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YEREMIN, N. I. (Candidate of Physical and Mathematical Sciences)

"Fhysical Methods Used in the Quality Control of Metals." p. 313 in book <u>Modern Trends in the Field of Machine Building Technology</u>; Collection of Articles, Moscow, Mashgiz, 1957 363 p.

The article presents a brief discussion of some of the latest methods of detecting structural defects in metals. The use of X-ray and Gamma-rays, ultrasonics, and magnetic and luminescent methods is described. There are no references.

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	137-58-2-3936
YER Translation	EMIN, N.I. from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 2, p 237 (USSR)
AUTHOR:	Veremin, N.I.
TITLE:	On the J Z V Phase Transitions on the Aging of Austenitic Nichrome Steels (O fazovykh prevrashcheniyakh J Z V pri starenii austenitnykh khromonikelevykh staley)
PERIODICA	L: V sb.; Fizkhim. issled. austenitn. splavov. Moscow, Mashgiz, 1957, pp 53-68
A BSTRA CT	Thermomagnetic and magnetic microstructural analysis was employed to study the processes of $\mathcal{A}_2 \longrightarrow \mathcal{A}_2$ phase transitions in EI572 and 4Khl4Nl4V2M steels in a depletion layer of austenite near the carbides. The thermomagnetic measurements were performed on an improved Akulov aniso- meter. It was shown that the $\mathcal{A}_2$ phase begins to convert to austenite near the carbides at 450-500°C. The transition ends at about 700°. The $\mathcal{A}_2$ change proceeds at different temperatures in different steels and is accompanied by con- siderable thermal hysteresis (about 200°), and by partial

CIA-RDP86-00513R001962720012-1

extra state of the second state 137-58-2-3936 On the A = O Phase Transitions (cont.) tion of a ferritic phase in the aging of Cr-Ni steels at 450-850° does not occur during the aging time, but during cooling to room temperature. In addition, stresses in the  $\alpha_2$  phase and the austenite arise due to increase in volume during the  $\gamma \rightarrow \alpha_2$  transition. The  $\gamma \rightarrow \alpha_2$  transition proceeds until -1800 and consequently is martensitic in nature. The relationship of the martensitic transition to alloy composition versus temperature was found. It was found that in a number of grade 18-8, 18-12 type steels, the  $\gamma - \alpha_2$  break-up proceeds through a metastable hexagonal  $\theta$  phase. V.R. 1. Chromium-iron-nickel alloys---Phase transitions---Magnetic analysis 2. Austenitic steels-Phase transitions-Magnetic analysis 3. Stainless steel --- Phase transitions--- Magnetic analysis Card 2/2

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<ul> <li>NEREMIN, N.I.</li> <li>Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 2, p 237 (USSR)</li> <li>AUTHOR: Veremin, N. L.: Lebedyanskaya, N.I.</li> <li>TITLE: An Investigation of the S and S O Phase Transforma- fazovykh prevrashcheniy S of Microstructure (Issledvoaniye dions by Magnetic Analysis of Microstructure (Issledvoaniye strukturnym metodom)</li> <li>PERIODICAL: V sb.: Fizkhim. issled. austenitn. splavov. Moscow. Mashgiz, 1957, pp 75-86</li> <li>ABSTRACT: Magnetic analysis of microstructure (magnetic particle inspection) was employed to study the conditions of formation of the O phase and its connection with the O phase in austen- itic grade 19-9, 25-10, 18-8-5, and 20-10-3 Gr-Ni steels. O fut was established that the temperature of formation of the O phase is not identical in the various steels, as resistance to phase is not identical in the various with diminishing Cr:Ni ratio. The rate of formation of the O phase is significantly ratio. The rate of formation of the O phase is significantly ratio. The rate of formation of the O phase is significantly ratio. The rate of formation of the O phase is significantly ratio. The rate of formation of the O phase is significantly ratio. The rate of formation of the O phase is significantly ratio. The rate of formation of the O phase is significantly ratio an intermetallic compound with a tetragonal lattice. The is an intermetallic compound with a tetragonal lattice. The is an intermetallic compound with a formation of the O phase is significantly rate of formation of the O phase in the O phase is significantly rate of formation of the O phase in the O phase is significantly rate of formation of the O phase in the O phase is significantly rate of formation of the O phase in the O phase is significantly rate of formation of the O phase in the O phase is significantly rate of formation of the O phase in the O phase is significantly rate of formation of the O phase in the O phase is significantly rate of formation of th</li></ul>		na an a	
<ul> <li>AUTHOR: Veremin, Nulse Lebedyalisher, and and an OPhase Transformations by Magnetic Analysis of Microstructure (Issledvoaniye tions by Magnetic Analysis of Microstructure (Issledvoaniye fazovykh prevrashcheniy and and an Ophase Transformation fazovykh prevrashcheniy and the Ophase Transformation fazovykh prevrashcheniy and the Ophase in austendation formation of the Ophase and the temperature of formation of the Ophase is not identical in the various steels, as resistance to phase is not identical in the various steels, as resistender to phase is not identical in the Ophase is significantly ratio. The rate of formation of the Ophase is significantly ratio. The rate of formation of the Ophase is significantly is an intermetallic compound with a tetragonal lattice. The is an intermetallic compound with a tetragonal lattice.</li> </ul>			137-58-2-3937
<ul> <li>AUTHOR: Yeremin, N. Les Lebedyanisme, G. C. Phase Transforma- fittle: An Investigation of the S d and C O Phase Transforma- tions by Magnetic Analysis of Microstructure (Issledvoaniye fazovykh prevrashcheniy d d d C magnitnym mikro- strukturnym metodom)</li> <li>PERIODICAL: V sb.: Fizkhim. issled. austenitn. splavov. Moscow, Mashgiz, 1957, pp 75-86</li> <li>ABSTRACT: Magnetic analysis of microstructure (magnetic particle inspection) was employed to study the conditions of formation of the O phase and its connection with the O phase in austen- itic grade 19-9, 25-10, 18-8-5, and 20-10-3 Cr-Ni steels. It was established that the temperature of formation of the phase is not identical in the various steels, as resistance to phase is not identical in the various steels, as resistance to phase is not identical in the various steels, as resisting formation of the O phase increases with diminishing Cr:Ni formation of the O phase increases with diminishing Cr:Ni formation of the o phase increases is significantly ratio. The rate of formation of the O phase is significantly is an intermetallic compound with a tetragonal lattice. The is an intermetallic of the O phase in the O phase is signifi-</li> </ul>	YEREN	nin, N.I. m: Referativnyy zhurnal, Metallur	giya, 1958, Nr 2, p 237 (USSR)
<ul> <li>An Investigation of the off of Microstructure (Issleuvoun) tions by Magnetic Analysis of Microstructure (Issleuvoun) fazovykh prevrashcheniy of off off magnitum mikrostrukturnym metodom)</li> <li>PERIODICAL: V sb.: Fizkhim. issled. austenitn. splavov. Moscow, Mashgiz, 1957, pp 75-86</li> <li>ABSTRACT: Magnetic analysis of microstructure (magnetic particle inspection) was employed to study the conditions of formation inspection) was employed to study the conditions of formation of the O phase and its connection with the O phase in austenitic grade 19-9, 25-10, 18-8-5, and 20-10-3 Cr-Ni steels. O itic grade 19-9, 25-10, 18-8-5, and 20-10-3 Cr-Ni steels. O itic grade 19-9, 25-10, 18-8-5, and 20-10-3 Cr-Ni steels. O itic mation of the O phase increases with diminishing Cr:Ni formation of the O phase increases with diminishing Cr:Ni formation of the O phase increases with diminishing Cr:Ni formation. The rate of formation of the O phase is significantly ratio. The rate of formation of the O phase is significantly is an intermetallic compound with a tetragonal lattice. The is an intermetallic compound with a tetragonal lattice.</li> </ul>	V	oremin. Nelter Lebedyanski )	(
<ul> <li>PERIODICAL: V sb.: Fizkhim. issled. austenitn. splavov. Moscow, Mashgiz, 1957, pp 75-86</li> <li>ABSTRACT: Magnetic analysis of microstructure (magnetic particle inspection) was employed to study the conditions of formation of the O phase and its connection with the O phase in austen- of the O phase and its connection with the O phase in austen- itic grade 19-9, 25-10, 18-8-5, and 20-10-3 Cr-Ni steels. It was established that the temperature of formation of the O phase is not identical in the various steels, as resistance to phase is not identical in the various steels, as resistance to if ormation of the O phase increases with diminishing Cr:Ni formation. The rate of formation of the O phase is significantly ratio. The rate of formation of the O phase is significantly is an intermetallic compound with a tetragonal lattice. The is an intermetallic compound with a tetragonal lattice. The</li> </ul>	FITLE: A	ions by Magnetic Analysis of Micro ions by magnetic Analysis of Micro	To magnitnym mikro-
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It was established in the various steels, mishing Cr:Ni phase is not identical in the various steels, mishing Cr:Ni formation of the O phase increases with diminishing Cr:Ni formation of the O phase is significantly ratio. The rate of formation of the O phase is significantly dependent upon the holding time in hardening. The O phase dependent upon the holding time in hardening. The O phase is an intermetallic compound with a tetragonal lattice. The is an intermetallic compound with a tetragonal signifi-	ABSTRACT:	of the phase and its connection w	nd 20-10-3 Cr-Ni steels. O
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An Investigation of the (cont.)

cantly dependent upon the rate of diffusion of Cr in the  $\partial$  phase. The rate of transition of  $\partial - \partial$  at first is very rapid, but then it slows down, so that even for exceedingly long holding periods (up to 6000 hours), the  $\partial$  phase does not completely transform into the  $\partial$  phase. Measurements of microhardness have shown that formation of the  $\partial$  phase induces a considerable increase in brittleness. The phase composition of the steel was monitored by x-ray analysis of the structure and by chemical etching. It is shown that magnetic determination of the microstructure is less complex than x-ray and metallographic methods.

1. Steinless Steel---Phase transitions---Magnetic analysis 2. Austenitic steels

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137-58-2-3939 Phase Transformations in Austenitic Steels During Plastic (cont.) cant deformation, the  $\int - \alpha'_2$  transition appears along the boundaries of twins. The rate of transition increases rapidly as temperature drops, and precipitation of the  $Q_0$  phase results in hardening. The  $\gamma - Q_0$  transition is reversible. The temperature interval of reversible transition is below the temperature of crystallization. Ni, Cr, Mn, Mo, and C stimulate formation of an  $\alpha_0$  phase to different degrees. The solid  $\beta$ -solution becomes less stable on precipitation of a carbide phase (Me, Cr)<sub>23</sub>C<sub>6</sub> during aging. Metallographic and x-ray analysis of structure yielded concordant results. Bibliography: 18 references. V.R. 1. Austenitic steels-Phase transitions-Effects of deformation 2. Austenitic steels-Deformation 3. Austenitic steels--Phase transitions--Magnetic analysis Card 2/2

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### CIA-RDP86-00513R001962720012-1

1 37-58-2-3942 Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 2, p 238 (USSR) Yeremin, N.I., Lashko, N.F. On the Distribution of Nitrogen Between Solid Solution and AUTHORS: معاديه والمنافعة والمستند والمعاد والمعادي والمعادية والمنافعة والمعادية والمعادية والمعادية والمعادية والمعادية Second Phases in Austenitic Steels (O raspredelenii azota mezhdu tverdym rastvorom i vtorymi fazami v austenit-TITLE: nykh stalyakh) V sb.: Fiz. -khim. issled. austenitn. splavov. Moscow, Mashgiz, 1957, pp 131-136 PERIODICAL: The effect of N on the stabilization of austenite and the distribution of N between the solid solution and the precipitation phases in E1572 steel was investigated, wherein the N ABSTRACT: concentration attained 0.26%. To distinguish the effect of N on the suppression of an  $\alpha$  phase of various types, a melt with a higher Cr concentration, facilitating formation of Sferrite even at high N content (0.165%), was smelted. The specimens were subjected to a special form of heat treatment (Prosvirin, V.I., Saverina, I.A. V sb.: Voprosy metallovedeniya austenitnykh staley. Moscow, Mashgiz, 1952). A precipitate was obtained by electrochemical separation of the Card 1/2APPROVED FOR RELEASE: 09/01/2001 CIA-RDP86-00513R001962720012-1"

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137-58-2-3943 Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 2, p 238 (USSR) Yeremin, N.Z., Lashko, N.F., Lebedyanskaya, N.I. AUTHORS: Phase Transformations in EI572 Steel During Forging (Fazovyye izmeneniya v stali E1572 pri kovke) TITLE: V sb.: Fiz.-khim. issled. austenit. splavov. Moscow, PERIODICAL: Mashgiz, 1957, pp 137-159 The changes in the phase composition of E1572 austenitic steel (19% Cr, 9% Ni, 0.26-0.36% C) were investigated with ABSTRACT: the object of determining optimum conditions for heating and cooling after forging. The processes of formation and change in  $\delta$  ferrite, ferrite in the vicinity of the carbide phase, and ferrite arising as a result of plastic deformation, were also studied. Separation of the carbide phases was performed by making use of the selective solubility of carbides of the Mo23C6 type in hot HC1. The type of carbide was determined by x-ray structural analysis. Ferromagnetic phases were identified by magnetic analysis of the microstructure. It was shown that  $\delta$  ferrite develops as a result of nonhomogeneous dendritic crystallization; its amount may be reduced by homo-Card 1/2

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CIA-RDP86-00513R001962720012-1

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# Phase Transformations in EI572 Steel During Forging

genation at 1250°. To avoid formation of  $\delta$  ferrite, the final stage of heating and forging of the bars should be conducted at a temperature  $\leq$ 1150°. The major ferrite formers are C, Cr, Mo, and Ti. The maximum amount of metastable  $\alpha$  ferrite is formed on slow cooling to 850° and depends upon the rate of diffusion of the alloying elements around the carbide inclusions. The change in the structure of the steel in the process of aging at 650° is attributable to the formation and growth of carbides of the Mo<sub>2</sub>3C<sub>6</sub> type. EI572 steel becomes less stable in the course of the aging process and acquires a tendency to formation of  $\alpha$  ferrite. Aging of the steel consists of the precipitation of a carbide phase (Nb, Ti)C and (Cr, Ni, Fe, Mo, W)<sub>2</sub>3C<sub>6</sub>, and sometimes due to formation of a  $\sigma$  phase of the (Cr, Mo)Fe type.

1. Steel-Transformations-Effects of forging 2. Steel--Defermation

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EMIN	$N' \cdot \mathcal{L}$	137-58-3-5559
Translation	from: Referativnyy zhurnal, Metallurgiya, 19	58, Nr 3, p 153 (USSR)
	Numeroin N.L.	•
TITLE:	On Structural Changes in the Surface Layer to High-temperature Oxidation (O strukturny poverkhnostnom sloye metalla pri vysokotem	peraturnom
PERIODICA	L: V sb.: Fizkhim. issled. austenitn. s Mashgiz, 1957, pp 172-183	of motal during
ABSTRACT	of the oxides (O). The O's formed are "hol of the oxides (O). The O's formed are "hol	e-type" semi- vement of ions in the rom the ideal state.
	O lattice depends on the store shows that the in Experimental investigation shows that the in theory is not justified in the case of high-te theory is not justified in the case of high-te	mperiect-fattice imperature oxidation mental material on
Card 1/2	of high alloy of Metals (M) is essentially concerne the O of Metals (M) is essentially concerne kinetics of the oxidation and the structure of Methods employed for these purposes in th	e investigations of
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## On Structural Changes in the Surface Layer (cont.)

oxidation do not yield good results owing to the diffusion of the alloying elements. Efforts are made to employ the magnetic microstructural method in the experimental studies of the diffusion of the alloying elements within the OF on steels with metastable austenite structure. The O layer, formed on Cr-Ni austenite steel at temperatures above 570°, is microscopically porous and, therefore, permits diffusion of ions through regions of O's adjacent to the M. It is established that local diffusion of M ions in the layer of M adjacent to the O's produces a local change in the composition of the solid solution, and that this, in turn, produces structural changes, i.e., phase decomposition. Changes occurring in the solid solution were studied by means of magnetic, microstructural, and thermo-magnetic analyses. By successively removing layers of M (by means of electropolishing) it is established that the phase decomposition decreases with increasing depth of M. The process of phase transformation  $(\gamma - \alpha_2)$  occurring underneath the OL must be accompanied by an increase in volume and by the appearance of surface stresses, which should lead to a strengthening of the surface layer. Thermo-magnetic analysis data indicate that structural changes in the surface layer of M underneath the OL are attributable to the passage of Cr from solid solution into the OL. V. G.

Card 2/2

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137-58-6-13826 Translation from: Referativnyy zhurnal, Metallurgiya, Nr 6, p 375 (USSR) AUTHOR: Yeremin. N.L. TITLE: Physical Methods of the Quality Control of Metals (Fizicheskiye metody kontrolya kachestva metallov) PERIODICAL: V sb.: Sovrem. napravleniya v obl. tekhnol. mashinostr. Moscow, Mashgiz, 1957, pp 313-332 ABSTRACT: A survey. The following methods of physical detection of defects were examined; X-ray and g-ray examination, magnetic, ultrasonic, and luminescence methods. The advantages, drawbacks, and field of applicability of each are indicated. The characteristics of domestic apparatus for the quality control of metals are described. A.F. 1. Metals--Quality control 2. Metals--Testing equipment Card 1/1

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1. T. T. T. T. T.

	129-58-7-6/17
AUTHOR:	Verenin N. T., Candidate of Technical Sciences
TITLE:	Investigation of the Dispersion of Ferromagnetic Separations in Austenitic Alloys Determined from the Demagnetization Curves (Issledovaniya dispersnosti Demagnetization kydeleniy y austenitnykh splavakh
FERIODICA	po krivym razmagnichivanije) L: Metallovedeniye i Obrabotka Metallov, 1958, Nr 7, pp 27-30 + 1 plate (USSR)
	pp 27-30 + 1 plate (observent) It was recently established that fine ferromagnetic powder particles have a high coercive force. In such particles no domain boundaries are formed and, therefore, particles no domain boundaries are formed and, therefore, the ordinary mechanism of magnetization caused by the displacement of boundaries cannot proceed. The change in the magnetization can take place only as a result of coherent rotation of the spins which takes place predominantly in intensive fields. There is reason to assume that in many hardened alloys possessing a fine heterogeneous structure with a fine dispersion of ferro- magnetic separations inside a non-magnetic phase, single domain particles exist. Such a conception on the single domain separations can prove useful for understanding

#### CIA-RDP86-00513R001962720012-1

129-58-7-6/17 Investigation of the Dispersion of Ferromagnetic Separations in Austenitic Alloys Determined from the Demagnetization Curves

numerous metallurgical problems. The domain theory leads to the conclusion that the most important information on the structural state of single domain separations can be obtained from the demagnetization curves. The characteristics of such curves give indications not only on the dimensions of these separations but also on the magnetic anisotropy of all the four types (crystalline anisotropy, stress anisotropy, anisotropy of the shape of separations and surface anisotropy). Therefore, the authors investigated the dispersion of the ferromagnetic separations in austenite on the basis of the demagnetization curves on the steel 18Cr = 18Ni with a gradually increasing dispersion of the ferrite separations. This was achieved by an appropriate heat treatment of the preliminarily deformed specimens leading to inverse  $\alpha_2 \rightarrow \gamma$  transformation. The results of the changes in the magnetic properties during demagnetization as a function of holding time and of the degree of deformation are entered in a table, p.29, and the demagnetization curves are plotted in the graphs, Figs.1-4. The graph, Fig.1, shows the demagnetization

Card 2/5

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#### CIA-RDP86-00513R001962720012-1

129-58-7-6/17 Investigation of the Dispersion of Ferromagnetic Separations in Austenitic Alloys Determined from the Demagnetization Curves

curves of three steel specimens after 10, 25 and 40% plastic deformation by drawing. The character of the demagnetization curves of the coercive force and of the residual magnetization correspond fully with the change of the plastic deformation, i.e. with the work hardening. The graph, Fig.2, shows the demagnetization curves of the same specimens after two-hour annealing at 650°C; the two-hour heat treatment brought about a sharp increase in the coercive force. The demagnetization curves (Fig.3) relate to steel specimens annealed at an equal temperature for durations of 6, 14 and 22 hours. Increase of the annealing time progressively reduces the This indicates the emergence coercive force (Fig.4). of a new factor, most probably the influence of the anisotropy in the shape of the single domain ferrite separations which are formed from the multi-domain separations during their dissolution. Decrease in the residual magnetization, which is almost linearly linked with the volume of the ferromagnetic phase, confirms that Card 3/5 the breaking up into finer separations proceeds with

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129-58-7-6/17 Investigation of the Dispersion of Ferromagnetic Separations in Austenitic Alloys Determined from the Demagnetization Curves

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increasing annealing time. For elucidating the causes of the change of the coercive force magneto-metallographic analysis was applied. The results of this analysis (Figs.5a and b, plate facing p.41) indicate that the increase in coercive force at this initial stage of ageing (up to two hours) is due to the sub-division of the ferromagnetic separations, i.e. to the loss of the magnetic contacts which leads to a weakening of the magnetic of the magnetic effect, i.e. to an increase of H. Fig.5B indicates that this sub-division develops further with increasing ageing duration. In addition to the general regular shift of the demagnetization curves, a slight deflection from this is also observed, for instance after 22 hours heat treatment. Apparently this is due to a non-uniform density in the distribution of the spearations and the fact that the loss of orientation of the ferrite separations does not take place simultaneously. Thus the conception of single domain separations in austenitic steels which may contain ferrite separations opens up a Card 4/5 new field in physical metallurgy. On the basis of this

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 24(3)
 PHASE I BOOK EXPLOITATION
 SOV/232

 Yeremin, Nikolay Ivanovich, and Pavel Mikhaylovich Yelchin

 Magnetizm v tekhnike (Magnetism in Engineering) /Moscow/, Moscovskiy rabochiy, 1959. 94 p. 12,000 copies printed.

 Ed.: S. Gurov; Tech. Ed.: A. Lil'ye.

 PUHPOSE: This book is intended for the general reader

 GOVERAGE: The book explains in popular form the importance and uses of applied magnetism. The physical nature of magnetic uses of applied magnetism. The physical nature of magnetic areading list of 9 Soviet works on p. 95. No personalities are mentioned.

 TABLE OF CONTENTS:
 3

 Introduction
 3

 The Nature of Ferromagnetic Phenomena and Magnetic Materiala
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 Card 1/2
 4

APPROVED FOR RELEASE: 09/01/2001

Magnetism in Engineering	S0V/2	332	
Fields of Application of Magnetism		16	
Magnetic Analysis		52	
Magnetic Testing and Quality Control of Metal		64	
Magnetic Fields in the Cosmos and in the Atom		80	
AVAILABLE: Library of Congress (QC753.E7) Card 2/2		JP/ec 10-16-59	



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YEREMIN, N. I., Cand Tech Sci -- (diss) "Study of physicochemical properties and the treatment of the technology of gallium recovery from products of aluminum production." Leningrad, 1960. 21 pp; (Ministry of Higher and Secondary Specialist Education RSFSR, Leningrad Orders of Lenin and of Labor Red Banner Mining Inst im G. V. Plekhanov); 200 copies; price not given; printed on duplicating machine; (KL, 17-60, 153)

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Solutions

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· 18.3100 AUTHOR: Yeremin, N. I.

TITLE:

Card 1/5

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Tsvetnaya Metallurgiya, 1960, Nr 1, pp 123-127 (USSR)

ABSTRACT: This article describes an experimental verification of French Patent 964009 (of March 31, 1948) by Frary, which consists in a precipitation, from solutions of soluble aluminates and gallates, of the insoluble calcium aluminate by CaO, while most of the gallate remains in the solution. These tests showed that when more than 3 moles of active CaO per mole of Al<sub>2</sub>O<sub>3</sub> are introduced, a noticeable quantity of Ga

follows into the precipitate. However, 84-86% Al content but no more than 10 to 12% Ga are precipitated, raising in the solution the ratio of the latter from 1:100 to 1:17. This separation is shown

Preparation of Gallium Concentrate From Aluminate

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Preparation of Gallium Concentrate From Aluminate Solutions 77729 S0V/149-60-1-18/27

sodium aluminates and gallates), a quantity of CaO was added to the pulp so as to causticize the soda content of the pulp. This was done by adding 1 mole active CaO per mole of  $Na_2O$  tied in carbonate. Further, 3 moles of CaO per mole of  $Al_2O_3$  were introduced to precipitate calcium aluminate from the solution. If both CaO portions were added simulta-

neously, gallium extraction was not as high as it appears from data in the Table. The reactions of the separation process can be described by formulas:

$Ca(OII)_2 + Na_2CO_3 \equiv 2NaOII + CaCO_3$	; <b>(1)</b>	
$Al_2O_1$ , $3H_2O$ + 2NaOH $\mp 2$ [NaAl (OH) 4],	(2)	
$Ga_2O_3 \cdot 3H_2O + 2NaOH \equiv 2[NaGa(OH)_3].$	(3)	
$2[NaA1(OH)_1] + 3Ca(OH)_2 = 3CaO A1_2O_3 6H_2O + 2NaOH,$	(4)	
$2[\text{NaGa}(\text{OH})_4] + 3\text{Ca}(\text{OH})_2 \implies 3\text{CaO} \cdot \text{Ga}_2\text{O}_3 \cdot 6\text{H}_2\text{O} + 2\text{NaOH}.$	(5)	

Card 3/5

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### CIA-RDP86-00513R001962720012-1

Preparation of Gallium Concentrate From Aluminate Solutions

77723 sov/149-60-1-18/27

Extraction of  $Me_2O_3$  into the solution depending on the ratio  $Na_2O$  (carbonated):  $Al_2O_3$  in the pulp

	-	1	.)
(3)	(b)	(d)	(e.)
0,5 ± 1	1,0	47.2	6,5
1:1	1,5 3,0 4,0	55.1 63.0 65.2 59.3	28,4 18,8 15,6 14,2
1,5+1	1,5 3,0 4,0	61.7 67,3	9,3 8,1

Key to Table: (a)  $Na_2O_{carb}$ :  $Al_2O_3$  in Initial pulp; (b) Processing time, hours; (c) Extraction into the solution  $\mathcal{H}$ ; (d)  $Ga_2O_3$ ; (c)  $Al_2O_3$ .

Card 4/5

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CIA-RDP86-00513R001962720012-1

Preparation of Gallium Concentrate From Aluminate Solutions The slowest reactions are (2) and (3); therefore they determine the precipitation. The rate of Ga extraction being 67% at best, another method was tried; namely, CaO addition in two portions, one for causticizing, the other for Al precipitation with a time interval of 30 min (at  $90^{\circ}$ ). Results improved considerably: gallium extraction rate rose to 87-90%, while only 14% of the initial Al content remained in the solution. The latter contained 9 g/liter Al and 0.53 g/liter Ga. Subsequent carbonization produced a concentrate of 53.0%  $A1_20$ , and 3.2%  $Ga_20_3$ . It was then dissolved in alkali and gallium extracted electrolytically on a stainless steel cathode. There are 4 figures; 1 table; and 7 references, 6 Soviet, 1 French. Leningrad Institute of Mining. Chair of Metallurgy of Light and Rare Metals (Leningradskiy gornyy institut.) ASSOCIATION: Kafedra metallurgiyi legkikh i redkikh metallov) SUBMITTED: May 18, 1959 Card 5/5

APPROVED FOR RELEASE: 09/01/2001

TEREMIN, M.I. Gallium recovery from wastes of the aluminum industry. Izv.vys. ucheb.zav.; tsvet.met. 3 no.2:108-112 '60. (MIRA 15:4) 1. Lemingradskiy gornyy institut, kafedra metallurgit legkikh i redkikh metallov. (Aluminum industry--By-products) (Gallium) Auminum industry-By-products Gallium Antional Antiona
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# CIA-RDP86-00513R001962720012-1

77518 507/80-33-1-27/49 5.1310 Yeremin, N. I., Gus'kov, V. M . AUTHORS: Electrochemical Preparation of Gallium TITLE: Zhurnal prikladnoy khimii, 1960, Vol 33, Nr 1, pp 157-PERIODICAL: 163 (USSR) Electrolytic preparation of gallium from synthetic aluminate-gallate solutions (of a low gallium content) ABSTRACT: was studied in order to find the best conditions of yield and recovery of gallium from such solutions. Deposition of gallium on the cathode in an alkali solution is contingent on the following reaction:  $H_20a0_3 + H_20 + 3e = 0a + 4011^-$ The electrolysis was conducted in a 500-ml beaker using steel plate (1Kh18N9T) electrodes (one cathode and two anodes). A small plastic crucible with a steel wire in its bottom was placed under the cathode (connected. Card 1/6

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CIA-RDP86-00513R001962720012-1

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77518

Electrochemical Preparation of Gallium

Table 1. Kinetics of the electrolytic deposition of gallium. Conditions of electrolysis: temperature, 78°;  $D_{cathode}$ , 0.27 amp/cm<sup>2</sup>;  $D_{anode}$ , 0.05 amp/cm<sup>2</sup>;  $D_{v} = 19.2$  amp/liter. Key to Table 1: (a) electrolyte composition (in g/liter); (b) Na<sub>2</sub>O<sub>total</sub>; (c) time (in hours); (d) recovery of Ga from the solution (in %).

	(a)		(2)	(.1)
Ga	AL, Os	(4)	12/	
3.2	0	200	2 4 6	68.5 91.8 97.3
6.3	0	200	2 4 6	70.1 91.4 97.0
3.2	,69	200	2 4 6	69.0 89.9 96.5
6,3	69	200	2 4 6	71.8 92.1 97.0
6.3	130	200	2 4 0	72. 91. 95.

Card 2/6

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· Electrochemical Preparation of Gallium

77518 30V/80-33-1-87/49

with the cathode) for the collection of the deposited (liquid) gallium. The effect of the solution alkalinity on the yield of Ga is shown in Fig. 2. The effect of S10, content on the deposition of Ga is shown in Fig. 3. Effect of the temperature and current density on the Da deposition were also studied. The following conclusions were made. Ga is deposited at more negative potentials than the potentials of Ma deposition (by using Hg cathode) and hydrogen (using Ga cathode). The following optimum conditions of electrolytic Ga preparation from aluminate-gallate solutions of low Ga content are given: the concentration of Na20 summary in the solution should be not less than equilibrium for the given content of Al<sub>2</sub>O<sub>2</sub> in the electrolyte at a given temperature; more concentrated solutions (130-140 g/liter of  $Al_20_3$ ) with the same  $Al_20_3: 0a_20_3$  ratio should be used; electrolyte\_temperature = 75-80°;  $D_{\text{cathode}} = 0.2-0.23 \text{ amp/cm}^2$ There are 5 figures;

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Electrochemical Preparation of Gallium 77518 SOV/80-33-1-27/49 1 table; and 6 references, 1 U.S., 5 Soviet. The U.S. reference is: Recentry, Giefillan, Bent, J. Am. Chem. Soc., 56, 1662 (1934). SUBMITTED: June 9, 1959 Card 6/6 APPROVED FOR RELEASE: 09/01/2001 CIA-RDP86-00513R001962720012-1

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## YEREMIN, N. I.

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Doc Tech Sci - (diss) "Magnetic metallography in metallophysics studies." Moscow, 1961. 29 pp; 1 p of illustrations; (State Committee of the Council of Ministers USSR for Automation and Machine-Building, Central Scientific Research Inst of Technology and Machine-Building "TSNIITMASh", ONTI); 170 copies; price not given; list of author's works on pp 28-29 (18 entries); (KL, 6-61 sup, 211)

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NAZAROV, S.T.; SHRAY HER, D.S.; <u>YEREMIN, N.I.;</u> ROZHDESTVENSKIY, S.M.; KHIMCHENKO, N.V.; LESNICHENKO, I.I., red. izd-va; UVAROVA, A.F., tekhn. red.; SOKOLOVA, T.F., tekhn. red.

> [Modern methods of nondestructive testing]Sovremennye metody kontrolia materialov bez razrusheniia. Pod red. S.T.Nazarova. Moskva, Mashgiz, 1961. 285 p. (MIRA 15:7)

1. Moskovskiy dom nauchno-tekhnicheskoy propagandy im. F.E. Dzerzhinskogo. (Nondestructive testing)

APPROVED FOR RELEASE: 09/01/2001

## CIA-RDP86-00513R001962720012-1

s/149/61/000/004/002/008 A006/A101

AUTHOR:
Yeremin, N. I.

TITLE:
Studying cathode polarization in electrolysis of gallate solutions

TITLE:
Studying cathode polarization in electrolysis of gallate solutions, no.4, 1961, 97-101

TEXT:
In electrolysis of alkaline sodium gallate solutions hydrogen and gallium metal are jointly deposited on the cathode. To analyze conditions of the joint deposition of hydrogen and gallate metal their depozition potential and the polarization curves of each individual reaction must be known, by taking into the polarization curves of each individual reaction for the potentials and the polarization curves of each individual for the formation of the potential for the

gailing methal and the first deposition of hydrogen and gallate metal their deposition potential and the joint deposition of each individual reaction must be known, by taking into account depolarization. There are only few data available on the potentials and polarization curves of gallium deposition from alkaline solutions. For the purpolarization curves of gallium deposition from alkaline solutions in gallate solutions pose of determining the potentials and the rate of gallium deposition from alkaline solutions polarization curves of cathode reactions in gallate solutions with low gallium concentration (3 - 10 g/l) were measured on mercury and gallium drop electrodes at low current densities and on a liquid gallium electrode at higher current densities. It was established that in the case of a liquid gallium electrode, hydrogen deposition was the basic cathode process at both low and high

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Studying cathode polarization ...

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current densities. The potential of gallium deposition is more negative than that of hydrogen deposition. The author employed experimental data on the current efficiency of gallium and hydrogen, depending on the gallium concentration in the solution, and the cathode current density, and decomposed summary polarization curves in order to determine the reaction rate of gallium and hydrogen deposition. The curves show that with higher current density the rate of hydrogen deposition grows more rapidly than that of gallium deposition. This signifies that the current efficiency of gallium decreases with higher current density and, in fact, the more the lower the gallium concentration in the electrolyte. This theory was confirmed by a number of experiments and is an important factor in selecting the current density for electrolytic deposition of gallium from alkaline solutions. As a result of the experimental investigation, the author recommends the following optimum values of current density on the cathode for different gallium concentrations in the electrolyte: Cathode current density amp/om2

Gallium concentration, 2 - 3 3 - 5 5 - 7 7 - 10	g/1	Cathode current den 0.15 - 0.20 0.20 - 0.20 0.25 - 0.20 0.30 - 0.20	20 25 30	
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# CIA-RDP86-00513R001962720012-1



APPROVED FOR RELEASE: 09/01/2001

CIA-RDP86-00513R001962720012-1

AUTHOR: Yeremin, N.I.

S/772/61/000/000/003/003

TITLE: Magnetic powder method for the detection of defects and magnetic metallography. <u>Section title</u>: Industrial magnetic defectoscopes.

SOURCE: Sovremennye metody kontrolya materialov bez razrusheniya. Ed. by S.T.Nazarov. Moscow, Mashgiz, 1961, 136-?. (Abstract of Section on pp. 151-161 only).

TEXT: The paper as a whole describes methods in which a magnetic field is created in a metallic production item and a suspension containing ferromagnetic particles (FP) is spread over the piece. The FP settle in the nonuniform dispersion zones created by structural defects and render them clearly manifest. The specific section reviewed describes the latest Soviet stationary magnetic defectoscopes which permit magnetization of production pieces in various directions, pour the magnetic suspension over them automatically, provide suitable illumination of the surface to be inspected, and demagnetize the part after the test. Thus, the function of the inspector is reduced to visual inspection. Such defectoscopes employ special electromagnets or solenoids fed via Se rectifiers and 4-12-v, >7,000-a, power transformers and autotransformers. The universal magnetic defectoscope AEC-3 (AYeS-3) of the TsNIITMash (Central Scientific Research Institute of Machine Technology), is described and depicted (full-page schematic cross-section and generalview photo) as a typical instrument of this type. It comprises a power transformer Card 1/3

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#### CIA-RDP86-00513R001962720012-1

Magnetic powder method for the detection...

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for circular magnetization and an electromagnet for the longitudinal magnetization in a constant field. The setting up of a circular magnetization by means of an alternate current, in which the device operates as a current transformer, and that of a longitudinal field, in which the device operates as an electromagnet, are described. The device consists essentially of a magnetic circuit in the form of a horizontal rectangular frame equipped with a tapped coil (relatively remote, at a safe distance from the actual test site) and a pair of moving packet shoes to provide gaps of up to 350 mm. The tips of the packet shoes are pressed firmly against the test object by means of handwheels. An a.c. (220 v, 9 kva) or a d.c. (60 v, 4.5 kw) power supply is required. Automatization provisions required in mass-production inspection are embodied in the MAB (MDV) defectoscope (TsNIITMash); a schematic diagram and a general-view photo are shown. In it the test object is placed on a prismatic support; a pressure on a pedal lifts the prism and the test object to the level of the polar shoes of the magnet, whereupon a lever actuates the shoe-compression drive. An overhead light fixture provides suitable illumination for visual appraisal. The device has two independent electrical circuits for fully automated a.c. and d.c. operation; a third, separate, circuit is provided for the demagnetization chamber. The a.c. circuit for the creation of a circular magnetic field and the d.c. circuit for longitudinal magnetization are described. A special magnetic defectoscope for the inspection of large cold-rolling rolls, developed at the TSNUTMash, is described. The device employs combined magnetization produced by a constant magnetic field Card 2/3

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CHEMIC PURCHER DEPENDENCEMON REPRESENTATION CONTRACTOR

#### CIA-RDP86-00513R001962720012-1

S/032/61/027/004/028/028 B103/B201

AUTHORS: Gubanova, M. R., Yeremin, N. I., Yermolov, I. N., and Matveyev, A. S.

TITLE: New methods and instruments for the nondestructive material control, developed at TENTITMASh

PERIODICAL: Zavodskaya laboratoriya, v. 27, no. 4, 1961, 499-501

TEXT: This is a report on the results of the principal studies on defectoscopy, conducted at the laboratoriya defektoskopii (Laboratory for defectoscopy) of the authors' institute (see Association) in the past 2-3 years. Immersion - ultrasonic method. Full immersion. It opens ample possibilities for automation in defectoscopy. The following methods and instruments belong here: A. Laboratory model of MAU-1(IDTs-1) defectoscope for the detection of faults in turbine disks. The device may be used also for other workpieces by allowing the tank, in which they are to be dipped, to be modified conformingly. B. Apparatus and methods of automatic control of thin-walled tubes by Lamb's waves. The MAU-2 (IDTs-2) defectoscope used for this purpose is able to detect

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New methods and instruments for ...

S/032/61/027/004/028/028 B103/B201

forgings on the basis of the amplitude of the reflected signal has been worked out. I. Resonance - ultrasonic method. The respective control systems have been improved. The resonance-defectoscope thickness gauges YPT-5 (URT-5) and YPT-6 (URT-6) permit thickness to be read off a scale without diagrams nor computation devices. This is achieved by an additional measuring circuit with a straight-line frequency adjustable condenser. J. Various disturbances have been eliminated. K. Radioscopy with X- and gamma rays. Optimum conditions have been worked out for this process, and models of scintillation recorders of radiation have been developed. L. Both advantages and drawbacks of the gamma scintillation method have been examined. M. A special magnetic defectoscope, 474-1 (DKN-1) has been developed for the control of drive shafts and other large workpieces with the greatest possible mechanization of the process. Test models are used for controlling the cold-rolling process and pipes at the Novo-Kramatorskiy mashinostroitel'nyy zavod (Novo-Kramatorskiy Machine-building Works), and axles at the Novocherkasskiy elektrovoznyy zavod (Novocherkassk Electric Locomotive Works). N. A special magnetic transportable defectoscope ALMR-2 (DMP-2) which operates with magnetic powder defectoscopy and serves for layer examination of defects deep Card 3/4

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New methods and instruments for ....

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inside welded joints, has been developed. The device is produced in series at the Kishinevskiy zavod "Elektrotochpribor" (Kishinev Works "Elektrotochpribor"). O. A demagnetization apparatus has been developed, which removes the remanence of magnetism better than all systems used hitherto. P. A device has been worked out on the basis of the resonance method, which determines the tendency to intercrystallite corrosion in austenite steels using electromagnetic high-frequency methods ("vortex" methods). Q. Studies have been conducted concerning the use of highfrequency defectoscopy in the automatic quality control of non-ferromagnetic products, especially of tubes. R. The physical and technological bases of capillary methods of defectoscopy have been examined, and a capillary ultrasonic control method has been devised. It bases upon the action of intensive ultrasonic waves on a product dipped into a

ASSOCIATION:

(TsNIITMASh) Tsentral'nyy nauchno-issledovatel'skiy institut tekhnologii i mashinostroyeniya (Central Scientific Research Institute of Technology and Machine Building)

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ALL STATES IN THE REPORT AND ADDRESS AND ADDRESS AND ADDRESS ADDR BONDAREV, Yuriy Alekseyevich; YEREMIN, -N. I., red.; KHAKHAM, Ya.M., tekhn. red. [Use of plastics in the manufacture of machinery] Ispol'zovanie plastmass v mashinostroenii. Ul'ianovsk, Ul'ianovskoe knizhnoe izd-vo, 1960. 36 p. (Machinery-Design and construction) (MIRA 16:7) (Plastics) APPROVED FOR RELEASE: 09/01/2001 CIA-RDP86-00513R001962720012-1"

## CIA-RDP86-00513R001962720012-1

. KARPILES, Isak Isayevich; TIKHIY, Yevgeniy Matveyevich; YEREMIN, N.I., red. [Chipless metalworking by pressure] Obrabotka metallov davleniem bez sniatila struzhki. Ul'ianovskoe knizhnoe izd-vo, 1963. 30 p. (MIRA 17:10) 1. Konstruktor Ul'yanovskogo avtomobil'nogo zavoda metallicheskikh izdeliy (for Karpiles, Tikhiy). CIA-RDP86-00513R001962720012-1" APPROVED FOR RELEASE: 09/01/2001



Role of schistosity and fracturing zones in the localization of pyritecomplex metal mineralization in the Dzhusa deposit (Southern Urals). Vest. Mosk. un. Ser. 4: Geol. 18 no.6:24-32 N-D '63. (MIRA 18:7)

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KRYLOV, M.K.; YEREMIN, N.I.

New methods for electromagnetic prospecting and the preliminary results of their application in the Dzhusy pyrite deposit (Southern Urals). Vest. Mosk. un. Ser. 4: Geol. 19 no.3:30-45 My-Je '64. (MIRA 17:12)

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YEREMIN, N.Ye., prepodavatel'; VOLKOV, N.N.

Testing stand used for checking traction substation equipment. Elek. 1 tepl. tiaga 2 no.7:28-29 Jl '58. (MIRA 11:7)

1. Tomskiy elektromekhanicheskiy institut inzhenerov zheleznodorozhnogo transporta (for Yeremin). 2. Nachal'nik remontno-revizionnogo tsekha Novosibirskogo uchastka energosnabzheniya Tomskoy dorogi (for Volkov).

(Electric railroads--Substations--Equipment and supplies) (Electric testing)

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#### CIA-RDP86-00513R001962720012-1

DUBROVSKIY, V. P., inzh.; YEREMIN, N. Ye, inzh.; SHALIMOV, M. G., kand. tekhn. nauk, dotsent Analysis of the operation of a three-phase three-winding trans-former in nonsymmetrical operation. Trudy OMIIT 37:91-101 462. (MIRA 17:5) CIA-RDP86-00513R001962720012-1" APPROVED FOR RELEASE: 09/01/2001




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	on from: Referativnyy Zhurnal, Metallurgiya, 1957, Nr l, p. 9 (USSR)
AUTHOR:	Yeremin, P.F.
TITLE:	Yeremin, P.F. Saturated and Unsaturated Mineral Granule Suspensions in water (O nasyshchennykh i nenasyshchennykh vzvesyakh mineral'nykh zeren v vode
PERIODIC	AL: Tr. Severo-Kavkazsk. gorno-metallurg. In-ta, 1995 Nr 13, pp. 21-34
ABSTRACT	netting and a flask with outlet ation of mineral sus-
	pensions (b) in finely granulated suspensions with suspensions with finely granules of a given sp.gr. with suspensions having granules of a different sp.gr.,
Card 1/	degree of dispersion of the suspensions. degree of dispersion of the suspensions of different

#### CIA-RDP86-00513R001962720012-1

137-1-104

Saturated and Unsaturated Mineral Granule Suspensions in Water (cont.)

size. Described are certain features characterizing the formation of suspensions belonging to Type 1, (a stream of granules in an ascending stream of water, both moving at the same rate), and to Type 2 (stream of granules either in quiescent water, or in an ascending stream of water, but each moving at a different rate). Studied was the effect of a number of factors on saturated and unsaturated suspensions: the granulometric composition of the suspension, the flow rate of the water and the sedimentation rate of the compressed stream of granules, the degree of dis-persion, etc. A detailed characteristic of suspensions, based on the performed tests, is presented. It was established that the granular suspension "abhors" the unsaturated phase. With an insufficient feed the unsaturated suspension reacts by a poorer dispersion. It was noted that Type 1 suspensions may show a degree of dispersion ranging from 1 to the initial, and that they are always saturated. Type 2 suspensions

Card 2/3

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CIA-RDP86-00513R001962720012-1

137-1-104 (cont.) may vary in degree from 1 to limit dispersion, and can be either saturated, or unsaturated. Since in hydraulic classifiers the process of granule segregation according to size takes place in compound suspensions belonging to Types 1 and 2, the conclusion is reached that a study of the phenomenon of suspension saturation may assist materially in improving the performance of mechanical classifiers. M.L.

APPROVED FOR RELEASE: 09/01/2001

CIA-RDP86-00513R001962720012-1

137-58-4-6395 Translation from: Referativnyy zhurnal, Metallurgiya, 1958, Nr 4, p 9 (USSR) Yeremin, P. F., Krokhin, S. I., Maksimovich, I. Yu. AUTHORS: Beneficiation of the Manganese Ore of the Labinsk Deposit (Obogashcheniye margantsevoy rudy Labinskogo mestorozh-TITLE: deniya) PERIODICAL: Sb. nauchn. tr. Severo-Kavkazsk. gorno-metallurg. in-ta. 1957, Nr 14, pp 118-126 The results of a study of the capabilities of beneficiation of the Mn ores of the Labinsk deposit, the major ore minerals of ABSTRACT: which are rhodochrosite and Ca rhodochrosite, are set forth. The chemical composition of various samples is presented. The properties of the ore minerals and their fine dissemination, with intimate intergrowth with calcite, provides the basis for classifying this ore as non-gravitational. Experiments in jigging and concentration on the table have confirmed this. Flotation car be attained only at a high cost in oleic acid and water glass and with two steaming operations performed at high temperature. Satisfactory results were obtained when liquid soap was substituted for oleic acid at steaming temperatures of up to 40°C. By Card 1/2

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137-58-4-6395 Beneficiation of the Manganese Ore of the Labinsk Deposit flotation with prior washing of the dissolved salts it is possible to obtain concentrates containing 29-30 percent Mn and 89 percent recovery thereof. The Mn contents may be increased to 40 percent by roasting at 400-500°. A. Sh. 1. Ores--Processes 2. Flotation--Applications Card 2/2APPROVED FOR RELEASE: 09/01/2001 CIA-RDP86-00513R001962720012-1"

AATIMA KATAMA

CIA-RDP86-00513R001962720012-1

80V/149-58-5-3/18

On the Design of a Constrained Settling Classifier (Sorter) With Periodic Discharge of the Individual AUTHOR: Classes (K voprosu rascheta klassifikatora stesnennogo TITLE: padeniya s periodicheskoy razgruzkoy klassov) - **Y** : Izvestiya Vysshikh Uchebnykh Zavedeniy, Tsvetnaya Metallurgiya, 1958, Nr 5, pp 18 - 26 + 1 plate (USSR) PERIODICAL: ABSTRACT: The author deals with the design calculations of a hydraulic classifier, a sketch of which is shown in Figure 1, p 18. The main part of this classifier is a bucket into which the grains are fed from a pyramid-shaped chamber. The processes taking place in such classifiers have been dealt with in earlier work of the author (Refs 1, 2). In this paper, the design calculations of the individual assemblies are described and detailed numerical calculations of all the assemblies are made for a concrete practical example, with the following details: Q = 200 tons/24 hours: specific gravity of the solidSubstance 2.65; particle size 2-0 mm; water consumption 400 tons/24 hours. Card1/2

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# YEREMIN, P.F.

Coefficient of equal settling in conditions of hindered settling. Law.wys.ucheb.zaw.; tavet.met. 3 no.2:27-36 460. (MIRA 15:4)

1. Severokavkazskiy gornometallurgicheskiy institut, kafedra obogashcheniya poleznykh iskopayemykh. (Ore dressing)

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38485 s/044/62/000/005/014/072 C111/C333 16.3000 AUTHOR: Yeremin, S. A. TITLE: On the best approximation of a function which is analytical in an elliptic polycylinder Referativnyy zhurnal, Matematika, no. 5, 1962, 42, PERIODICAL: abstract 5B191. ("Issled. po sovrem. probl. teorii funktsiy kompleksn. peremennogo". M., Fizmatgiz, 1961, 211 - 213A lemma by S. N. Bernshteyn on the best approximation of TEXT: functions of a complex variable that are analytical in the ellipse  $|-z + \sqrt{z^2-1}| = R, R > 1$  (Bernshteyn, S. N., Ekstremal'nyyo svoystva polinomov [Extremal properties of a polynomial], part 1, L.-K., 1937) is generalized to the case of functions of K complex variables z,, z,.. ..., z,, which are regular in the area defined by the inequalities:  $z_{i}^{2} - 1 / < R, R > 1, i = 1, 2, ..., k.$ Abstracter's note: Complete translation.] Card 1/1

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(MIRA 16:2)

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YEREMIN, S.A.; SHADROV, A.F. Complete systems and bases in the spaces of functions analytic in Hartog's regions. Dokl. AN SSSR 148 no.3:500-503 Ja '63.

1. Kuybyshevskiy inzhenerno-stroitel'nyy institut im. A.I. Mikoyana. Fredstavleno akademikom V.I. Smirnovym. (Functions, Analytic)

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	ACCESSION NR: AP4019	004 S/0	)146/64/007/00	01/0149/0152	.•.
	AUTHOR: Yeremin, S. A	.; Shchevelev, M. I.	•		
:	TITLE: Device for meas	uring transient respo	onse of semicor	nductor diodes	
	COUNCE. WIIZ Pribore	stroveniye, v. 7, no	), 1, 1964, 149	-152	
	TOPIC TAGS: semicondu transient response, semi	ctor, diode, semico	nductor diode,	semiconductor diode	
•	ABSTRACT: A new instr generator and an oscillos semiconductor diodes und Elementary physical phen Operating procedures for described Orig. art. h	ument is described v cope, permits measure der conditions of a si nomena that transpir the measuring sche as: 2 figures.	which, in conju uring the trans ingle current p e in a diode ar me presented b	ulse or switching. e considered. In Enclosure 1 are	
	ASSOCIATION: Voronez Institute)			•	<b>ب</b>
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