

CIA-RDP86-00513R032932930002-8

MATVEYEV G.A.

MATVEYEV, G. A. (Ed.; Doctor of Technical Sciences)

Moscow. Energeticheskly institut

- Istoriya energeticheskoy tekhniki SSSR v trekh tomakh. t. 1: Teplotekhnika (History of Power Engineering in the USSR in Three Volumes. v. 1: Heat Engineering) Moscow, Gosenergcizdat, 1957. 479 p. 5,000 copies printed.
- Ed.-Compiler: Konfederatov, I.Ya., Doctor of Technical Sciences; Authors: Badyl'kes, I.S., Doctor of Technical Sciences; Belindkiy, S.Ya., Candidate of Technical Sciences; Gimmel'farb, M.L., Candidate of Technical Sciences; Kalafati, D.D., Gandidate of Technical Sciences; Kertselli, L.I., Professor; Kovalev, A.P., Doctor of Technical Sciences; Konfederatov, I.Ya., Doctor of Technical Sciences; Lavrov, V.N., Doctor of Technical Sciences; Lebedev, P.D., Doctor of Technical Sciences; Lukinskiy, V.V., Doctor of Technical Sciences (deceased); Petukhov, B.S., Doctor of Technical Sciences; Satanovskiy, A.Ye., Doctor of Technical Sciences; Semenenko, N.A., Doctor of Technical Sciences; Smel'nitskiy, S.G., Candidate of Technical Sciences; Sokolov, Ye.Ya., Doctor of Technical Sciences; Chistyakov, S.F., Candidate of Technical Sciences, and Shcheglyayev, A.V., Corresponding Member, USSR Academy of Sciences; Editorial Board of set: Bel'kind, L.D., Doctor of Technical Sciences; Glazurov, Doctor of Technical Sciences; Colubtsova, V.A., Doctor of Technical Sciences; Zolotarev, T.L., Doctor of Technical Sciences; Izbash, S.V., Doctor of Technical Sciences; Kirillin, V.A., Corresponding Member, USSR Academy of Sciences; Zolotarev, T.L., Doctor of Technical Sciences; Izbash, S.V., Doctor of Technical Sciences; Kirillin, V.A., Corresponding Member, USSR Academy of Sciences;

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Konfederatov, I.Ya., Doctor of Technical Sciences; Margulova, T.Kh., Doctor of Technical Sciences; Meshkov, V.V., Doctor of Technical Sciences; Petrov, G.N., Doctor of Technical Sciences; Sirotinskiy, L.I., Doctor of Technical Sciences; Styrikovich, M.A., Corresponding Member, USSR Academy of Sciences; and Shneyberg, Ta.A., Candidate of Technical Sciences. Ed.: <u>Matveyev, G.A.</u>, Doctor of Techniccal Sciences; Technical Ed.: Medvedev, L.Ya.

PURPOSE: The book is intended for technicians in all branches of heat engineering.

COVERACE: This book presents the development of the basic branches of heat engineering in the Soviet Union and it is the first volume of 3 volumes entitled History of the Power Technology in the USSR. The first chapter gives a concise history of the development of heat engineering from its very beginning to the middle of the 19th Century when the fundamentals of the theoretical heat engineering were established. A detailed Lescription of the development of heat engineering in pre-Revolutionary Russia is given in Ch. 2 to 5 and its status before 1917 is described. In the main part of the volume, Ch. 6 to 16, the development of worious branches of the Soviet heat engineering is presented. The theoretical fundamentals of heat engineering, of manufacturing boilers, turbine installations of heat power plants, district heating, heat control, automation of thermal processes, and cooling techniques are covered extensively. Each chapter is supplemented with a bibliography. The took is illustrated with photographs, charts and diagrams, worked out by the authors of the respective chapters. At the end of the book there is a chronological list of significant events in the development of heat engineering.

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AUTHOR:	Markov, N.M. and Matveyev, G.A., Candidates of Technical Sciences.	ж ч.
TITLE :	On detemining the flow rate of the operating medium through the ring (cascade) of turbine blades (K voprosu ob opredelenii raskhoda pabochego beshchestva cherez venets (reshetku) turbinnykh lopatok.)	
PERIODICAL:	"Energomashinostroenie" (Power Machinery Construction) 1957, No. 2, pp. 14 - 15, (U.S.S.R.)	
ABSTRACT :	Existing methods are reviewed and a new method is proposed, which is based on utilising the epures of the pressure (speed) distribution along the contour of the profile. The increasing initial steam parameters bring about a considerable decrease of the flow surfaces in the first stages of the turbines and lead to a reduction of the height of the blades in these turbines and, thus, to a decrease in the efficiency cwing to the increase of the relative importance of the end losses. For reducing their influence, blades with small outflow angles (8 to 11) of the stream are used. It is shown that, for such cascades, utilisation of experimental data of the outflow angles of the flow may lead to considerable errors in deter- mining the rate of flow of the operating medium. Modern, experimental, aerodynamic methods enable determination of the outflow angle of the flow with an accuracy of $\pm 1\%$ and for such accuracy, the error in determining the rate of flow of	
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SOV/96-58-11-7/21 Styrikovich, M.A., Corresponding Member of the AUTHOR: Academy of Sciences JSSR Doctor of Technical Science Matveyer, G.A., Engineer Popyrin, L.S., The Selection of End Pressure (Vacuum) for Large TITLE: Regional Electric Power Stations (Vybor konechnogo davleni, a dlya GRES bol'shoy moshchnosti) PERIODICAL: Teploenergetika 1958, Nr 11, pp 42-46 (USSR) In designing large power stations it is not usual to make individual prescriptions for the technical ABSTRACT: and economic features of the condensing equipment and water-supply systems. On the contrary, to secure the greatest possible standardisation, the turbine manufacturers make a single type of condenser for a given type of turbine. As will be seen from Table 1, all Soviet turbines now produced or projected are intended for a vacuum of 0.03 - 0.035 atm and have condensers with a specific steam loading in the range $35 - 46 \text{ kg/m}^2 \text{ nr}$. The power station water-supply is designed in accordance with the manufacturer's data on the Card 1/4

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SOV/96-58-11-7/71 The Selection of End Pressure (Vacuum) for Large Regional Electric Power Stations This leads to irrational results; in condensers. a number of large power stations with turbines of 200 MW located in various climatic regions and burning fuels of different costs, identical condensers are used as observed in Table ?. The turbine manufacturers should now provide a range of condenser sizes for each type of turbine. Fuel costs are particularly important in this matter since they may range from 140 roubles per ton in the European part of the country to 10 roubles per ton in Siberia. Local climatic conditions and, therefore, coolingwater temperature, vary widely. Cooling-water conditions are at present simply taken from an All-Union standard. Determination of the vacuum from the annual mean cooling-water temperature gives rise to considerable error and it would be better to use monthly mean figures. The conditions that should be assumed for technical and economic calculations on condensers are then discussed. In Card 2/4

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SOV/96-58-11-7/21 The Selection of End Pressure (Vacuum) for Large Regional Electric Power Stations

> determining the power consumption of circulating pumps, allowance is made for a considerable reduction in output during the winter season. Fig.2. graphs the relationship between power expenditure on circulation-pump drive and power loss in the turbine resulting from impaired vacuum for three different climatic regions of the country. The method of making economic comparisons between different types of condensing conditions is explained. Replacement and repair costs for two variants are compared in table 3. A graph showing various condenser characteristics as a function of fuel cost and cooling-water temperature is given in Fig.3. The increased useful output of electricity as a function of the cooling-water temperature and fuel costs is seen in Fig.4. The results of calculations of the best water-velocity in the condenser are plotted in Fig.5. The following conclusions are drawn from the calculations. The optimum vacuum in the condenser of a turbine type PVK-200 depends considerably on the cooling-water

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	temperature and the price of fuel; it ranges from 0.075 atm for a cooling-water temperature of 6°C and expensive fuel to 0.45 atm for 15°C and cheap fuel. The standard condenser supplied by the Leningrad Metal Works for turbine type PVK-200 does not permit the greatest economy to be obtained particularly in southern regions or where fuel is expensive. A further two or three types of condenser should be designed for this turbine and characteristics are recommended. Various other recommendations of the
ASSOCIAT	<pre>same kind are made about condenser design. There are 5 figures, 3 tables and ? literature references both of which are Soviet. ION: Energeticheskiv institut AN SSSR (Power Institute,</pre>

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CIA-RDP86-00513R032932930002-8

AUTHOR:

Matveyev, G.A., Professor

SOV/26-59-1-22/34

TITLE: Ways of Power-Engineering Development in the USSR (Puti razvitiya energetiki v SSSR)

PERIODICAL: Priroda, 1959, Nr 1, pp 73 - 82 (USSR)

ABSTRACT : The author gives a brief survey on the electrification of Russia after the October Revolution. In 1957, nearly 210 billion kwh of electric energy were produced in the USSR, 233 billion kwh in 1958. Of this power. about 70% is used for industrial purposes. By 1960 electric-energy production is to reach 320 and by 1965 500 to 520 billion kwh. (grph 1). In order to neet this last figure, the capacity of the elec-tric power stations is to be 108 to 112 million kw, which requires a capacity of 60 tc 65 million kw to be provided for in addition to the existing 50 million kw. The present annual accretion rate of 5 to 6 million kw is to rise to 8 to 9 million kw dur-ing the individual years of the new 7-Year Plan, and to 10 to 11 million kw toward the end of the plan Card 1/7 period. By 1975, the production of electric energy

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is to reach 1,200 billion kwh or a total power plant capacity of 200 million kw. When the Volzhskaya GES (Volga Hydroelectric Power Plant), having a capacity of 2,100,000 kw (20 turbines operating), was put into operation, Khrushchev pointed out that the construction of large thermal power plants during the new plan period will be more important than that of hydro -power plants. While the construction of the Volga Hydroelectric Power Plant took seven years and the cost per installed kw was about 4,000 rubles, the construction of a thermal power plant of a similar capacity would not exceed 4 to 5 years with a cost of 600 to 700 rubles per installed kw. Consequently, the electric power stations with a total capacity of 60 to 65 million kw, to be built by 1965, will consist of thermal power plants with a total capacity of 53 to 55 million kw and hydroelectric power plants with a total capacity of about 8 million kw. With respect to the country's consumption of the principal kinds of fuel for industrial purposes, the

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"APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R032932930002-8 SOV/26-59-1-22/34 Ways of Power-Engineering Development in the USSR swing will be from coal to oil and natural gas (table 1). Hydroelectric power at present contrib-utes 18.7% or 40 billion kwh of the USSR's power production, thermal power over 80%. Stress will be placed on the construction of thermal power plants, while hydroelectric power plants will assume special importance in certain areas. A survey of past and recent turbines and boiler units (Figures 3 and 4) shows that both grew in size, capacity and useful parameters to equal any similar product of any firm on earth. The establishment of powerful condensing stations will permit the construction of ever larger power aggregates. By 1965, the unit capacity of the thermal condensing stations will grow to 2,400,000 kw and that of turbogenerators to 300 to 600 thousand kw at steam parameters of 2"0 atmospheres, a temper-ature of 580°C and an intermediate heat of 565°C. These conditions will increase the importance of continuously operating coil boilars suitable for operation in the supercritical parameters of pressures Card 3/7

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Ways of Power-Engineering Development in the USSR

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over 225 atmospheres. These boilers for 240/580°/565⁽ will comprise 30% of the new installations by 1965. The plan provides for the installation of 100 turbines of 100,000 kw each, over 100 of 150,000 and 200,000 kw, over 40 of 300,000 kw, and 3 of 600,000 kw each. The capacity of one of the latter would equal the total capacity of the Dnepr GES, or that of 10 Volkhov GESes, while three such turbines would equal the capacity of all electric power stations in Russia in 1913. Automation and remote control and improvements will many other technical and mehmical be added, while expenses will be lowered, construction time reduced and fuel consumption lessened. The Yuzhno-Ural'skaya elektrostantsiya (South-Urals Electric Power Station - fig. 8) is a good example of a present-day large thermal power plant which may serve as a model for other projects. The use of natural gas for fuel _1. poses will bring forth the installation of gas turbine units of about 3 million kw capacity. Outside of the general energy system, isol-

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ated gas-turbine electric stations with aggregates of 25 to 50,000 kw each and a combined capacity of 100 to 200,000 kw are planned. Seven such stations would have an aggregate capacity of over 1 million kw with no worse indices than steam-turbine stations have. The installation of 9 electric power stations of the open type of an aggregate capacity of 4 million kw and of 11 stations of the half-open type of about 14 million kw is imminent. Projects on steam para-meters of 400 atmospheres and 700° and still more powerful units for condensing stations are under way. Their production requires new ty s of steel. The plan also provides for the installation of hydrostations of a total capacity of about 8 million kw . The ratio of the projected Yeniseyskaya GES (Yenisey GES), 6,000,000 kw and turbines of 300,000 kw , seems to be much more effective than those of existing hydro power plants (table 2). It will have a mean annual energy output of about 35 billion kw/h at a cost price of about 0.4 kopeks per kw/h. The

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"APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R032932930002-8 . . . SOV/26-59-1-22/34 Ways of Power-Engineering Development in the USSR 1. Volga cascade of 12 GESes (Figure 8) will have an annual energy output of 30 billion kw /h a year. The Siberian GESes are of paramount importance for the establishment of a united energy grid for Siberia. The USSR's first atomic power station (Figure 9) of 5,000 kw capacity consumes about 30 grams of fuel for its energy production in 24 hours as compared with 100 tons of coal that would be required for a similar non-atomic station. At the end of 1958, construction of the first section of a large atomic power station of 100,000 kw, to become a 600,000-kw power station upon completion of all planned sections, was started. The 1956 to 1960 period provides the start of construction of atomic power stations of an ag-gregate capacity of 2 to 2.5 million kw. Several atomic power stations of 400 to 600,000 kw each Card 6/7

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"APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R032932930002-8 SOV/26-59-1-22/34 Ways of Power-Engineering Development in the USSR are to be built in regions that are far away from any fuel deposits. There are 5 graphs, 2 diagrams, 2 photos, and 1 Soviet reference. Energeticheskiy institut im. G.M. Krzhizhanovskogo AN SSSR /Moskva (The Power Engineering Institute ASSOCIATION: imeni G.M. Krzhizhanovskiy of the AS USSR /Moscow) Card 7/7 Л 0

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 Sov/96-59-4-6/2. AUTHORS: Styrikovich, M.A., Corresponding Member of the Academy of Sciences of the USSR, Matweysv, G.A., Doctor of Technical Sciences and Fopyrin, L.S., Engineer TITLE: Selection of the Best Unit Outputs for Single and Two-shaft Turbines (Vybor optimal'nykh yedinichnykt moshchnostey odnoval'nykh i dvukhval'nykh turbin) PERIODICAL: Teplcenergetika, 1959, Nr 4, pp 31-38 USSR) ABSTRACT: The advantages of using very large turbines are first discussed. The problem then arises of when to make them with one and when with two shafts. The common Soviet practice of making single shaft turbines of up to 400 MW with a minimum number of exhausts does not adequately take account of actual operating conditions in the majority of regions of the Soviet Union. The maximum output that can be obtained from a single exhaust condensing turbine with given initial steam conditions and regenerated cycle is governed by the flow of stean through the section of the last stage of the turbine. In the next few years the turbine manufacturers will use actual back 940 mm bare of 2000 mm wheth does not adequately the section of the last stage of the turbine. 		
 AUTHORS: Styrikovich, M.A., Corresponding Member of the Academy of Sciences of the USSR, MatveyJv, G.A., Doctor of Technical Sciences and Popyrin, L.S., Doctor of Technical Sciences and Two-shaft Turbines (Vybor optimal'nykh yedinichnykh moshchnostey odnoval'nykh i dvukhval'nykh turbin) PERIODICAL: Teplcenergetika, 1959, Nr 4, pp 31-38 (USSR) ABSTRACT: The advantages of using very large turbines are first discussed. The problem then arises of when to make them with one and when with two shafts. The common Soviet practice of making single shaft turbines of up to 400 MW with a minimum number of exhausts does not adequately take account of actual operating conditions in the majority of regions of the Soviet Union. The maximum output that can be obtained from a single exhaust condensing turbine with given initial steam conditions and regenerated cycle is governed by the flow of steam through the section of the last stage of the turbine. In the next few years the turbine manufacturers will use 		
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 Matury Jv, G.A., Doctor of Technical Sciences and Popyrin, L.S., Engineer TITLE: Selection of the Best Unit Outputs for Single and Two-shaft Turbines (Vybor optimal'nykh yedinichnykh moshchnostey odnoval'nykh i dvukhval'nykh turbin) PERIODICAL: Teplcenergetika, 1959, Nr 4, pp 31-38 (USSR) ABSTRACT: The advantages of using very large turbines are first discussed. The problem then arises of when to make them with one and when with two shafts. The common Soviet practice of making single shaft turbines of up to 400 MW with a minimum number of exhausts does not adequately take account of actual operating conditions in the majority of regions of the Soviet Union. The maximum output that can be obtained from a single exhaust condensing turbine with given initial steam conditions and regenerated cycle is governed by the flow of steam through the section of the last stage of the turbine. In the next few years the turbine manufacturers will ise 	AUTHORS:	Styrikovich, M.A., Corresponding Member of the Academy of
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	ABSTRACT: Card 1/4	discussed. The problem then arises of when to make them with one and when with two shafts. The common Soviet practice of making single shaft turbines of up to 400 MW with a minimum number of exhausts does not adequately take account of actual operating conditions in the majority of regions of the Soviet Union. The maximum output that can be obtained from a single exhaust condensing turbine with given initial steam conditions and regenerated cycle is governed by the flow of steam through the section of the last stage of the turbine.
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Selection of the Best Unit Outputs for Single and Two-shaft Turbines area of 7.3 sq m. Further increase in the total exhaust section and consequently in the turbine output can be obtained by subdividing the steam flow in the last stages of the turbine. There are two practical ways of doing this: either by increasing the number of exhausts to three or four for a single shaft turbine or by using two shaft turbines. The advantages of these approaches are considered in relation to normal cooling water temperatures. The influence of fuel cost on the best size of turbine is also considered. Technical and economic calculations were made for a turbine type PVK-400 in the five variants illustrated in Fig.1 in order to determine the best final steam conditions and the best value of loading of the exhaust section of the last stage. The first variant uses a single shaft, the second and third use two shafts each running at 3,000 mpa with 6 and 8 exhausts respectively. The fourth and fifth variants are two shaft sets running at different speeds. Curves showing the variation in output of these variants Card 2/4

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Selection of the Best Unit Outputs for Single and Mo-shaft Turbines

as the pressure in the condenser is altered are given in Fig.2. The factors that were taken into account in the calculation are described, they include the cost of the turbine, the cost of the generator and the cost of the foundations. These cost data are collected together in table 1. The construction and operating costs are compared using eq.4 with a pay-off time of ten yaars. Efficiency and output curves for the different variants are given in Fig.4. When the final steam conditions the have been adopted for currently produced and proposed future sets, which are given in table 2, are compared with the optimum values, see Fig.3, it will be found that the turbines of the Leningrad and Khar'kov Works cover a very narrow range of variation of the magnitudes that govern the final steam conditions and this reduces the efficiency of power stations using these turbines because insufficient attention is paid to actual operating conditions. Curves relating the best limiting output o? a single shaft turbine with the price of fuel and the cooling water temperature are given in Fig.5. It is seen that in a number of regions of the Soviet Union that

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SOV/96-59-4-6/21 Selection of the Best Unit Outputs for Single and Two-shaft Turbines limiting output of a single shaft turbine ranges as follows: 200 - 250 MW for the South-West and Central European part and 350 - 400 MW for Siberia and the Sout . The best limiting output for two shaft turbines with various total exhaust areas, fuel prices and cooling water temperatures are given in Fig.6. It will be seen from this figure that in different regions of the Soviet Union the best maximum output of a two-shaft turbine varies over a wide range or, to put it enother way. for a turbine of a given output the total exhaust area of the last stages should vary over a wide range to suit diffe:ent conditions. There are 6 figures, 2 tables and 1 Soviet reference. ASSOCIATION: Energeticheskiy Institut AN (SSR (Power Institute Ac.Sc. USSR) Card 4/4

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"APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R032932930002-8 2 STYRIEDVICH, N.A.; MATVEYEV, G.A., doktor tekhn, nauk; RELYAYEV, V.I., insh. Selecting the optimal temperature for flue gases of power boilers. Teploenergetika 7 no.7:27-32 J1 '60. (MIRA 13:7) 1. Energeticheskiy institut AN SSSR. 2. Chlen-korrespondent AN SSSR (for Styrikovich). (Boilers)

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[Power equipment of atomic electric power plants; steam generators and flame steam superheaters] Energooborudovanie atomnykh elektrostantsii; parogeneratory i ognevye paroperegrevateli. Pod red. I.I.I.ovikova. Moakva, Gos.izd-vo lit-ry v oblasti atomnoi nauki i tekhniki, 1961. 197 p. (MIRA 15:1)

1. Chlen-korrespondent AN SSSR (for Kevikov). (Atomic power plants--Equipment and supplies)

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TITLE: The prospects of establishing naval power installations on the basis of magnetohydrodynamic interaction	26.2311 AUTHORS:	8/124/62/00/00 1006/1242 Matweyew, G.A. and Ivanov, P.D.	8/015/030
(Sudostroyeniw, no.2, 1962, 32-36) TEXT: The possibility of utilization of magnetohydrodynamic inter- action for direct conversion of heat (muclear or hydrocarbon) into electrical energy is discussed with regard to neval power installations. Basic equa- sions which characterize the flow of conducting gas in the presence of elect- cic and magnetic fields are considered as an illustration of magnetohydro- lynamics in power conversion. Some information is given on the mechanism of the electrical conductivity of gas and on means for its increase. A basic liagram of a power installations which utilises a magnetohydrodynamic genera- sor is given as an illustration. Mostrailer's note: templete translation.	TITLE:	The prospects of establishing naval power installations	on
Action for direct conversion of heat (muclear or hydrocarbon) into electrical energy is discussed with regard to neval power installations. Basic equa- tions which characterize the flow of conducting gas in the presence of elect- ric and magnetic fields are considered as an illustration of magnetohydro- lynamics in power conversion. Some information is given on the mechanism of the electrical conductivity of gas and on means for its increase. A basic diagram of a power installations which utilises a magnetohydrodynamic genera- tor is given as an illustration.	PERIODICAL:	Referctivnyy zhurnal, Mekhanika, no.8, 51, abstract 883 (Sudostroyeniy, no.2, 1962, 32-36)	30 . /a
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Translation	15-57-3-3846 from: Referati nyy zhurnal, Geologiya, 1957, Nr 3, p 193 (USSR)	
AUTHOR:	Matveyev, G. I.	
title :	New Constructions of Hydraulic-Feed Bits for Drilling in Weak Rocks (Novyye konstruktsii gidromonitornykh dolot dlya bureniya v myagkikh porodakh)	
PERIODICAL:	Novosti neft. tekhniki. Neftepromysl. delo, 1956, Nr 6, pp 4-6	
ABS TR ACT :	Oil Drilling Division of the All-Union Scientific Research Institute has developed a bit, GS-9M (214 mm in diameter), with lateral perforations for the drilling fluids. The drilling muds are led to the hole bottom through a pipe, which is made in one piece with paddles. A strong jet of drilling fluid is directed toward the peripheral part of the hole bottom, flushing it. Large, widely spaced teeth are arranged on the surface of the cutting tool. The teeth in the last two rows are stag-	a .
Card 1/2	gered. The axis of the cutting tool is displaced 5 mm.	

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Pranslation	15-57-3-3849 from: Referativnyy zhurnal, Geologiya, 1957, Nr 3, p 193
AUTHORS:	Matveyev, G. I. Travkin, V. S.
ri tle :	The Construction of a Bit Which Helps in Maintaining the Gauge of Drill Heles (Konstruktsiya dolota, uluch- shayushchaya kalibrovku skvazhin)
PERIODICAL:	Novosti neft. tekhniki. Neftepromysl. delo, 1956, Nr 6, pp 8-10
ABS TR ACT :	All cutting bits "lose" in diameter because of wearing of the peripheral teeth, and the drill holes acquire the form of a cone tapering downward. Consequently, when a new bit is lowored the shaft of the hole must be enlarged, which leads to premature wear on the cutting- tool bearing. The Oil Drilling Division of the All- Union Scientific Research Institute has made several experimental bits with strengthened bearings. They allow only a minimum slippage of the head of the peri-
Card 1/2	pheral teeth in the cutting tool. In planning the bit,

•••

2 15-57-3-3849 The Construction of a Bit (Cont.) the minimum angle for the teeth was taken as 1930'. The angle of inclination of the shank to the axis of the bit was taken as 50°. In the new bits the points of the cutting tool, which gauge the hole, are so close to each other that the diameter of the hole is uniform throughout. Industrial testing has shown that footage of cutting with the bit is increased on the average from 18 to 20 percent. During the testing it was observed that the diameter of the hole remained constant. The whole series c2 bits used for enlarging the drill hole were lowered to the bottom of the hole one after the other without encountering an obstruction. M. G. M. Card 2/2

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Jet bit for geological exploration drilling. Mash. i neft'. obpr. no.1:5-11 '63. (MIRA 17:1)

<u>.</u>

1. TSentral'noye konstruktorskoye byuro Ministerstva geologii i okhrany nedr SJSR.

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AG: none TTLE: Adoption of <u>rolling</u> large round profiles from titanium alloys DURCE: Tswetnyye metally, no. 8, 1966, 77-80 DPIC TAGS: titanium alloy, metal rolling, metal forming BSTRACT: The rolling of large diameter (25 - 60 ma) titanium alloy stock was studied rior to rolling the specimens were heated for 10 min in an induction furnace up to a
ITLE: Adoption of <u>rolling</u> large round profiles from titanium alloys DURCE: Towetnyye metally, no. 8, 1966, 77-80 DPIC TAGS: titanium alloy, metal rolling, metal forming ESTRACT: The rolling of large diameter (25 - 60 mm) titanium alloy stock was studied
DURCE: Tevetnyye metally, no. 8, 1966, 77-80 DPIC TAGS: titanium alloy, metal rolling, metal forming ESTRACT: The rolling of large diameter (25 - 60 mm) titanium alloy stock was studied.
OPIC TAGS: titanium alloy, metal rolling, metal forming SSTRACT: The rolling of large diameter (25 - 60 mm) titanium alloy stock was studied.
BSTRACT: The rolling of large diameter (25 - 60 mm) titanium alloy stock was studied.
Emperature of 12701370%, and for 5 min in a silit furnace at a temperature of 1270- 1370%. A schematic of the rolling scheme is presented (see Fig. 1). The rolling argin was calculated after the formula of N. Ye. Krasnikov and N. P. Skryabin Nevetnyye metally, 1965, No. 4)
$\Delta h = \frac{\Delta h \cdot B_n \sqrt{\Delta h \cdot r}}{(H+h)!} \times \left[1.7 - \frac{B_n \sqrt{\Delta h \cdot r}}{(H+h)!}\right].$
here Δh is the absolute compression, B_0 - width of some before passage, H and h - might of some before and after passage respectively, and r - the radius of the
orking roller. It was found that the experimental data were is good agreement with

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5(4) MTLOR:	Matveyev, G.M.	
TITLE:	On the Computation of the Thermo Compounds in Silicate Technology svoystv binarnykh soyedineniy si	(O raschete termodinamicheskikh
PERIGPICAL:	Izvestiya vysshikh uchebnykh zav tekhnologiya, 1958, Nr 2, pp 135	edeniy. Khimiya i khimicheskaya - 141 (USSR)
ABSTRACT:	cates is obstructed by the lack the problem mentioned in the tit present paper an approximate com dynamic properties of cristallin MeC - RO, and MeC - R ₂ O ₂ type wh	ich play an important part in sili-
	cate technology is described. Al are heterodynamic compounds (Ref makes possible the separation of mentioned type: a) of a main (sk (cation) part, which are to repu	1 compounds of the mentioned type 1). The concept of heterodynamism 2 tarts in any compound of the

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APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R032932930002-8"

"APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R032932930002-8 SOV/153-58-2-22/30 On the Computation of the Thermodynamic Properties of Binary Compounds in Silicate Technology 1) Formation of the main structure (skeleton) by R-O bindings, and 2) Formation of the side (cation) part on the basis of wesker Me-O bindings. If the number of the binding Me-ions (at a constant molar content of MeO) then remains constant the change of the thermodynamic property (G) in the formation from elements is solvely letermined by the molar content of RO₂. At the increasing ratio RO2 the bindings within the structure are not subjected to any M aO fundamental change. For this reason the assumption is possible that the change of any thermodynamic property during the formation of a compound MeO.pRO₂ (or MeO.pR₂O₃) will be due to its change in the course of the formation of the fundamental structure and the change in the course of the addition of Me cations. According to the above considerations this will be constant for all compounds of the series MeO.pRO2. Therefore the difference of the properties in the formation of these compounds is determined by the corresponding differences of the properties during the formation of the fundamental structure of the mentioned compounds. Since the difference Card 2/4

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On the Composition of the Thermodynamic Properties of Binary Compounds in Silicate Technology

> in the changes of the thermodynamic properties for the main structures of the compounds MeO.RO₂ and MeO.pRO₂ (or MeO.pR₂O₃) is determined only by the total number of the R and O atoms participating in the formation of these structures it can be said that the change of any thermodynamic property in the formation of the main structure will be $\Delta G_R^P = p\Delta G_R^{\prime}$ (1), where ΔG_R^P and ΔG_R^{\prime} denote the changes of the properties in the course of the formation of the main structure of MeO.pRO₂ and MeO.RO₂. In view of the above fact the change of the property during the addition of the Me cations (Ref 2) will be constant for all compounds of the series MeO.pRO₂ (or MeO.pR₂O₃) i.e. $G_{Me} = \text{Const}$ (2). Thus, the thermodynamic properties of any other compounds in the system MeO-RO₂ or MeO-R₂O₃ can be determined on the basis of any 2 values of a thermodynamic property. This theorem is explained by means of examples. Further equations are derived which make possible the

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. On the Composi of Binary Comp	tion of the Thermodynamic Properties SOV/153-58-2 bounds in Silicate Technology	-22/30
	determination of the thermodynamic properties of any comp their formation in the corresponding system. The suggeste can be applied also directly for the table values of corr properties. Figures 1 - 4 reveal a geometrical interpreta this method. There are 4 figures, 2 tables, and 11 referen- which are Sovie.	esponding tion of
ASSOCIATION:	Moskovskiy khimiko-tekhnologicheskiy institut im. D.I.Men (Moscow Chemical and Technological Institute imeni D.I.Me Kafedra obshchey tekhnologii silikatov (Chair of General Techrology)	nceleyev)
SUBMITTED:	October 5, 1957	
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MCHEDLOV-PETROSYAN, O. P.; MAIVEYEV, G. M.; SAFONOV, V. S. "Investigation of energetics of devisrification processes as a method for studying glass structure." report submitted for 4th All-Union Conf on Structure of Glass, Leningrad, 16-21 Mar 64.

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CCESSION NR: AP4040505	s/0063/64/009/003/0354/0355
UTHORS: <u>Matveyev, G. M.;</u> Matveyev, M. A	•
ITLE: Thermodynamic analysis of solid p	hase reactions in the BeO-540 ₂ system
SOURCE: Vsesoyusnoye khimicheskoye obaho 354-355	hestvo. Zhurnal, v. 9, no. 3, 1964,
COPIC TAGS: refractory material, berylli milicate, beryllium silicate enthalpy, is	un oxide, silicon dioxide, beryllium obar potential, beryllium orthosilicate
BSTRACT: The present investigation was with SiO, is of great importance in the p glass. The thermodynamic analysis of Beg	undertaken because the interaction of Beo production of refractory materials and SiO ₄ and BeSiO ₃ of the formation from
oxides was conducted. After the thermode BeSiQ ₃ formation from the components was	emical data were assembled, the enthalpy of calculated by using the equation
$\Delta H_{\text{BeSIO}_{B}} = -\frac{T}{2} \left(\Delta H_{\text{BeSIO}_{B}} - \Delta H_{\text{MSSSIO}_{B}} \right) + \Delta H_{\text{MSSIO}_{B}}$	from an earlier paper by G. M. Matveyev
	·
(Trudy WENTI in. D. I. Mendeleyeva, No. $\Delta Z \simeq f(T)$ were calculated for the two be	24, M., 1957, p. 233). The $\triangle H = f(T)$ and all reactions: $BeO + SiO_1 = BeO \cdot SiO_1$. $2BeO + SiO_2 = 3BeO \cdot SiO_2$

"APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R032932930002-8 . 1. • 54°° ACCESSION MR: AP4040505 "The values for the exthalpy and the isobar potential within the temperature range of 500-1800K are presented in the graph (see Fig. 1 on the Enclosure). The authors conclude that in all instances beryllium orthosilicate would be the most stable comprund and that it should be produced by crystallisation from a melt or glass. Some of the thermochemical data were calculated by G. M. Matveyev. Orig. art. has: 1 table, 1 chart, 2 formulas, and 1 equation. ASSOCIA.ION: Moscow khimiko-tekhnologicheskiy institut im. D. I. Mendeleyeva (Moscow Chemicotechnological Institute) SUBMITTED: 22May63 DATE ACQ: 06Jul64 ENCL: 01 SUB CODE: GC, MT NO REP SOV: 005 OTHER: 000 Card 2/3 2

APPROVED FOR RELEASE: 06/14/2000



CC NR: AR60	EWT(:=)/EWP(=) 16780	SOURCE C	ODE: UR/0081/55/00	ე/023/B076/B076
UTHOR: M	tveyer, G. M.			6
		MnL, Fe ₂ O ₃ , Ka ₂ O an asses in the Cao-MgC	d P ₂ O ₅ additions on -Al ₂ O ₃ -SlO ₂ system	n the crystallisa-
OURCE: Ref	. sh. Khimiya, Ab	ı. 238553		
		. sostoyaniye T. 3.	Vyp. 4. Hinak, 196	4, 89-92
	•	perty, crystallisat		
ABSTRACT: of 2 to 8% SiO ₂ system crystallis limit of c	The effect of add on the crystallis m was studied. On ation. A minimum rystallisation. 7	ing B ₂ O ₃ , BaO, MnO, ability of alkalifr ly B ₂ O ₃ is effectiv 3.5 to 45 edditive he addition of smal	Fe203, Na20 and P2 e glasses in the C in lowering the u of B203 guarantees 1 quantities of P2C of Be0 the upper	pper limit of an optimal upper by results in a limit of cryst
14 mat 4 am 20	aachaa 1417. A I	TILPETON THE APPART	203 00000000000000000000000000000000000	extended the upper
crystallis	ation limit up to		•	
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ACC NR: AP6029826 (N) SOURCE CODE: UR/0363/66/002/008/1505/1513	
AUTHOR: Matveyev, M. A.; Pevzner, R. L.; Matveyev, G. M.; Kharitonov, F. Ya	
ORG: Moscow Chemical Engineering Institute in. D. I. Mendeleyev (Moskovskiy Vteknolo- gisheskiy institut)	
TIME: Use of ceramic materials in a water vapor medium of high parameters	· .
SOURCE: AN SSSR. Izvestiya. Neorganicheskiye materialy, v. 2, no. 8, 1966, 1505-1513	<u>\$</u> .
TOPIC TAGS: coremics, water vapor, corrosion rusisfance.	
ABSTRACT: The reactions of ceramic materials of various phase and chemical composi-	
to 1000/hr. An extensive attack of water-glass composited by The attack causes a de- celain, steatite, forsterite and wollastonite was observed. The attack causes a de-	
sult of the formation of hydrated lons of the corresponding interials based on corundum anions. Loss subject to attack under these conditions are materials based on corundum	
the hydration of the tested materials involving the use of known tendents. Orig. dynamic potential of the original silicates and hydrated cations and anions. Orig.	
art. has: 4 tables.	2
SUB CODE: 11/ SUBM DAT_: 12Jun65/ ORIG REF: 015 Cord 1/1 //	
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Subject	: USSR/Aeronautics - training AID P - 4595
Card 1/1	Pub. 135 - 7/23
Author	
Title	
	s objens a geo bomber at night in a two-snip element
	: Vest. vozd. flota, 3, 38-41, Mr 1956
Abstract	: A detailed description of the training of pilots for night flying in formation is given. The article is of informative value.
Institution	: None
Submitted	: No date

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"APPROVED FOR RELEASE: 06/14/2000 CIA-RDP86-00513R032932930002-8 1. 1. MATVEYEV, G.V. Device for reducing vibration. Transp. stroi. 14 no.7:50 J1 164. (MIRA 18:1) 1. Mavnyy inzh. tresta Sevtransstrom,

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GLAZACHEV, B.; MATVEXEV, I.
Mechanizad station. Zashch. rast. ot vred. i bol. 10 no.3:31 'téf. (MIRA 19:..)
1. Zaveduyvshchiy otdelom vnedreniya peredovogo opyta Ukrainskoy opytnoy stantsii tavetochnykh i dekorativnykh rasteniy (for Glazachev). 2. Direktor Kiyevskoy stantsil zashchity zelenykt nasazhdeniy (for Matveyev).

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CIA-RDP86-00513R032932930002-8

SOV/191-58-10-5/25

AUTHOR: <u>Matrix I.B.</u> Shchetinin, T.A.

TITLE: The Choice of the Crank Shaft Speed of Plunger Pumps (Vybor dhisla oborotov kol_enthatogo Wala krivoshiploplunzhernykh Nasosov)

PERIODICAL: Stanki 1 Instrument, 1958, Nr 10, pp 17-19 (USSR)

ABSTRACT: In crank-driven plunger pumps of a given pressure and delivery there is a speed of rotation which yields the minimum sum of pressure and inertia forces in the crank mechanism. A formula (equation 10) is given for the optimum rpm in terms of the mumber of cylinders, the pump delivery, the bore to stroke ratio and a factor expressing the mass of the moving parts. This optimum rpm is independent of pressure and is proportional to the fifth root of the number of cylinders and inversely proportional to the fifth root of the delivery. The best bore to stroke ratios are in the range of 0.8 - 1.5 increasing with pressure and delivery. The optimum rpm is much higher than in

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hammers. Pressur be separated from (operating component	he overall pressure network (100-1) based on consumption of electricity kgm, bammor unit 1000 kg for 596	700 kg/cm ² and the unit should 50 kg/cm ²). Calculations of to operate the M-211 unit (max.	
savings of 322,000 proposed system as 670 m ³ /hr) and co	compared to 67 kwh for present con	npressed oir section	-
savings of 322,000 m proposed system as 670 m ³ /hr.), and su hydraulic operation. ASSOCIATION: none	compared to 67 kwh for present con ggest the advisability of 1 lodifying p Orig. art. has: 2 diagrams and 4 i	npressed oir section	•
savings of 322,000 1 proposed system as 670 m ³ /hr.), and su hydraulic operation. ASSOCIATION: none SUBMITTED: 00	ggest the advisability of 1 hodifying p Orig. art. has: 2 diagrams and 4 i	npressed oir section	
savings of 322,000 m proposed system as 670 m ³ /hr.), and su hydraulic operation. ASSOCIATION: none	compared to 67 kwh for present con	npressed air requirement of 2.3sent steam-air hammers to formulas.	

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