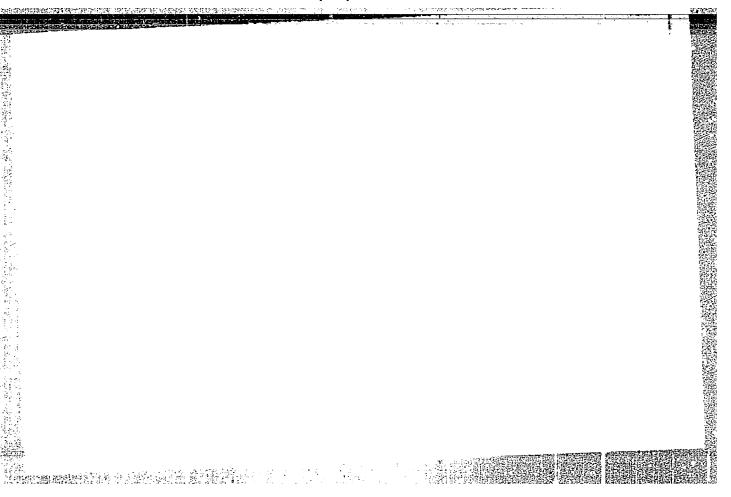
intensive destruction sets in for a chosen life-time. It is pointed out that the method is subject to the same errors as all extrapolation methods. Sometimes deviations from linearity occur, which diminish the reliability of the calculations of the long-life strength. It is recommended, therefore, to collect experimental data by the suggested method and to test their applicability to different materials. There are 3 figures and 2 tables.

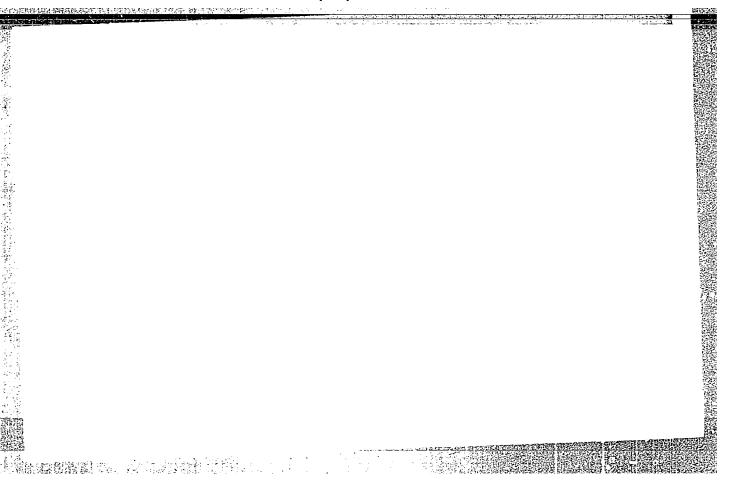
ASSOCIATION: Tsentral'nyy nauchno-issledovatel'skiy institut tekhnologii i mashinostroyeniya (Central Scientific Research Institute

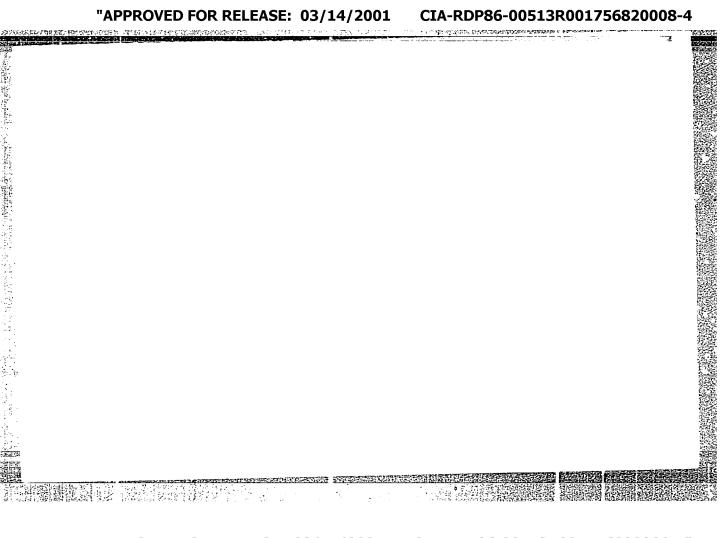
of Technology and Machine Building)

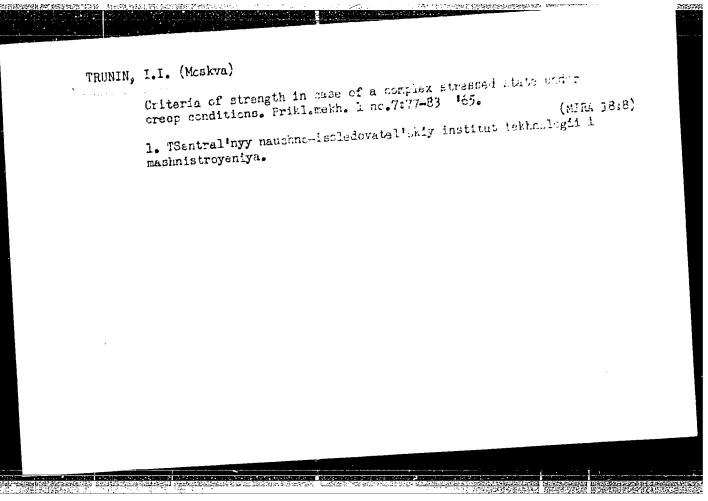
Card 2/2

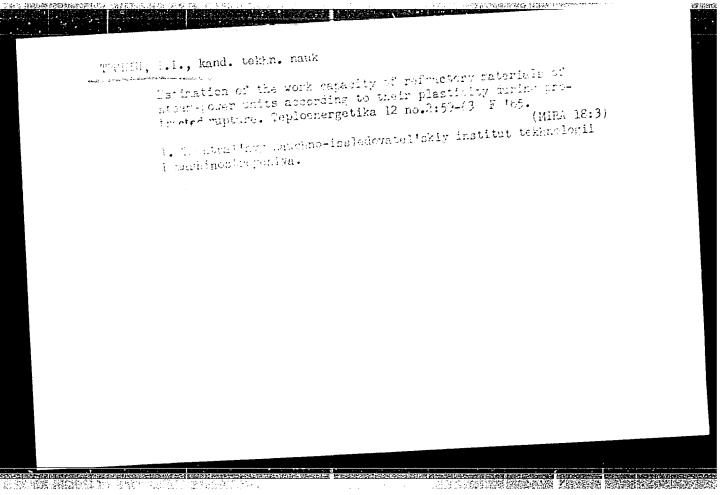


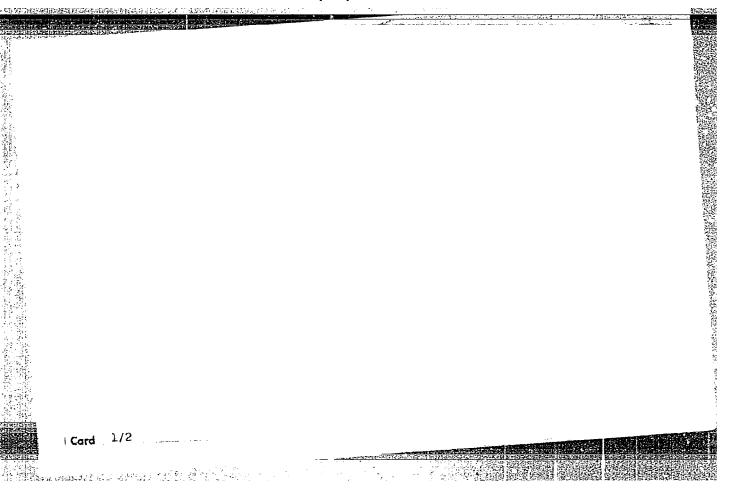




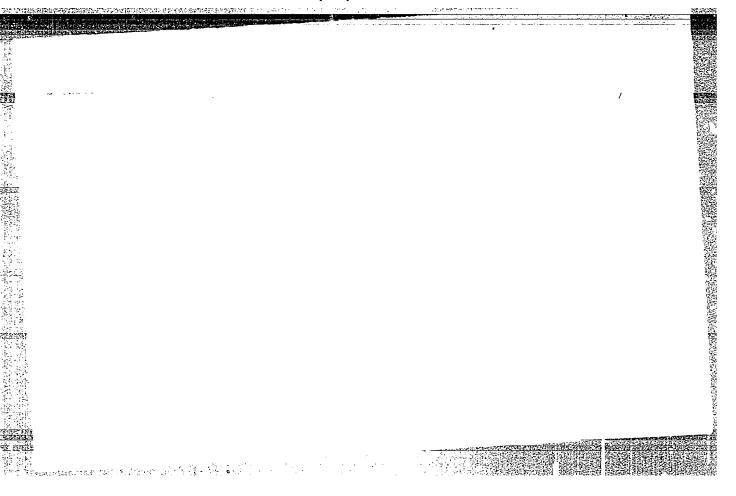








APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"



Possibility of restoring the initial heat-resistance characteristics of materials by intermediate therma treatment. Teploener-tics of materials by intermediate therma (MIRA 18:2) getika ll no.12:5-8 D 64

1. TSentral'nyy nauchno-issledovatel'skiy institut tekhnologii i mashinostroyeniya.

TRUNIN, I.I. (Moscow)

" The criterion of strength in creep under combined stresses"

report presented at the 2nd All-Union Congress on Theoretical and Applied Mechanics, Moscow 29 Jan - 5 Feb 64.

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

GEMINOV, V.N.; TRUNIN, I.I.; TARKHANOV, G.V.; BORZDYKA, A.M.; AYVAZYAN, S.A.

Discussion concerning the interpretation of the results of testing of the stress-rupture strength of a metal of several smeltings.

(MIRA 16:8)

Zav.lab. 29 no.7:827-837 '63.

1. Institut metallurgii im. A.A.Baykova (for Geminov). 2. TSentral'nyy nauchno-issledovatel'skiy i proyektnyy institut tekhnologii i mashinostroyeniya (for Trunin, Tarkhanov). 3. TSentral'nyy nauchno-issledovatel'skiy institut chernoy metallurgii im. nauchno-issledovatel'skiy institut chernoy metallurgii im. I.P.Bardina (for Borzdyka). 4. Matematicheskiy institut im. V.A.Steklova AN SSSR (for Ayvazyan). (Metals—Testing)

GEMINOV, V.N.; TRUNIN, I.I.; TARKHANOV, G.V.; BORZDYKA, A.M.; AYVAZYAN, S.A.

Discussion concerning the interpretation of the results of testing of the stress-rupture strength of a metal of several smeltings.

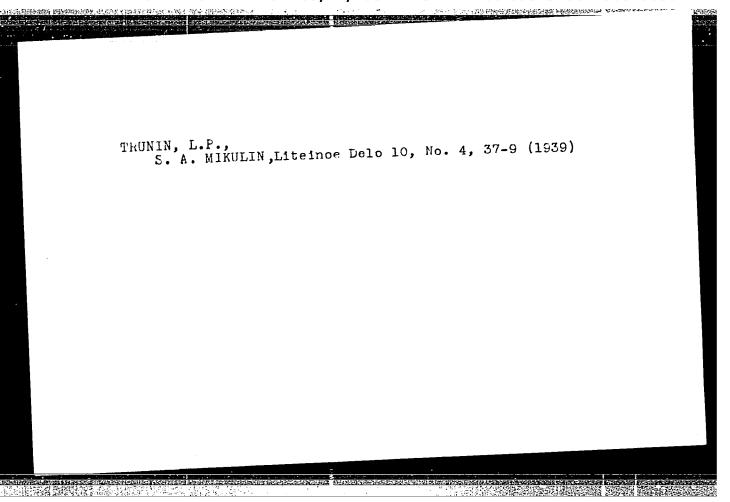
(MIRA 16:8)

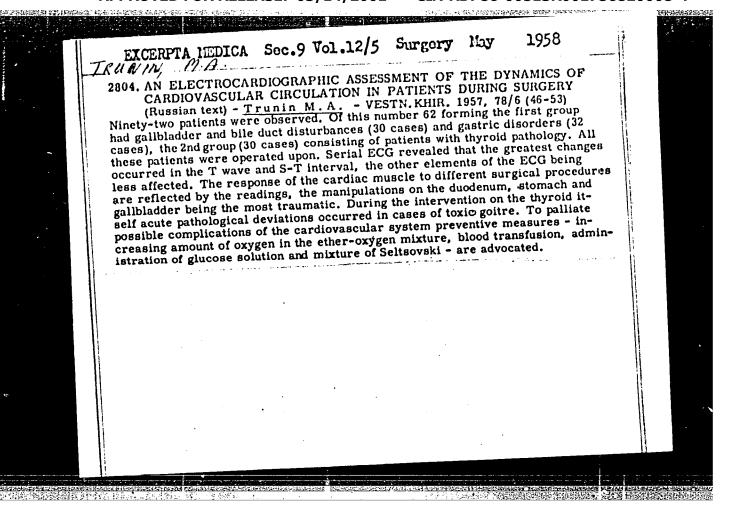
Zav.lab. 29 no.7:827-837 '63.

1. Institut metallurgii im. A.A.Baykova (for Geminov). 2. TSentral'nyy nauchno-issledovatel'skiy i proyektnyy institut tekhnologii i mashinostroyeniya (for Trunin, Tarkhanov). 3. TSentral'nyy nauchno-issledovatel'skiy institut chernoy metallurgii im. nauchno-issledovatel'skiy institut chernoy metallurgii im. I.P.Bardina (for Borzdyka). 4. Matematicheskiy institut im. V.A.Steklova AN SSSR (for Ayvazyan). (Metals-Testing)

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

医多次连续 编数 医唇 经生工





KOPOSOV, Ye.S.; TRUNIN, M.A.; PECHENKIN, A.L.

Plastic materials in surgical clinical practice. Truly ISGH 59: 43-47 160.

1. Gospital'naya khirurgichoskaya klinika Leningradskogo sanitarnogigiyenicheskogo meditsinskogo instituta (zav. klinikoy - prof. A.V. Smirnov) i Leningradskiy nauchno-issledovatel'skiy institut polimeri-zatsionnykh plastmass (dir. instituta - N.M.Yegorov).

(PLASTICS) (SURGERY, PLASTIC)

CIA-RDP86-00513R001756820008-4" **APPROVED FOR RELEASE: 03/14/2001**

"APPROVED FOR RELEASE: 03/14/2001

CIA-RDP86-00513R001756820008-4

TRUNIN, M.A., kand.med.nauk

Some data on polyvinylpyrrolidone, a synthetic highly molecular (MIRA 14:9)

compound. Trudy LSGMI 59:39-42 '60.

1. Gospital'naya khirurgicheskaya klinika Leningradskogo sanitarno-gigiyenicheskogo meditsinskogo instituta (zav. klinikoy - prof. A.V.Smirnova).

(PYRROLIDINONE)

NIKITIN, G.D., dotsent; TRUNIN, M.A., kand.med.nauk

Reimplantation and primary dermatoplasty in extensive skin avulsions of the leg and hip. Trudy LSGMI 59:59-63 '50. (MIMA 14:9)

1. Gospital 'naya khirurgicheskaya klinika Leningradskogo sanitarno-gigiyenicheskogo meditsinskogo instituta (zav. klinikoy - prof. A.V.Smirmov).

(EXTREMITIES, LOWER—WOUNDS AND INJUMIES) (SKIN GRAFTING)

TRUNIN, M. A., kand. med. nauk

位据基件数据行为中心。

Hemodynamic changes in renal and ureteral diseases in connection with surgical treatment. Urologiia no.6:14-20 (MIRA 15:4)

1. Iz khirurgicheskoy kliniki (zav. - zasluzhennyy deyateli nauki prof. A. V. Smirnov) Leningradskogo sanitarno-gigiyenicheskogo meditsinskogo instituta.

(BLOOD_CIRCULATION) (KIDNEYS_DISEASES) (URETERS_DISEASES)

CIA-RDP86-00513R001756820008-4" **APPROVED FOR RELEASE: 03/14/2001**

TRUNIN, M.A.; DAVIDENKOVA, V.V.

Prolonged peridural anesthesia with the use of polyvinyl pyrrolidone. Eksper. khir. i anest. 9 no.5:82-84 S-0 64. (MIRA 18:11)

1. Klinika obshchey khirurgii No.1 (zav. - prof. A.V. Smirnov) Leningradskogo sanitarno-gigiyenicheskogo meditsinskogo instituta i Leningradskiy institut vysoko-molekulyarnykh soyedineniy AN SSSR.

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

KOPOSOV, Ye.S. (Leningrad, Moskovskiy pr. d.50, kv.3); TRUNIN, M.A.; LESHCHINSKAYA, A.F.

Follow-up and successive treatment of goiter in the polyclinic (MIRA 15:1) and hospital. Vest.khir. no.1:45-52 '62.

1. Iz gospital noy khirurgicheskoy kliniki (zav. - prof. A.V. Smirnov) Leningradskogo sanitarno-gigiyenicheskogo meditsinskogo instituta i endokrinologicheskogo kabineta polikliniki No.16 (gl. vrach - A.F. Glebushko) g. Leningrada. (GOITER)

TRUNIN, M.A., kand.med.nauk

Diffuse peritonitis. Trudy LSCMI 59:251-254 '60. (MIRA 14:9)

1. Gospital 'naya khirurgicheskaya klinika Leningradskogo sanitamogigiyenicheskogo meditsinskogo instituta (zav. klinikoy - prof.
A.V.Smirnov). (PERITONITIS)

Modification of the "Rekord" syringe for extensive infiltration
anesthesia. Trudy ISCAU 59: 320-321 '60.

1. Gospital'naya khirurgicheskaya klinika Leningradskogo sanitarnogigtyenicheskogo meditsinskogo instituta (sav. klinikoy - prof.
A.V.Smirnov).

(ANESTHESIOLOGY-APPARATUS AND INSTRUMENTS)

MARTINCHEV, A.N., kand.med.nauk

TRININ, M.A., kand.med.nauk

Surgery on patients in the middle and advanced age groups. Vest.khir.

(MIRA 13:1)

83 no.8:57-64 Ag '59.

1. Iz gospital'noy khirurgicheskoy kliniki (zav. - prof. A.V. Smirnov)

Leningradskogo sanitarno-gigiyenicheskogo meditsinskogo instituta.

(SURGERY, OPERATIVE in old age)

TRUMIN, M. A.

TRUNIN, M. A.: "Dynamic investigation of the cardiove scular system in surgical patients (using the method of electrocardiography)." Min Health RSFSR. Leningrad Sanitary-Hygiene Medical Inst. Leningrad, 1956. (Dissertation for the Degree of Candidate in Medical Sciences.)

Source: Knizhnaya letopis! No h0 1956 Moscow

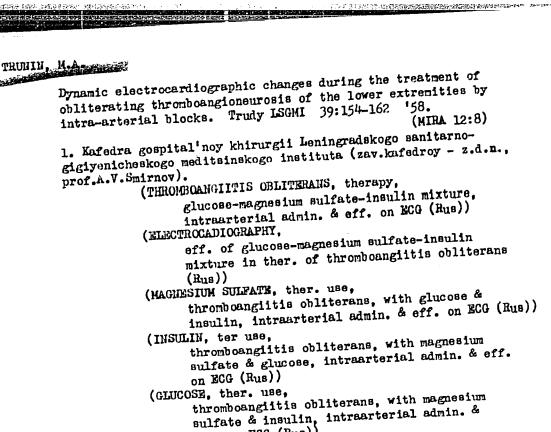
TRUNIN, M.A.

Dynamic examination of the cardiovascular system in surgical patients using electrocardiography [with summary in English, p.158]. Vest. khir. 78 no.6:46-53 Je '57. (MIRA 10:8)

1. Iz gospital'noy khirurgicheskoy kliniki (zav. - prof. A.V.Smirnov)
Leningradskogo sanitarno-gigiyenicheskogo meditsinskogo instituta.
Adres avtora: Leningrad, bol'nitsa im. Mechnikova, 15-y pavil'on.
(ELECTROCARDICGRAPHY, in various dis.

in preop. care)
(HYPERTENSION, prev. and control
control in preop. care)
(PREOPERATIVE CARE
ECG & control of hypertension)

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"



eff. on ECG (Rus))

Indications for surgical removals of foreign bodies from intestines. Vest. khir. 77 no.1:117 Ja '56 (MIRA 9:5)

1. Iz gospital noy khirugicheskoy kliniki (saveduyushchiy professor A.V. Smirnov) leningradskogo sanitarno-gigiyenicheskogo meditsinskogo instituta.

(ABDOMEN--SURGERY) (INTESTINES--FOREIGN BODIES)

MARTYNCHEV, Anatoliy Nikolayevich; NIKITINA, Nadezhda Ivanovna;

TRUNIN, Mikhail Aleksandrovich; TAL'MAN, I.M., red.;

SAFRONOVA, I.M., tekhn. red.

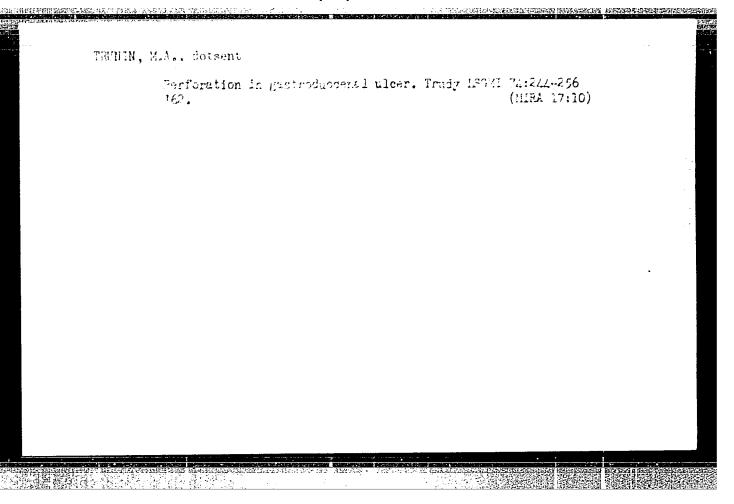
[Venous pressure in a surgical clinic] Venoznoe davlenie v

khirurgicheskoi klinike. Pod red. A.N.Martyncheva. Leningrad,
Medgiz, 1963. 123 p.

(BLOOD PRESSURE) (OPERATIONS, SURGICAL)

KOFOGOV, Ye.S., kand. med. rank; TERMIN, M.A., kand. med. rank
the of a biological antisopula tampon in hile duct surges; and
trannatology. Trudy ISCMI 72:172-176 162.

(MIRA 17:10)



AUTHOR:

Trunin, N.

SOV/2-58-11-16/18

TITLE:

A Regional Meeting of the Chairmen of Cooperative Committees with Regard to the All-Union Census (Krayevoye soveshchaniye predsedateley komissiy sodeystviya Vsesoyuznoy perepisi naseleniya)

PERIODICAL:

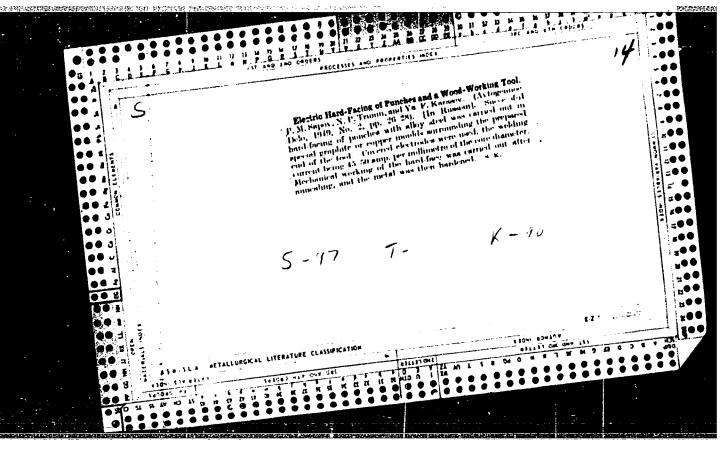
Vestnik statistiki, 1958, Nr 11, p 87 (USSR)

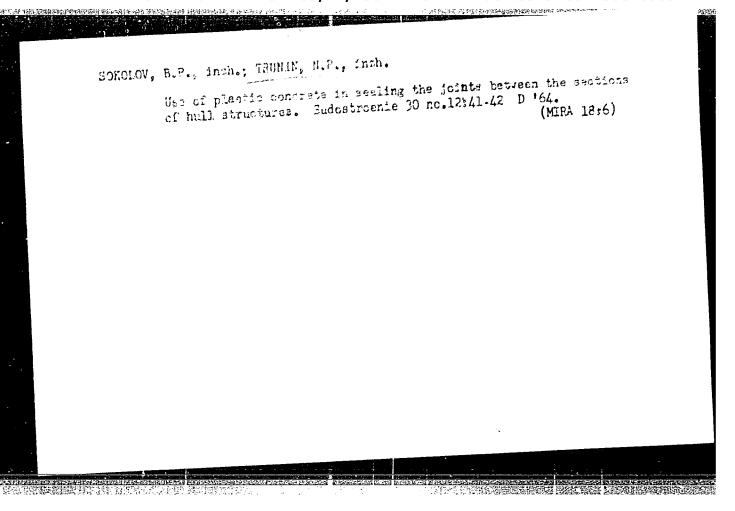
ABSTRACT:

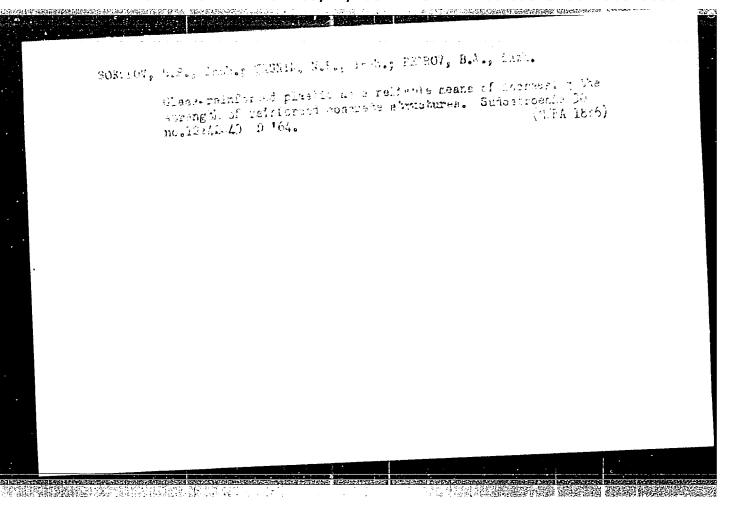
On the 30th of October 1956, a meeting of the chairmen of the cooperative committees took place in Krasnodar; at this meeting the preparations for the forthcoming census were discussed. The Chief of the Regional Board of Statistics, D. A. Kolyako, reported on the present situation, the measures taken in the kray, and on the tasks of the cooperative committees. The second Kraykom Secretary of the KPSS, M.S. Velichkin, stressed the political and economic significance of the census and called upon those present to prepare better the census and to carry it out in an exemplary manner.

Card 1/1

CIA-RDP86-00513R001756820008-4" APPROVED FOR RELEASE: 03/14/2001







TRUNIN, N. P.

TOOL P7 M7 SAPOV. N.P. TRUNIN, AND YA. F. KARASEV. (AVTO. DE.O. 1949, No. 2, pp/ 26-28) (In ussian) Success ful hard facing of punches with alloy steel was car ied out in speci 1 graphite or copper moulds surrounding the prepared end of the tool. Covered electrodes were used, the welding current being 45-50 amp/per millimetre of the core diameter. Mechanical working of the hard-face was carried out after annealing, and the metal was then hardened. Sk

TRUNIN. N. P., SAFOV, P. M., KARASEV, Ya. F.

Laboratory Welding Instruments, Rost Agricultural Machine Works, -c1949-.

Engineer

"Electrosmelting of punching dies and woodworking tools," Avtogen. Delo, No. 2, 1949

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

SAFOV, P. M., TRIMIN, N. P., MARASSIV, Ya. F.

Laboratory Welding Instruments, Rost Agricultural Machine Morks, -c1949-.

Engineer

"Electrosmelting of punching dies and woodworking tools," Avtogen. Delo, No. 2, 1949

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

SAPOV, P. H., TRUNID. N. P., KANASEV, Ya. F.
Laboratory Welding Instruments, Rost Agricultural Machine Works, -c1949-.

Engineer

表情情**想**的特殊。在1975年,至1975年,

"Electrosmelting of punching dies and woodworking tools," Avtogen. Delo, No. 2, 1949

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

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KURNYCHEV, Yevgeniy Fedorovich; TRUNIN, W.P., dots., retsenzent;
SAAK'YAN, Yu.A., red.; BOROVINSKAYA, L.M., tekhn. red.

[Handbook for the adjusters of machine tools] V pomoshch'
nastroishchiku metallorezhushchikh stankov. Rostov-na-Donu,
Rostovskoe knizhnoe izd-vo, 1963. 122 p. (MIRA 16:10)

(Machine tools)

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001756820008-4"

SOV/20-121-1-17/55

AUTHORS:

Trunin, R. F. Al'tshuler, L. V., Bakanova, A. A.,

TITLE:

Phase Transformations When Mater Is Compressed by Strong Shock Waves (Fazovyve prevrashcheniya pri szhatii vody sil'-

nymi udarnymi volnami)

PERIODICAL:

Doklady Akademii nauk SSSR, 1958, Vol. 121, Mr 1,pp. 67-69

(USSR)

ABSTRACT:

This paper gives a report on the shock-like compression of water in the range of prescures from 20 000 to 800 C00 atmospheres. On this occasion the kinematic parameters of the shock wave, namely, its velocity of propagation D and mass velocity U of matter behind the wave front, were measured. Because of the laws of conservation of mass and momentum these parameters are connected with the density of the shocklike compression $Q = Q_0 D/(D - U)$ and with the pressure $P = Q_0 DU$; Q_0 denotes the density of matter before the com-

pression. The method of investigation can be simplified very much when the shock wave is lead to the layer of the substance to be investigated through shields of a material with known

Card 1/2

SOV/20-121-1-17/55

Phase Transformation Then Water Is Compressed by Strong Shock Waves

Hugoniot (Gyugonio) adiabatic line of the shock compression. The quantities measurable by experiment are the speed of the shock waves in the shield and in water. The dynamical adiabatic line of water consists of two sections which with their ends fix the region of phase transition. The existence of the phase transition is also proved by the decrease in transparency of water when a shock wave of sufficiently high parency of water when a shock wave of sufficiently high amplitude of pressure P > P₁ goes through. In the case of shock waves with an amplitude of pressure P < P₁ the transparency does not change. There are 4 figures and 5 references,

1 of which is Soviet.

January 17, 1958, by Yu. B. Kharitonov, Member, Academy of PRESENTED:

Sciences, USSR

November 26, 1957 SUBMITTED:

2. Water--Properties 3. Phase transitions

1. Water--Pressure 4. Shock waves-Velocity 5. Shock waves-Physical effects

Card 2/2

82415

S/056/60/038/03/14/035 B006/B014

24.5300 AUTHORS: Al'tshuler, L. V., Kormer, S. B., Bakanova, A. A., Trunin, R. Fequation of State for Aluminum, Copper, and Lead in the High-

TITLE:

PERIODICAL:

Zhurnal eksperimental'noy i teoreticheskoy fiziki, 1960, Vol. 38, No. 3, pp. 790-798

TEXT: In the present paper, the authors discuss the conclusions applying to aluminum, copper, and lead, as result from an equation deviating from the aluminum, copper, and lead, as result from an equation considered by the authors Mie - Grueneisen solid-state equation. The equation considered by the authors deviates in that it holds within a wide pressure- and temperature range, and deviates in that it holds within a wide pressure- and temperature range, and that the thermal electron components of energy and pressure are taken into that the thermal electron components of energy and pressure compression of account. Moreover, data are furnished concerning dynamic compression of aluminum up to pressures of 2.10° atm, and results of new measurements of aluminum up to pressures of 2.10° atm, and iron at 10°, 2.10°, and 4.10° atm the compressibility of copper, lead, and iron at 10°, 2.10°, and 4.10° atm are offered. Numerous theoretical and experimental details concerning the are offered. Numerous theoretical and experimental details concerning the adiabatics of these three metals are discussed in the introduction, with special regard to the collision adiabatics (Ye, I, Zababakhin, Yu, F, Card 1/3

62415

Equation of State for Aluminum, Copper, and Lead S/056/60/038/03/14/033 in the High-pressure Range S/056/60/038/03/14/033

Alekseyev). Ansatzes for the equation of state and internal energy have the form $P = P_{int} + P_{therm} + P_{exc}$ and $E = E_{int} + E_{therm} + E_{exc}$ (2). The first terms of these sums characterize the interaction of atoms at $0^{\circ}K$, the second terms are thermal ones determined by lattice vibrations, and the third terms are determined by the thermal excitations of electrons. In the following, the various terms are written down explicitly; and finally, the following explicit expressions are obtained for pressure and temperature:

$$P = P_{int} + \frac{\delta_p^2 C_{vp}}{v} \left[T - T_o + E_o / C_{vp} \right] + \frac{1}{4} ?_o \beta_o \left(v_o / v \right)^{1/2} T^2 \text{ and}$$

$$E = \begin{cases} v_{\text{ok}} \\ p_{\text{int}} dv + E_{\text{o}} + C_{\text{vp}} (T - T_{\text{o}}) + \frac{1}{2} \beta_{\text{o}} (v/v_{\text{o}})^{1/2} T^{2} \\ p_{\text{int}} dv + E_{\text{o}} + C_{\text{vp}} (T - T_{\text{o}}) + \frac{1}{2} \beta_{\text{o}} (v/v_{\text{o}})^{1/2} T^{2} \\ p_{\text{int}} dv + E_{\text{o}} + C_{\text{vp}} (T - T_{\text{o}}) + \frac{1}{2} \beta_{\text{o}} (v/v_{\text{o}})^{1/2} T^{2} \\ p_{\text{int}} dv + E_{\text{o}} + C_{\text{vp}} (T - T_{\text{o}}) + \frac{1}{2} \beta_{\text{o}} (v/v_{\text{o}})^{1/2} T^{2} \\ p_{\text{int}} dv + E_{\text{o}} + C_{\text{vp}} (T - T_{\text{o}}) + \frac{1}{2} \beta_{\text{o}} (v/v_{\text{o}})^{1/2} T^{2} \\ p_{\text{o}} dv + p_{\text{o}} d$$

for the dynamic adiabatics $P_G = \sum_{a_k} (G - 1)^k$, dynamic experiments permitted a determination of pressure P_G and also of energy $E_G = E_0 + \frac{1}{2} P_G (v_0 - v)$. Results of computations for aluminum are given in Table 5, for copper in Table 6, and for lead in Table 7. As is shown by Figs. 1 and 2, thermal

Card 2/3

921:15

Equation of State for Aluminum, Copper, and Lead in the High-pressure Range

S/056/60/038/03/14/035 B006/B014

pressure plays an important part in the compression of metals by strong shock waves. For the pressures 216.10¹⁰ bars (Al), 388.10¹⁰ bars (Cu), and 401.10¹⁰ bars (Pb), the thermal pressure components amounted to 59.10¹⁰, 115.10¹⁰, and 124.10¹⁰ bars. For the same pressures, the thermal energy component was 57% (Al), 60% (Cu), and 69% (Pb). Finally, the authors thank ponent was 57% (Al), 60% (Cu), and 69% (Pb). Finally, the authors thank A. I. Funtikov, R. V. Malyshev, and I. P. Dudoladov, as well as Professor K. A. Semendyayev for their assistance, advice, and discussions. L. D. Landau is also mentioned in this article. There are 2 figures, 7 tables, and 14 references, 4 of which are Soviet.

SUBMITTED:

Cctober 7, 1959

Card 3/3

34000

s/056/62/042/001/015/048

B104/B102

18.8100

Al'tshuler, L. V., Bakanova, A. A., Trunin, R. F. AUTHORS:

TITLE:

Shock adiabats and zero isotherms of seven metals at high

pressures

PERIODICAL:

Zhurnal eksperimental'noy i teoreticheskoy fiziki, v. 42,

no. 1, 1962, 91-104

TEXT: The wave velocity D and the mass velocity U behind the shock-wave front were measured in Fe, Ni, Cu, Zn, Cd, Sn, and Pb. Pressure and degree of compression were determined from $P = Q_0DU$ and $\sigma = D/(D-U)$.

passing from the shock adiabat to the zero isotherm, the following simple equations were obtained for pressure and energy:

$$P_{x}(\delta) = Q[\delta^{1/2} \exp\{q(1-\delta^{-1/2})\} - \delta^{1/2}],$$

$$E_{\mathbf{x}}(\delta) = (3Q/\rho_{0k})[q^{-1}\exp\{q(1-\delta^{-1/s})\} - \delta^{1/s}]$$

where Q and q are unknown constants, δ = $v_{_{\mbox{\scriptsize 0}}}/v,$ v being the specific volume,

Card 1/5

我們當到的描述[15]。 1974年 于一日時,但是由于

34000 5,056/62/042/001/015/048 B104/B102

Shock adiabats and zero isotherms...

and $v_0 = v$ at P = 0 and $T = T_0$. In the case of ionic compounds, the first terms in (5) determine the ionic repulsion potential and the second terms determine the Coulomb attraction. In the case of metals, the positive and the negative term in (5) express the repulsive and the attractive forces, respectively. Similar equations were obtained for transition metals in the same way. Shock adiabats and zero isotherms were approximated by a suitable combination of Q and q (Figs. 5 and 6). Using the equation $P_{x, extra} = b + B(\sigma - a)^n$, the zero isotherms were extrapolated into pressure and density ranges, to which quantum statistical methods are applicable. The extrapolation constants are presented in Table 8.

K. K. Krupnikov, M. I. Brazhnik (ZhETF, 34, 886, 1958), S. B. Kormer, V. D. Urlin, L. T. Popova (FTT, 3, 223, 1961), V. S. Zharkov, and V. A. Kalinin (DAN SSSR, 135, 811, 1960) are mentioned. V. N. Zubarev is thanked for his assistance in interpreting experimental data, M. I. Brazhnik, A. A. Gubkin, and I. P. Dudoladov for their help in experiments and calculations, and S. B. Kormer and V. D. Urlin for discussions. There are 9 figures, 8 tables, and 14 references:

Card 2//52

34000 s/056/62/042/001/015/048 B104/B102

Shock adiabats and zero isotherms...

9 Soviet-bloc and 5 non-Soviet-bloc. The four most recent references to English-language publications read as follows: R. G. McQueen, S. P. Marsh. J. Appl. Phys. 31, 1253, 1960; J. M. Walsh et al. Phys. Rev. 108, 196, 1957; J. J. Gilvarry. Phys. Rev. 102, 317, 1956; J. S. Dugdale; D. K. McDonald. Phys. Rev., 89, 832, 1953.

SUBMITTED: August 10, 1961

Table 1. Experimental results. Legend: (1) shock-wave parameters.

Table 2. Experimental results. Legend: (1) material of impact mass; (2) velocity of impact mass.

Table 8. Extrapolation constants.

Fig. 5. Shock adiabats and zero isotherms of Ni and Zn.

Fig. 6. Shock adiabats and zero isotherms of Fe.

Card 3/52

TRUNIN, R.F.
AID Nr. 971-19 20 May
IMPACT COMPRESSIBILITY OF Ti, Mo, Ta, and Fe (USSR)

Krupnikov, K. K., A. A. Bakanova, M. I. Brazhnik, and R. F. Trunin. IN: Akademiya nauk SSSR. Doklady, v. 148, no. 6, 21 Feb 1963, 1302-1305.

S/020/63/148/006/012/023

The impact compressibility of Ti, Mo, and Ta at pressures up to $5 \cdot 10^6$ atm, and of Fe at a pressure of ~ $9 \cdot 10^6$ atm, has been determined. The pressure was generated by shooting aluminum plates at a velocity of 5600 m/sec or steel pins at a velocity of 8640 or 9100 m/sec onto test specimens 3-4 mm thick which were shielded by an Al or Fe shield. The pressure and the degree of compression were calculated from the experimentally determined velocity D of the shock wave. The state of impact compression and the values of pressure P and mass velocity behind the front of shock wave U were determined graphically. The compression density ρ was calculated from the equation $\rho_0 D = \rho(D-U)$, where ρ_0 is the initial density. From the obtained shock-wave parameters the adiabatic curves for shock waves and zero isotherms were calculated and plotted.

Card 1/1

SOURCE CODE: UR/0387/65/000/009/0001/0012 EWT(1) L 9433-66 ACC NR: AP5025074 AUTHORS: Trunin, R. F.; Gon'shakova, V. I.; Simakov, G. V.; Galdin, N. Ye. 4 44,55 44,55 TITLE: A study of rocks under the action of the high pressures and temperatures of shock compression SOURCE: AN SSSR. Izvestiya. Fizika Zemli, no. 9, 1965, 1-12 TOPIC TAGS: geophysical research, geophysics, earth science, earth crust, seismology, PETROLOGY ABSTRACT: A discussion of the results obtained in an experimental study of the shock compressibility of alkaline and ultra-alkaline rocks under various pressures is presented. The theoretical sequence of transitions in the structure of the earth's mantle (see A. E. Ringwood. Mineralogical Constitution of the Deep Mantle, J. Geoph. Res., 67, No. 10, 1962) is discussed in some detail. Eleven alkaline and ultra-alkaline rocks (mineral groups of magnesium, plagioclase, titano-magnetite, chromite, biotite, and serpentine) were used as test specimens. UDG: 550.311;539.89 Card 1/3

L 9433-66

ACC NR: AP5025074

A table showing the mineral content and density of the rock specimens is included. The method of determining the dynamic compressibility of the substances is based upon the measurement of the kinematic parameters of shock waves: the velocity of propagation of the wave D and the mass velocity of motion of the substance beyond the front U. These quantities are related to pressure according to

$$P = \rho_0 DU$$

and to the degree of compression according to $\sigma = \frac{\rho}{\rho_0} = \frac{D}{D-U} \, ,$

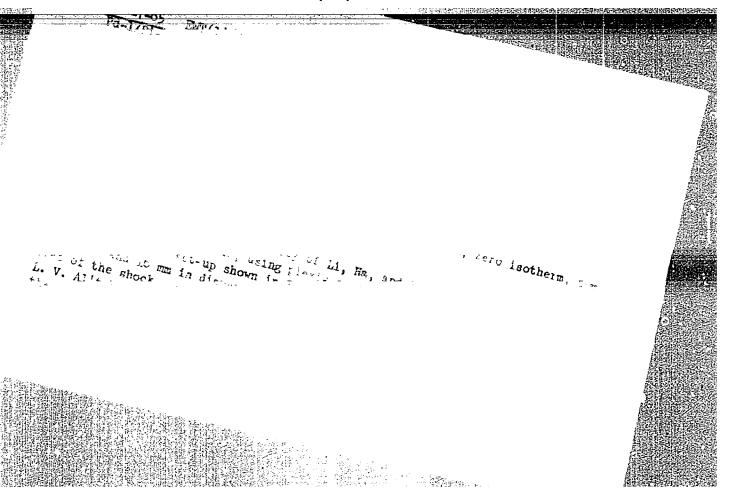
$$\sigma = \frac{\rho}{\rho_0} = \frac{D}{D - U},$$

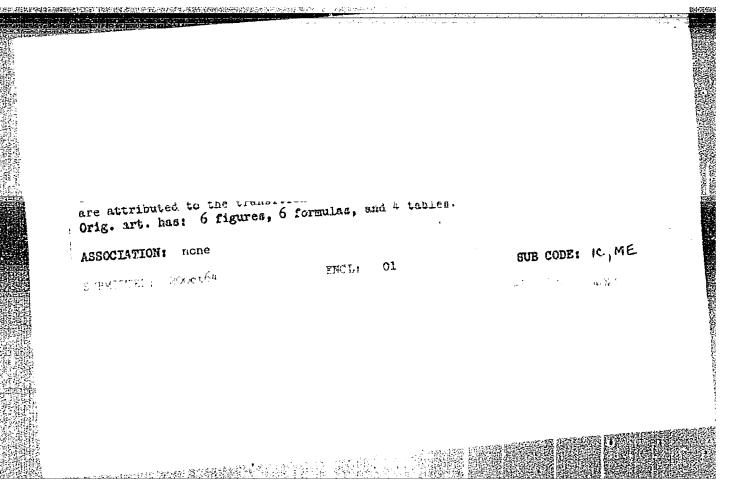
where O is the initial density and O is the density beyond the shock front. The experimental technique of measuring the dynamic compressibility follows the method of reflection (L. V. Al'tshuler, K. K. Krupnikov, and M. I. Vrazhnik. Dinamicheskaya szhimayemost' metallov pri davleniyakh ot 400 000 do 4 000 000 atmosfer. Zh. eksperim. i teor. fiz., 34, vyp. 4, 1958). The experimental results are tabulated, and graphs showing the variation of D vs U are presented. The results were studied in order to compare groupings of the experimental data in an effort to match the P - P curve characteristic of the earth. The authors

Card 2/3

CIA-RDP86-00513R001756820008-4" APPROVED FOR RELEASE: 03/14/2001

	L 9433-66 ACC NR: AP5025074										
	conclude with some deductions of the consistency and uniformity of the B and layers of the earth's mantle. Orig. art. has: 6 figures, 3 tables, and 3 equations.								the B and D , and 3	D : !	
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PRYAKHIN, V.A., inzh.; TRUMIN, S.F., inzh.; NOVOSEL'TSEV, P.I., inzh.

Type GR-3 explosion-preof mine locomotive with gyroflywheel. Ugol'
Ukr. 4 no.10:40-41 0 '60.
(MIRA 13:10)

(Hine railroads)

(Gyroscope)

KHLISTUN, V.I., inzh.; TRUNIN, S.F., inzh.

Results of factory tests of leading models of the GR-4 mine gyroflywheel locomotive. Vop. rud. transp. no.5:324-336 '61. (MIRA 16:7)

1. Teretskiy mashinostroitel'nyy zavod.

(Mine railroads—Testing)

(Gyroscopic instruments)

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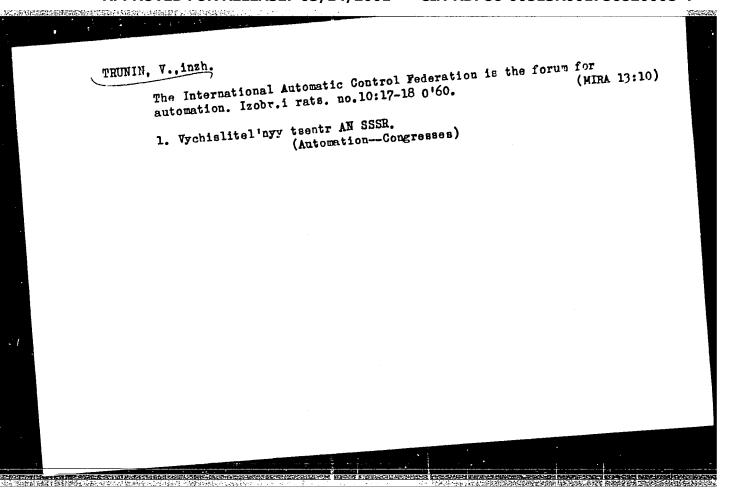
Strength, tensile and vibration testing machines. Isobr.i rats.

(MIRA 14:1)

(Moscow—Exhibitions)

(Germany, East—Testing machines)

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The TV-4 thickness measuring instrument. Biul.tekh.-ekon.inform.
(MIRA 13:10)

(Thickness measurement)

S/193/60/000/009/008/013 A004/A001

AUTHORS:

Trunin, V.G., Nikitin, A.I., Grishko, S.P.

TITLE:

The TG (TV)-4 Thickness Gage

PERIODICAL:

Byulleten' tekhniko-ekonomicheskoi informatsii, 1960, No. 9,

pp. 38-40

TEXT: The Ukrainskiy nauchno-issledovatel skiy trubnyy institut (UkrNITI) (Ukrainian Scientific Research Institute for Tubes) has developed in 1959 the TV-4 thickness gage for the measurement of the wall thickness and nonuniformity in thickness of tubes of nonmagnetic metals. With the corresponding graduation, the device can be used for the measurement of tube and rod diameters. The operating principle of the thickness gage is based on eddy currents. The device is composed of the tube generator, pick-ups, amplifier, indicator, automatic switch-off unit of the tube-drawing mechanism and power unit. The automation unit is represented by two trigger circuits, of which one acts on thinning, the other on thickening, while simultaneously signal lamps are lighted and the motor of the tube-drawing mechanism is switched off. For the connection of a recorder, a cathode follower is included in the device. A number of outside factors affect

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The TG (TV)-4 Thickness Gage

8/193/60/000/009/008/013 A004/A001

the indicating accuracy of the device, such as diameter and ovalness of the tubes, electric conductivity of the metal, distance of the pick-up from the metal and temperature of surrounding medium. The effects of these factors can be eliminated by using various constructional and radiotechnical methods and utilizing the dependence of the readings of the device on the tube diameter. Owing to the use of the method of constant unbalance and the special automation unit, it is possible to measure with a high degree of accuracy the nonuniformity in pipe thickness and switch off the tube-drawing mechanism if the given allowances are exceeded. The reading instability of the device does not exceed 2 μ in the course of 8 hours. The time constant of the device is equal to 15 milliseconds. The author presents the following technical data: measuring range of tube wall thickness = 0.1-3.0 mm; range of tube diameters = 8-60 mm; measuring error of thickness = 1%; scale multiplying factor for the measurement of thickness = 10 μ ; scale multiplying factor for the measurement of nonuniformity of pipe thickness = 10μ ; permissible voltage variations of the mains: from -15 to +10%; required power = 140 w; overall dimensions of the device (length x width x height) = $500 \times 300 \times 300$ mm; weight = 19 kg. There is 1 figure.

Card 2/2

S/263/62/000/011/005/022

AUTHOR:

Trunin, V. G. and Nikitin, A. I.

1007/1207

TITLE:

Wall thickness measurements in austenitic steel pipes by attachable induction-coils

PERIODICAL: Referativnyy zhurnal, otdel'nyy vypusk. 32. Izmeritel'naya tekhnika, no. 11, 1962, 16, abstract 32.11.97. In collection: "Proiz-vo trub" Kharkov, Metallurgizdat, no. 5, 1961, 175-181

TEXT: Results of investigation of wall-thickness measurements by eddy currents created in an attachable induction-coil, are reported and a device of the TB-5 (TV-5) type, designed on the basis of these results, is described. The device is intended for one-side measurement of wall thickness differences in austenitic steel pipes of the size of $8-60 \times 0.2-0.6$ mm, with a maximum measuring error of 1% and a measuring rate of 1-3 m/min. The thickness gage contains a current generator, two induction transducers, an amplifier, an electric indicating device and an automatic unit for disconnecting the pipe-feeding mechanism and for control of the optical signaling system. Alternating voltage is applied to the primary (winding) of the transducers, whose magnetic flux induces in the walls of the pipe to be measured, eddy currents that weaken the intensity of the primary magnetic flux. The self-induction electromotive force generated in the secondary windings is proportional to the wall thickness of the pipe. The difference between the opposite-connected secondary windings is amplified and fed to the indicating device. There are 7 figures and 4 references

[Abstracter's note: Complete translation.]

Card 1/1

ACCEPTABLE.

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