

CIA-RDP86-00513R001963710005-9

 ZALISHCHAK, B.L.; KIZYURA, V.Ye.

 Discovery of endialyte in the Maritime Territory. Zapeygees.min. Obvra 90 no.3:291-294 '61.

 All'newostochnyy geologicheskiy institut Dal'newostochnogo filiale Sibirskogo otdeloniya AN SSSR, Vladivostok. (Maritime Territory--Eudialyte)

APPROVED FOR RELEASE: 09/19/2001

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CIA-RDP86-00513R001963710005-9

ALFEROV, A.A.; ARTEMKIN, A.A.; ASHKENAZI, YO.A.; VINOGRADOV, G.P.; GAISYEV, A.U.; GRIGOR'YEV, A.N.; D'YACHENKO, P.YO.; ZALIT, H.W.; ZAKHAROV. P.M.; BOBNIN, N.P.; IVANOV, I.I.; IL'IN, I.P.; KHETIK, P.I.; KUDRYA-SHOV, A.T.; IAPSHIN, F.A.; HOLYARCHUK, V.S.; PERTSOVSKIY, L.M.; POGODIN, A.M.; RUDOY, M.L.; SAVIN, K.D.; SIMONOV, K.S.; SITKOVSKIY, I.P.; SITNIK, M.D.; TETEREV, B.K.; TSETYERIN, I.Ye.; TSUKANOV, P.P.; SHADIKYAN, V.S.; ADELUNG, N.N., retsenzent; AFAHAS'YEV, Ye.V. retsenzent; VLASOV, V.I., retgenzent; VOROB!YNV, I.Yo., retgenzent; VORO-NOV, N.M., retsenzent; GRITCHENKO, V.A., retsenzent; ZHNFEBIN, M.N., retsenzent; IVLIYEV, I.V., retsenzent; KAPORTSEV, N.V., retsenzent; KOCHUROV, P.M., retsenzent; KRIVORUCHKO, N.Z., retsenzent; KUCHKO, A.P., retgenzent; LOBANOV, V.V., retgenzent; MOROZOV, A.S., retgenzent; ORLAW, S.P., retsenzent; PAVIUSHKOV, E.D., retsenzent; POPOV, A.N., retsenzent; PROKOF YAV, P.F., retsenzent; RAKOV, V.A., retaenzent: SINEGUBOV, N.I., retsenzent; TERENIN, D.F., retsenzent; TIKHO-MIROV, I.G., rotsenzent; URBAN, I.V., rotsenzent; FIALKOVSKIY, I.A., retsenzeat; CHEPYZHEV, B.F., retsenzeat; SHEBYAKIN, O.S., retsenzent, SHCHERBAKOV, P.D., retsenzent; GARNYK, V.A., redaktor; LOHAGIN, N.A. redaktor; MORDVINKIN, N.A., redaktor; NAUMOV, A.N., redaktor; POBE-DIN, V.F., redaktor; RYAZANTSEV, B.S., redaktor; TVERSKOY, K.N., redaktor; CHEREVATYY, N.S., redaktor; ABSHINOV, I.M., redaktor; BABELYAN, V.B., redaktor; BERNGARD, K.A., redaktor; VERSHINSKIY, S.V., redaktor; GAMBURG, Ye.Yu., redaktor; DERIBAS, A.T., redaktor; DOMEROVSKIY, K.I., redaktor; KORNEYEV, A.I., redaktor; MIKHEYEV, A.P., (Continued on next card) redaktor

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ALFEROV, A.A. ---- (continued) Card 2. MOSKVIN, G.N., redaktor; RUBINSHTEYN, S.A., redaktor; TSYPIN, G.S., redaktor; CHERNYAVSKIY, V.Ta., redaktor; CHERNYSHZY, V.I., redaktor; edaktor
Railroad handbook] Spravochnaia knizhka zheleznodorozh, ika, Izd. 3-e, ispr. i dop. Pod obshchei red. V.A.Garnyka, Moskva, Gos. 3-e, ispr. i dop. Pod obshchei red. V.A.Garnyka, Moskva, Gos. 3-tanap.zhel-dor. izd-vo, 1956. 1103 p. (MERA 9:10)
1. Nauchno-tekhnicheskoye obshchestvo zheleznodorozhnogo transporta. (Bailroads)

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ZALITIS, L. K .: Master Biol Sci (diss) -- "Evaluation of the results of dermoelectrometric and dermoreactivemetric investigations of milch cows during the stable and pesture periods". Riga, 1958. 24 pp (Acad Sci Iatvian SSR, Inst of Experimental Med), 220 copies (KL, No 5, 1959, 146)

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CIA-RDP86-00513R001963710005-9 "APPROVED FOR RELEASE: 09/19/2001 • ZALIVADNYY, B., mladshiy nauchnyy sotrudnik Instrument for measuring ship speed through the water. Mor. flot 21 no.2:18-20 F '61. 1. Gosudarstvennyy vsesoyuznyy dorozhnyy nauchno-issledovatel'skiy institut "Soyuzdornii." (Ultrasonic waves-Industrial applications) (Nautical instruments)



CIA-RDP86-00513R001963710005-9

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AUTHOR: Zalivadnyy, B. S.

TITLE:

RIODICAL: Akusticheskiy zhurnal, v. 7, no. 1, 1961, 94-96

Velocity broadband microphone

PERIODICAL: AKUSTICHESKLY manual man

Card 1/3

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Velocity broadband microphone

(20.25 mm, wire distance 1 mm), the distance between emitter and collector was 6 mm. Emitter and collector net are fastened onto a ceramic head, and are protected by a cylindrical screen. The midrophone described was checked by means of plane and standing waves. It was found that, with this instrument, the sound-particle velocity could actually be determined with great accuracy. The low sensitivity of about 10 watt·sec/cm, and the high noise level, as well as the bulky auxiliary equipment were considered to be grave disadvantages of this microphone. At present, the author is working on a similar microphone at which a tritium preparation is to be used as emitter. He expects to attain an improvement of the instrument. He thanks S. N. Rzhevkin and K. M. Ivanov-Shits for valuable advice, as well as M. N. Tsingarelli and B. A. Shilov for taking part in the experiments. There are 4 figures and 2 references: 1 Soviet-bloc and 1 non-Soviet-bloc.

ASSOCIATION: Kafedra akustiki Moskovskogo gosudarstvennogo universiteta (Department of Acoustics of Moscow State University)

SUBMITTED: March 24, 1960

Card 2/3

APPROVED FOR RELEASE: 09/19/2001



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ZALIVADNYY, S. YA.

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USER/Chemistry - Sodium Nitrate Chemistry - Crystals - Twinning

"Effect of Mosaic on the Resistance of the Mechanical Twinning of Sodium Nitrate," R. I. Garber, S. Ya. Zalivadnyy, V. I. Startsev, Physicotechnical Instituto, Academy of Sciences of the USSR, Khar'kov, 2pp

"Dok Ak Hack" Vol LVIII, No 4, p 571-2

Process of twinning in both sodium nitrate and potassium nitrate crystals is very similar. Authors attempt to show that a further study of this process has resulted in the observation that some multicrystals of sodium nitrate show anomalies of great resistance to mechanical twinning. Submitted by Academician M. A. Leyontovich, 13 May 1947.

PA 38T10

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有在目前目的自己的自己的自己的自己的情况和自己的自己的思想。 AREA THE REPORT OF THE PARTY OF S Ya. ZALIVADNYY CA Hermation of slipping roass in monocrystals of sodium milliste. N. Y.a. Zaliveduyi. Dobledy Abed. Nauk S.N.S.R. 81, 1003-471951;::::A study of the deformation of NaNOs noncerpitals. The monocerpitals were prepd. by crystal of NaNOs from melts, and the monocrystallinity was verified by ortical and z-ray methods. The urientation axis was detd. by the plane of clearage cracks and the double refraction. in a press designed for the purpose. During deformation the samples were beated and cooled at a rate of 1° per min. Simples were beated and cooled at a rate of 1° per min. Simples were beated and cooled at a rate of 1° per min. Simples were beated and cooled at a rate of 1° per min. Simples were beated and cooled at a rate of 1° per min. Simples were beated and cooled at a rate of 1° per min. Simples were beated and cooled at a rate of 1° per min. Simples were beated at a rate of a per sec. Photo-were deformed at a rate of the slipping somes in monocrystals graphs showing some of the slipping somes in monocrystals graphs thowing some of the slipping somes is shown. press in which the crystals were deformed is shown. Gladya S. Macy A LOS INTERIORISTICATION

CIA-RDP86-00513R001963710005-9

67670 sov/126-8-6-18/24 18.7100 Zalivadnyy, S.Ya. and Mikhaylovskiy, V.M. AUTHORS: on Bicrystals of Influence of Cyclic Heat Treatment TITLE: Uranium PERIODICAL:Fizika metallov i metallovedeniye, 1959, Vol 8, Nr 6, . pp 904-907 (USSR) This study has been carried out in order to elucidate the influence of the interaction between crystals on the ABSTRACT: nature of changes in the material during cyclic heat treatment and to clarify further the mechanism of the phenomenon under investigation under simplified conditions (absence of surrounding grains). Prismatic billets with coarse columnar grains were prepared from technically pure uranium by a method described by Gerber et al (Ref 4). Bicrystal specimens were cut out by a wire saw from the billets. Further preparation of the specimens was carried out on polishing papers and by electrolytic polishing. The final specimens were $3.2 \times 1.3 \times 0.7$ mm in dimension. The bicrystals were electrolytically etched and inspected in polarized light by a metallographic microscope. The relative grain orientation was determined by the X-ray method of inverse Laue exposure. In order to Card 1/4

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67670 SOV/126-8-6-18/24

Influence of Cyclic Heat Treatment on Bicrystals of Uranium control the relative displacement of grains graduation . lines were applied perpendicular to the adjacent boundary. These lines were made with the diamond indenter of a micro-hardness tester. For the cyclic heat treatment the specimens were placed in an iron boat provided with a lid lined with tantalum foil in order to exclude interaction between uranium and iron. The specimens were heated by passing electric current through the boat and cooled by conducting away the heat through the massive copper grips of the boat which were water cooled. The temperature was measured by a Pt/Pt-Rh thermocouple welded to the boat. The experiments were carried out in vacuum at a pressure not exceeding 3×10^{-6} mm Hg and a temperature range of 100 to 600°C. The sequence was as follows: heating to the maximum temperature - 5 minutes, holding at 600°C for 1 minute, cooling to the minimum temperature - 4 minutes. The investigation was carried out up to 1000 cycles with intervals for the inspection of the specimens after 100, 200, 300, 400, 500 and 750 cycles. After 1000 cycles the specimens were subjected to electrolytic polishing and etching in order to expose the changes in microstructure.

Card 2/4

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67670 sov/126-8-6-18/24 'Influence of Cyclic Heat Treatment on Bicrystals of Uranium In the table on p 905 results of the investigation of 3 specimens after 1000 cycles are given. Fig 1 is a photomicrograph of a portion of the specimen (a - original condition, polarized light, x 40; b - after 300 cycles, x 40; v - after 1000 cycles, x 40; g - the same after electrolytic polishing and etching, polarized light, x 160). Fig 2 shows graphically the dependence of the magnitude of displacement along the boundaries on the number of cycles for a bicrystal of uranium. Fig 3 is a photomicrograph of a uranium specimen without the middle portion (a - before cyclic heat treatment, polarized light; b - after 100 cycles). The authors arrive at the following conclusions: The relative displacement of bicrystal grains per cycle under similar conditions of cyclic heat treatment coincides in the order of magnitude with the relative displacement of grains of approximately the same dimensions in polycrystalline specimens of uranium. A change in the relative disposition of grains can take place due both to the difference in residual elongation and to the displacement of one grain as a whole Card 3/4

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制制的相关数据存储并原因中国主义与结论 ar de statement de la service de la serv 81616 s/181/60/002/00/04/050 B122/B063 • استاد ما ا اتر Garber, R. I., Zalivadnyy, S. Ya., Mikhaylovskiy, V. M. 21.1330 Change in the Microstructure of Uranium by Cyclic Heat 18,8100 AUTHORS: Fizika tverdogo tela, 1960, Vol. 2, No. 6, pp. 1052-1059 TITLE: TEXT: When subjected to cyclic heat treatment, uranium exhibits irreversible growth which has been given different explanations in PERIODICAL: publications. In order to clarify this problem, the authors of the present paper examined the change in the microstructure of uranium, i.e., the process taking place inside and on the grain boundaries of polycrystalline uranium during cyclic heat treatment. The metal surface Was examined microscopically and photographed with a camera of the type was examined microscopically and photographed with a camera of the Wanium MOH-1 (MFN-1). Fig. 1 shows the scheme of the system. The uranium Samples were prepared in such a way that coarse, columnar grains samples were prepared in such a way that course, columnar grains developed in the center of the sample (Fig. 2). The deformation of the grains may charge by the charge is at the sample (Fig. 2). grains was observed by the changes in etched lines. Sample No. 1 was Card 1/3

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Change in the Microstructure of Uranium by Cyclic Heat Treatment

heated 200 times from 100 to 600°C, No. 2 300 times, and No. 3 50 times in the course of 5 min, cooling took 4 min, the peak temperature lasted 1 min. Figs. 3-6 illustrate the changes undergone by the samples No. 1-3. A curvature in the etched lines and a mutual displacement of the grains was observed in all samples. In some cases, a distortion of the grain boundaries was observed in addition to the mutual displacement. It was further observed that at peak temperature there was a jump in the lines, which again vanished on cooling. The direction of these jumps changed after about 10 cycles, and remained the same on a further cyclic treatment. This thermoelastic deformation is assumed to be related with the anisotropic thermal expansion of uranium. The disorientation of the grains in the course of the cyclic treatment is examined roentgenographically. The greatest possible displacement of grains was determined from the degree of disorientation and the difference between the thermal expansion coefficients of touching bodies; the displacement corresponding to the mechanism of "thermal wedging" is likewise determined and compared with the displacement observed experimentally. The displacement observed was found to differ only little from the one determined by the

Card 2/3

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Change in the Microstructure of Uranium by Cyclic Heat Treatment 81616 S/181/60/002/06/04/050 B122/BC63

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mechanism of "thermal wedging", whereas it is two orders smaller than the greatest possible, i.e., only a small part of the thermoelastic displacements becomes irreversible. It was further established by X-ray pictures (multiplication of the original spots on the single crystals) that a splitting of the grain takes place in blocks by cyclic thermal treatment. The residual displacement of grains, which ultimately causes the uranium growth, is ascribed to the formation of undersize grains, the plastic deformation in the boundary zone of weak grains, and the displacement of grains on their cooling. There are 8 figures, 1 table, and 11 references: 7 Soviet and 1 British.

ASSOCIATION: Fiziko-tekhnicheskiy institut AN USSR, Khar'kov (Physicotechnical Institute of the AS UkrSSR, Khar'kov)

SUBMITTED: February 24, 1958

Card 3/3

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5.2100	E032/E314 E032/E314 E.S.
AUTHORS :	Garber, R.I., Zalivadnyy, S.Ya. and E32/E314 Microhardness of
TITLE:	Determination of the Anisotropy
PERIODICAL	: Fizika metallov i metallovedeniye, 1900, tor 7,
ABSTRACT:	The aim of the present work was to study the united of beryllium.
	The study was made unstallization was carried out at
	10 ⁻⁶ mm Hg in the apparatus shown schematic crucible Figure 1, in which 1 is a beryllium oxide crucible which has a hemispherical bottom and conical side wal.s, which has a hemispherical bottom and 6 are electrical
	heaters, 7 15 a July are apertures for thermocouples a support, 11, 12, 13 are apertures for the electrical and 14, 15, 16, 17 and 18 are leads for the electrical was
Card1/3	brought up to 1 400 °C (120 °C above the mercing per about of beryllium). It was held at that temperature for about one hour and then uniformly cooled from the bottom upwards.

CIA-RDP86-00513R001963710005-9

THE PURCHASE STREET, ST 68630 s/126/60/009/02/019/033 Determination of the Anisotropy in the Microhardness of Beryllium Crystals The crystallized beryllium was then removed from the apparatus after being cooled down to room temperature. The specimens were worked into a spherical form and suitably polished and the microhardness was determined at the points indicated in Figure 2 (circles). The specimens were orientated with the aid of X-ray diffraction photographs which were also used to judge the quality of the specimens. The microhardness was then measured using the PMT-2 microhardness gauge with a load of 100 g. Typical polar diagrams are shown in Figures 4 and 5 which refer to the plane containing C6 and the plane perpendicular to C_6 , respectively. It is concluded that the microhardness diagram for beryllium is close to an ellipsoid of revolution about the sixfold axis, the ratio Card 2/3

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24477 s/126/61/011/006/003/011 21,2100 E193/E483 Garber, R.I., Zalivadnyy, 3.Ya. and Mikhaylovskiy, V.M. AUTHORS : Variation of the microstructure of uranium during cyclic TITLE: thermal treatment. II PERIODICAL: Fizika metallov i metallovedeniye, 1961, Vol.11, No.6, pp.889-892 This is a continuation of earlier published work of the TEXT: authors (Ref.1: FTT, 1960, 2, 6, 1052 and Ref.2: FMM, 1959, 8, 904) relating to the mechanism of distortion of uranium during thermal cycling on bi-crystal specimens and on coarsely crystalline material with columnar grains. In this paper the authors investigate the laws governing the thermal cycling-induced changes in finely-crystalline technical grade uranium. To ensure uniform grain-size of the required magnitude, cylindrical uranium specimens (66 mm long, 8 mm in diameter) were annealed and then compressed (in the direction normal to the axis) to approximately 50% reduction in thickness and the resultant blanks were machined to produce prismatic specimens measuring $60 \times 4 \times 3$ mm. After recrystallization, these specimens were plastically deformed in Card 1/5

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Variation of the microstructure ...

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compression (8% reduction in thickness) in the direction normal to the longitudinal axis and to the direction of the first compressing operation; this was done to develop texture in the material The specimens were then cut into several prismatic test pieces which, after polishing (mechanical and electrolytic) and recrystallization, measured $6 \times 2.5 \times 1.5 \text{ mm}$. On 3 faces of each other states of the On 3 faces of each test piece a set of lines, spaced at 0.1 mm intervals, was inscribed by making scratches $2\,\mu$ wide and $0.5\,\mu$ deep. Annealing, recrystallization and the thermal cycling tests were all carried out Each thermal cycle consisted of the in vacuum of 5×10^{-6} mm Hg. following: heating to 600°C in 5 minutes; holding at 500°C for The specimens (whose 1 minute; cooling to 100°C in 4 minutes. original grain size was 25µ) were examined after 200, 400, 600, 800, 1300 and 2000 cycles. The dimensional changes of several test pieces after 600 cycles are tabulated. It will be seen that the length of the test pieces increased, their width and thickness Metallographic examination revealed that thermal decreased. cycling had brought about both the deformation in the interior of the grains and relative displacement of the grains. The latter effect was reflected in increased roughness of the Card 2/5

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S/126/63/015/001/011/029 E073/E420

Simultaneous influence ...

with a tensile stress of 100 g/mm^2 ; 2) 50 cycles with a tensile stress of 600 g/mm². Another batch of specimens was subjected to 1200 thermal cycles without any external load. The results are given in Table 1. Metallographic studies indicate that the elongation of the specimens was due primarily to slip in the grains; mutual displacement of grains and porosity are less important. No qualitative difference was observed in the behaviour of the specimens during simultaneous application of cyclic heat treatment and an external tensile load and cyclic heat treatment alone. There are 2 figures and 2 tables.

SUBMITTED: March 26, 1962

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men No,	Treatment	Experiment duration, hours	Dimensi Length	onal ch Width	anges, %	
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3	$\sigma = 100 \text{ g/mm}^2$ 400 thermal cycles with an external load	80	+0.6	-0.3	-0.3	4
4	$\sigma = 100 \text{ g/mm}^2$ 50 thermal cycles	80 10	+11.0 +0.3	-0.5 Very	-9.0 very	
5	External load			small	small	
6	$\sigma = 600 \text{ g/mm}^2$ 50 thermal cycles with an external load	10	+4.3	-1.8	-2.7	
	$\sigma = 600 \text{ g/mm}^2$	10	+33	-8.5	-16	
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<u>ALIVAKHA, Petr Il'ich</u>, aktivnyy ratsionalizator, izobretatel', iokar', udarnik komm. truda; CHML', L.N., red.; KOZINCHENKO, V.Ya., tekhn. red.
We are reducing auxiliary time] Sokrashchaem vepomogatel'ne vremia; iz opyta raboty na zavode "Svet shakhtera." no khar'kov, Khar'kovskoe knizhnoe izd-vo, 1962. 43 p. (Min ing machinery—Technological innovations)
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9 (6) 507/32-25-6-17/53 Zelivelov, F. P., Tyukina, M. N., AUTHORS: Tomashov, N. D. Investigation of the Microstructure of Anodic Oxide Films on TITLE: Aluminum by the Aid of the Electron Microscope (Issledovaniye mikrostruktury anodnykh okisnykh plenok na alyuminii pri pomoshchi elektronnogo mikroskopa) Zavodskaya Laboratoriya, 1959, Vol 25, Nr 6, pp 696-698 (USSR) PERIODICAL: A method was devised, permitting the determination of the cell ABSTRACT: structure of anodic oxide films on aluminum (Fig 1). By this method no impression is taken of the film on the metallic anode surface (Ref 1); instead, replicas are prepared of such films. The method is based on the operation of taking off and subsequently comminuting the oxide film, thus obtaining microscopic particles which are split along the side-(longitudinal section) or bottom- (cross section) plane of the hexagon lattice structure. Reproductions of these planes of shear may be obtained by the carbon-replica method (Ref 2). The preparation procedure is described. Observations were made with the electron microscope EM-3 or UEM-100, and the samples under investigation were of AVOUO aluminum (99.99 % Al), which Card 1/2网络瑞典斯斯特 计数据标识 网络斯特尔斯特

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Investigation of the Microstructure of Anodic Oxide 507/32-25-6-17/53 Films on Aluminum by the Aid of the Electron Microscope were oxidized anodically in a 4 % sulphuric acid solution by the method of the hard anodization (Refs 3, 4) (Figs 2, 3). The figures show that the oxide film is a dense packing of cells in the form of hexagon prisms. Data are supplied of the dimension and quantity of cells (Table); they agree with data obtained with an earlier described method (Ref 1). There are 3 figures, 1 table, and 4 references, 2 of which are Soviet. Institut fizicheskoy khimii Akademii nauk SSSR (Institute o: ASSOCIATION: Physical Chemistry of the Academy of Sciences, USSR) . Card 2/2

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28 (5) AUTHORS:	
	Tomashov, N. D., Byalobzheskiy, A. V., SOV/32-25-6-31/53 Val'kov, V. D., Zalivalov, F. P.
TITLE:	Device for the Rapid Determination of the Quality of Anodic Oxide Films on Aluminum and The All
	Oxide Films on Aluminum and Its Alloys (Pribor dlya bystrog) opredeleniya kachestva anodnykh okisnykh plenok na alyuminii i yego splavakh)
PERIODICAL:	Zavodskaya Laboratoriya, 1959, Vol 25, Nr 6, pp 738-739 (USSR
ABSTRACT:	For the detection of defective parts of anodic films the device K-1 by G. V. Akimov and Ye. N. Paleolog is usually used. The device partice the device partice the
	the film; another disadvantage is the use of a sodium chloride solution which may load to
· · ·	K-1; the mode of operation of the new device is based upon the fact that the conductivity of the anodic oxide film is the greater the more porces it is
Card 1/2	detector of defects (Fig 1) is somewhat modified, stainless steel 1 Kh18N9 or zink serve e. g. as electrode as copper and aluminum may together form an electric cell. The device

Anouic Oxide F	Rapid Determination of the ilms on Aluminum and Its All	Quality of SOV/32-25-6-31/	/53
	(Fig 2, Scheme) has piles a	s direct-current transmitter ding electrolyte may be used m- or sodium bichromate). Th	
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CIA-RDP86-00513R001963710005-9

S/128/61/000/012/001/004 A004/A127

AUTHORS: Zalivalov, F.P.; Tyukina, M.N.; Ignatov, N.N.

TITLE: Deep anodizing of aluminum chill molds

PERIODICAL: Liteynoye proizvodstvo, no. 12, 1961, 11

TEXT: Referring to former works (Ref. 1: N.D. Tomashov, "Vestnik inzhenerov i tekhnikov", no. 2, Moscow, 1946; Ref. 2: N.D. Tomashov, M.N. Tyukina, "Issledovaniya po korrozii metallov", no. 1, Trudy Instituta fizicheskoy khimii, AN SSSR, no. 2, izd-vo AN SSSR, Moscow 1951; Ref. 3: N.D. Tomashov, A.V. Byalobzheskiy, "Issledovaniya po korrozii metallov", no. 4, Trudy Instituta fizicheskoy khimii AN SSSR, no. 5, Izd-vo AN SSSR, Moscow - Leningrad, 1955) the author points cut that deep ancdizing produces on the surface of aluminum and its alloys a hard oxide coat which possesses a considerable resistance to high temperatures. The low heat conductivity of anode coats (0.001 - 0.003 cal/cm · . sec O C) of at least 150 - 300 μ thickness limits the heat transfer to the mold metal and prevents its melting. This property of the aluminum oxide coat was utilized in the manufacture of molds for the casting of h-f aluminum and magnesium alloys. The mold was made of pure AB000 (AV000) aluminum (99.99%)

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Deep anodizing of aluminum chill molds

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and ABO (AVC) commercial aluminum. The inner mold surface was coated with a thick oxide layer obtained in a 2N-solution of sulfuric acid at a constant current density of 2.5 amp/dm^2 and an electrolyte temperature of 0 - 3°C. The surfaces not being ancdized were covered with AK-20 (AK-20) nitro lacquer. The anodizing time was 3 h, the obtained coat was 150 - 180 μ thick. Ingots of six aluminum alloys with copper (3 - 8% Cu) and four magnesium alloys with zinc (3 -5% Zn) were cast in the molds, the maximum alloy temperature prior to casting being 720 - 740°C. The alloys were melted under a flux, which, for the aluminum alloys consisted of 55% KCl and 45% NaCl, for the magnesium alloys of 54% KCl and 46% LiCl. After the casting of these 10 ingots the anode coat remained completely intact while its hardness even increased somewhat due to dehydration. The walls of aluminum molds should be thicker than those of iron molds. The use of additional external cooling makes it possible to use aluminum chill molds also for metals with higher melting points. There are 1 figure and 4 Sovietbloc references.

Card 2/2

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CIA-RDP86-00513R001963710005-9

22003 8/076/61/035/004/019/018 B106/B201 also 1043, 1208, 1087 18.7400 Zalivalov, F. P., Tyukina, M. N., and Tomashov, N. D. AUTHORS: Effect of conditions of electrolysis upon the formation and TITLE: growth of anodic oxide coatings on aluminum PERIODICAL: Zhurnal fizicheskoy khimii, v. 35, no. 4, 1961, 879 - 886 TEXT: A study has been made of the microstructure of anodic oxide coatings on aluminum with the aid of an 3M-3 (EM-3) electron microscope. The coatings were obtained in sulphuric medium by the method of hard anodizing. This special procedure, which has been developed at the authors' institute (Ref. 4: N. D. Tomashov, Vestn. inzh. i tekhn., no. 2, 59, 1946; Ref. 5: N. D. Tomashov, M. N. Tyukina, Issledovaniya pc korrozii metallov (Tr. In-ta fiz. khimii AN SSSR) vyp. II, Ne. 1, Isdave AN SSSR, M., 1951), ensures an efficient protection of the surface of aluminum alloys not only from corresion, but also from wear by friction and other erosive actions. The coatings are thermally stable, and provide an insulation against heat and electric current. A Y9M -3 (UEM-3) electron Card 1/5

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Effect of conditions of ...

microscope was also used for certain examinations. The pictures were obtained in enlargements of 8000 to 12000. A maximum 60000-fold enlargement was obtained by further photographic enlargement. The specimens consisted of AB 000 (AV000) aluminum (99.99% Al) and were 15*15*2 mm in size. Prior to anodizing, the specimens were ground, pollshed with a fine aluminum oxide suspension, and degreased. The anodic oxidation took place in 4 N sulfuric acid at 0.5°C and at current densities of 25, 50, and 100 ma/cm², or initial voltages of 22, 25, and 27 v. The duration of oxidation was varied between a few seconds and 120 minutes. The microstructures of very thin and very thick coatings could thus be intercompared. During oxidation the electrolyte was vigorously intermixed in order to obtain more homogeneous coatings. The diameter of the pores of the coatings that were obtained was determined with the electron microscope. The number of pores per unit area of coating was established from the quantity of oxide cells per unit area. The very thin coatings $(d = 0.05-0.08\mu)$ obtained in the initial stage of anodic oridation were examined directly in the electron microscope after being detached from the aluminum surface in a sublimate solution. A copy was prepared of the thick coatings ($\delta = 50-100 \mu$) resulting from longer anchizing under the Card 2/5

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Effect of conditions of ...

same conditions. For this purpose, a very thin layer of collocion or quartz was applied to the surface of oxidized aluminum, which took up the relief of the oxide coating concerned. This copy was studied in the electron microscope. Results: The coatings submitted to investigation are no dense oxide layers irregularly traversed by channel-shaped pores, but constitute dense packings of cells in the form of hexagonal prisms resting normally to the metal surface, and connected to one another at the side faces. These results were compared with the structures of coatings obtained under usual conditions of anodic oxidation in sulfuric acid, For this purpose, aluminum specimens were anodically oxidized at 20° C and a current density of 10 ma/cm², and an initial voltage of 10 v. The mean diameter of the pores in the coatings was found to be independent of the method of anodizing in sulfuric acid, and to amount to 120 A. It was established on the other hand that coatings produced by the above described method of hard anodizing exhibit basically new properties. They display a great hardness and stability against wear by friction. These improved properties are based upon an enlargement of oxide cell dimensions (by a thickening of the walls) and upon the reduction of the number of pores per unit area of the coating. The scientific workers of the

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F.P., Tyukina, M.N., Tomashov, N.D.

Properties and microstructure of thick layers of anodic films

AUTHORS:

TITLE:

Zhurnal vsesoyuznogo khimicheskogo obshchestva imeni D.I. Mendeleyeva, v. 7, no. 2, 1962, 235 - 236 PERIODICAL:

The effect of the conditions of electrolysis in sulfuric acid on microstructure characteristics of anodic layers was demonstrated in earlier papers. The effect of the microstructure of anodic layers on their properties is investigated in the present work. Electrodes of A B 000 (AV 000) aluminum containing 99.99% Al were used and anodic oxidation was carried out in 4 N $\rm H_2SO_4$, according to a method of the present institute. These conditions allowed the preparation of layers with different, but exactly defined structures. It was observed that an increase of the oxide cell of structure (distance between two parallel planes of the cell, which increases with current density) also increases the micro-hardness and strength of the anodic layer. Thus with an increase of aluminum oxide cell from 280 Å to 547 Å micro-hardness increased from 350 to 600 kg/nm².

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Properties and microstructure

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Since the diameter of the pores remains constant and the increase of the cell is effected by an increase of the thickness of the walls; the rise in micro-hardness and endurance is easily to explain. Therefore, in the manufacture of anodic coatings with high mechanical properties, electrolytic conditions must be applied which allow formation of coarse structure cells. No protection can be effected by the aluminum oxide layer in modia which dissolve the oxide. In these media the layer between metal and oxide film protects the metal. The thickness of this barrier layer was determined by a method described by N. Vernik and R. Pinner. Chemical resistance of the anodic layer increases with the thickness of the barrier layer, since the latter prevents the penetration of agressive ions through 102 Å to 266 Å increases more than twice the time necessary for the penetration of agressive ions. There are 2 figures and 4 references.

ASSOCIATION:

Institut fizicheskoy khimii Akademii nauk SSSR (Institute of Physical Chemistry of the Academy of Sciences, USSR)

SUBMITTED: May 14, 1961

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<u>I. 1652-66</u> <u>ETT(m)/HPF(c)/T/EMP(t)/I</u>	EHP(k)/ENP(b)/ENA(c) LJP(c) EW/JD/EW/DJ
ACCESSION NR: AP5021583	UR/0286/65/000/013/0055/0055 665.5
	5%
AUTHOR: Veyler, 8. Ye.; Petrova, N Tomashov, N. D. 14.51	V.; Malivalov. F. P.; Likhtman, V. I.;
44.55	
TITLE: Method for applying lubricat	ing film. Class 23, No. 172445
SOURCE: Byulleten' inobreteniy i t	ovarnykh znakov, no. 13, 1965, 55
TOPIC TAGS: lubrication, film lubr	ication, solid indricent
ABSTRACT: This Author Certificate	introduces a method for hot working aluminum and yer serves as the lubricant. (2 27 [Aii]
its alloys in which the snodized is	yer serves as the <u>indricant</u> . 10 27 [Aui]
ASSOCIATION: none	
SUBMITTED: 16Jul62	ENCL: 00 SUB CODE: IE ,HH
NO REF SOV: 000	OTHER: 000 ACD PRESS: 409;
NO WEF DOA:	
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28533-66 EWT (m)/EWA (d)/EWP(t)/ETI IJP(c) JH/JD/WD/GD CC NR: AT6013799 / ()) SOURCE CODE: UR/0000/65/009/000/0200/020	70	
JTHOR: Tomashov, N. D.; Zalivalov, E. F.	8-41	
RG: none		
ITLE: Investigation of the barrier layer of thick anodic films on aluminum	1	
DURCE: Korroziya metallov i splavov (Corrosion of metals, and alloys), no. oscow, Izd-vo Metallurgiya, 1965, 200-207		· .
OPIC TAGS: loop oscillograph, anodization, aluminum, oxide formation, corride ielectric breakdown, surface film/ <u>MPP-2</u> loop oscillograph, AV000 extra-pur 20 BSTRACT: Considering the widespread use of the method of thick-film anodi he definite effect of the barrier layer on such properties of porous anodi- orrosion resistance and resistance to dielectric breakdown, the authors in he thickness of the barrier layer as a function of applied voltage, temper lectrolyte concentration and anodizing time. The tests were performed on 20x20x2 mm) of AV000 extra-pure cast aluminum (99.997 Al), anodically oxid	zing and c films as vestigate ature, specimens ized in	
20x20x2 mm) of AV005 extra-pure cast alonatidat (South and a second seco	, 481;	
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ACC NR: AT6013799	2	
voltage applied (at the rate of somewhat more than 10 Å/v and decreases increasing electrolyte temperature (owing to the attendant increase in power of the electrolyte); it also decreases with increasing ll_2SO_4 conc (from 2N to 8N), though not as steeply as with increasing temperature. effect of anodizing time on barrier-layer thickness, this thickness cha during the first few seconds, when the curve passes through a peak, whe remains constant even for films whose anodizing time lests for 15 min at Curves plotted with the aid of an MPP-2 loop oscillograph show that the barrier-layer thickness is accompanied by an increase in terminal volta firmed by measurements of ohmic resistance, which increases from 10 to when the layer thickness increases from 56 to 300 Å; as in the case of anodizing time, however, this increase soon passes through its peak and owing to the cnset of the formation of the porous structure since the current intensity enhances the aggressive effect of the acid (the ohmi- of the oxide film decreases in the pores). Hence, the following theor offered; the first pores in the oxide film arise at some defective spo or at the crystallite boundaries. The growth of the pore at the outer barrier film is accompanied, at the film-metal interface, by the growt layer of oxide whose individual cells are shaped like a semisphere who faces the metal. During the first few seconds of anodizing, when the	centration As for the anges only ereupon it and longer. e increase it. age, as con- 18 ohm-cm the effect of d steadies out he increase in c resistance y may be its, e.g. cracks part of the ch of a new as convex side	
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法财产的保险 计可能计记录器 L 28533-66 \mathcal{O} ACC NR: AT6013799 voltage applied (at the rate of somewhat more than 10 Å/v and decreases with increasing electrolyte temperature (owing to the attendant increase in the dissolving power of the electrolyte); it also decreases with increasing H_2SO_4 concentration (from 2N to 8N), though not as steeply as with increasing temperature. As for the effect of anodizing time on barrier-layer thickness, this thickness changes only during the first few seconds, when the curve passes through a peak, whereupon it remains constant even for films whose anodizing time lasts for 15 min and longer. Curves plotted with the aid of an MPP-2 loop oscillograph show that the increase in barrier-layer thickness is accompanied by an increase in terminal voltage, as confirmed by measurements of ohmic resistance, which increases from 10 to 18 ohm-cm when the layer thickness increases from 50 to 300 Å; as in the case of the effect of anodizing time, however, this increase soon passes through its peak and steadles out owing to the onset of the formation of the porous structure -- since the increase in current intensity enhances the aggressive effect of the acid (the obnic resistance of the oxide film decreases in the pores). Hence, the following theory may be offered: the first pores in the oxide film arise at some defective spots, e.g. cracks or at the crystallite boundaries. The growth of the pore at the outer part of the barrier film is accompanied, at the film-metal interface, by the growth of a new layer of oxide whose individual cells are shaped like a semisphere whose convex side faces the metal. During the first faw seconds of anodizing, when the peak thickness Card 2/3

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covered by the "building block electrolyte rea of new layers o oxide film, what	layer is reached pores, with the cs" of porcus and aches the barrien of oxide. Thus, atever its thicks Orig. art. has:	attendant grou odic films. In c layer via the it may be assu- ness, grows abo	wth of oxide the course pores, thus med that the ove the barri	cells represe of film growt leading to t	enting the in the the formation of the enough	
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	للمالية والمحمد بالمراجع والمتصوصية الامتمار	حفيه هم الله المحمدي من المحمد حارف م	وأحصد بالمشامين والاحتار ويؤتد المس			

1	<u>28535-66</u> EWI(m)/EWP(t)/ETI LJP(c) JH/JD/WB/GD ACC NR: AT6013797 (N) SOURCE CODE: UR/0000/65/000/000/0160/0190
•	AUTHOR: Tomashov, N. D.; Zalivalov, F. P. B+
T	TITLE: Formation and growth of anodic oxide films on sluminum alloys
	SOURCE: Korroziya matullov i splavov (C <u>orrosion of metals</u> and alloys), no. 2. Soscow, Izd-vo Metallungiya, 1965, 180-190 (4
	OPIC TAGS: anodization, aluminum base alloy, intermetallic compound, electric notential, corrosion
a o	BSTRACT: Considering that the anodizing of alloys with a substantial content of alloy components involves special difficulties and, on the other hand, the anodic exidation of homogeneously structured Al alloys has been fairly well investigated, this study deals with the anodic exidation of heterogeneous Al alloys. To this end,
t 5	the authors melted special binary alloys (15% Mn, 35% Si, 12% Fe, 46% Cu, 45% Mg, 55% Zn) in which the intermetallic compounds represented large crystals with surface area of from 1 to 2-3 mm ² . Voltage-time curves were plotted for the overall surface
o c	of the alloy as well as for the individual components of the alloy the eutectic a prystal. In addition, the alloy potential before and after anodic oxidation was measured with respect to a Hg_2SO_4 reference electrode. The anodizing was performed

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Found that, in the process of inAl6 get covered with a thin bual3 crystals, during anodiz anodic film depending on the smaller crystals, as well as to dissolve, while larger cry baset of anodizing pass into and Al-Zn alloys leads to an as evidenced by the fact that its original value immediated individual Al alloy displays its structural components; of guished as regards the effect with Mn and Si, for which the (MnAl6 and Si crystals) get of includes alloys with Fe and (protected against corrosion of concludes alloys with Mr and Z	anodizing, such alloy component i oxide film and pass into anodic ing they may either completely d location of crystals in the allo crystals present at the alloy su ystals not present directly at the the anodic film. By contrast, t intensive dissolution of their i the potential of the Al-Mg and by after the anodic current is di special features of its own dependent to f anodic oxidation: the first to of anodic oxidation: the first covered with a thin dense oxide fil to, whose intermetallic compounds even when covered by an oxide fil to, which completely lack a prote orig. art. has: 6 figures and b	issolve or pass into issolve or pass into y and their size; arface are most prone te alloy surface at the the anodizing of Al-Mg intermetallic components Al-Zn alloys returns to isconnected. Thus, every ending on the lature of alloys may be distin- group includes alloys the structural components film; the second group are insufficiently im; and the third group active oxide film and so
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ACC NRI ATGO13798	/EHF(t)/ETI (N))	SOURCE CODE:	ur/0000/65/00	0/000/0191/019	19i
					51
UTHOR: Tomishov,	N. D.; Zelivel	ov, F. P.			49 1
RG: none					Bt /
		ton sin sin sin sin sin sin sin sin sin si			
ITLE: Electric in	sulation prope	rties of this	ek anodic oxide	ELIDE ON ALU	unum and its
lloys			·		-1
OURCE: Kornoziya	metallov i spl	avov (Corros	Lon of metals/s	ind alloys), no	. 2
loscow, Izd-vo Meta	11ungiya, 1965	5, 191-199	د)		-
OPIC TAGS: test r	in alastria i	neuletion A	folgetric brack	down artife f	mation.
	ig. electric i	usuration, a	rerective preas	answirt ovrage re	
				allov	1
				al.loy	
modic oxidation, a BSTRACT: The arti	nodization/UPU cle deals with	I-l test rig, I the effect (AMts aluminum of certain fact	ors (the compo	osition of
nodic oxidation, a BSTRACT: The arti 1 alloys, the dens	nodization/UPU cle deals with ity of anodic	I-1 test rig, the effect current, pre	AMts aluminum of certain fact heating of the	cors (the compo film, and nate	re of dis-
modic oxidation, a BSTRACT: The arti 1 alloys, the dens uptive current) on	nodization/UPU cle deals with ity of anodic the breakdown	J-1 test rig, the effect current, pre- voltage U _{br}	AMts aluminum of certain fact heating of the each of thick (cors (the compo film, and nato (33-75 µ) anode	re of dis- films.
BSTRACT: The arti BSTRACT: The arti 1 alleys, the dens uptive current) on the tests were perf evice (Fig. 1) att	nodization/UPU cle deals with ity of anodic the breakdown onned at room ached to a sta	I-1 test rig, the effect current, prei voltage U _{br} temperature indard UPU-1	AMts aluminum of certain fact heating of the eakd of thick (with the aid of test rig for de	film, and nate (33-75 µ) anode a specially of etermining die	re of dis- films. leveloped lectric
BSTRACT: The arti BSTRACT: The arti 1 alloys, the dens uptive current) on the tests were perf evice (Fig. 1) att strength with the a	nodization/UPU cle deals with ity of anodic the breakdown ormed at room ached to a sta id of direct a	I-1 test rig, the effect current, pred voltage U _{br} temperature andard UPU-1 and alternation	AMts aluminum of certain fact heating of the eakd of thick (with the aid of test rig for de ng currents (on	tors (the composition, and nate (33-75 µ) anode a specially of etermining diel utput voltage	re of dis- films. leveloped lectric imits: 0-1,
nodic oxidation, a BSTRACT: The arti 1 alloys, the dens uptive current) on he tests were perf evice (Fig. 1) att trength with the a	nodization/UPU cle deals with ity of anodic the breakdown ormed at room ached to a sta id of direct a	I-1 test rig, the effect current, pred voltage U _{br} temperature andard UPU-1 and alternation	AMts aluminum of certain fact heating of the eakd of thick (with the aid of test rig for de ng currents (on	tors (the composition, and nate (33-75 µ) anode a specially of etermining diel utput voltage	re of dis- films. leveloped lectric imits: 0-1,
nodic oxidation, a BSTRACT: The arti 1 alloys, the dens uptive current) on the tests were perf evice (Fig. 1) att	nodization/UPU cle deals with ity of anodic the breakdown ormed at room ached to a sta id of direct a	I-1 test rig, the effect current, pred voltage U _{br} temperature andard UPU-1 and alternation	AMts aluminum of certain fact heating of the eakd of thick (with the aid of test rig for de ng currents (on	tors (the composition, and nate (33-75 µ) anode a specially of etermining diel utput voltage	re of dis- films. leveloped lectric imits: 0-1,
nodic oxidation, a BSTRACT: The arti 1 alloys, the dens uptive current) on he tests were perf evice (Fig. 1) att trength with the a	nodization/UPU cle deals with ity of anodic the breakdown ormed at room ached to a sta id of direct a	I-1 test rig, the effect current, pred voltage U _{br} temperature andard UPU-1 and alternation	AMts aluminum of certain fact heating of the eakd of thick (with the aid of test rig for de ng currents (on	tors (the composition, and nate (33-75 µ) anode a specially of etermining diel utput voltage	re of dis- films. leveloped lectric imits: 0-1,
nodic oxidation, a BSTRACT: The arti 1 alloys, the dens uptive current) on he tests were perf evice (Fig. 1) att trength with the a	nodization/UPU cle deals with ity of anodic the breakdown ormed at room ached to a sta id of direct a	I-1 test rig, the effect current, pred voltage U _{br} temperature andard UPU-1 and alternation	AMts aluminum of certain fact heating of the eakd of thick (with the aid of test rig for de ng currents (on	tors (the composition, and nate (33-75 µ) anode a specially of etermining diel utput voltage	re of dis- films. leveloped lectric imits: 0-1,

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alloys display high electric insulating properties. In certain cases the breakdown voltage of these may reach 2000-2500 v. Generally, the breakdown voltage varies with every type of alloy. Thus, for all plastically worked alloys (except <u>Duraluminum</u> and <u>AMts</u>) the absolute values of U_{breakd} exceed 1000 v in the presence of 40-70 μ thick¹⁰ films, whereas U_{breakd} for cast Al alloys (on which the films obtained are 50-65 μ thick) baraly exceed 500 v, i.e. are about one-half as high. The markedly lower values of U_{breakd} recorded for cast alloys, as opposed to homogeneous plastically worked alloys, may be attributed to the presence in the anodic film of Si crystals (since cast Al alloys contain larger amounts of Si) which, during anodizing, pass from the alloy to the film. Ubreakd is also affected by the geometry of the speci-men: on convex surfaces U breakd is higher than on concave surfaces; this is due to the cracks on the film surface, which are greater on a concave surface than on a convex one. Likewise, Upreakd also increases with increasing preheating temperature of the film. The use of AC in breakdown tests also reduces the electric insulating; properties of the films. The decisive factor affecting Ubreakd of the film is its thickness and structure: U_{breakd} increases with film thickness; the anodizing con-ditions (electrolyte composition, density and nature of current) affect Ubreakd only to the extent to which they affect the thickness and structure of the film. Or g. art. has: 6 figures, 2 tables OTH REF: 003 007/ SUB CODE: 21, 07 SUBM DATE: 19Jul65/ ORIG REF: Card

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ACC N	R: AT7004173 . SOURCE CODE: UR/0000/66/000/000/0221/0226
UTHOF	: Veyler, S. Ya.; Petrova, N. V. Zalivalov, F. P.; Tomashov, N. D.; Likhtman, (Deceased)
ORG:	none
TTLE:	Effect of anodizing on friction in hot and cold drawing of aluminum
i onny	: AN SSSR. Institut fizicheskoy khimii. Korroziya i zashchita konstrukt- kh splavov (Corrosion and protection of structural alloys) Moscow, Izd-vo 1966, 221-226
OPIC lumin	TAGS: METAL drawing, adminum cold drawing, adminum anodic oxidatior, um drawing lubricant, DRAWN ALUMINUM, ALUMINUM OXIDE, METALFILM
vestig mens t lrawin of met	CT: The role of oxide films in cold and hot drawing of aluminum has been in- ated. It was found that aluminum-oxide films formed on the surface of speci- y long exposure to the atmosphere at 20-300°C did not affect the process of g. However, aluminum-oxide films formed by anodizing prevented the sticking al to the die and decreased the resistance to drawing. Oxide film, 10 μ thick,
ance a lrawin out an	sed the cold drawing resistance from 600 to 210 kg, and the hot-drawing resist- t 300°C from 200 to 150 kg. Anodizing was particularly beneficial in hot g: without lubrication it was impossible to draw aluminum even at 1% reduction, odized aluminum was hot drawn with up to 13-15% reduction.
SUB CC Card	DE: 13/ SUBM DATE: 27Sep66/ ORIG REF: 007/



"APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963710005-9 ZHURAVIEVA, Yekaterina Ivanovna; SERBA, Vladimir Nikitovich; LUNIN, O.G., kand.tekhn.nauk, retsenzent; ZALIVANSKAYA, S.M., retsenzent; SOKOLOVSKAYA, T.A., red.; SETAROVA, A.M., tekhn. red. [Manufacture of caramel] Ptoizvodstvo karameli. Moskva, Pishchepromizdat, 1962. 106 p. (MIRA 15:7) (Caramel)

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"APPROVED FOR RELEASE: 09/19/2001 CIA-RDP86-00513R001963710005-9 ZALIVCHIY, V.N. 112-2-4764 TRANSLATION FROM: Referativnyy zhurnal, Elektrotekhnika, 1957, Nr 2, p. 327 (USSR) Zalivchiy, V.N., Zipir, A.D. Research by the Pulse Method Along the Saturation Line AUTHORS: on the Absorption of Ultrasound in Ortho-and Metaxylols (Issledovaniye pogloshcheniya ul'trazvuka v orto-i TITLE: mitaksilolakh impul'snym metodom po linii nasyshcheniya) PERIODICAL: Sbornik stud. nauch. rabot po yestv.-matem. tsiklu. Mosk. obl. ped. in-t, 1956, Nr 1, pp. 32-38 The pulse method used differed from the methods described previously. Here a quartz crystal generating bilateral radiation and two (instead of one) reflectors disposed at fixed distances along both sides of the crystal radiator were used. ABSTRACT: Absorption was determined by comparing the amplitudes of the pulses received from the reflectors. The absorption factor of orthoxylol was measured at the frequency 7.5 mc and in the tem-perature interval 19.5° to 325°, and for metaxylol at the fre-quency 15.1 mc and in the temperature interval 17° to 275°. It was determined that the absorption factor relative to the square Card 1/2

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112-2-4764 Research by the Pulse Method Along the Saturation Line (Cont.) of the frequency increases in the whole temperature interval. The space viscosity and that part of the absorption due to drift viscosity (Stokes absorption) were calculated from the experimental data. It was determined that qualitatively, absorption determined experimentally and absorption as calculated by the Stokes law methods did not agree in the whole temperature interval. The Stokes absorption was less than the absorption determined experimentally. In the entire temperature interval, absorption determined experimentally for metaxylol is somewhat higher than in the case of orthoxylol at the same temperatures. L.M.L. ASSOCIATION: Moscow Oblast Pedagogical Institute (Mosk. obl. ped. in-t) Card 2/2

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	PHASE I BOOK EXPLOITATION SOV/5644	
	 Vserossiyskaya konferentsiya professorov i prepodavateley pedagogicheskikh institutov Primeneniye ul' traakustiki k issledovaniyu veshchestva. vyp. 10. (Utilization of Ultrasonics for the Investigation of Materials. no. 10) Moscow, Izd-vo MOPI, 1960. 321 p. 1000 copies printed. 	
	Eds.: V. F. Nozdrev, Professor, and B. B. Kudryavtsev, Professor.	
	 PURPOSE: This book is intended for physicists and engineers interested in ultrasonic engineering. COVERAGE: The collection of articles reviews present-day research in the application of ultrasound in medicine, chemistry, physics, metallurgy, ceramics, petroleum and mining engineering, defectoscopy, and other fields. No personalities are mentioned. References accompany individual articles. 	 •
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了这些意义的保持,我们的时候,但可能们就是这些问题,我们一般,你还能是有些非常有些意义的,你必须不可能让你的问题。""San and an	
Utilization of Ultrasonics (Cont.) SOV/5644	
Belinskaya, L. B., and B. A. Belinskiy [Moscow Oblast Poly- technical Institute imeni Krupskaya]. Energy Losses in the Electrical and Acoustical Lines of a Pulsed Ultrasonic Device	255
Gershenzon, Ye. M. [MGPI im. V. I. Lenina - Moscow State Pedagogical Institute]. The Passage of Electromagnetic Centimeter-Length Waves Through a Longitudinal Ultra- sonic Screen	265
Zakurenov, V. M. [Shuyskiy pedinstitut - Shuya Pedagogical Institute]. The Problem of Ultrasonic-Wave Absorption in Complex Esters of Formic Acid	269
Zalivchiy, V. N. [Moscow Oblast Polytechnical Institute imeni N. K. Krupskaya]. The pulse Method of Studying	
Card 9/10	

CIA-RDP86-00513R001963710005-9

5 s/081/62/000/008/022/057 B160/B101 Zalivchiy, V. N., Perepechko, I. I. 10 Ultrasonic interferometer for measuring the speed of ultra-AUTHORS: sound in liquids and gases Referativnyy zhurnal. Khimiya, no. 8, 1962, 147, abstract TITLE: 8Ye5 (Sb. "Primeneniye ul'traakust. k issled. veshchestva". no. 12, M., 1960, 132 - 134) 115 PERIODICAL: TEXT: A description is given of the design of an interferometer designed for measuring the speed and absorption of ultrasonic waves in gases and liquids with precise adjustment of the parallelness of the radiating quartz crystal and the reflector. The oscillator used is a standard instrument which will permit a smooth change in frequency when the quartz radiating elements are changed. The reflector is set parallel to the radiator from the maximum stress across the crystal. [Abstracter's note: Complete translation.] Card 1/1

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